

# Evaluation of Remedy Performance of the Uranium Plume in the 300 Area of the Hanford Site

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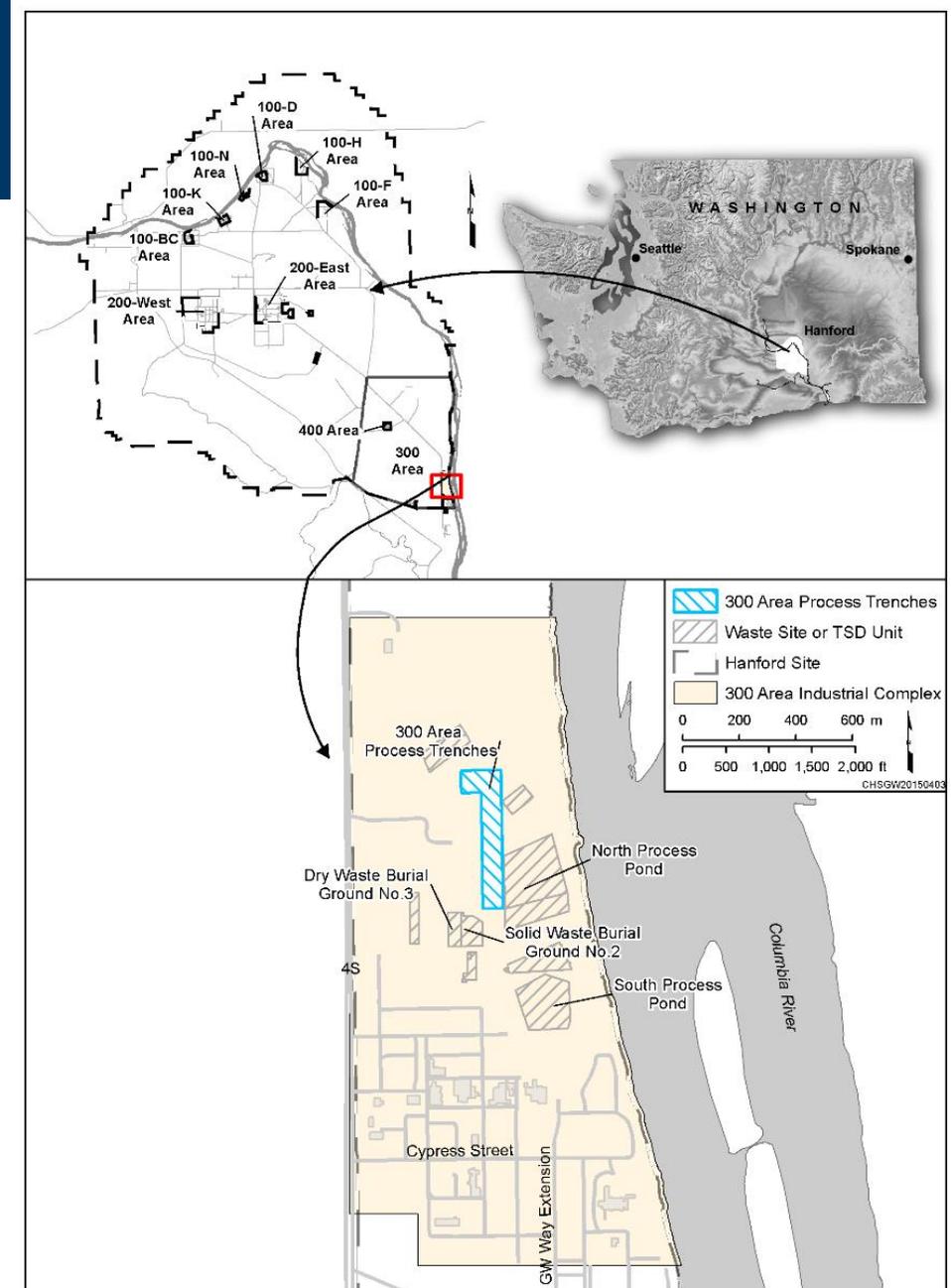
INTERA Inc, Richland, Washington

November 16, 2023



# Hanford Site and 300 Area

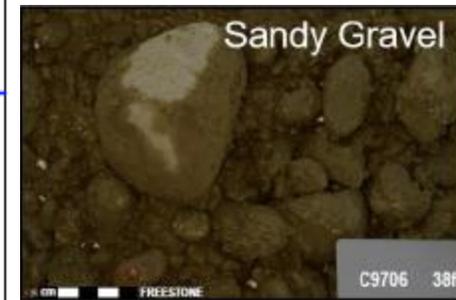
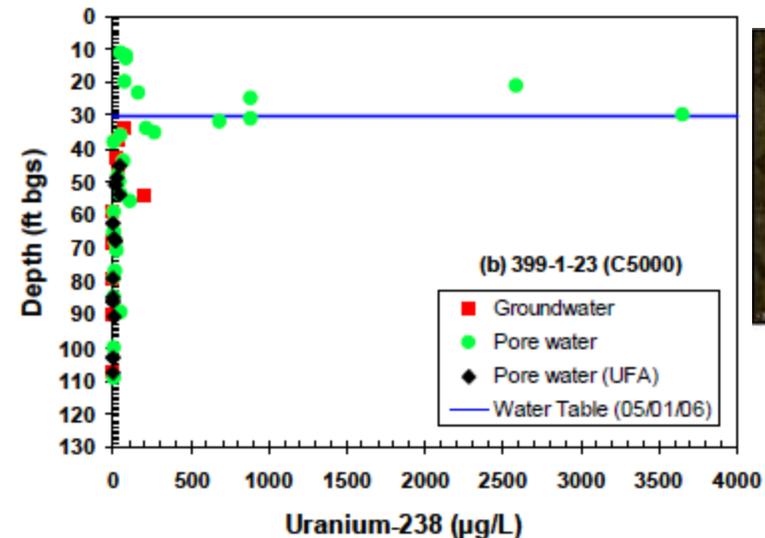
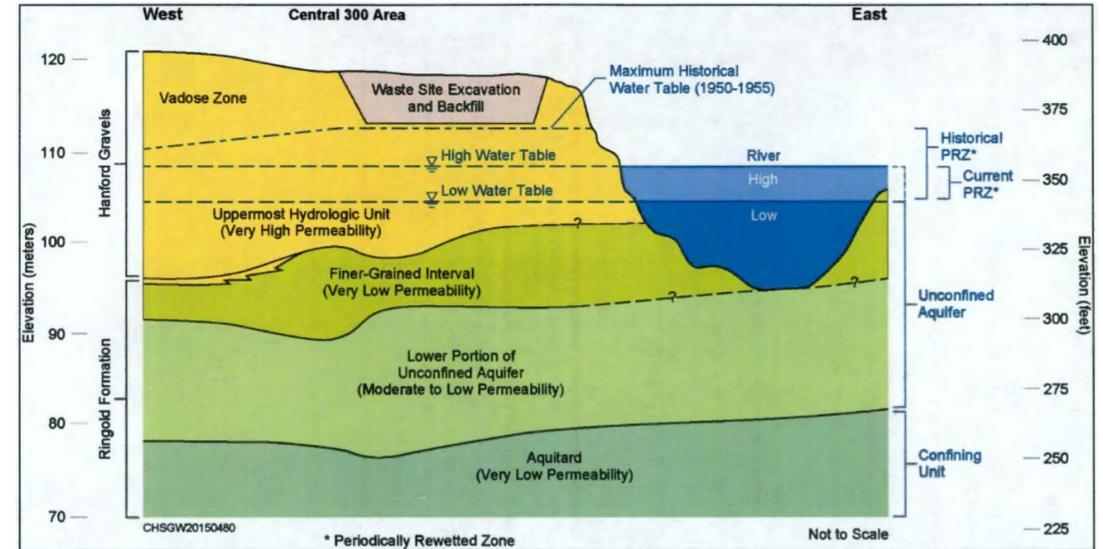
- Hanford Site was used to produce nuclear material to support the defense mission of United States from 1943-1987
- The 300 Area
  - Uranium fuel fabrication activities generated waste was discharged to surface ponds and trenches
  - Persistent uranium groundwater plumes
- Selected remedy is monitored natural attenuation with enhanced attenuation in 3-acre area (12,140 m<sup>2</sup>) of highest contamination
  - In-situ treatment with polyphosphate solutions
- Columbia River forms the Site boundary





# Site Conceptual Model

- Columbia River stage fluctuations impacts water-table
  - Daily fluctuations and seasonal variations are important
- Vadose zone encompassing the historically high and low water table elevations is called the Periodically Rewetted Zone (PRZ)
- Highly variable contamination in vadose zone
- Majority of the uranium associated with <2 mm size fraction (sand, silt, and clay)
- Leachable (labile) uranium variable (up to 60% of total uranium)
- U(VI) exists primarily in form of
  - Precipitated phases (carbonates and phosphates)
  - Adsorbed surface complexes on phyllosilicates and iron oxides



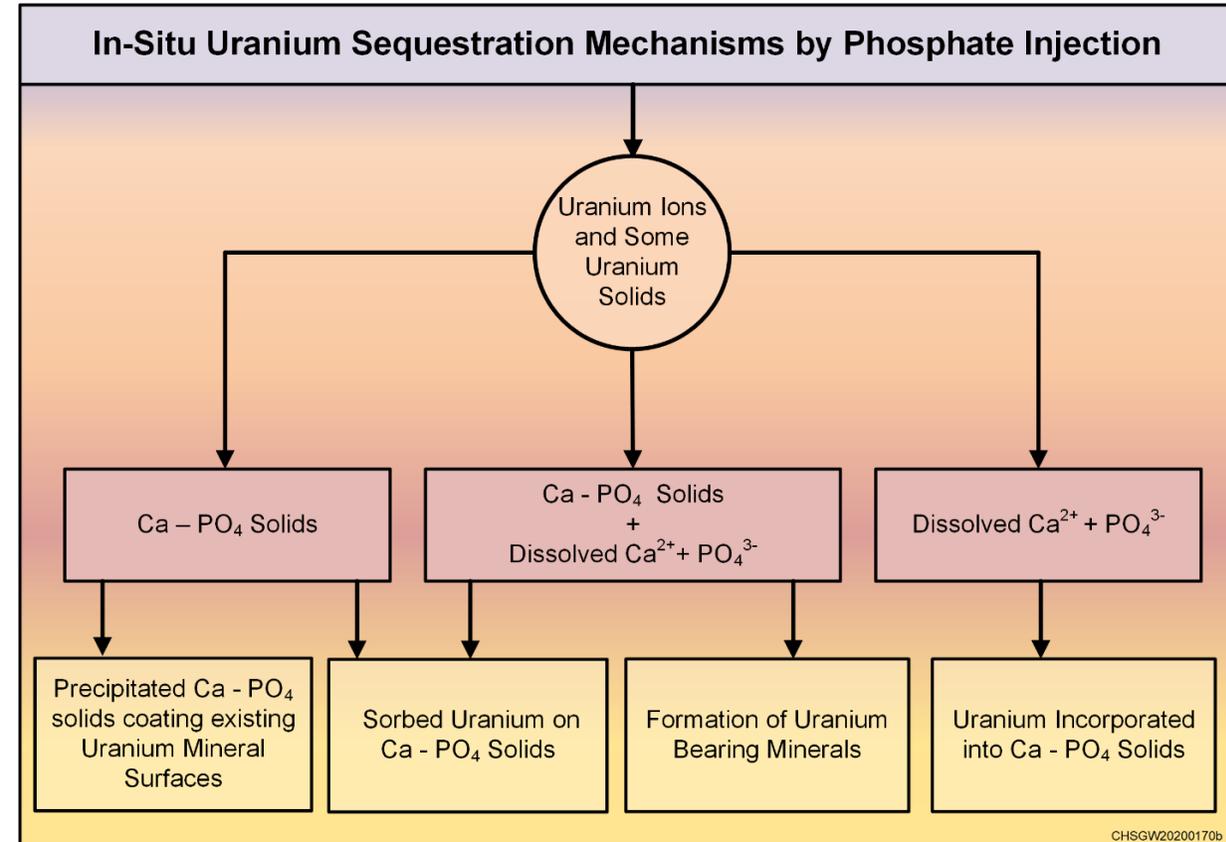
# Study Approach

## ■ Enhanced Attenuation

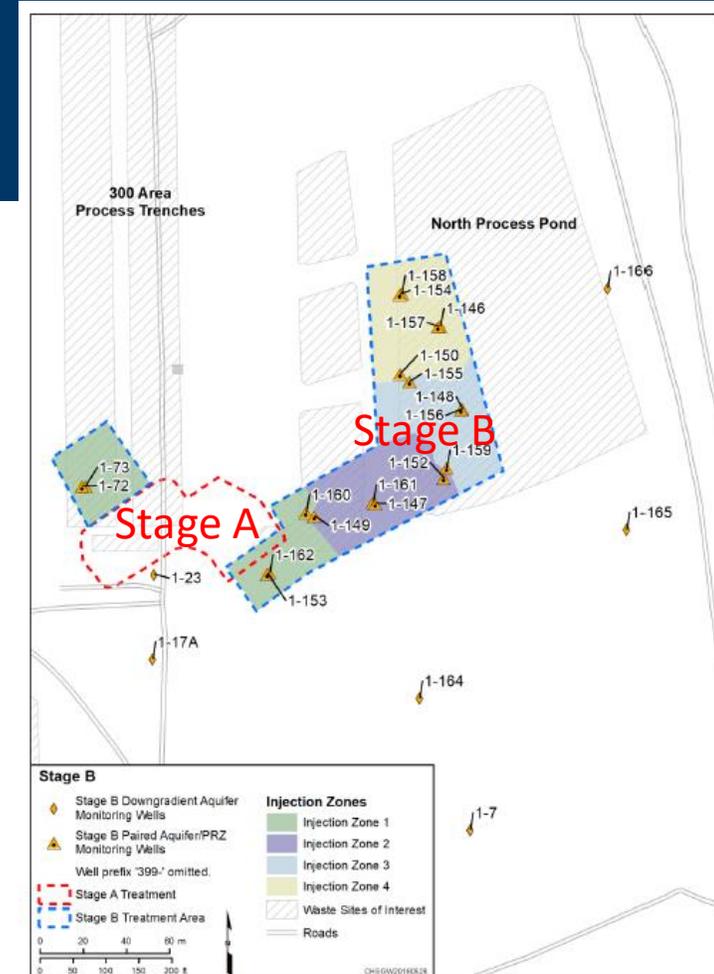
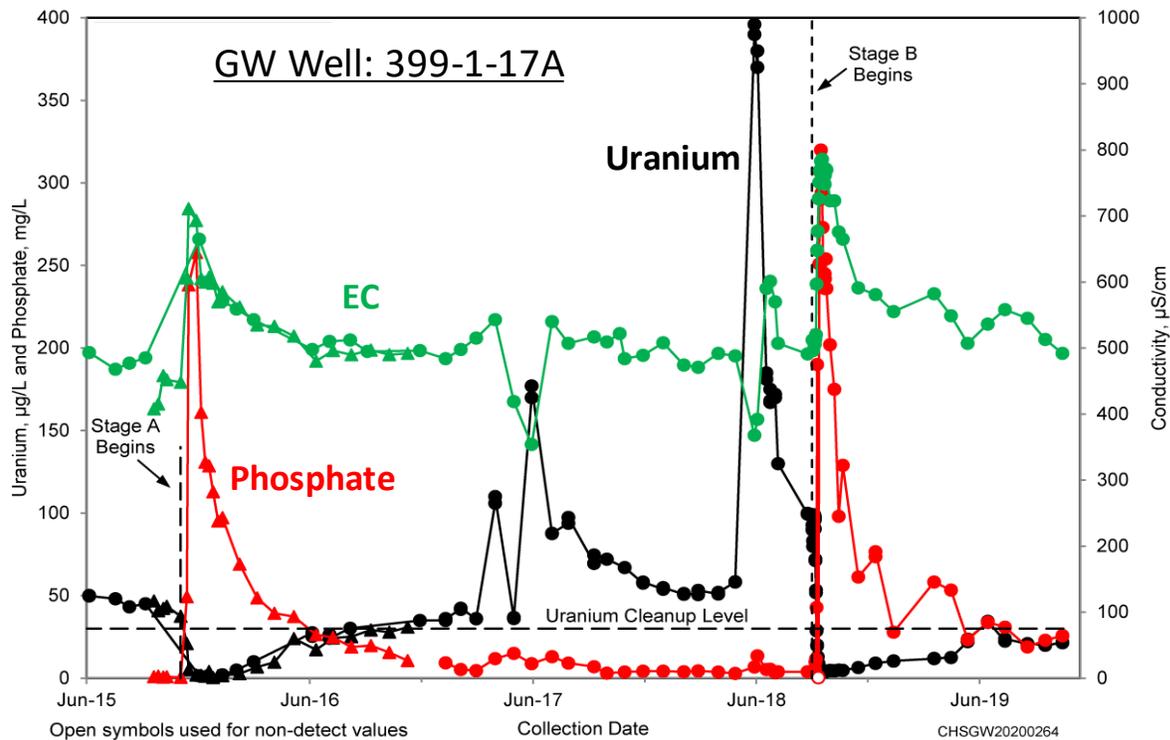
- In-situ uranium sequestration by injecting polyphosphate solutions
- Field monitoring (including ERT)
- Laboratory analyses
- Reactive transport modeling
- System scale flow and transport modeling

## ■ Monitored Natural Attenuation

- Development of large-domain model
- Model calibration
- Model prediction



# Enhanced Attenuation: Remedy Implementation



- Stage A: smaller area (0.75 acres); November 2015; surface infiltration and 9 injection wells
- Stage B: larger area (2.25 acres); September 2018; 48 injection wells
  - Mixture of Orthophosphate ( $\text{NaH}_2\text{PO}_4$  and  $\text{KH}_2\text{PO}_4$ ) and Pyrophosphate ( $\text{Na}_4\text{P}_2\text{O}_7$ )
  - Target phosphate conc: 8,250 mg/L; Injection rate: 189 L/min (50 gal/min) for 16 hours per well
  - Total volume injected:  $16 \times 10^6$  Liters ( $4.2 \times 10^6$  gallons); Phosphate mass delivered: 133,500 kg

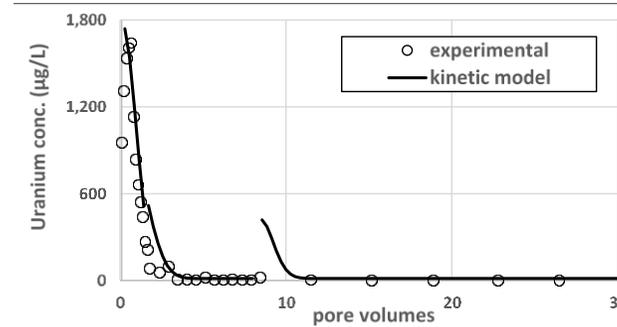


# Enhanced Attenuation: Laboratory Analyses

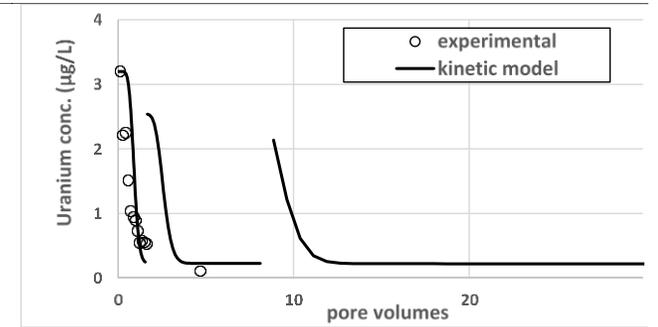
- Laboratory analyses performed on *pre*-treatment and *post*-treatment sediment samples collected from six co-located boreholes from approximately same depths
- Sequential extractions indicate dissolution of uranium carbonate and hydrous uranium silicates in post-treatment samples and reprecipitation as lower solubility uranium phosphate bearing mineral phases
- Total uranium that could be extracted from post-treatment samples was on average 33% lower compared to pre-treatment samples (based on sequential extraction)
- Labile uranium fraction was about 63% lower following treatment (based on 1000-hr carbonate extraction)

# Enhanced Attenuation: Reactive Transport Modeling

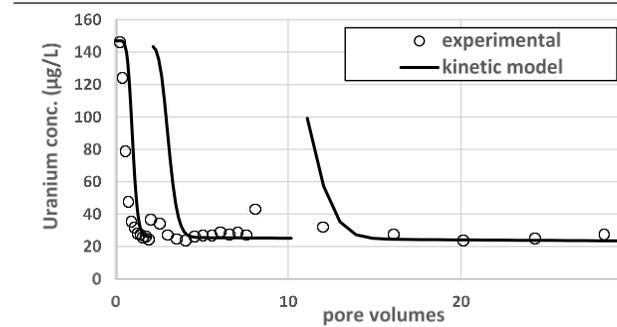
- Uranium leaching rate estimated using single-site kinetic rate constants
  - Due to complex assemblage of uranium bearing mineral phases the relative influence of each mineral phase is difficult to estimate
- 1-D finite-difference transport model used to fit and estimate the forward and reverse kinetic rate constants
  - Rate constants matched with other independent estimates



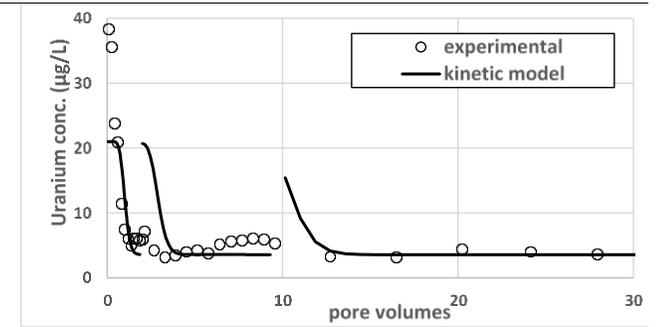
a. Sample G-29 (pre-injection pair)



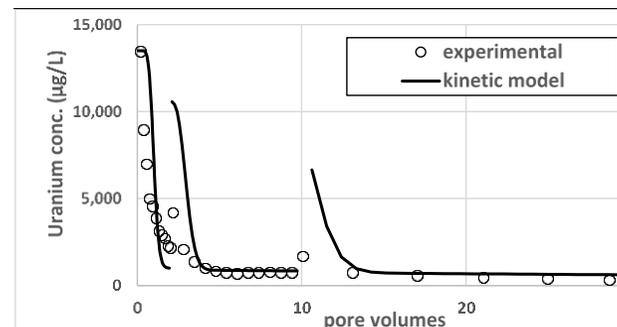
b. Sample G-118 (post-injection pair)



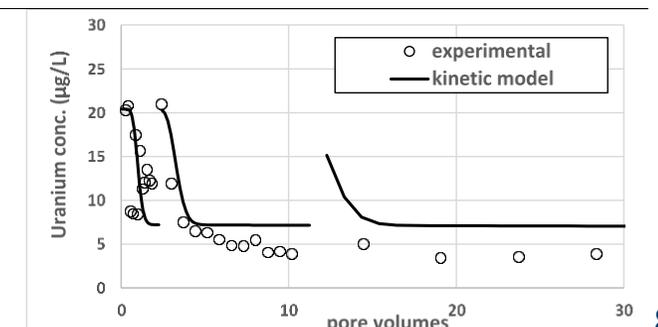
c. Sample G-20 (pre-injection pair)



d. Sample G-112 (post-injection pair)



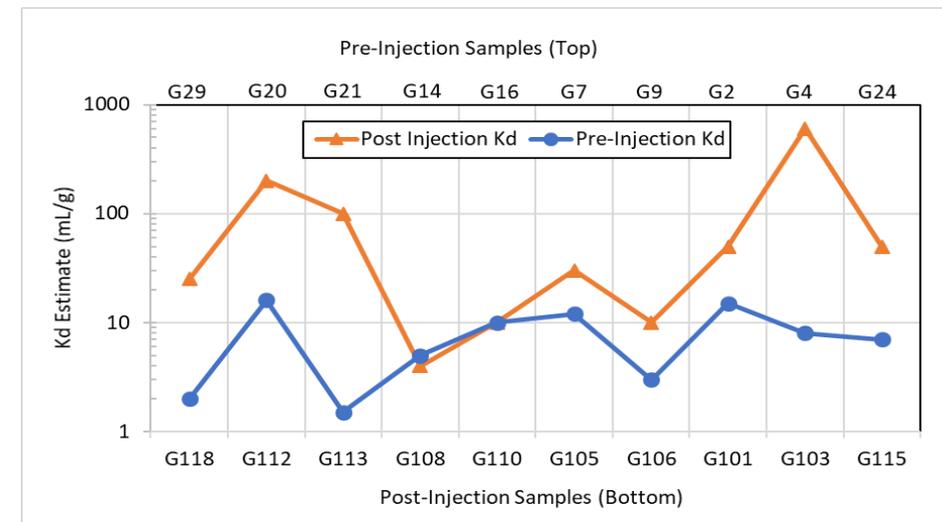
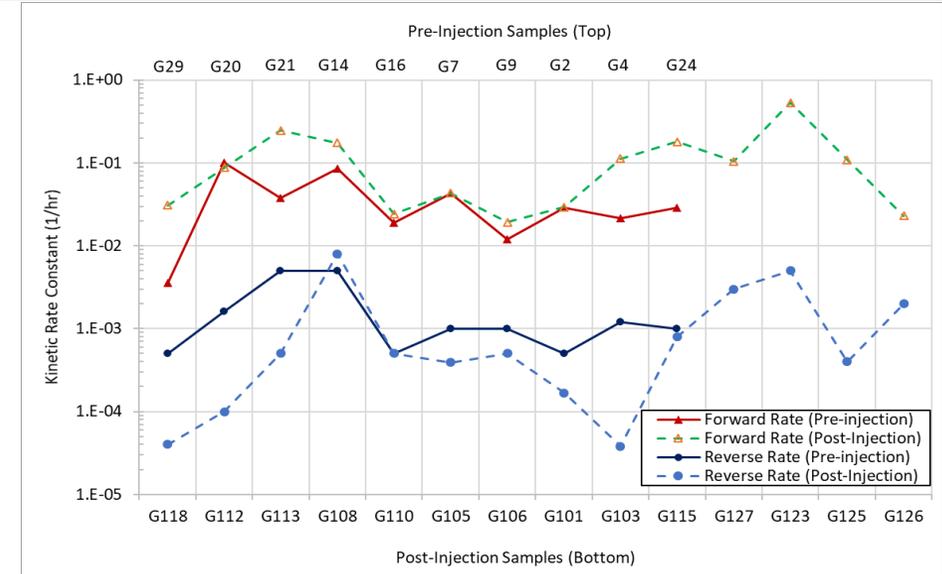
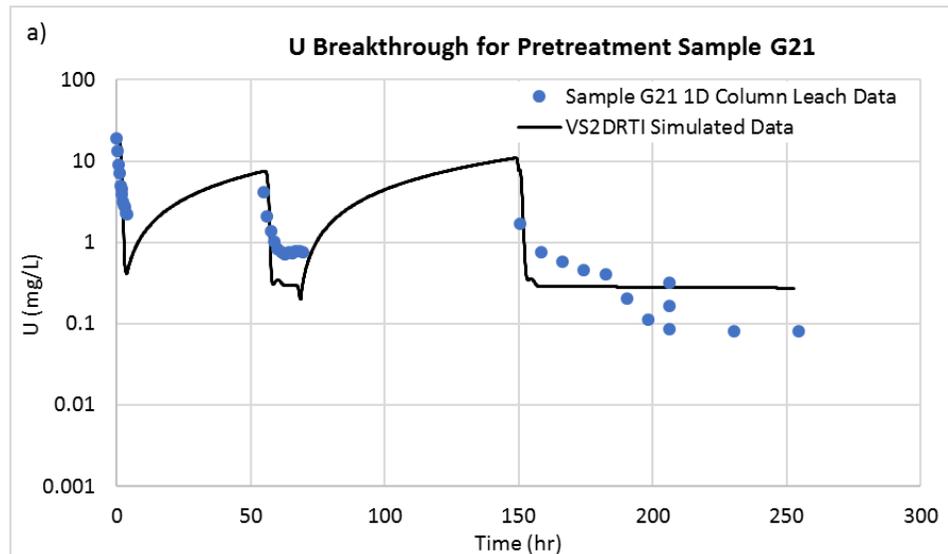
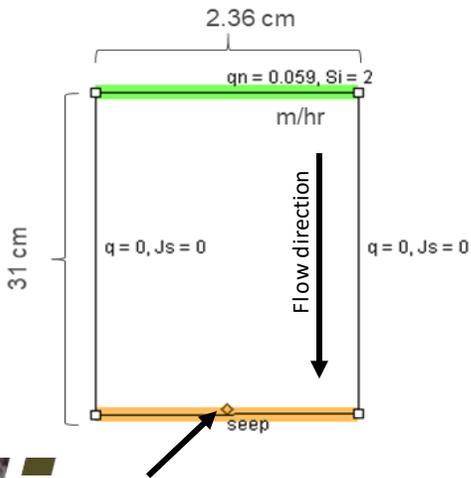
e. Sample G-21 (pre-injection pair)



f. Sample G-113 (post-injection pair)

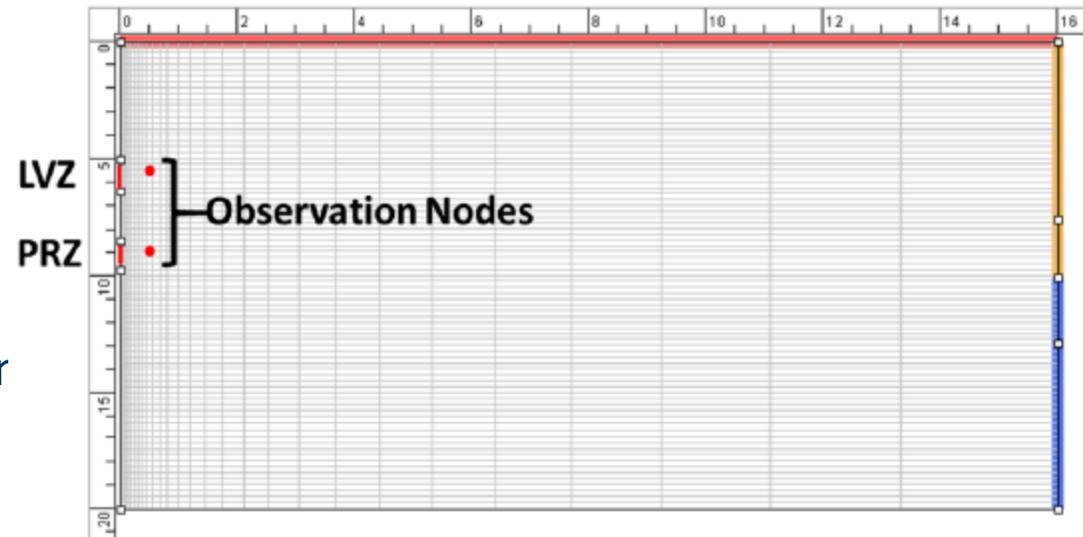
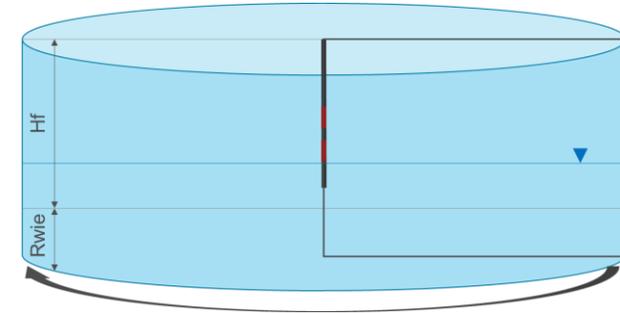
# Enhanced Attenuation: Reactive Transport Modeling

- The reverse rate constants are smaller by factor 10 for the post-injection samples
  - Effectively 10x increase in “Kd value”
- Kinetically controlled release with geochemical controls modeled using VS2DRTI\* coupled to PhreeqcRM and compared to Column test results (core-scale modeling)

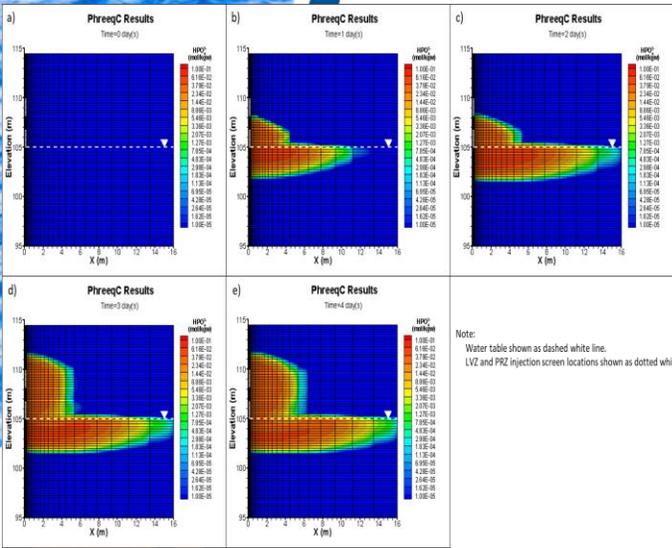


# 3-D Reactive Transport Model Using VS2DRTI

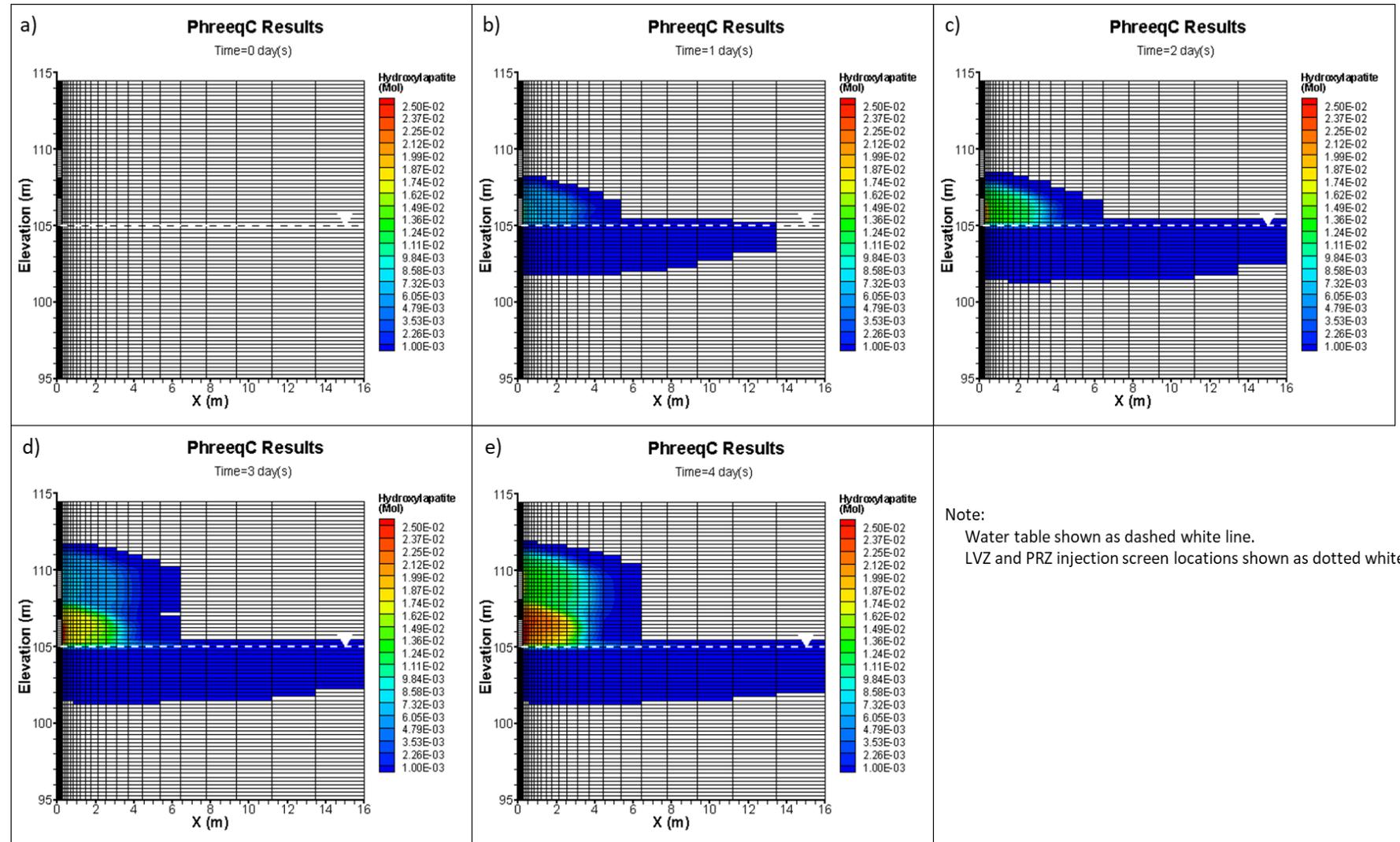
- Simulate 3-D injections at a single well in radial coordinates (near-field modeling)
- Incorporate unsaturated and saturated zones
- Include local geologic model
- Model flow and reactive transport
  - Aqueous chemistry
  - Cation exchange
  - Simplified single site surface complexation
  - Mineral precipitation/dissolution
  - Kinetically mediated dissolution/precipitation of calcite and uranium



# Reactive Transport Model : $\text{HPO}_4^{2-}$ injection and formation of Hydroxylapatite



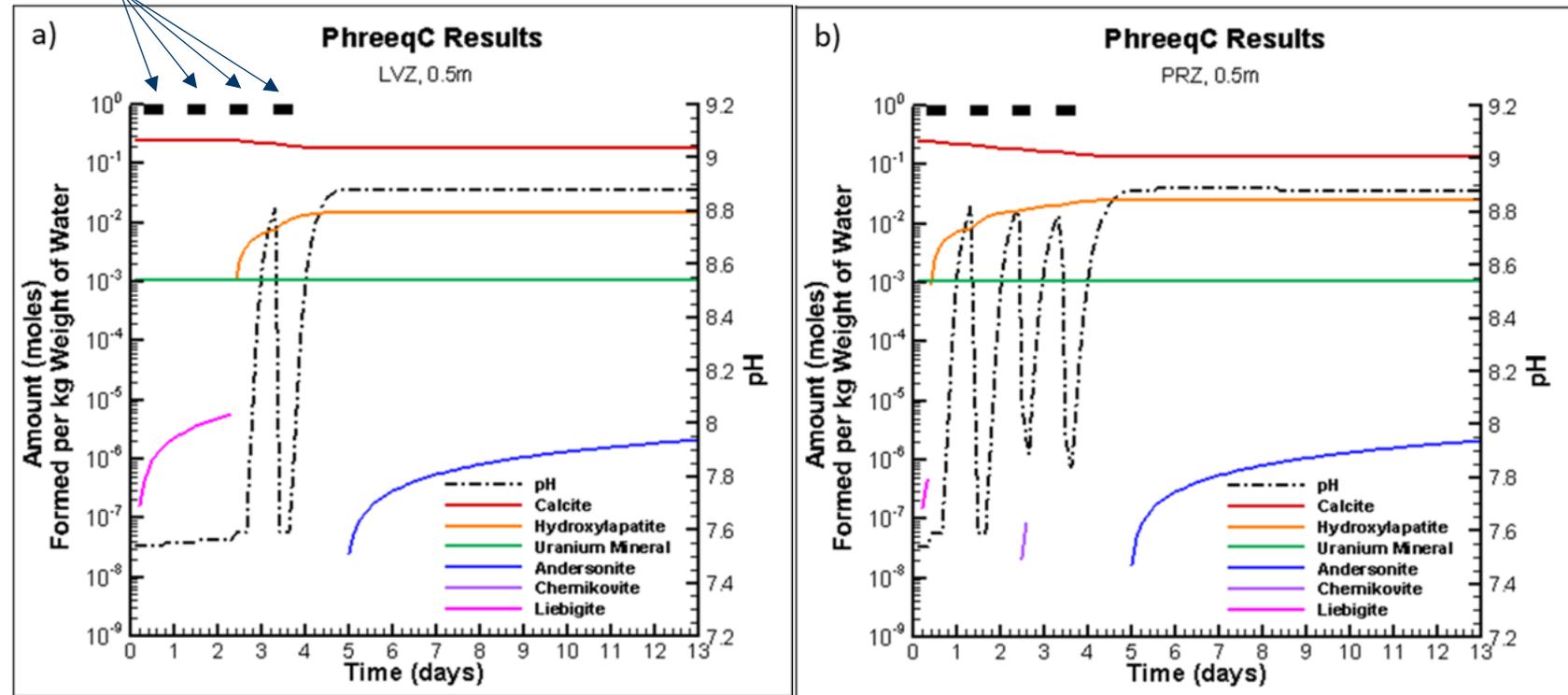
Note:  
Water table shown as dashed white line.  
LVZ and PRZ injection screen locations shown as dotted white lines.



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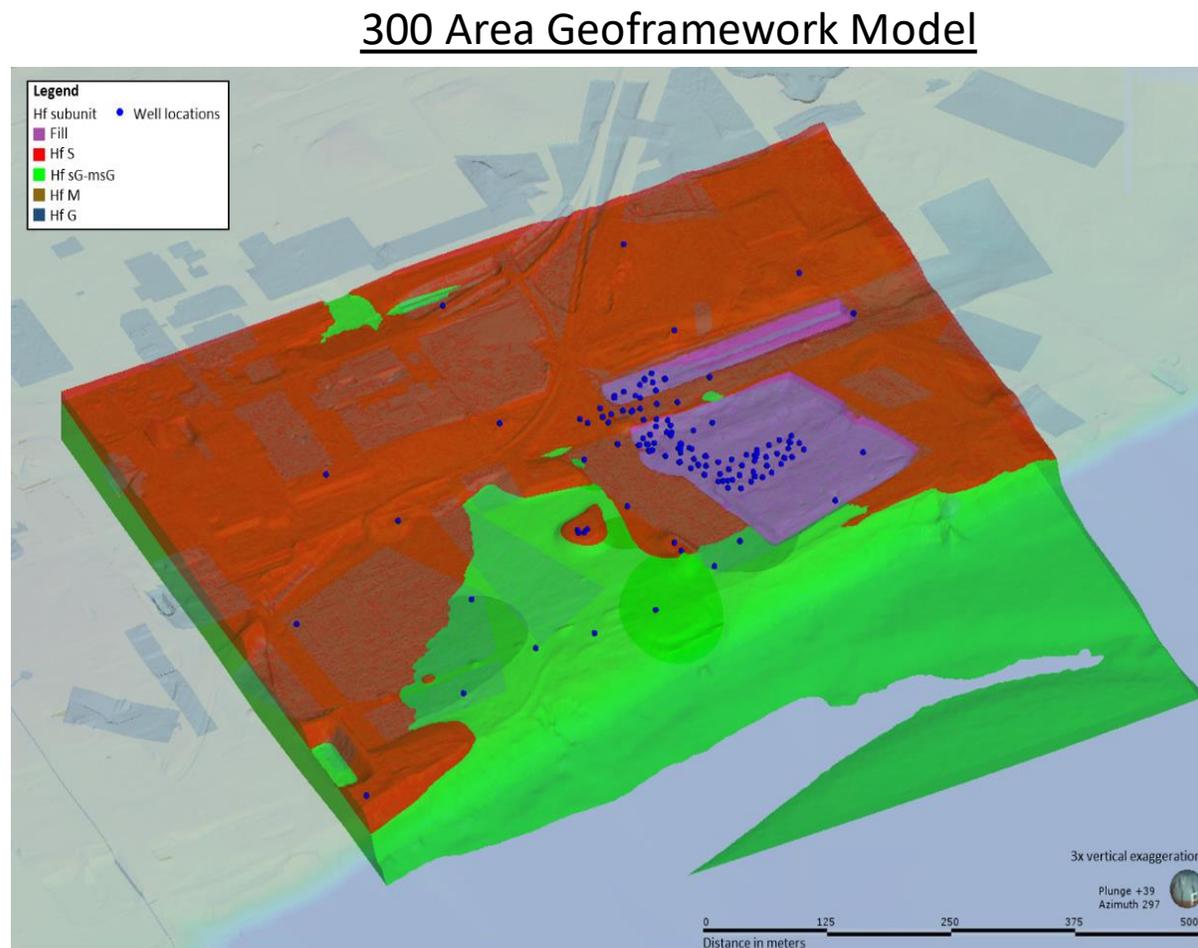
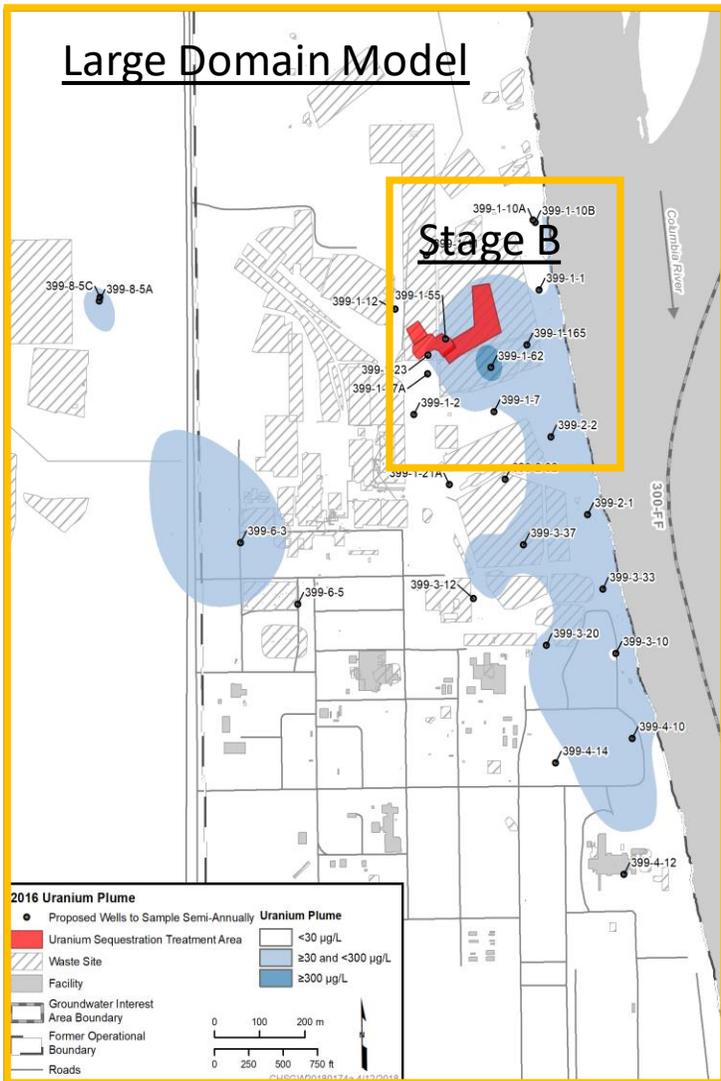
# 3-D Reactive Transport Model: Observation Pts

■ = simulated injection period



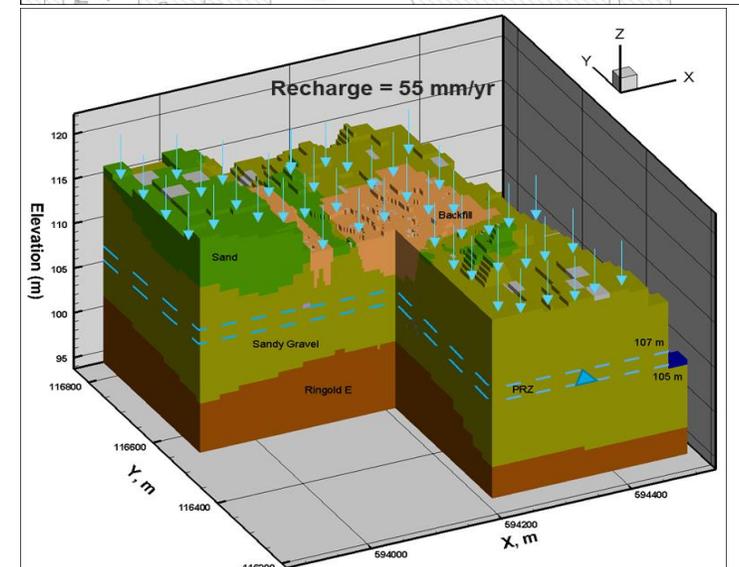
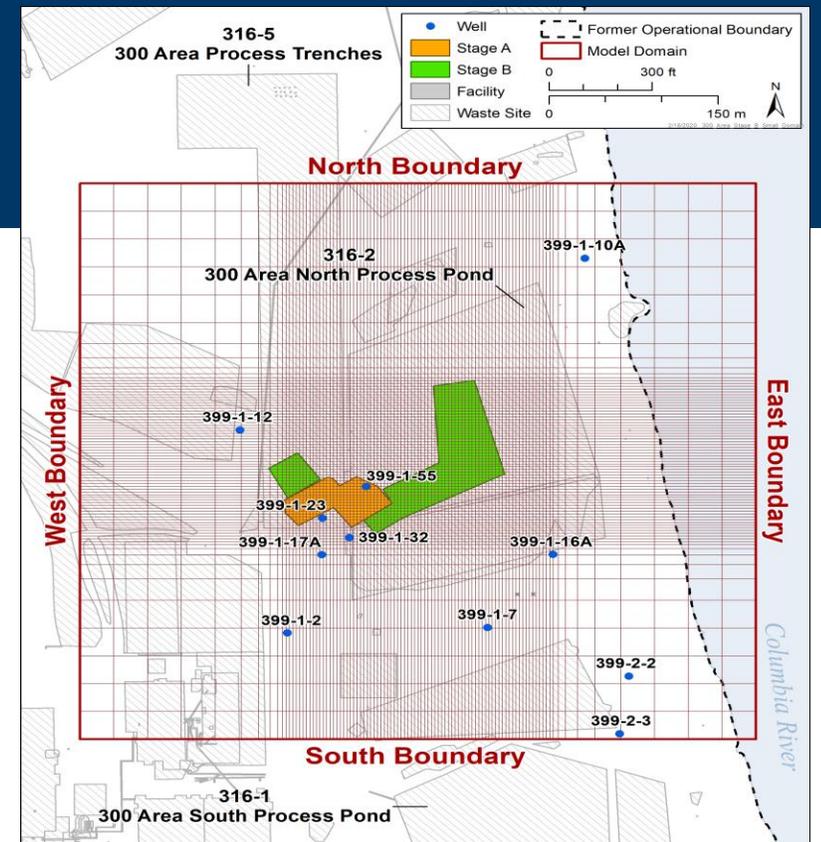
| Mineral         | Equation   | log K   |
|-----------------|--|---------|
| Hydroxylapatite | $\text{Ca}_5(\text{OH})(\text{PO}_4)_3 + 4\text{H}^+ = \text{H}_2\text{O} + 3 \text{HPO}_4^{2-} + 5 \text{Ca}^{2+}$  | -3.0746 |
| Andersonite     | $\text{Na}_2\text{CaUO}_2(\text{CO}_3)_3(\text{H}_2\text{O})_6 = 2\text{Na}^+ + \text{Ca}^{2+} + \text{UO}_2^{2+} + 3\text{CO}_3^{2-} + 6\text{H}_2\text{O}$ | -37.5   |
| Chernikovite    | $(\text{UO}_2)\text{HPO}_4(\text{H}_2\text{O})_4 = \text{UO}_2^{2+} + \text{HPO}_4^{2-} + 4\text{H}_2\text{O}$   | -22.73  |
| Liebigite       | $\text{Ca}_2\text{UO}_2(\text{CO}_3)_3(\text{H}_2\text{O})_{10} = 2\text{Ca}^{2+} + \text{UO}_2^{2+} + 3\text{CO}_3^{2-} + 10\text{H}_2\text{O}$             | -36.9   |

# System Scale Flow and Transport Models



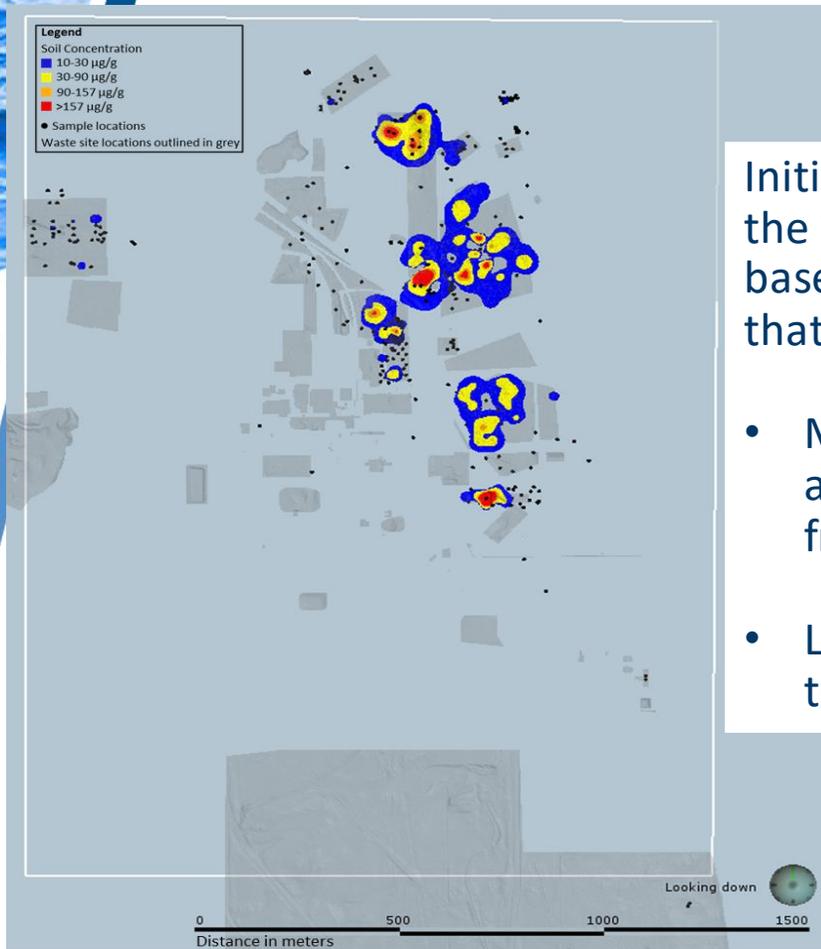
# System Scale: Stage B Model

- 3-D model built using eSTOMP code
  - To handle variably saturated conditions
  - 600 m x 600 m x 20 m domain
- Vadose zone and saturated zone comprised of multiple Equivalent Homogeneous Media (EHM)
  - Each heterogeneous hydrostratigraphic unit is treated as an anisotropic EHM having upscaled (effective) flow and transport properties
- Daily averaged hydrostatic pressure boundary conditions based on hourly record of Columbia River stage and water levels in monitoring wells
  - Complete record from 2008 - 2018
- Kinetic model implemented for uranium transport calculations + injections simulated
- Hydraulic conductivity field based on model calibration to hydraulic heads and river water-groundwater mixing based on EC measurements



# System Scale: Stage B Model

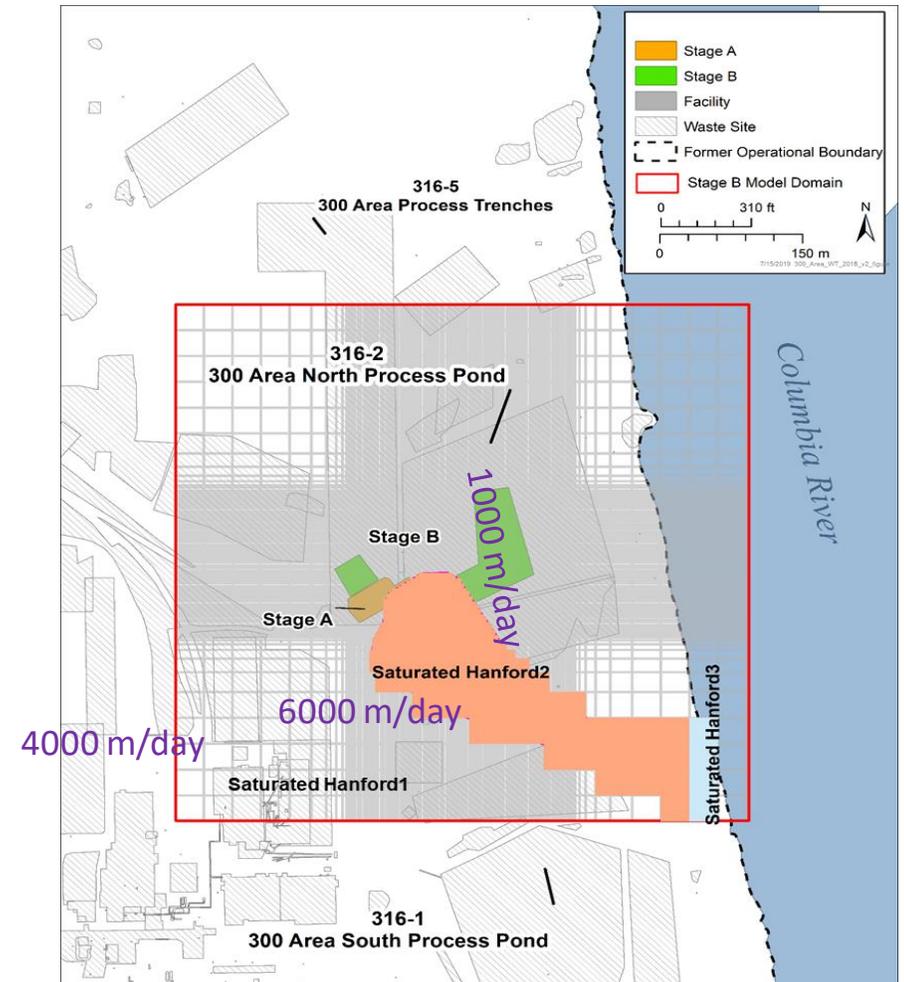
## Uranium Soil Distribution



Initial labile uranium mass in the 3-D Model was introduced based on the understanding that:

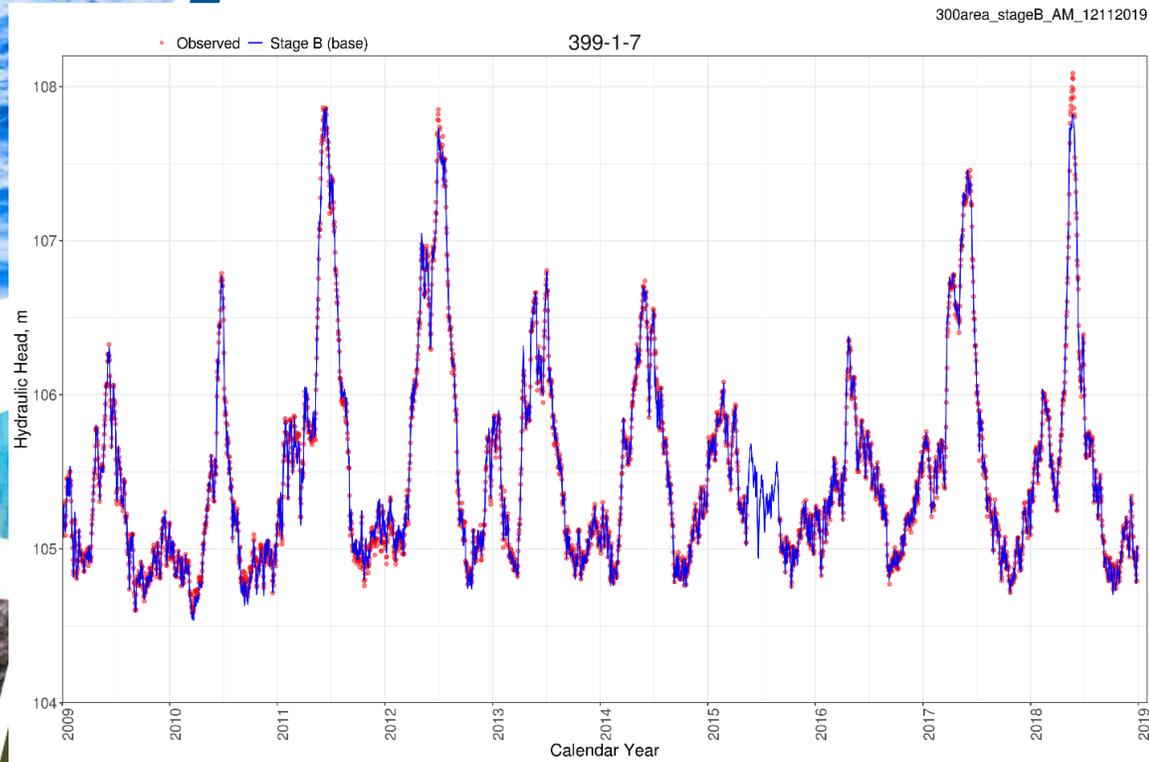
- Majority of the uranium is associated with <2 mm size fraction (sand, silt, and clay)
- Labile uranium variable (up to 60% of total uranium)

## Zones of Variable Hydraulic Conductivity

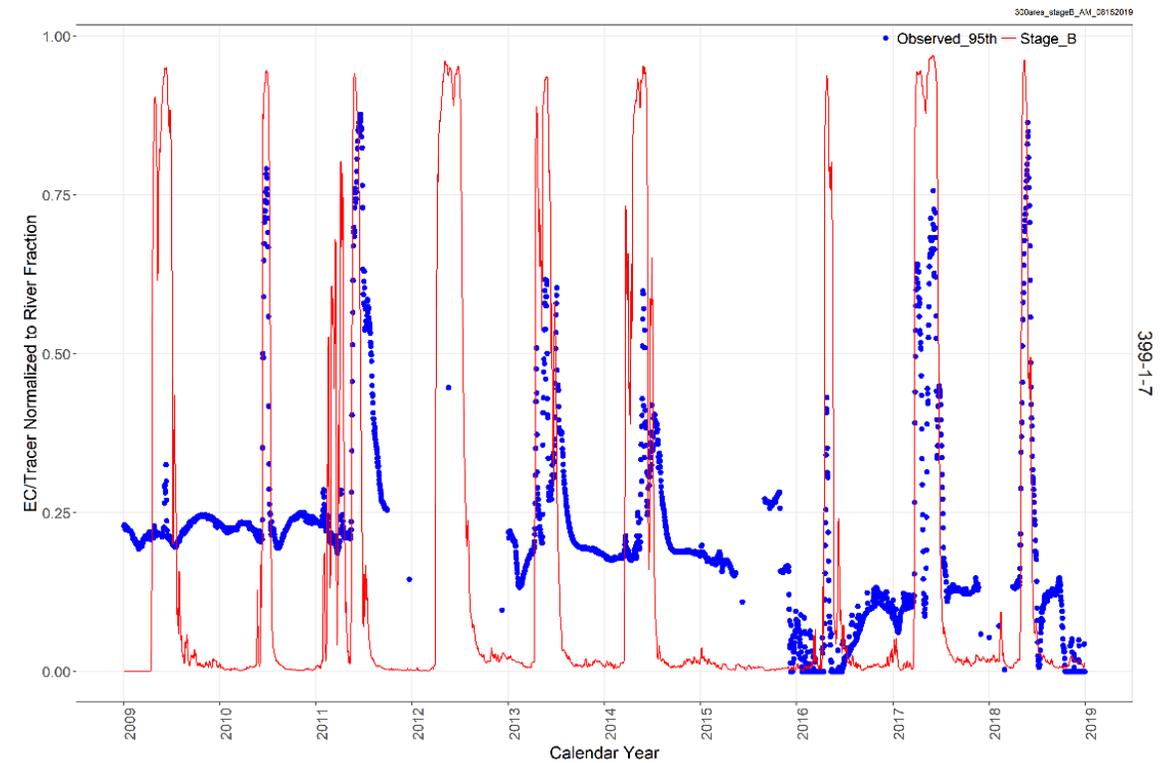


# System Scale: Stage B Model

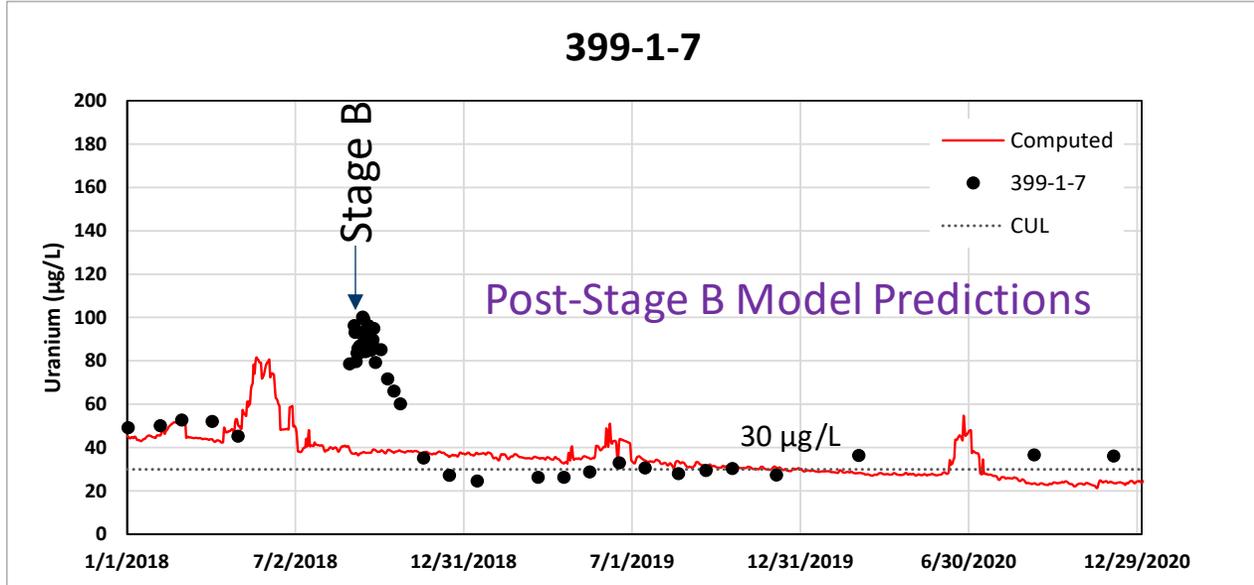
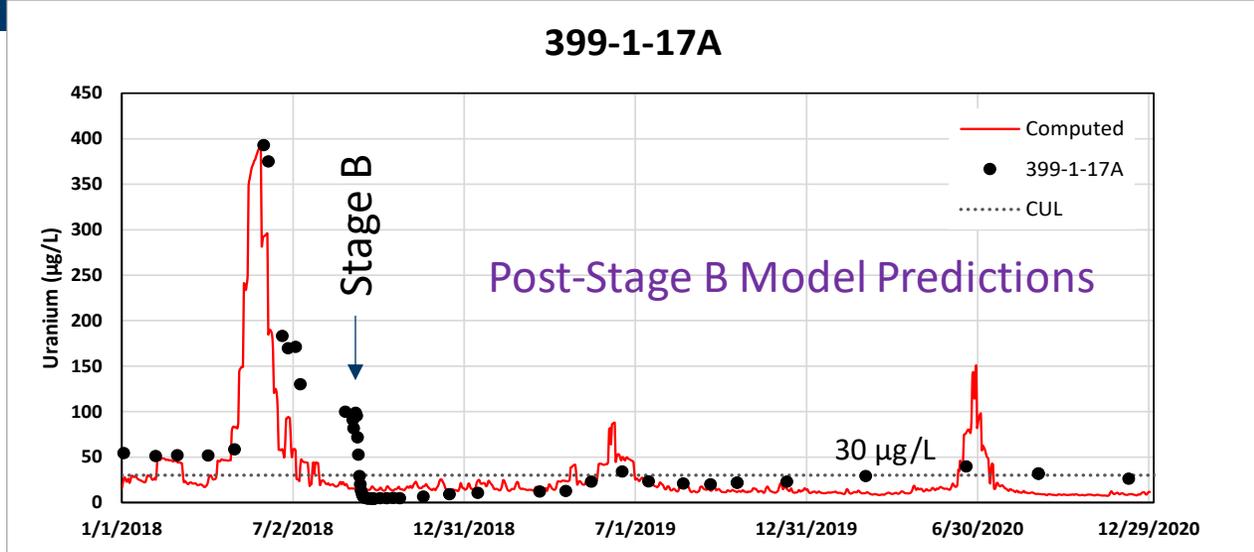
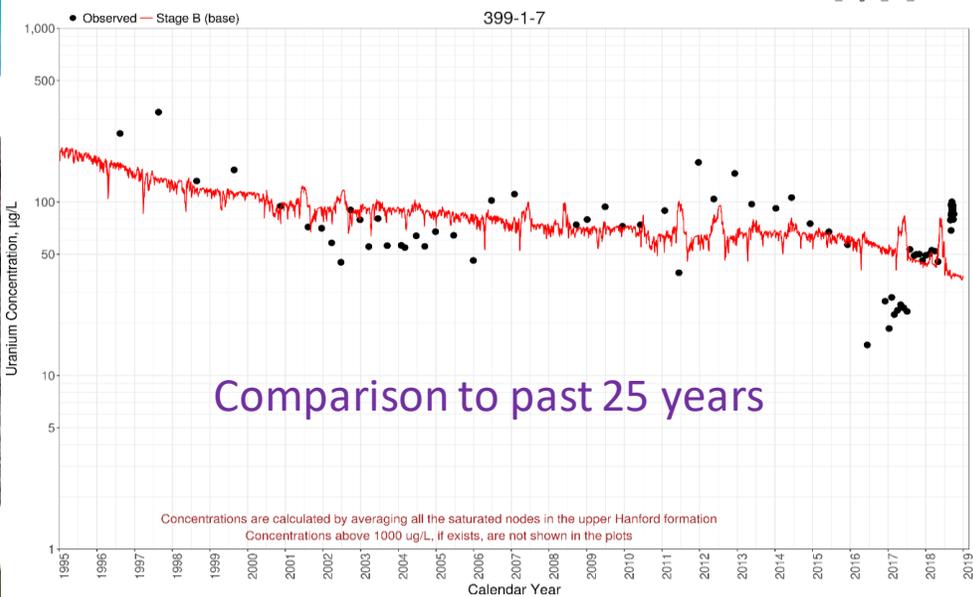
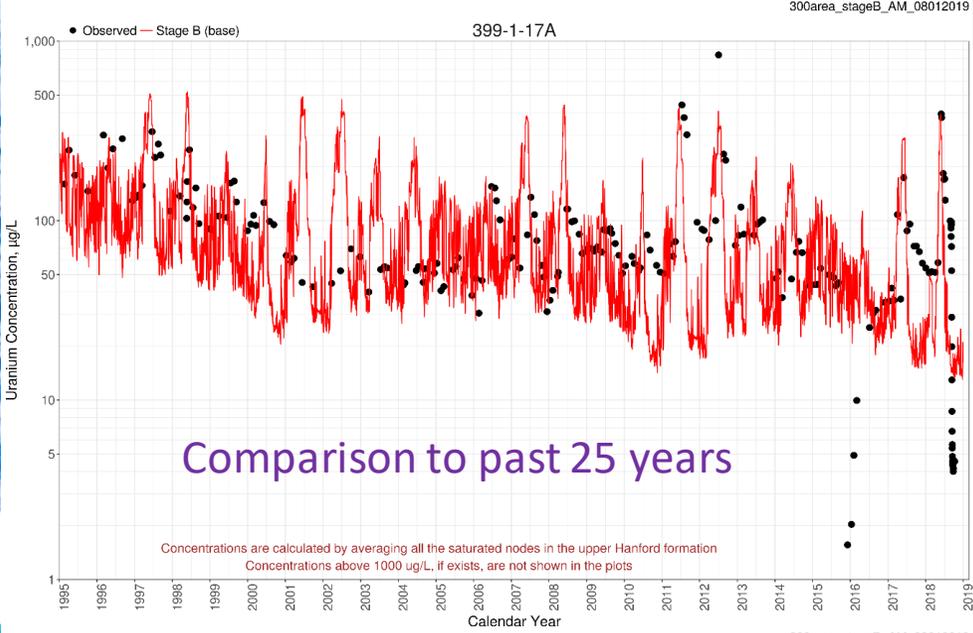
## Calibrated Flow Model



## Calibrated Tracer Model: Riverwater-GW mixing



# System Scale: Stage B Model

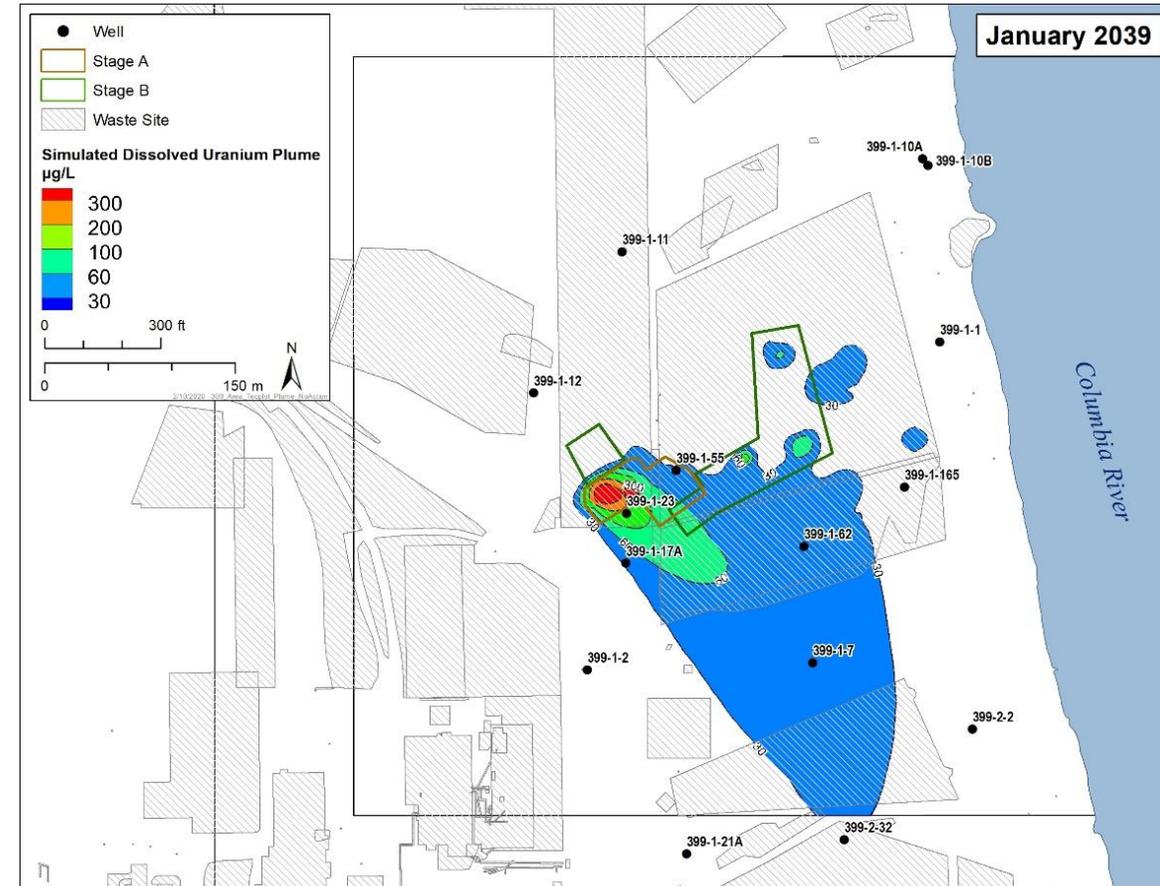


# System Scale: Stage B Model

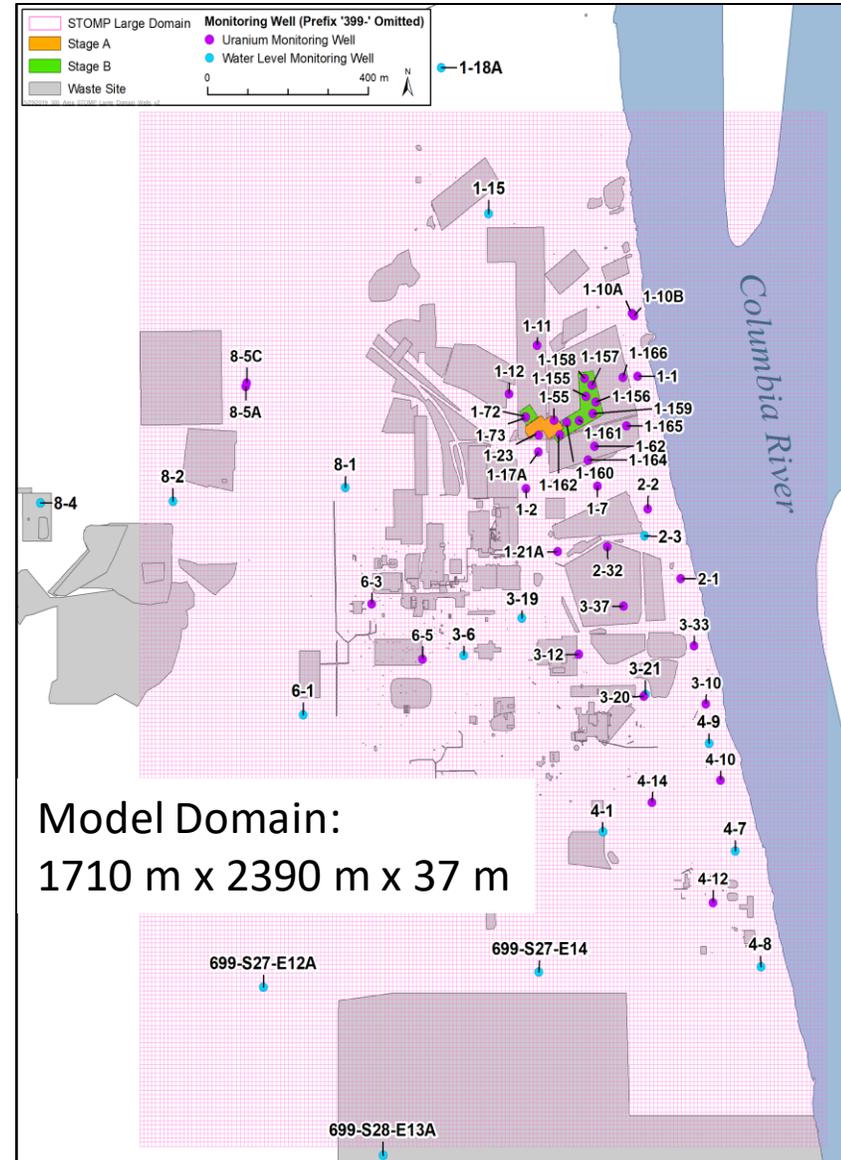
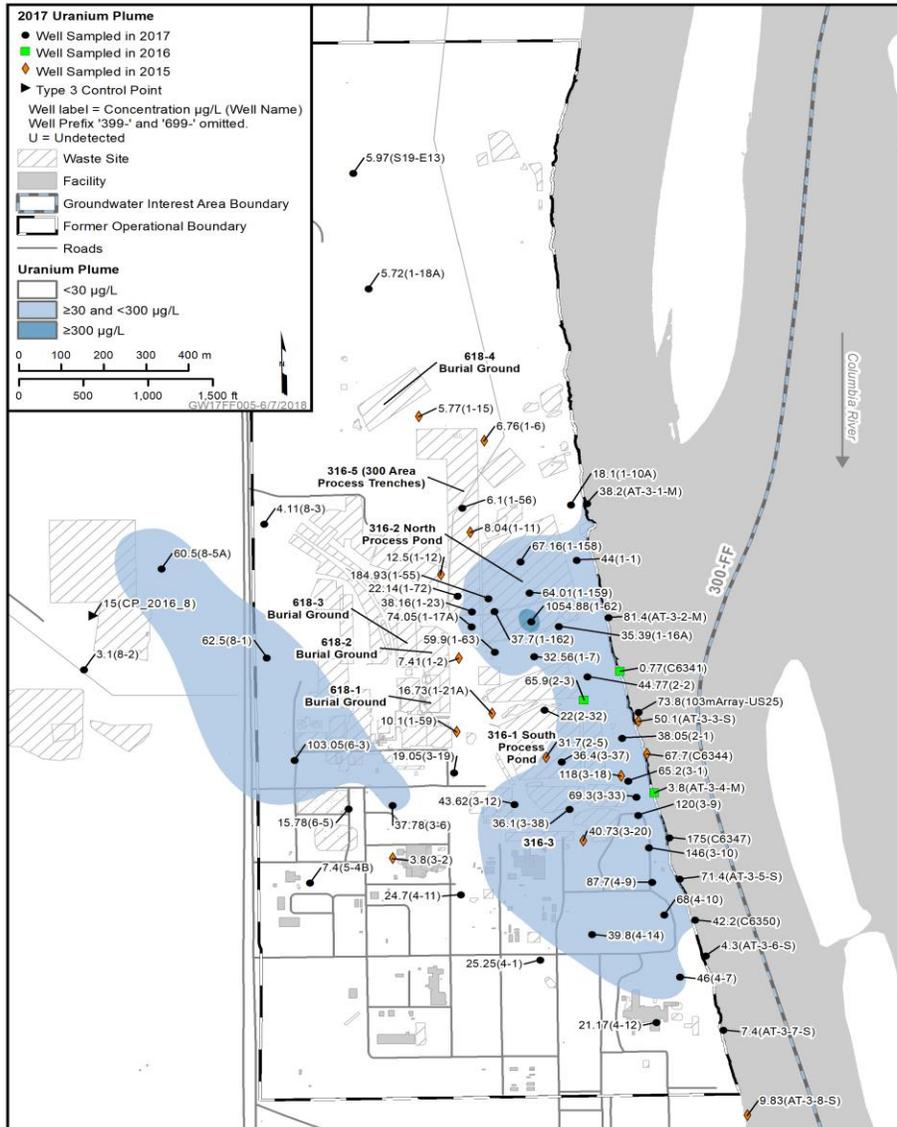
Model Prediction: Enhanced Attenuation Remedy



Model Prediction: Under No Action Scenario

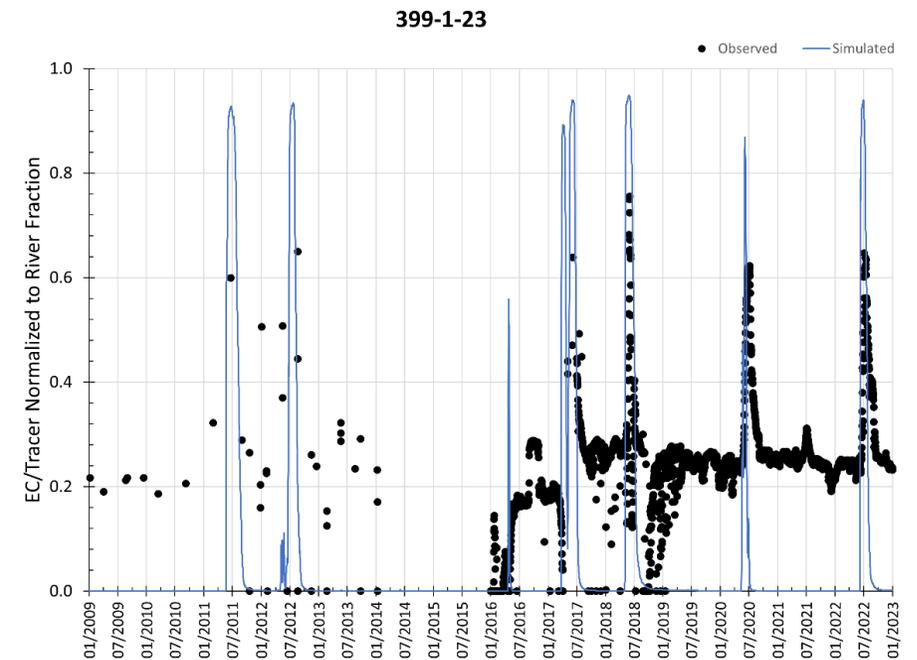
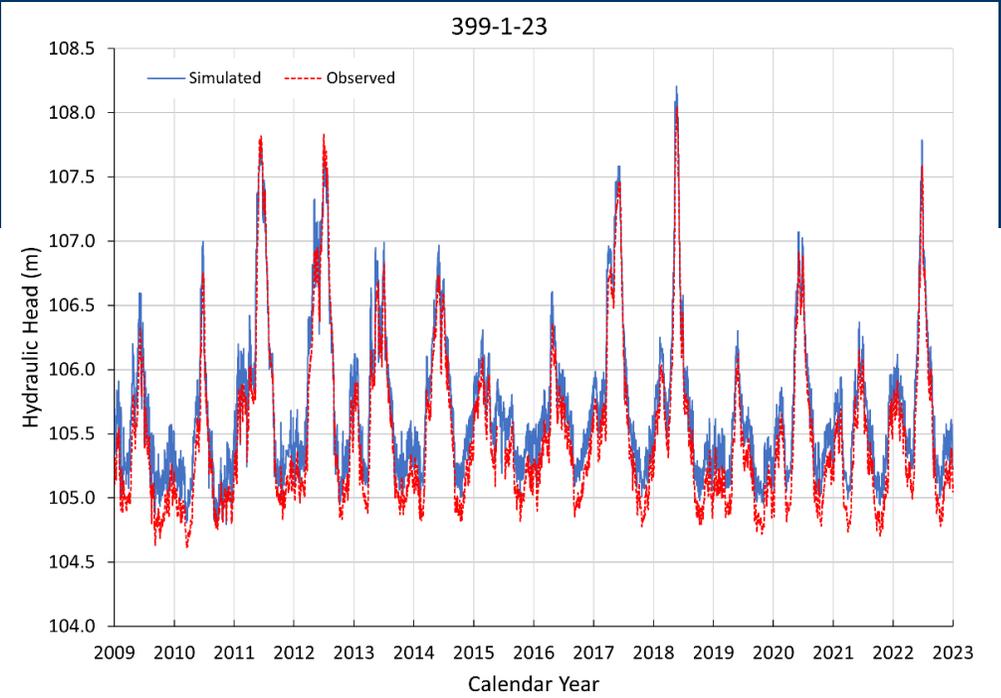
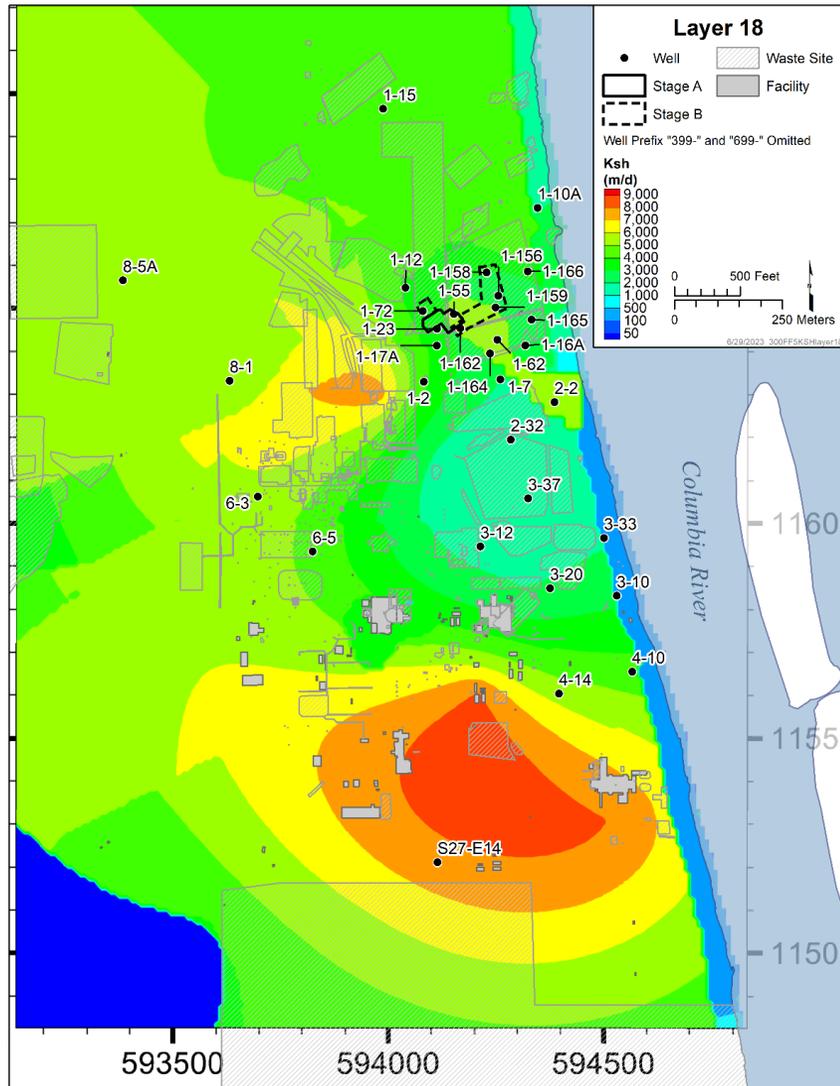


# Large Domain Model

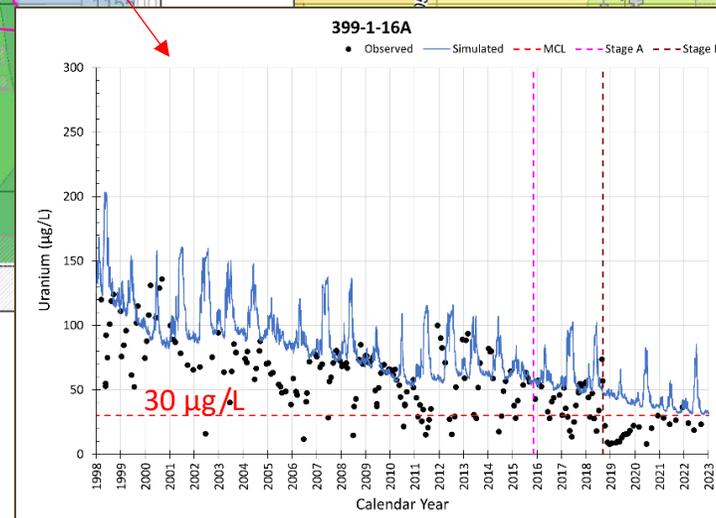
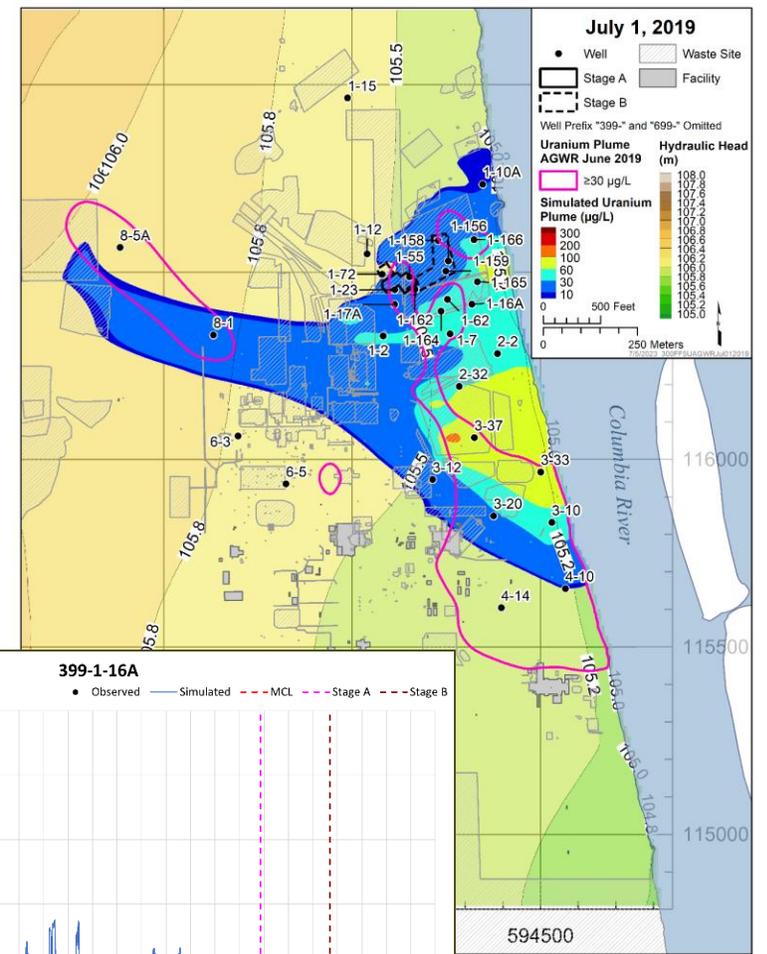
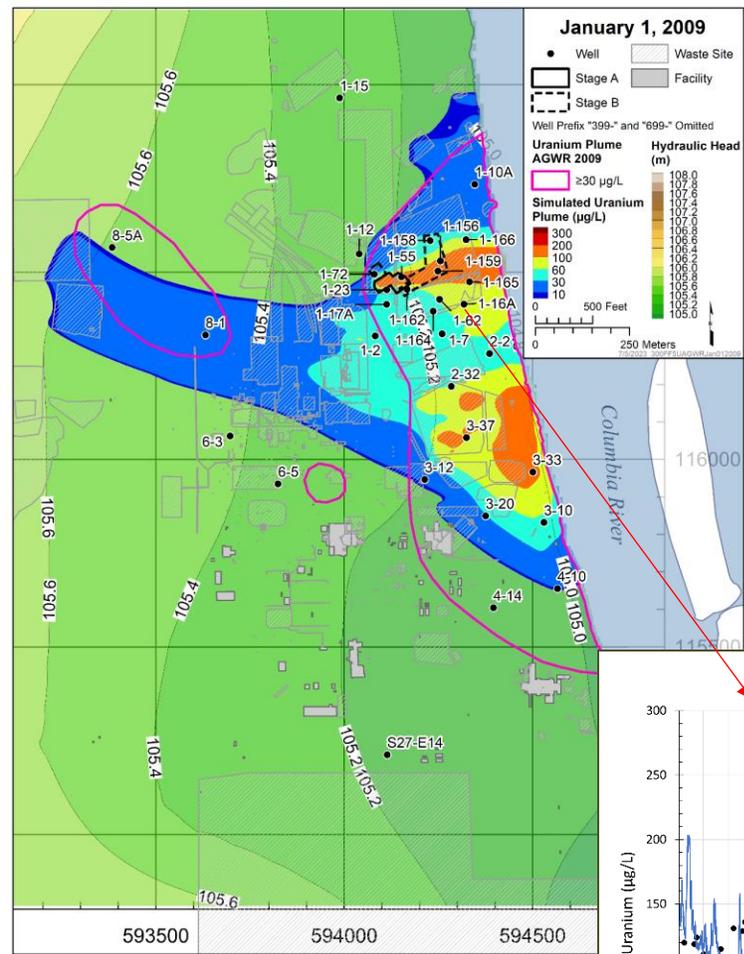
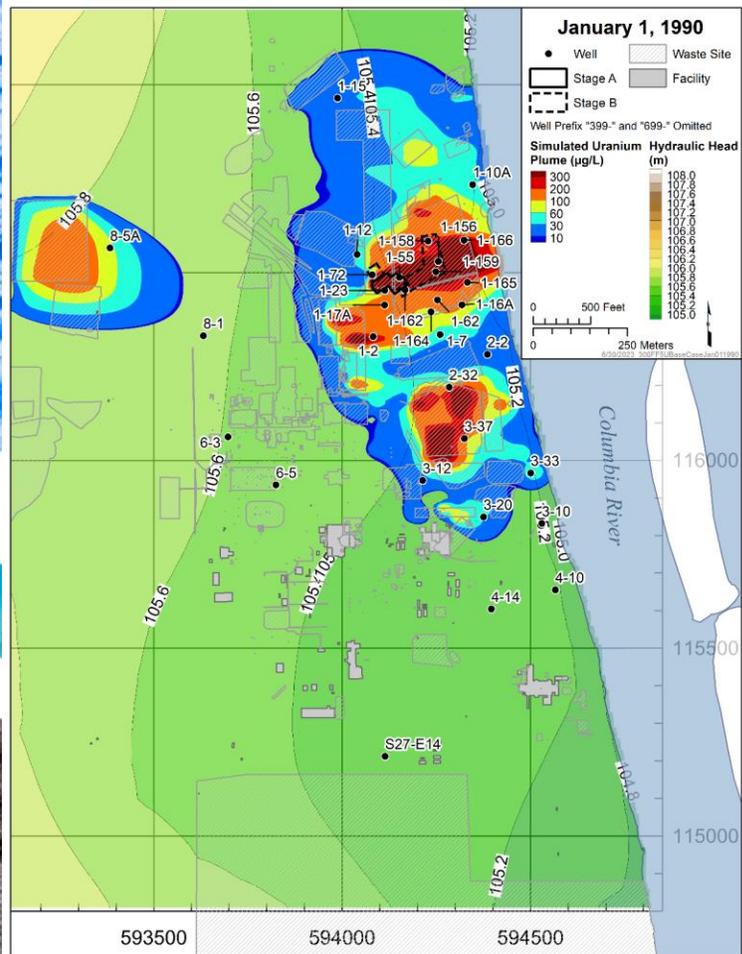


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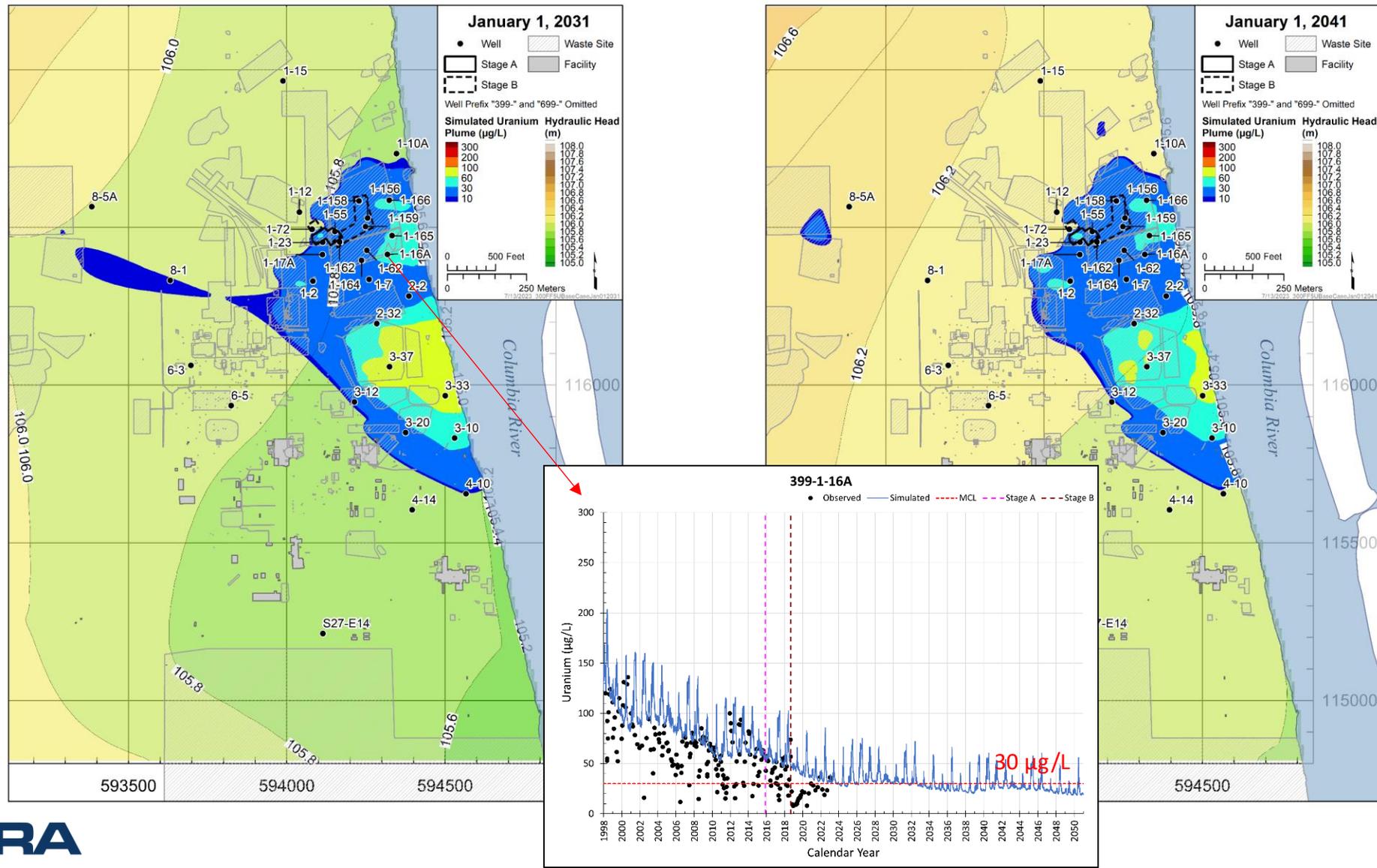
## Calibrated Hydraulic Conductivity Field (using PEST)



# Large Domain Model: Comparison to Observations



# Large Domain Model: Predictions



# Conclusions

- Evaluation of remedy performance of uranium plume in the 300 Area of the Hanford Site was performed using multiscale modeling
  - Kinetic sorption/desorption parameters based on flow-through column tests (core scale)
  - Effect of polyphosphate solution injections evaluated using a detailed reactive transport model near an injection well
  - Focused system-scale modeling performed to evaluate Stage A & B injection impact in the subsurface (for evaluation of enhanced attenuation)
  - Larger scale modeling performed to evaluate overall remedy performance over next two decades
- Enhanced attenuation through polyphosphate injection appears to be effective in reducing the mobilization of uranium (sequestration)
- Uranium concentrations continue to decline and by 2050 the plume area is predicted to be significantly reduced