



INTEGRATED CARBON CAPTURE AND CONVERSION: A ROADMAP FOR ECONOMICALLY CAPTURING AND RECYCLING CO₂

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PNNL-SA-182652



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Energy Sciences Center
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PNNL is one of DOE's **most diversified** national laboratories



\$1.34B Spending



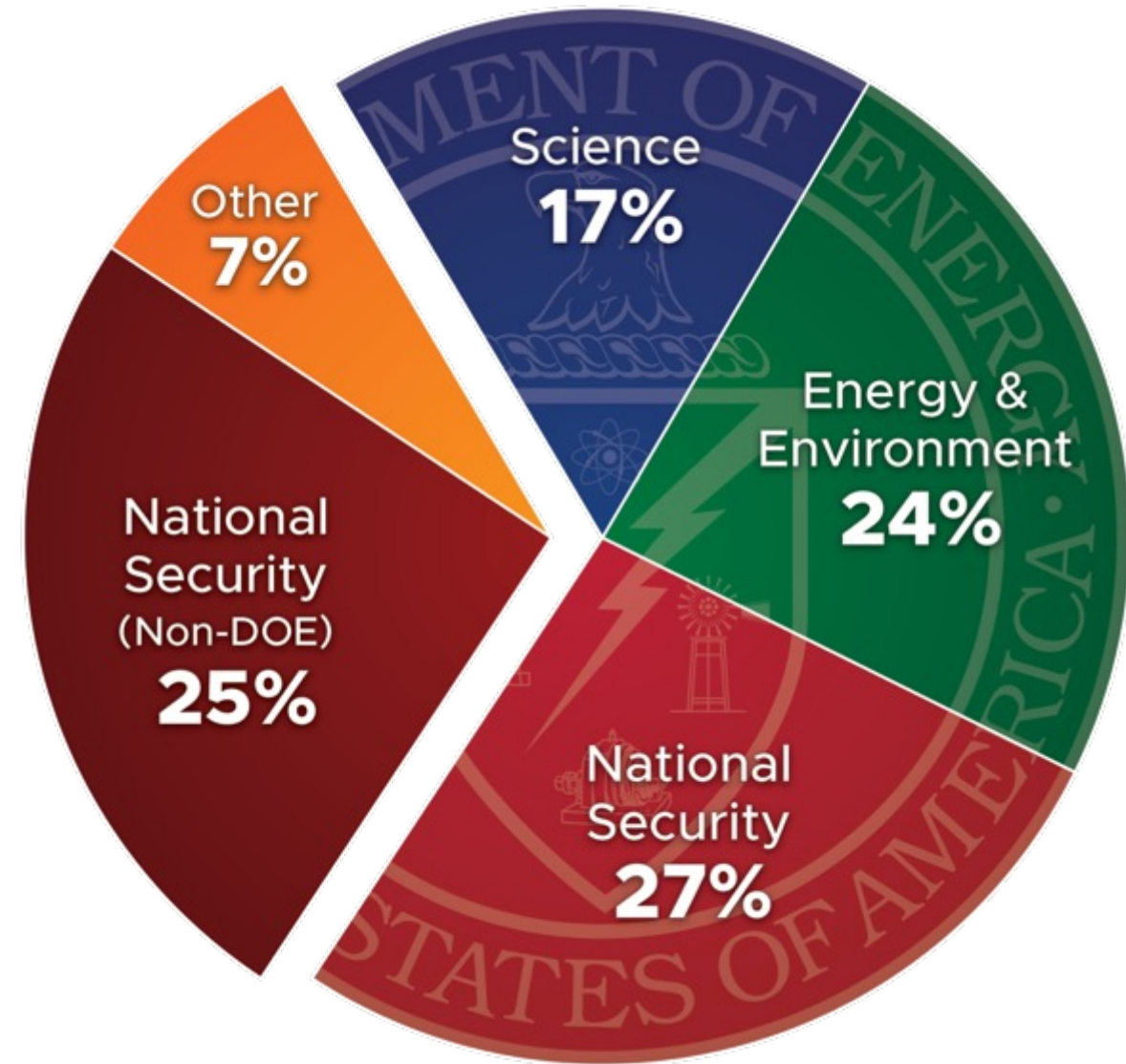
5,700 Staff



1,755 Peer-reviewed Publications*



272 Invention Disclosures

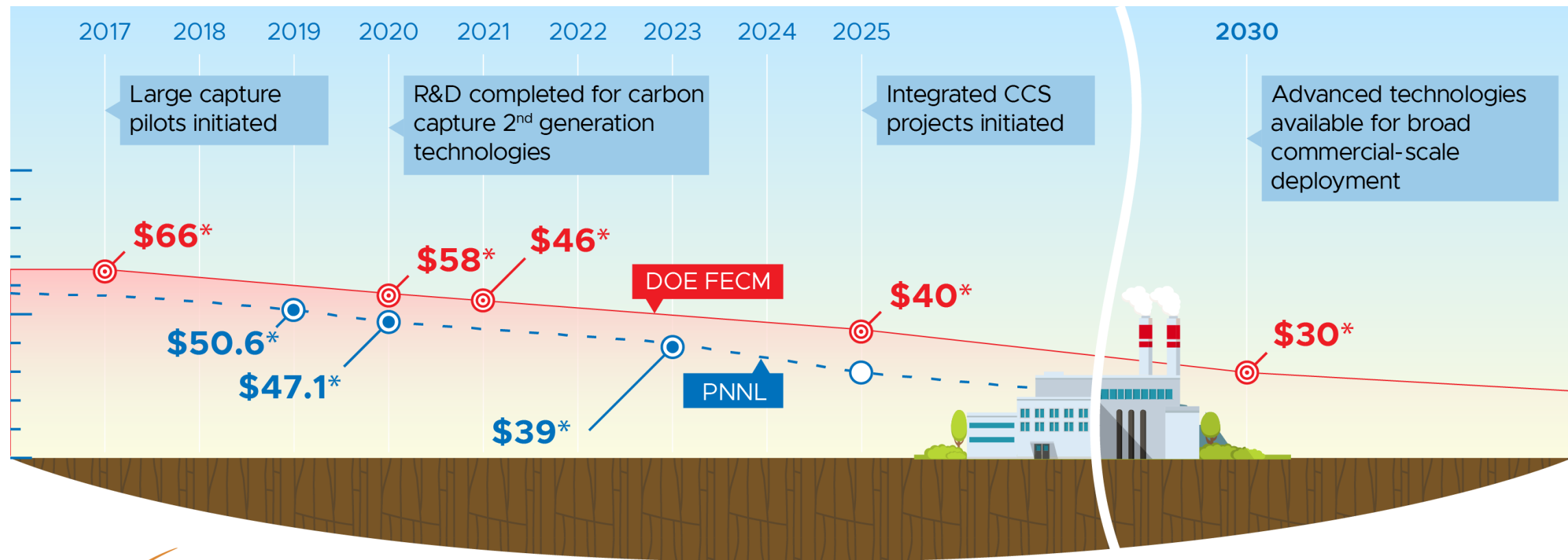


FY 2022 Spending

*Available peer-reviewed publication data are from FY 2021

Research Objective: Achieve Potential Step-Change Reductions in Total Costs of Capture

PNNL's goal is to make step-change progress towards the DOE target of \$30/tonne CO₂—well before year 2030.



What factors into the costs of CO₂ capture?

The costs in \$/tonne CO₂ are 1/2 energy, and 1/2 equipment costs.

Reactivating a solvent requires 2.3-3.6 GJ/tonne CO₂, enough power for 23,000-36,000 100W light bulbs

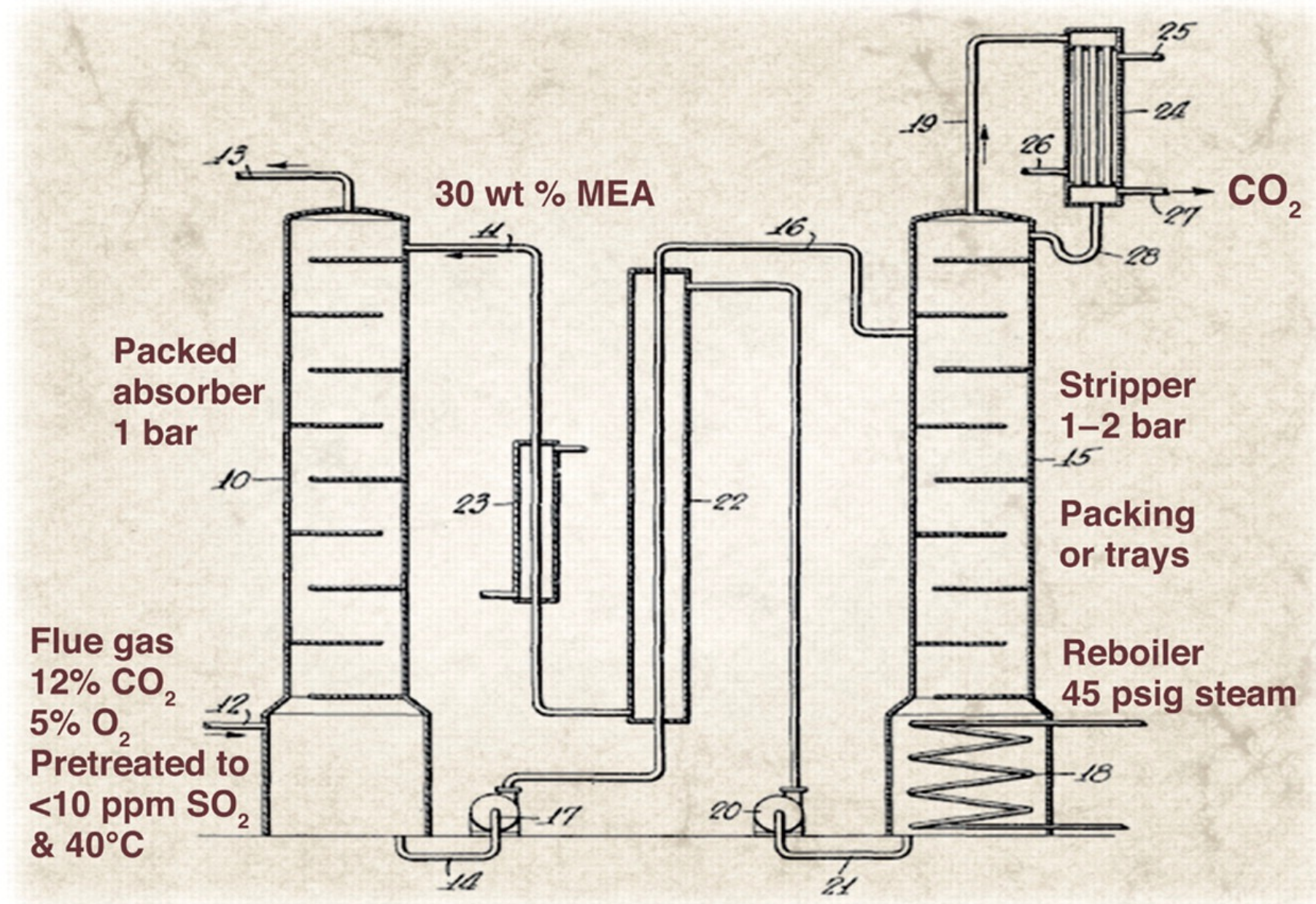


- A capture unit for a 650 MW powerplant costs \$739 M USD.
- Capture costs scale to point source

**We have to reduce energy costs and capital costs.*

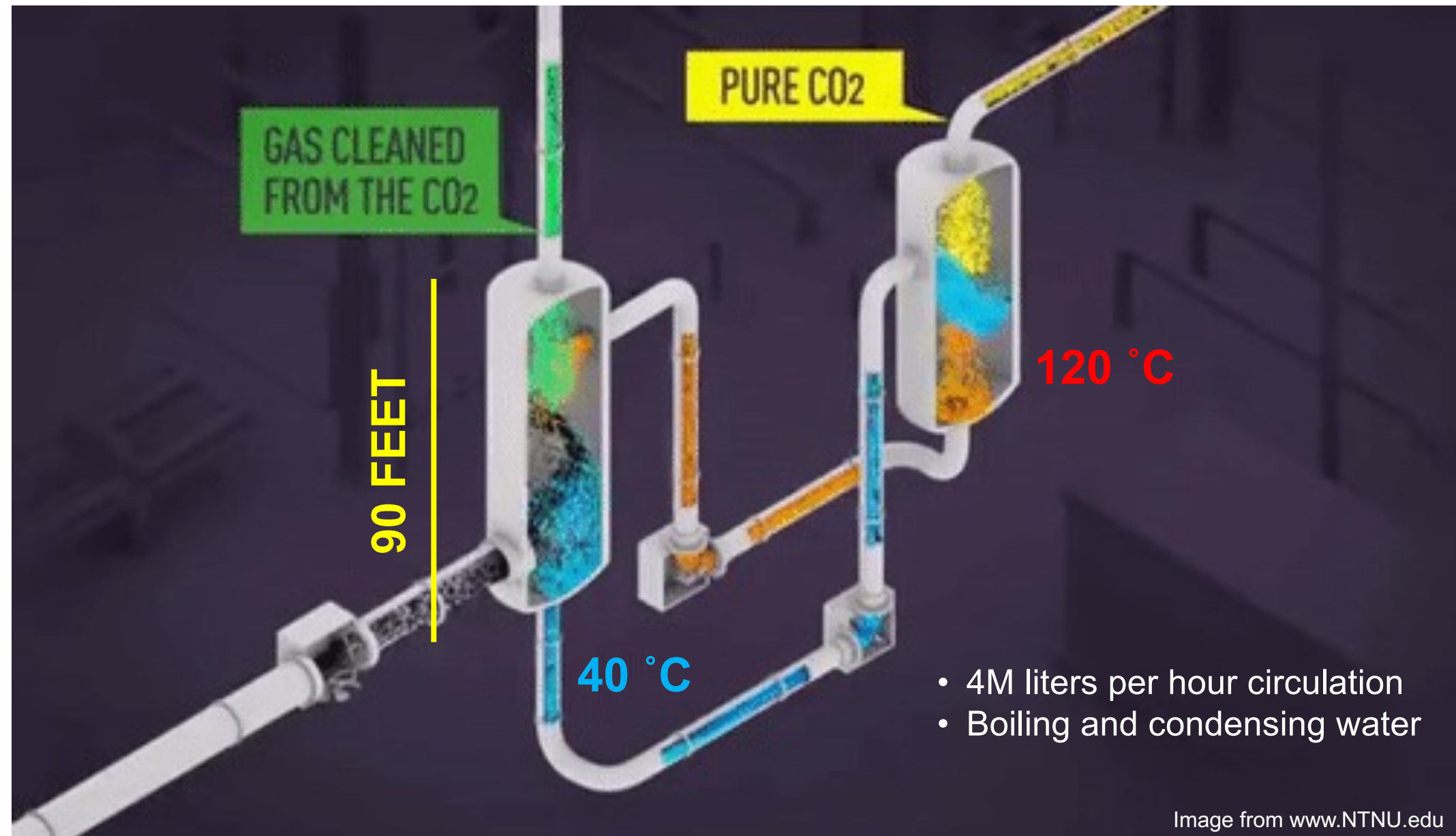
History of Solvent-Based Flue Gas Purification

CO₂ Capture has been around for 90 years, having first been patented by R. R. Bottoms in 1930, MEA first discovered in 1897.



Modern Day Solvent-Based Flue Gas Purification

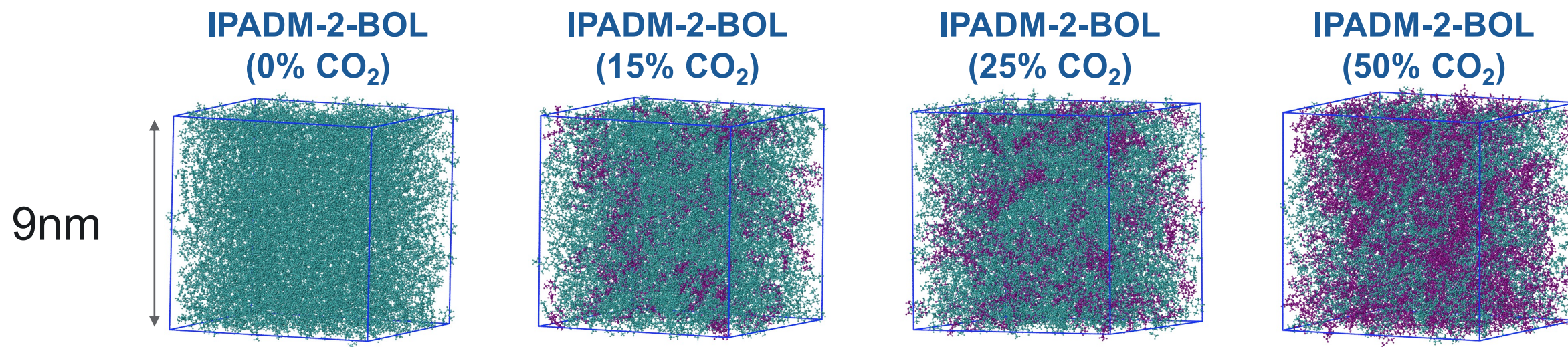
21st century engineering with 19th century solvents.



Our Approach: 21st century chemistry, replace the aqueous (70%) solvent with >95% organics.

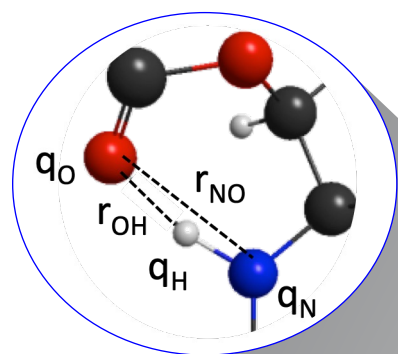
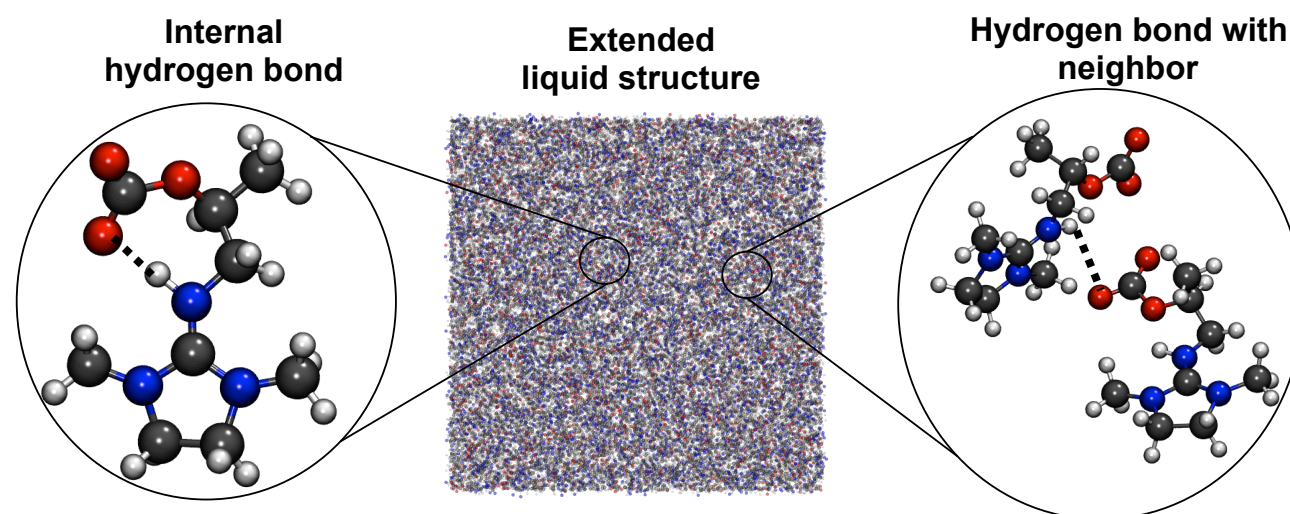
Concentrated Solvents Differ vs. Aqueous Solvents

We've looked at molecular structures to identify how behavior emerges.¹

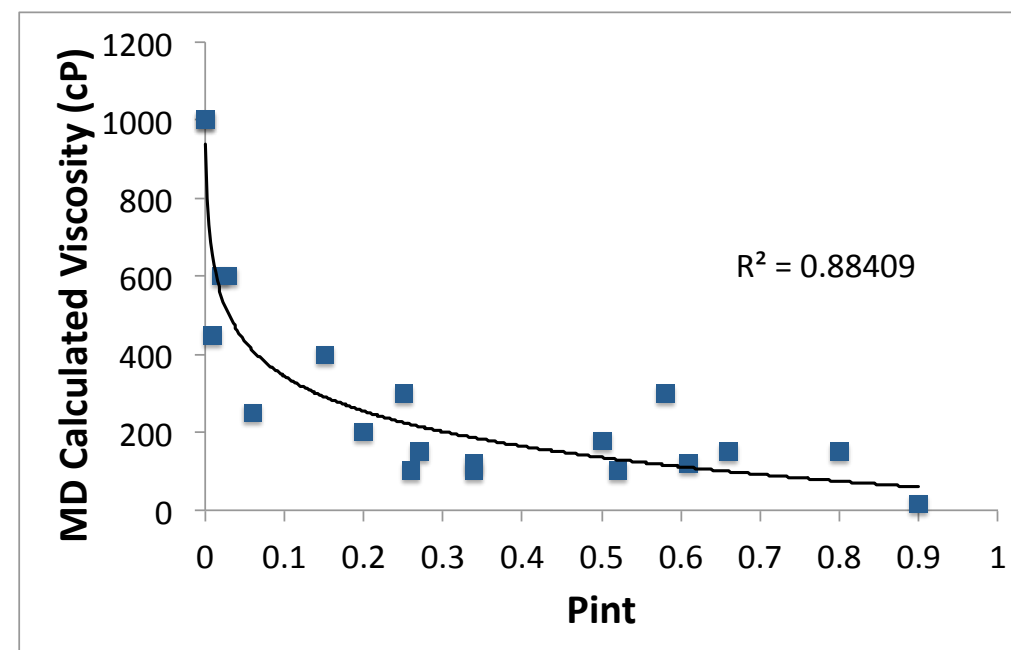
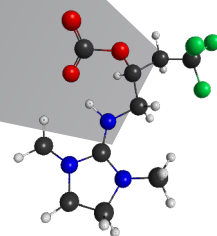


Re-designing Solvents While Retaining Desired Properties

We use theory to visualize molecular-level changes and explain phenomena such as viscosity, vapor pressure etc.



$$X = \frac{q_N q_O}{r_{NO}} - \frac{q_O q_H}{r_{OH}}$$



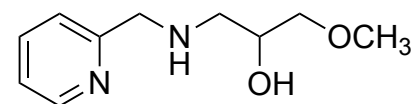
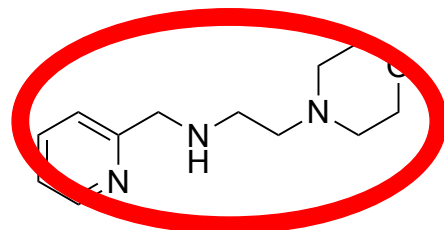
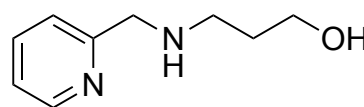
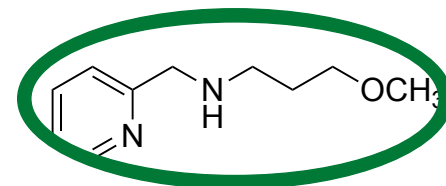
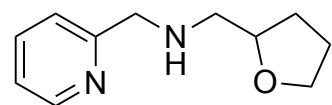
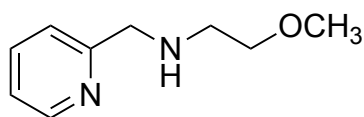
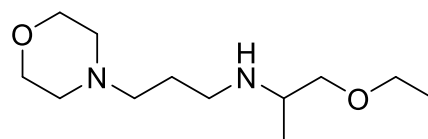
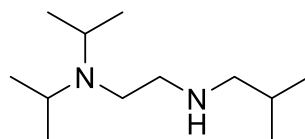
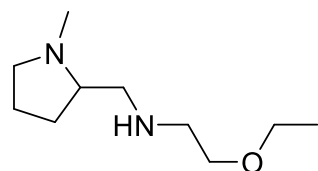
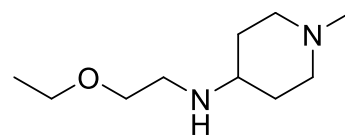
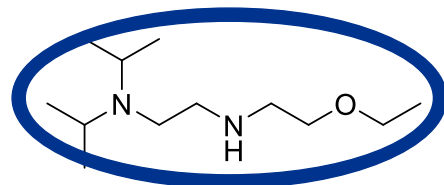
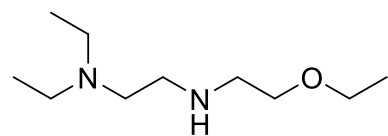
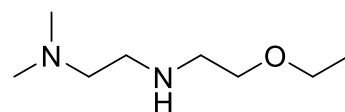
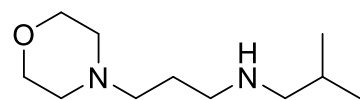
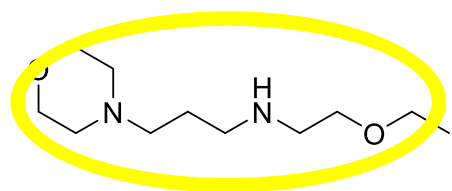
$$P_{int} = c_1 X + c_2$$

Important Design Criteria:

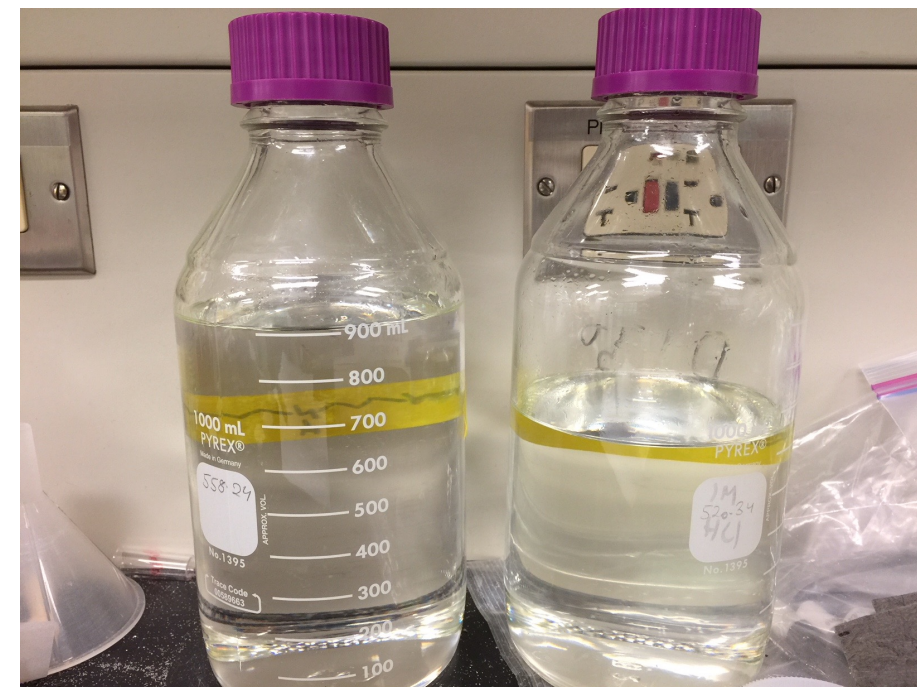
- Vapor pressure
 - < 0.0001 atm
- Binding enthalpy
 - -60 to -85 kJ/mol
- Synthesis Cost
 - <\$10/kg
- Toxicity
- No halogens

Designing and Synthesizing Bespoke 3rd Gen Solvents

Molecular library for down-selection using our reduced order model to down-select from remaining non-viscous derivatives.



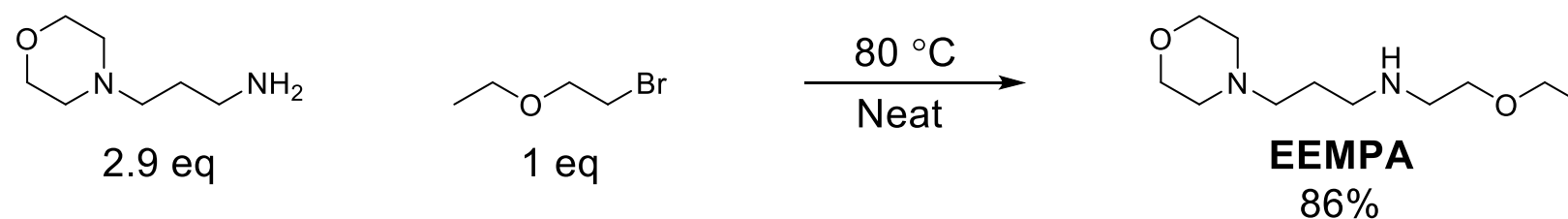
GE Global Research



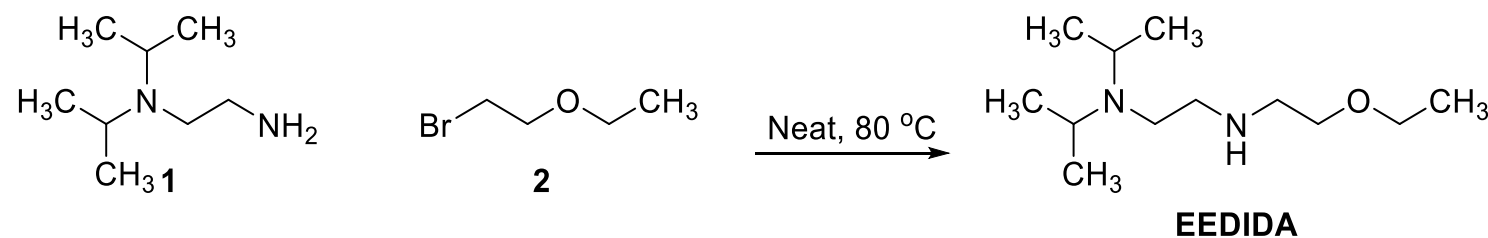
Synthesis of 3rd Gen Solvents, \$10/kg Target

Synthesis uses off-the-shelf reagents available at tonnage quantities.

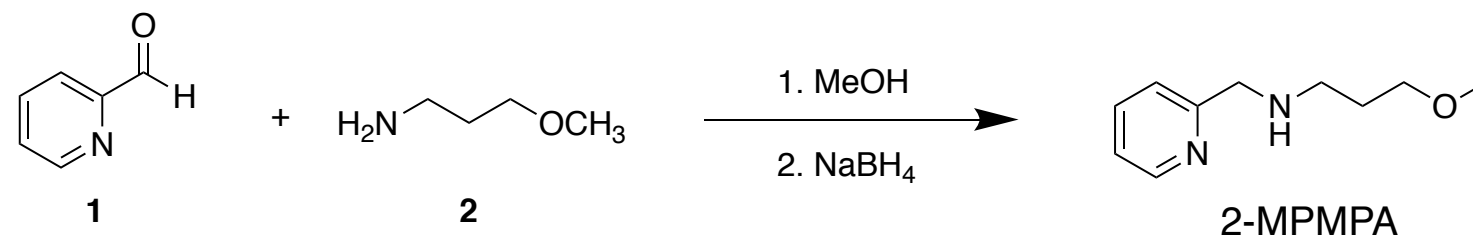
- Commercial scale synthesis via more complex routes using cheaper reagents projected to bring costs to ~\$5/kg.



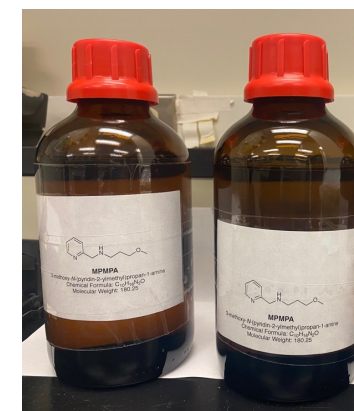
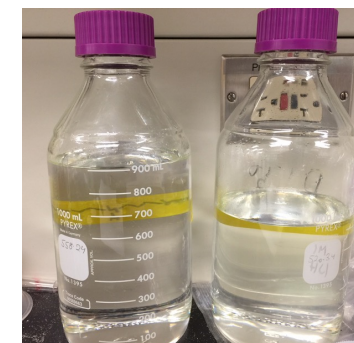
Zheng et al. *Energy Environ. Sci.*, **2020**, *13*, 4106-4113.



Barpaga et al. *ACS Env. Sci. Tech.*, **2022**, *10*, 14, 4522-4528.

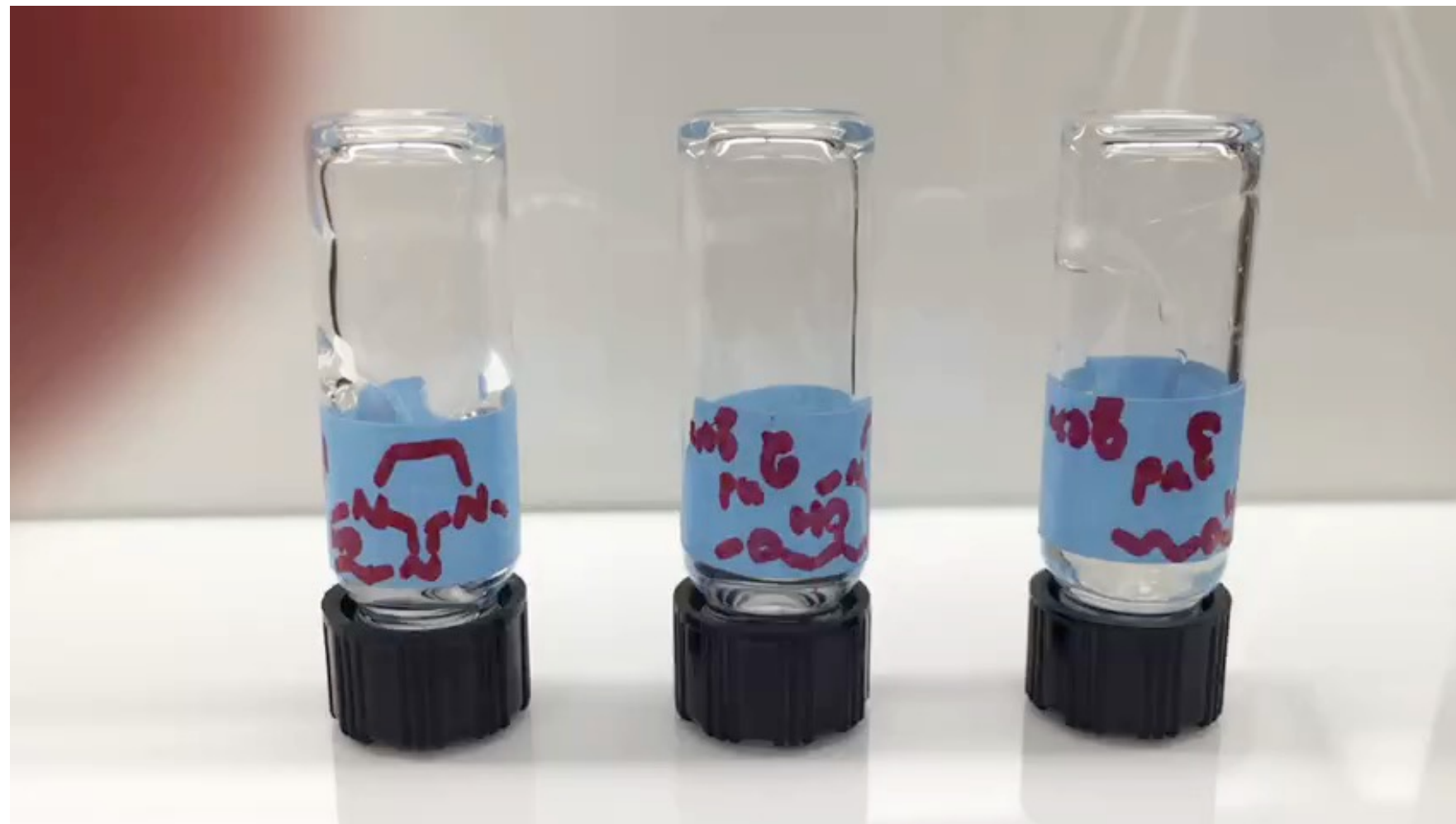


Jiang et al. **2022**, *J. Clean. Prod.* doi.org/10.1016/j.jclepro.2022.135696.



Testing 3rd Gen Candidates

New derivatives are 98% lower in viscosity while retaining other properties.

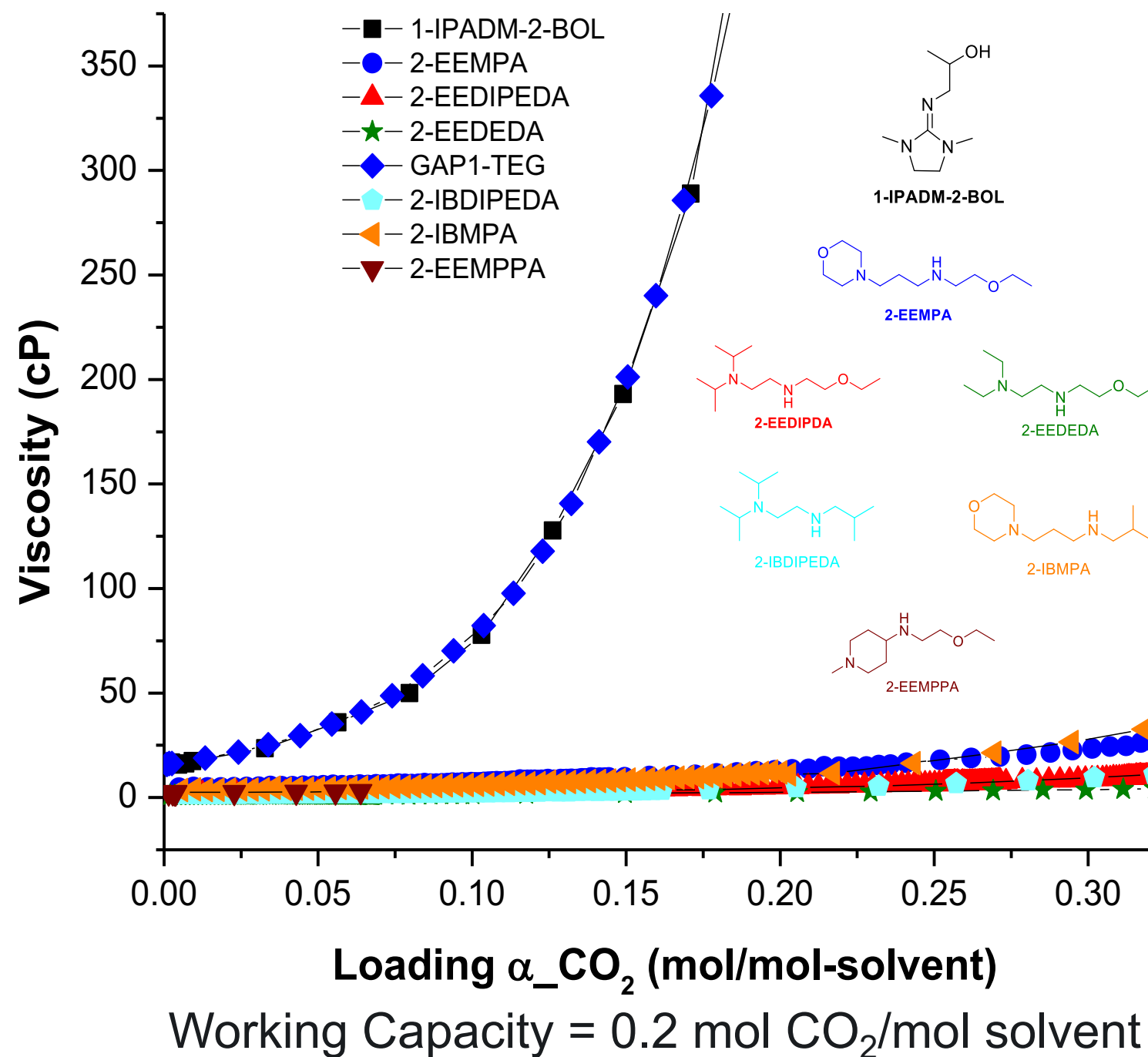


CO₂BOL Generations



Testing 3rd Gen Candidates

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Measuring Solvent Properties With Custom Instrumentation

Rigorous measurements of vapor-liquid equilibria (PTx) and mass transfer.



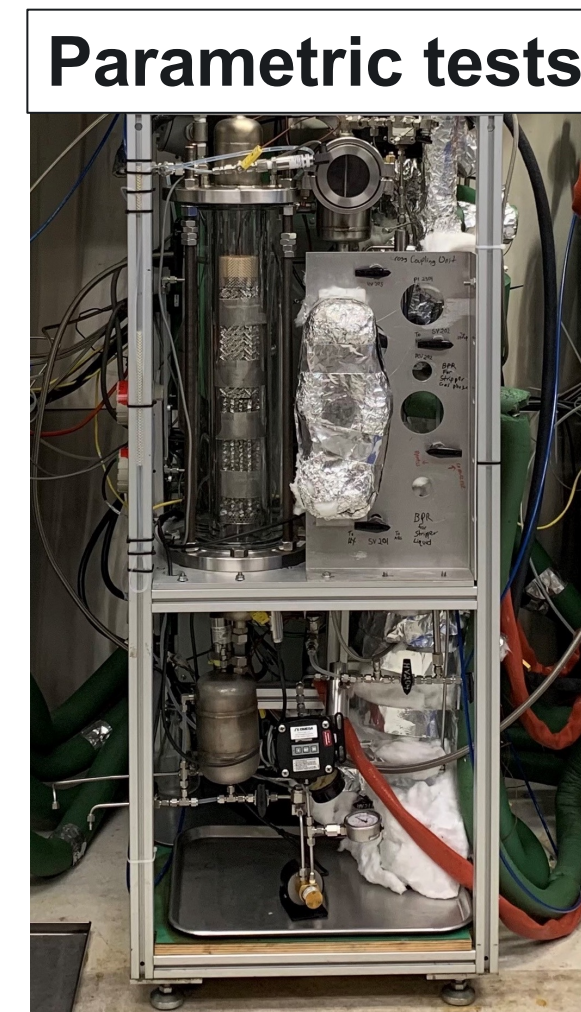
Pressure Volume
Temperature (PVT Cell)

50 milliliter



Wetted Wall
Column (WWC)

1 liter

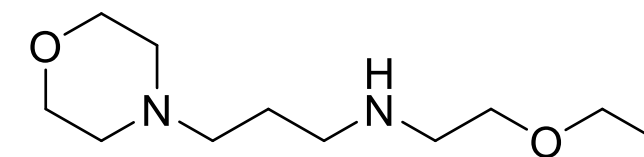


Lab Continuous Flow
System (LCFS)

5 liter

5L Lab Scale Continuous Flow Testing

Tested performance on simulated flue gas*
continuously for 40 hours.

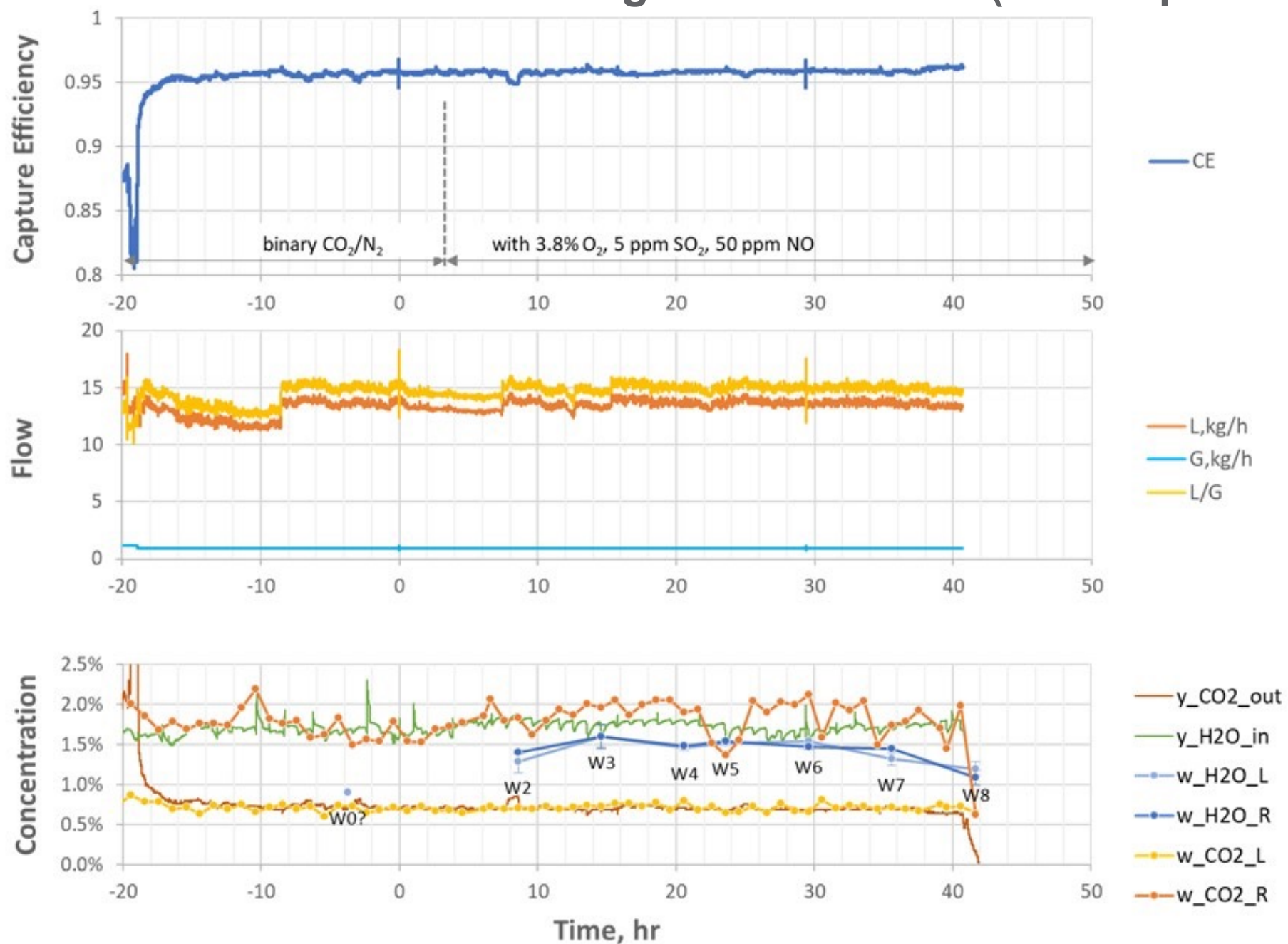
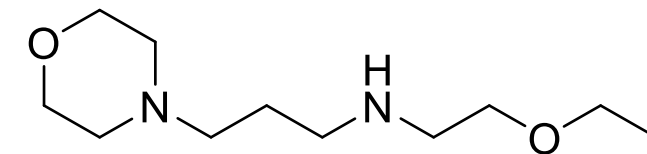


*NO_x, SO_x, O₂, H₂O set to NETL Case 12B.

	MEA ^(a)	Cansolv ^(b)	EEMPA	
NETL Reference	Case 12	Case B12B	Case B12B	Case B12B
Configuration	SS	LVC	SS	AH/IHC/ LVC
Process metrics				
Lean Loading [mol CO ₂ /mol solvent]	0.27	-	0.045	0.045
Water Loading [wt%]	70	-	1.4	1.4
Regeneration Temperature [°C]	115	-	119	113
Equivalent Work [kJ _e /mol CO ₂] ^(c)	50.1	39.4	35.2	32.7
Reboiler Duty [GJ _e /tonne CO ₂]	3.55	2.48	2.27	2.00

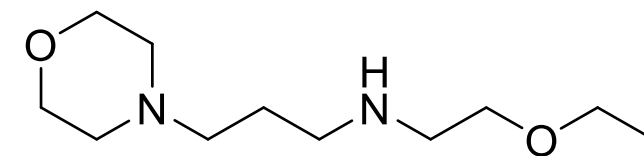
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Running our solvent to test performance on simulated flue gas for 40 hours (96% capture rate).



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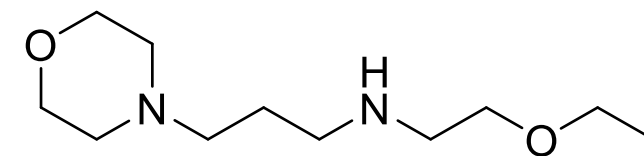


Key test results:

- High capture rates (~96%)
- Water balance (1.5 wt.%)
- Steady-state operation with O₂, NO_x, SO_x
- No foaming, aerosols, phase separations or precipitation

5L Lab Scale Continuous Flow Testing

Running our solvent to test performance on simulated flue gas for 40 hours (96% capture rate).



50L Testing On a 2-Stage Flash

Testing performance on simulated flue gas for 40 hours (90% capture rate).

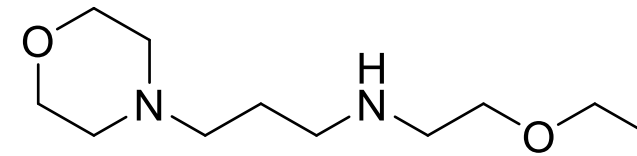


Absorber

- 3" SS316 (8.5 m)
- Mellapak 350X
- Temp: 30-55°C
- Pressure: Up to 200 kPa
- Gas Vel: 0.33-1.5 m/s
- L: 15-75 kg/h

Regenerator

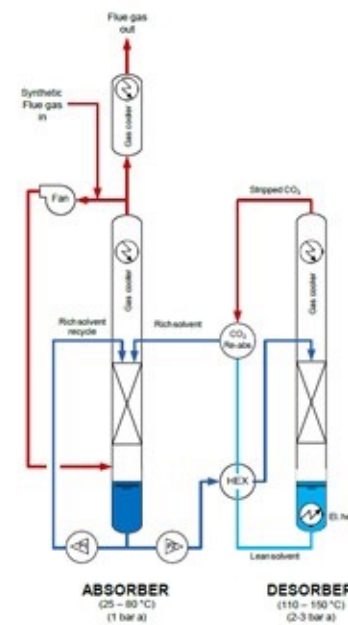
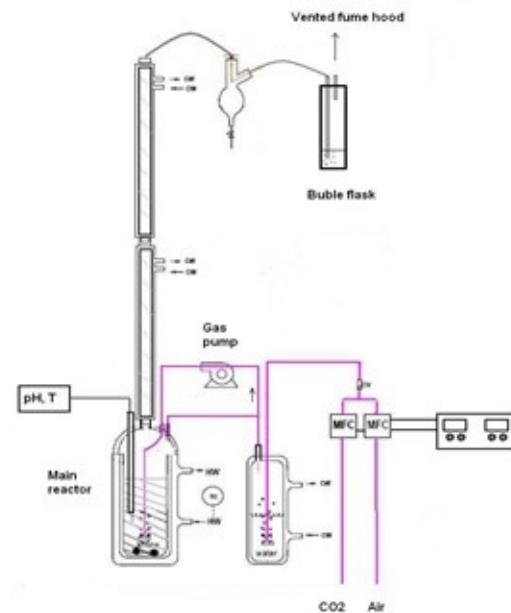
- 3" SS316 (7.1 m)
- Mellapak 350x
- Temp :Up to 150°C
- Pressure: Up to MPa



Assessing Solvent Durability

EEMPA is more durable than MEA under comparable Oxidative and Thermal Degradation conditions.

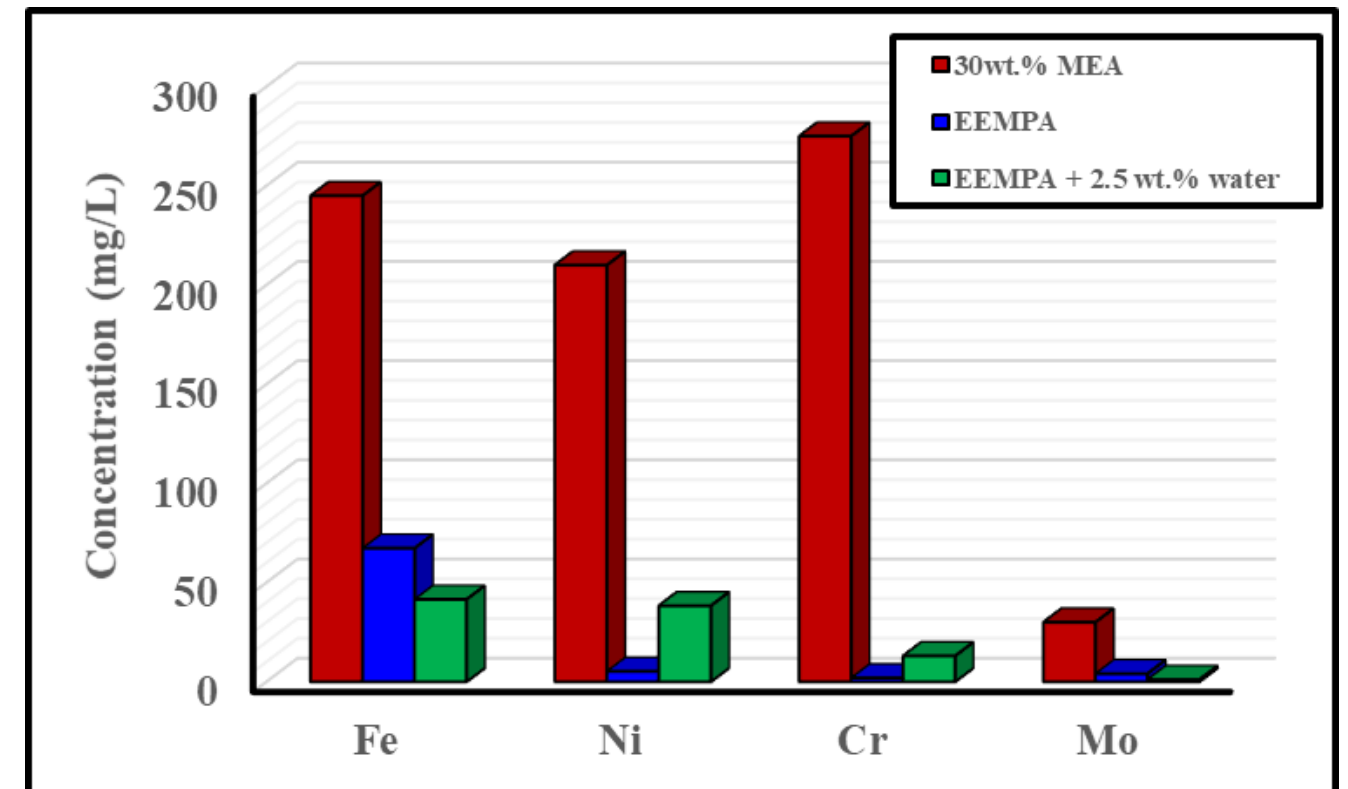
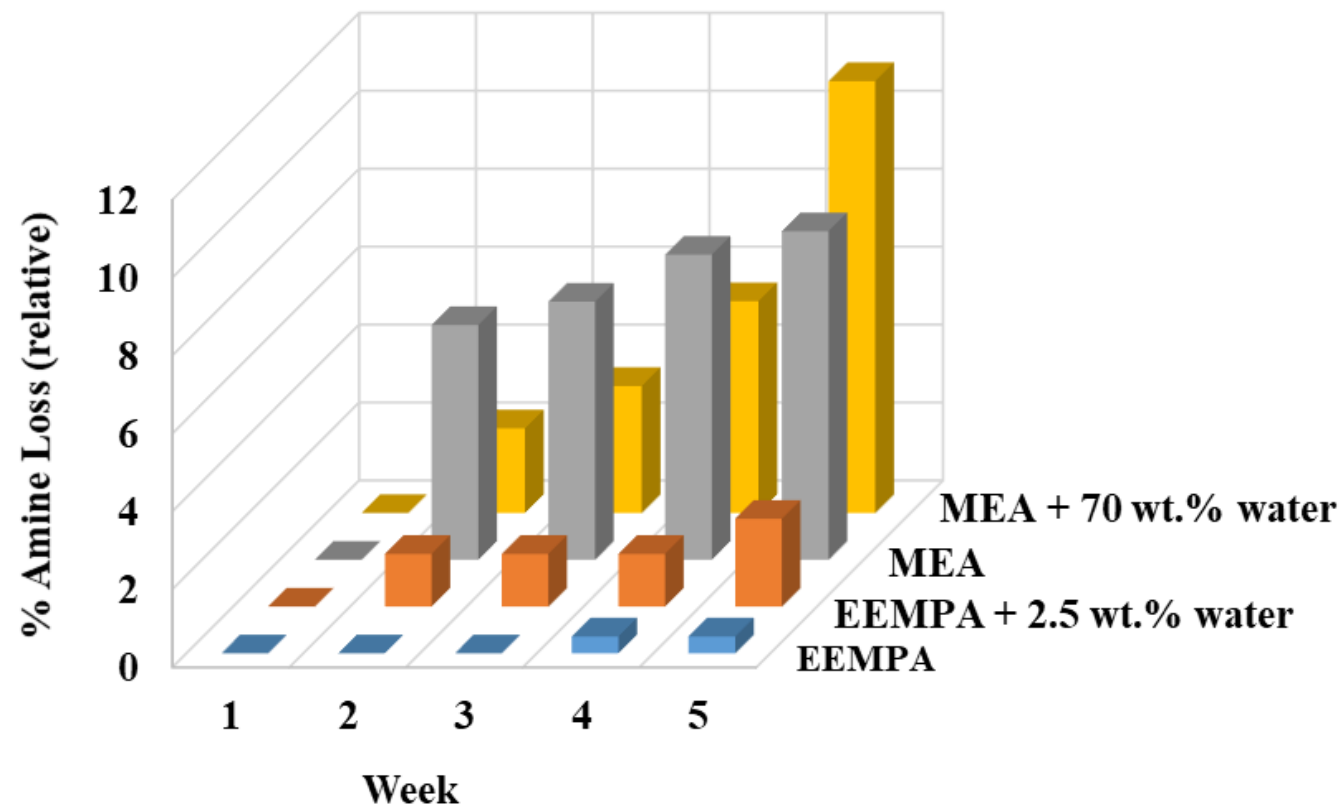
- Thermal: 117°C for 5 weeks.
- Absorber and stripper impurities (O₂, NO_x, SO_x)
- Catalytic leached metals



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- Absorber and stripper impurities (O₂, NO_x, SO_x)
- Catalytic leached metals



Techno-Economic Analysis

Assessing the cost and energetics of simple stripper (SS) and two-stage flash (TSF) configuration using Rev4 Case B12B baseline

- Net power output = 650 MW
- Pricing basis of Dec 2018

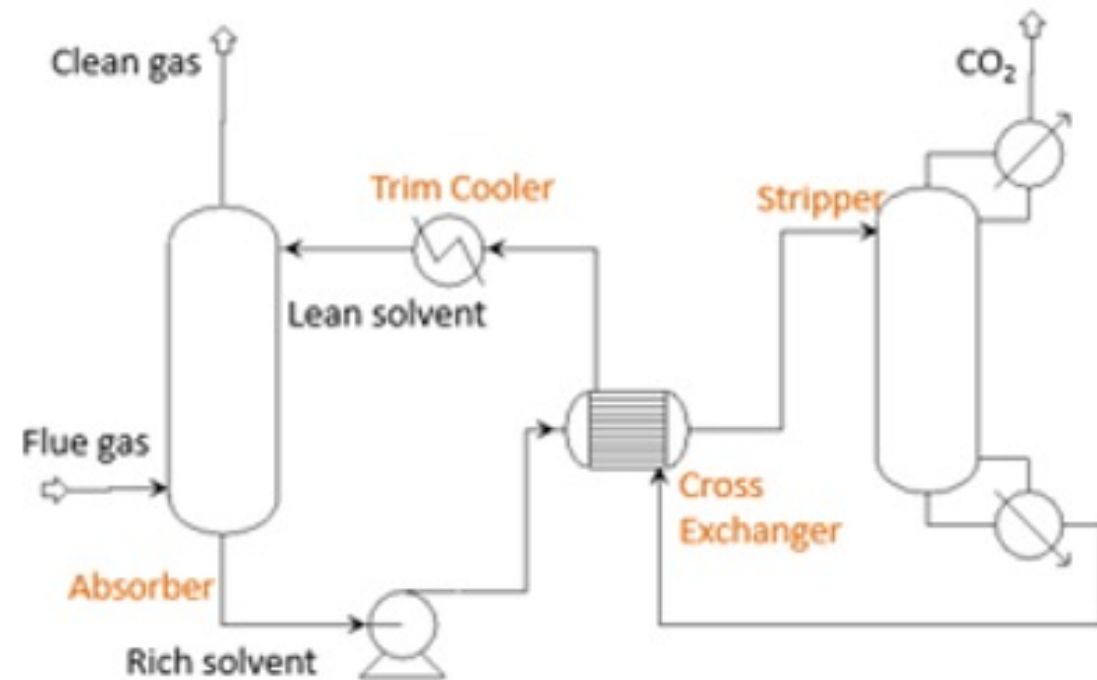


U.S. DEPARTMENT OF
ENERGY

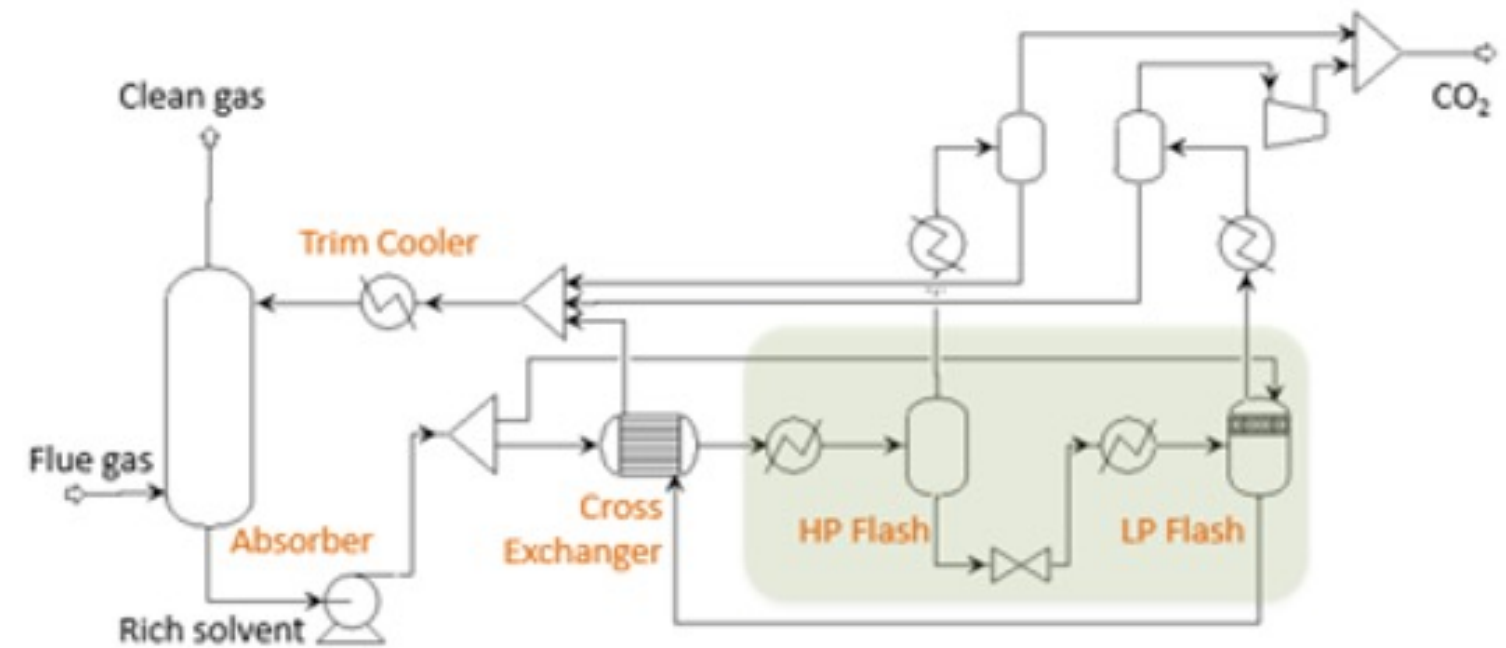


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*NETL-PUB-22638



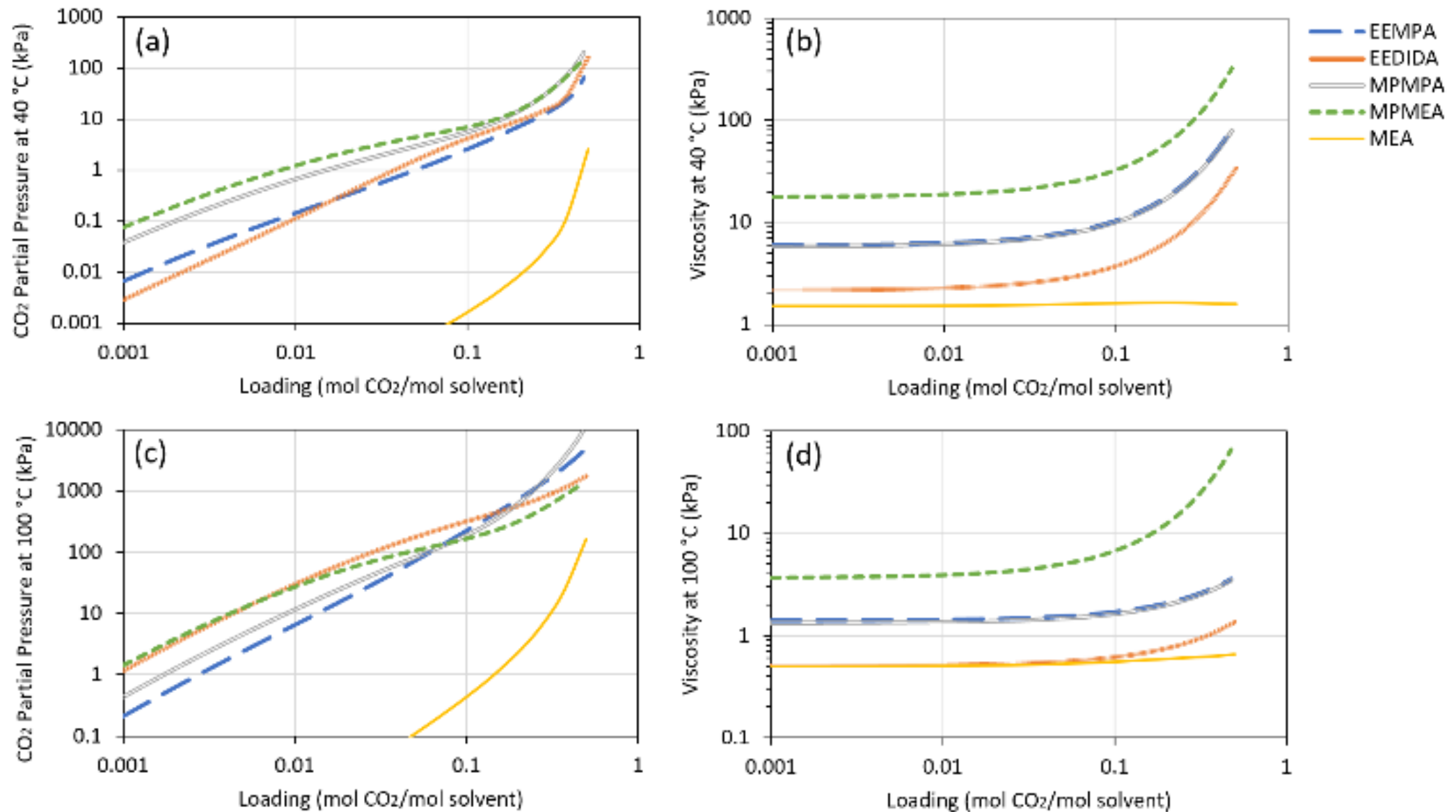
(a) Simple stripper (SS)



(b) Two-stage flash (TSF)

Crafting the Thermodynamic Package

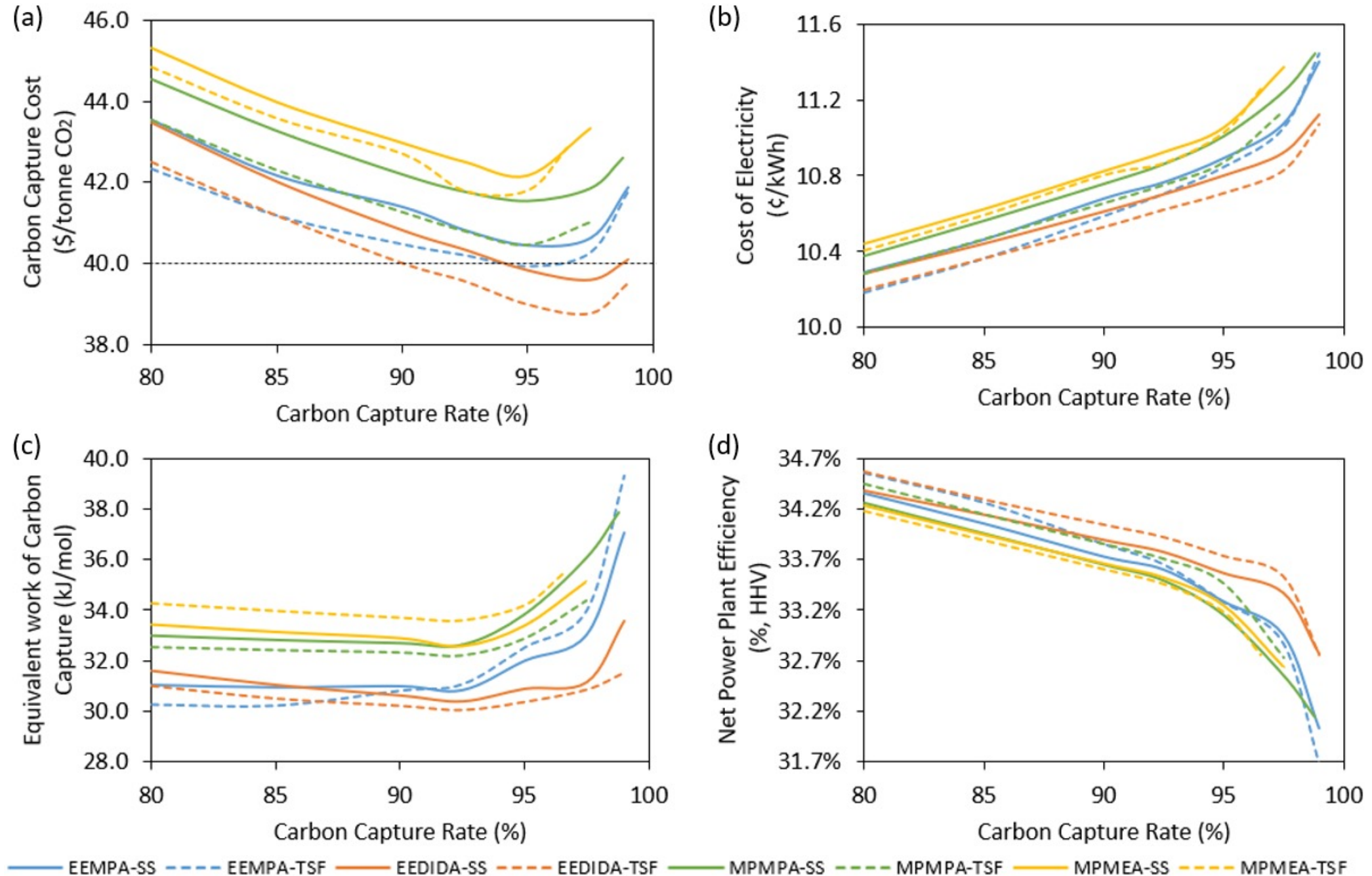
Measured and modeled properties of the 4 solvents to feed ASPEN Plus.



- Equilibrium CO₂ partial pressure and viscosity of CO₂ loaded CO₂BOL solvents and comparison to 30wt% MEA.

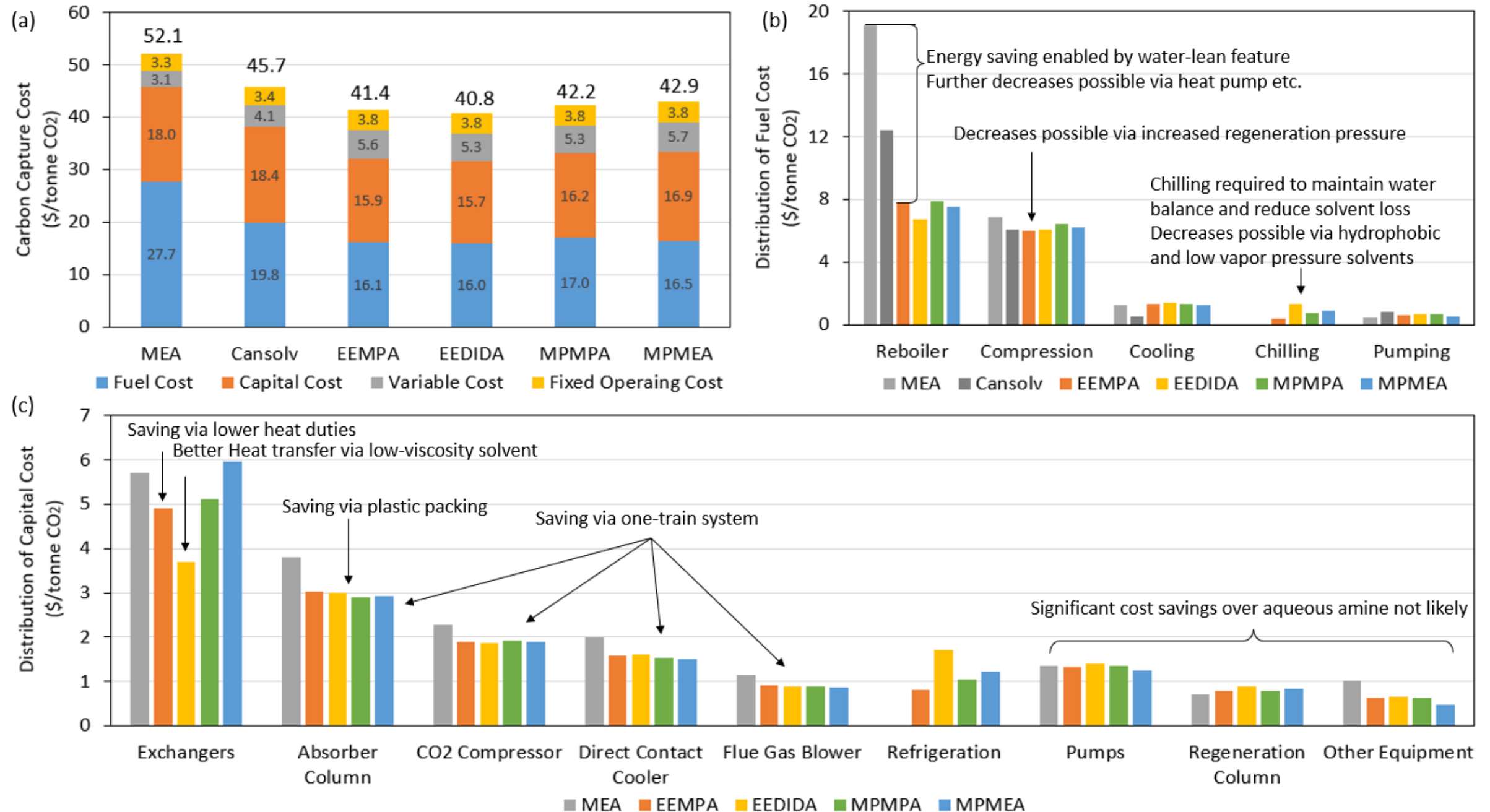
Modeling Varied Process Configurations

Cheapest carbon capture occurs at 95-97%, with 3 solvents < \$40/tonne CO₂.



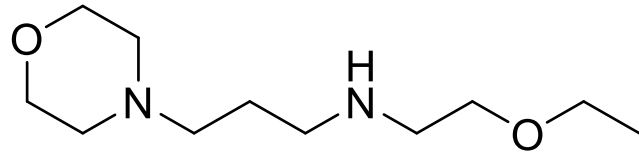
Comparing Energy and Cost for Each Solvent.

Future reductions in carbon capture cost will be primarily CAPEX, not OPEX.



EEMPA is Slated for a Pilot Test in 2023

Project led by EPRI in partnership with RTI International.



- National Carbon Capture Center
 - Alabama, US
 - 0.5 MW scale
 - 2,000 gallons being synthesized
- 6-month test campaign
 - Expected start in November 2023
 - 3 months on coal exhaust
 - 3 months on NGCC exhaust

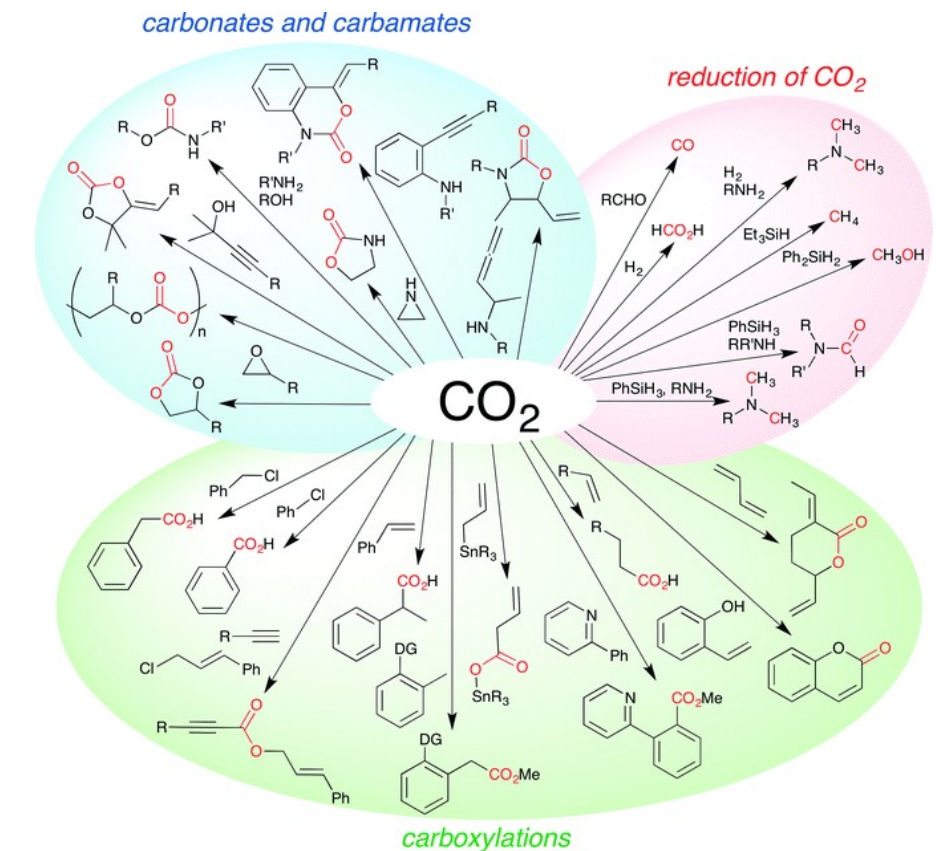


INTEGRATION WITH CONVERSION



Integrated Capture and Conversion of CO₂ into Materials (IC³M)

Vision: A solvent-based CO₂ capture unit becoming a refinery capable of making (many) materials from CO₂.



Near term targets

carbon-neutral fuels and chemicals:
CH₃OH, CH₄

Intermediate term targets

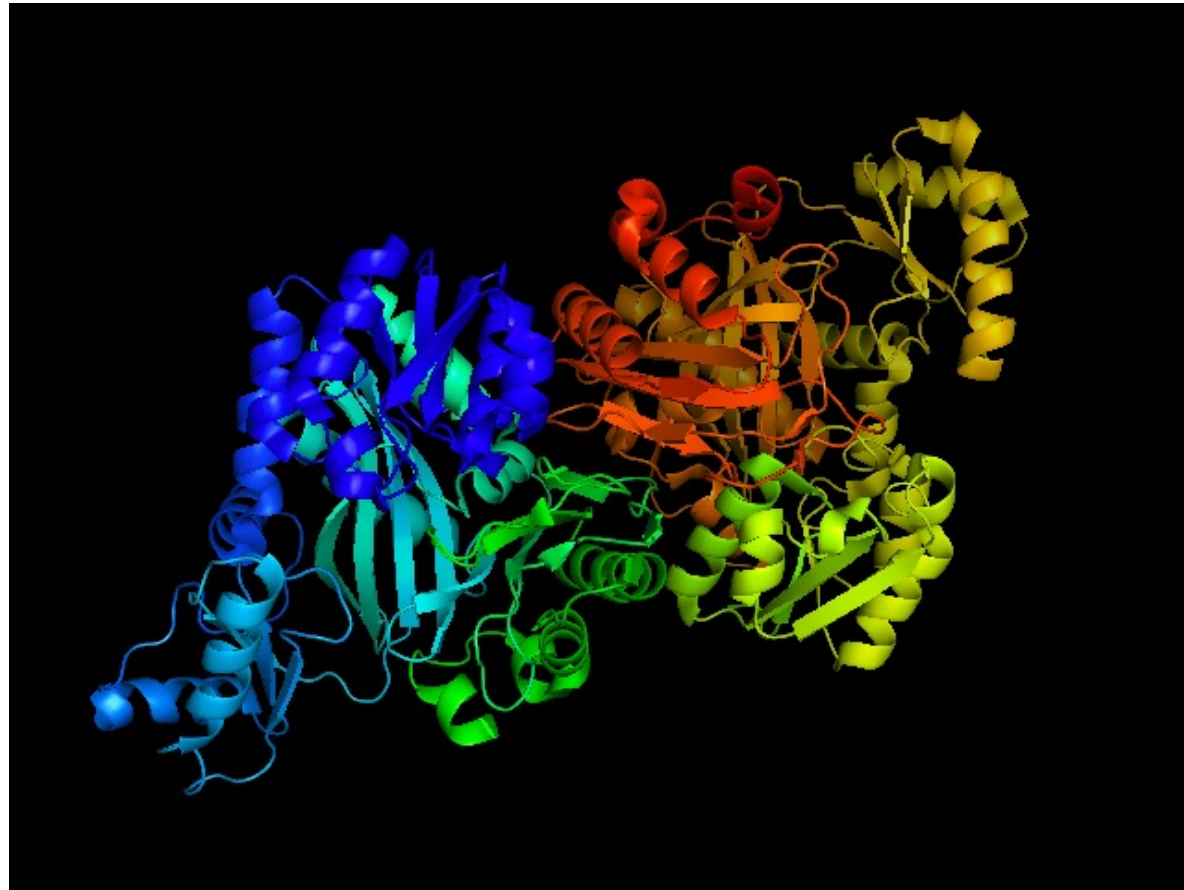
carbon-negative building materials:
CO₂LIG

Long term targets

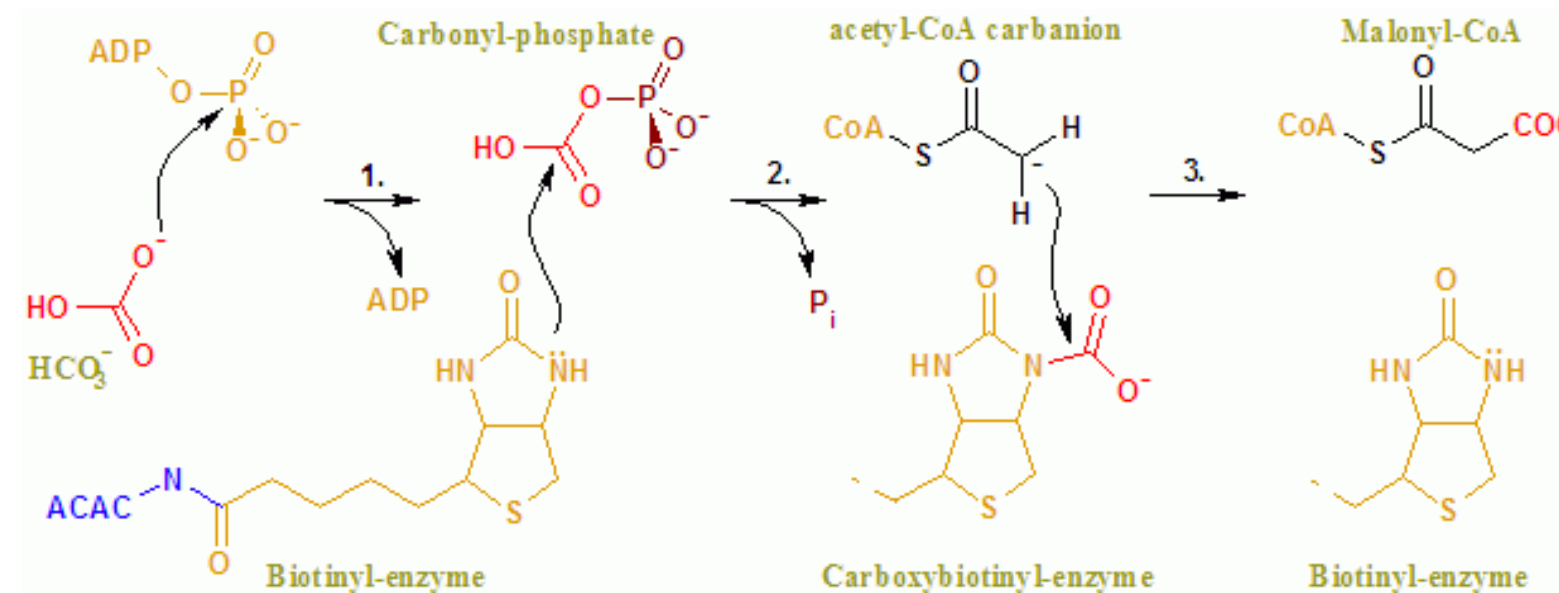
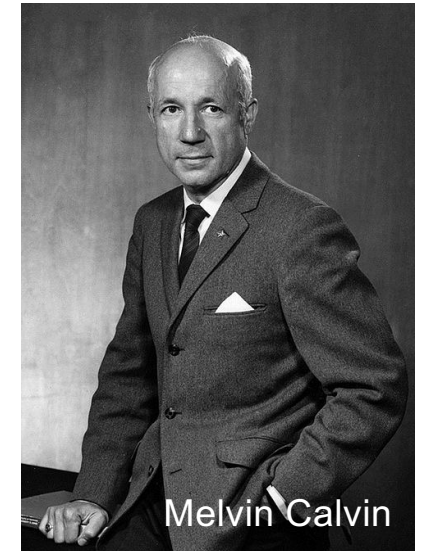
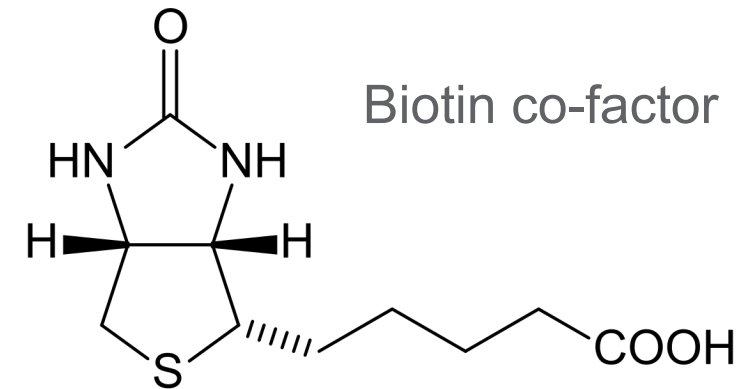
Mineralization materials:
CaCO₃ or MgCO₃

Nature Has Perfected CO₂ Capture and Conversion

Biotin transfers anionic carboxylates in solution to grow fatty acids via the Calvin cycle.

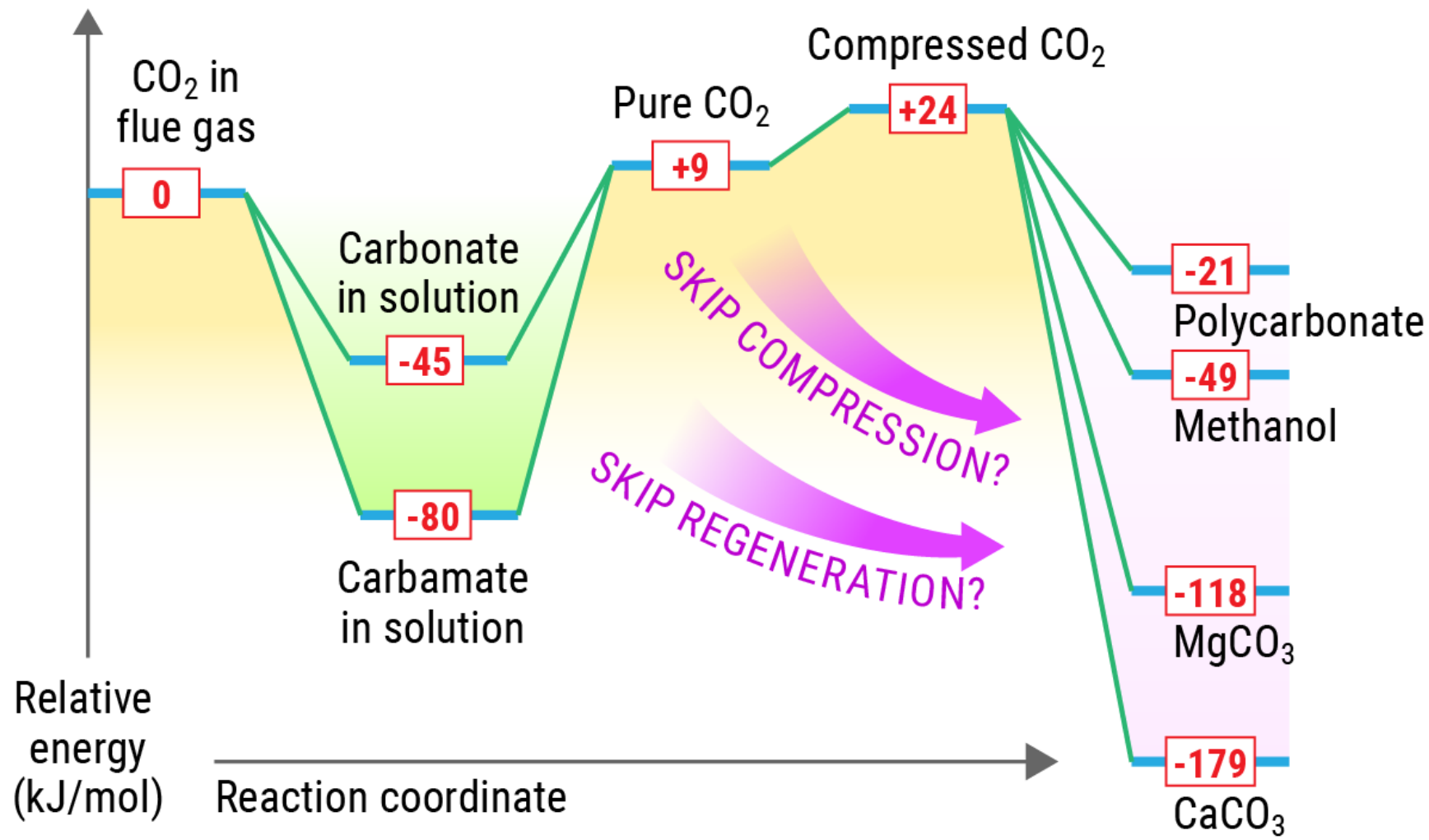


Biotin carboxylase subunit of *E. coli*
acetyl-CoA carboxylase



The Primary Case for Integrating CO₂ Capture With Conversion

Integrated systems for converting CO₂ products have many potential benefits.



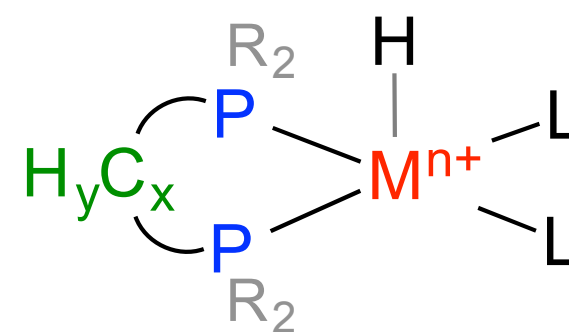
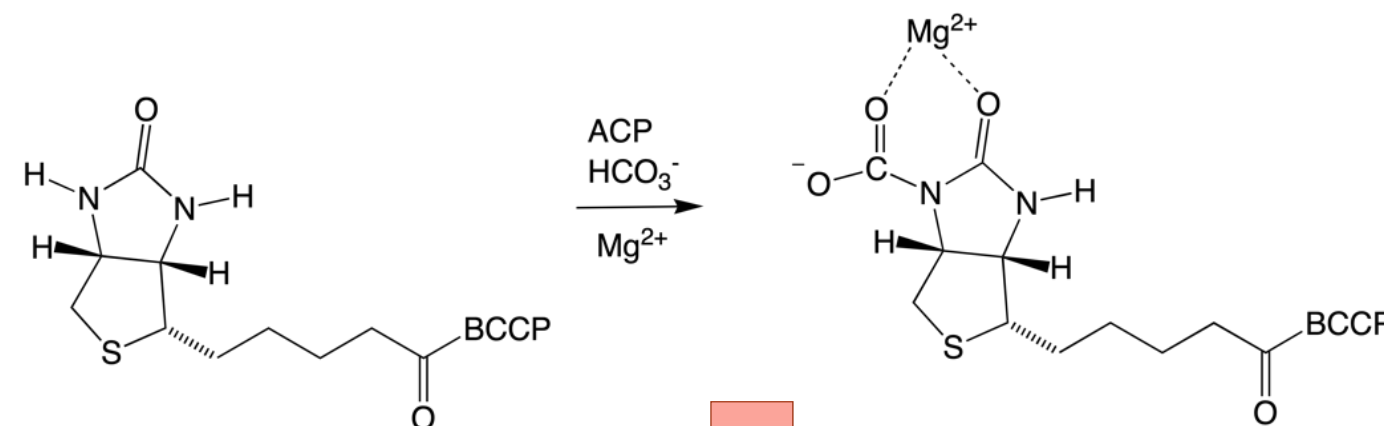
- Catalytic with respect to solvent
- Catalytic exothermic reduction offsets solvent regeneration
- Bypasses CO₂ compression
- Move product not CO₂
- Produces multiple products

Converting Captured CO₂ in the Condensed Phase

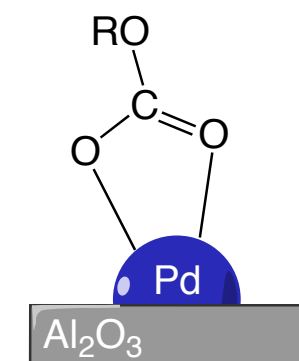
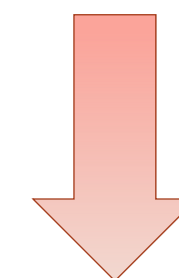
Condensed-phase reactions provide energy and cost benefits and new reactive landscapes.

- Same solvent used for both steps
- Bypasses limiting chemical equilibria of gas-phase reactions
- Potentially lower free-energy pathways
- Catalysis at atmospheric (CO₂) pressures
 - CO₂ concentration >5 wt% in at 1 atm
- Heterogeneous or homogeneous viable
 - Direct coordination to catalysts

Like Biotin, catalysts can operate on captured CO₂



Inner-sphere chelation of “captured” CO₂ (L)

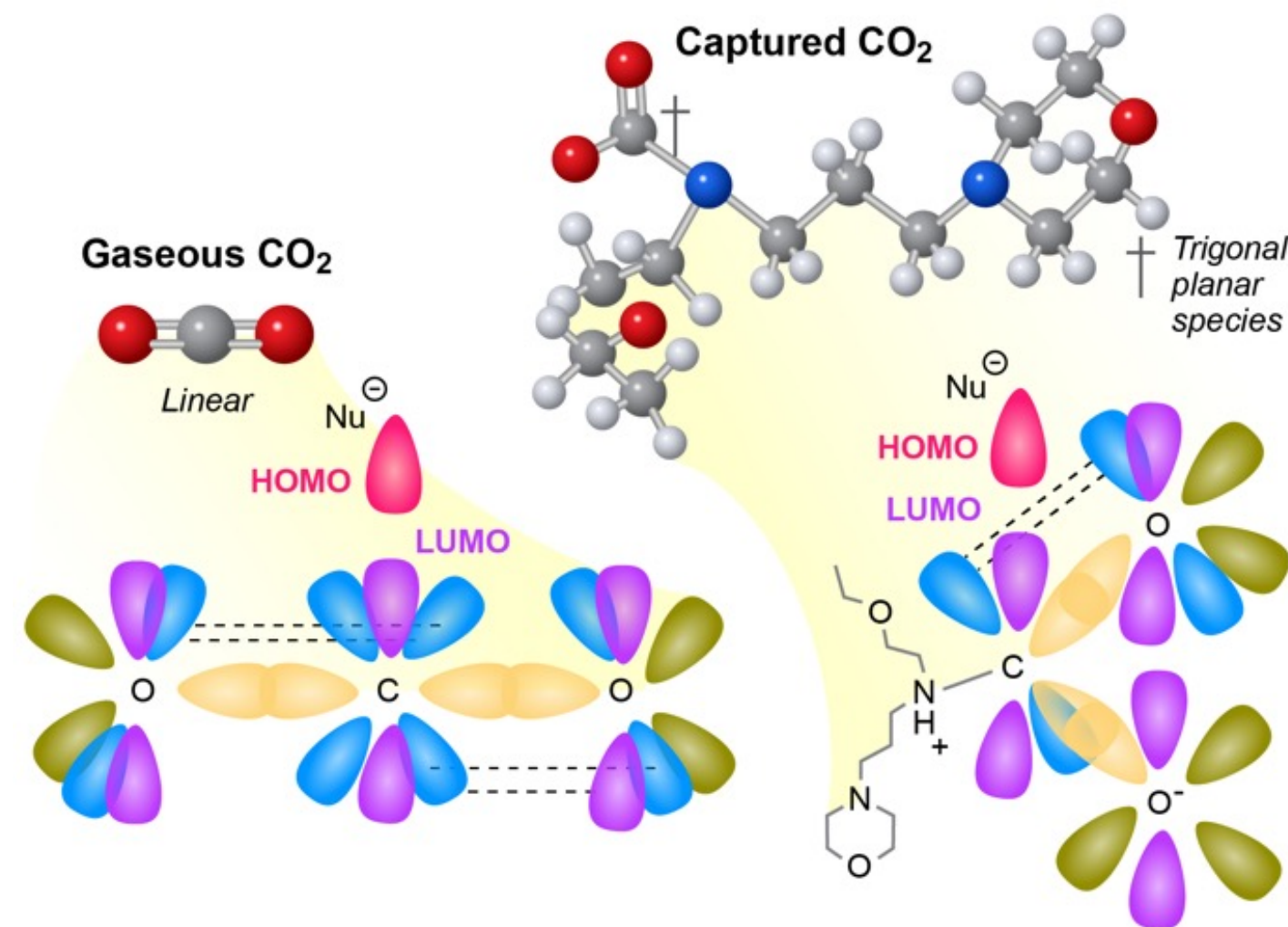


Chelation of “captured” CO₂ to metal surfaces

Converting Captured CO₂ in the Condensed Phase

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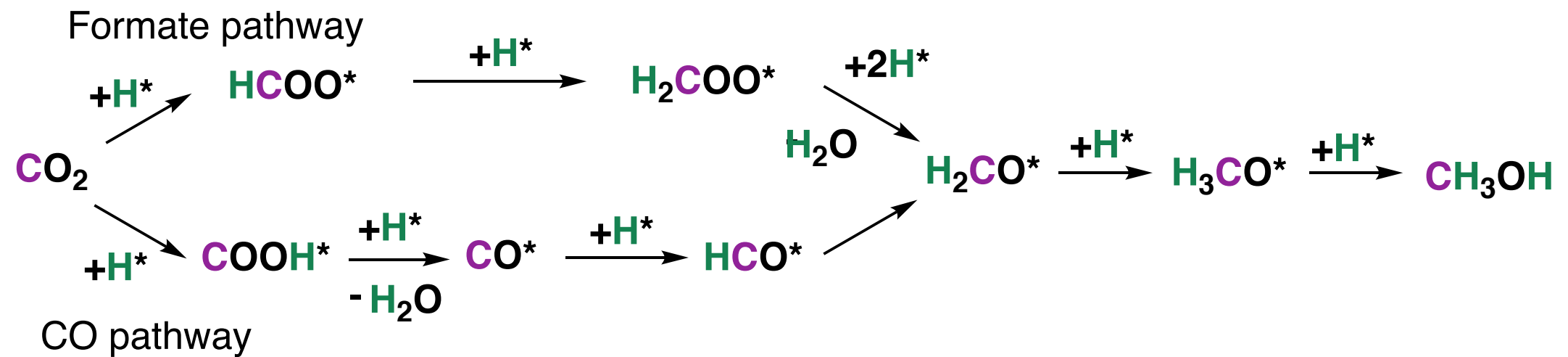
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Methanol is our 1st Target

The same chemicals (alcohols and amines) that promote capture also promote conversion.

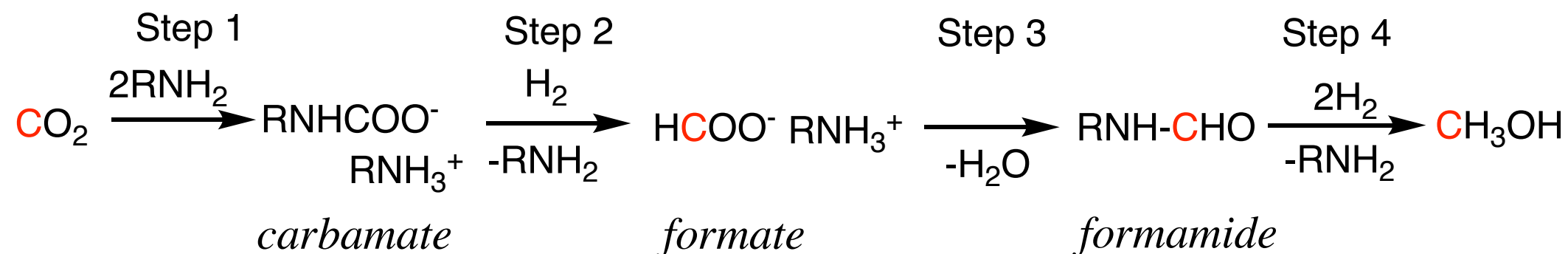
(A) Gas-phase methanol synthesis



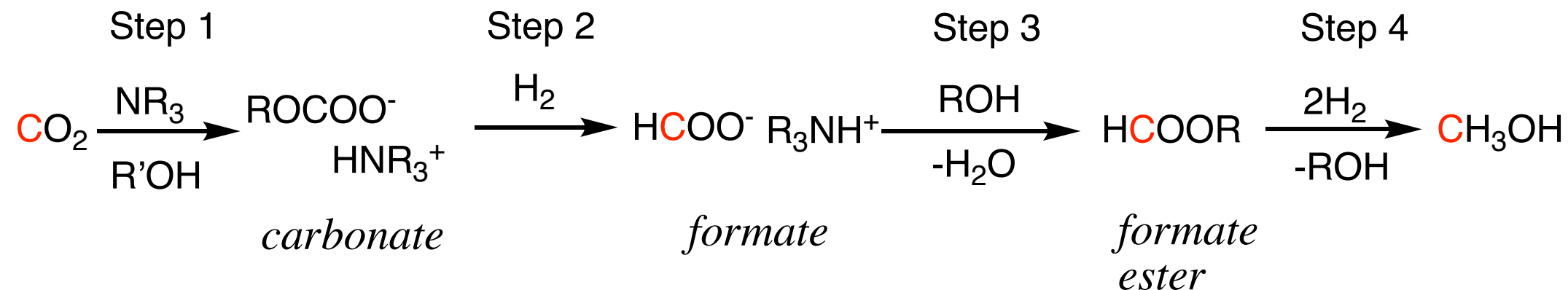
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Pathway (a)



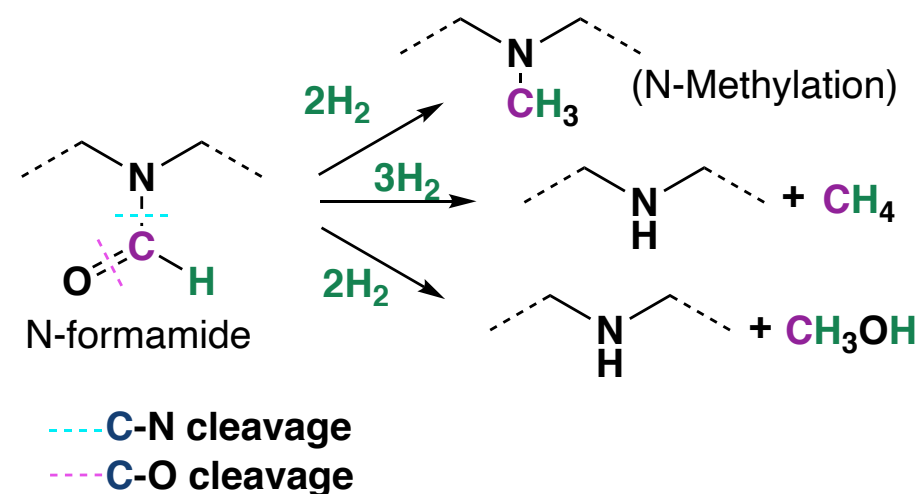
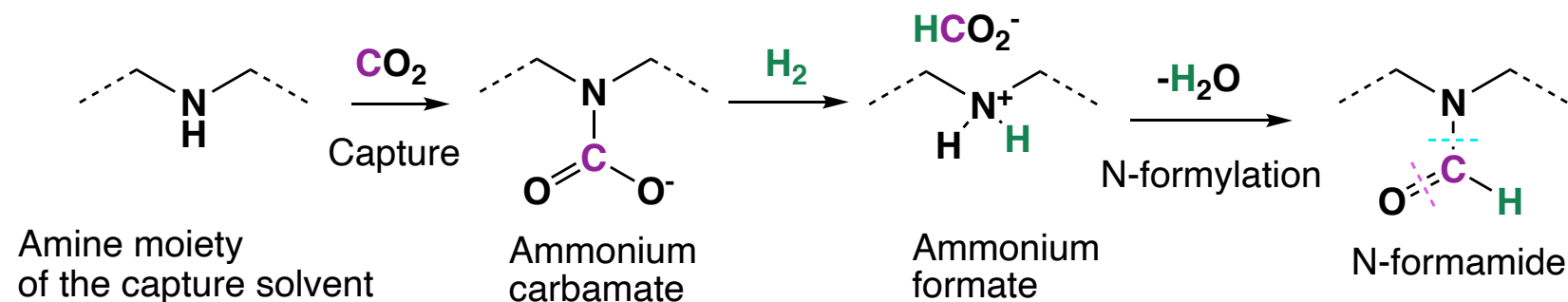
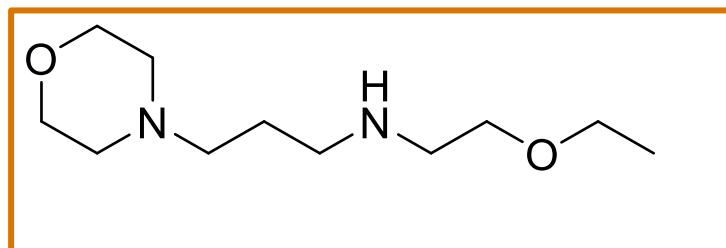
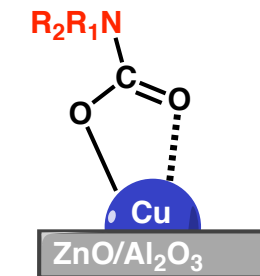
Pathway (b)



The Disconnect: Thermocatalytic conversion of captured CO₂ in viable post-combustion solvents.

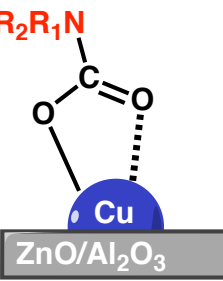
Condensed-Phase Hydrogenations Proceed via Different Routes

Condensed-Phase hydrogenations introduce new challenges using conventional gas-phase catalysts.

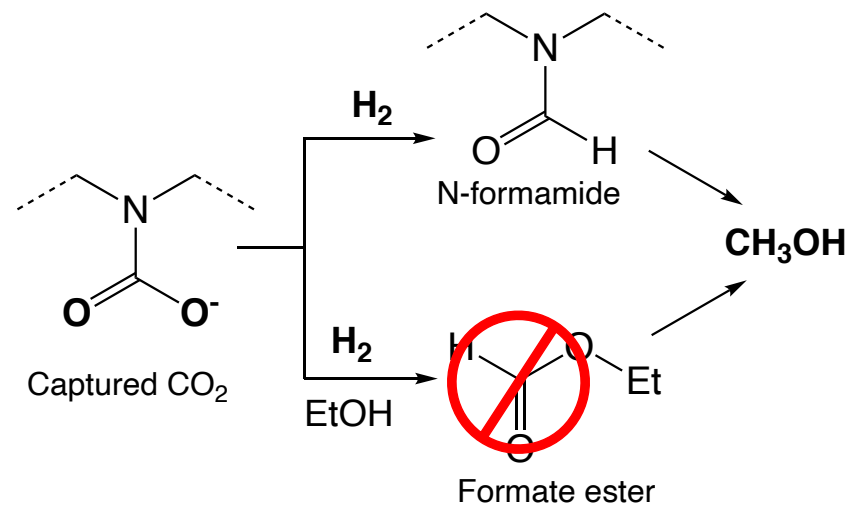


- Solvent deactivation via N-methylation of 2° amines
- Selective C-N cleavage desired to prevent solvent deactivation and improve selectivity
- Limited examples of heterogeneous catalysts selective for C-N cleavage in condensed phase

Hydrogenation of EEMPA-Carbamate Using Conventional Methanol Synthesis Catalysts



Thermocatalytic reduction in the presence of a post combustion solvent demonstrated for the first time using off the shelf heterogenous catalyst.

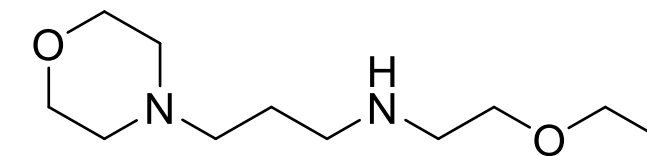


Entry	Capture solvent	Exp. No	CO ₂ /H ₂ bar	time (h)	Formamide mmol	N-methyl amine mmol	CH ₃ OH mmol	CH ₃ OH Selectivity (%)
1	EEMPA	62711-153	15/45	12	0.8	2	0.65	24.5
2	EEMPA	62711-148	15/45	48	0.45	5.1	1.23	19.4
3	EEMPA	62711-147	5/55	48	0.04	5.85	1.19	16.9
4 ^a	EEMPA + ethanol	62711-150	5/55	48	traces	1	2.4	70.6

Catalyst A=200mg, 100 mL reactor, EEMPA=23mmol, P=60 bar (CO₂:3H₂), T=170 °C, t=12 h, ^a ethanol=200 mmol.

- **Low selectivity to methanol** through *N-formamide* intermediate when using conventional gas-phase catalyst.
- **Ethanol co-feed** facilitates reaction through *formate ester* intermediate makes **methanol with 71% selectivity**.
- Focus was on process conditions to improve methanol selectivity through *N-formamide* without co-feeds.

New Heterogeneous Catalysts Selective for C-N Cleavage Identified



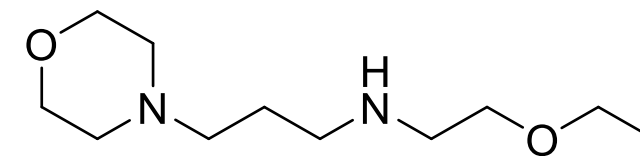
Catalysts with acidic supports are selective for methanol.

Hydrogenation of captured CO₂ over Pt-supported catalysts using a batch reactor system.

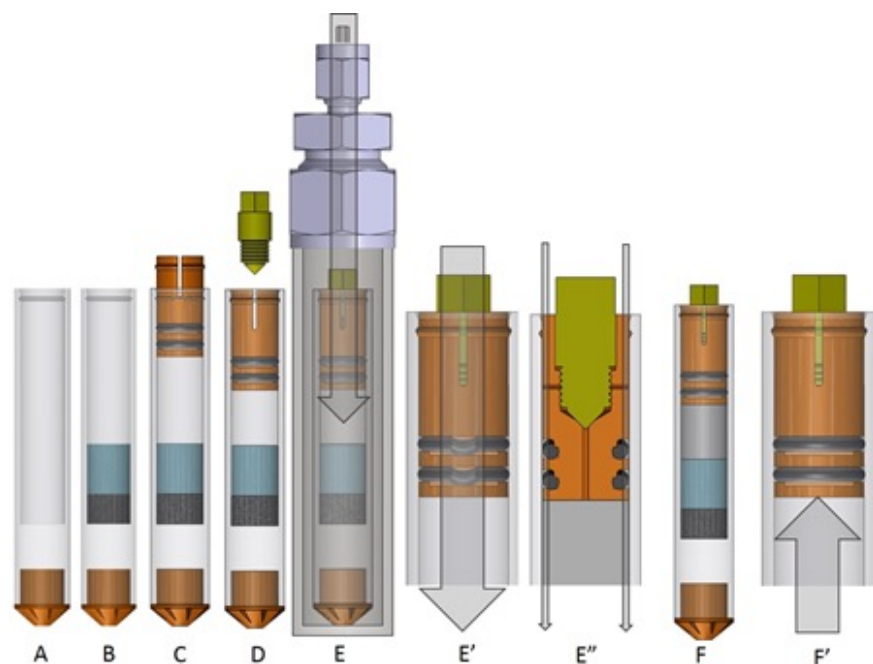
Entry	Cat.	CO ₂ conv. (%)	Product selectivity (%)				Methanol yield (%)	C–N cleavage selectivity (%)	
			CO	CH ₄	2-EEMPA-N-CHO	2-EEMPA-N-Me			Methanol
1	5wt% Pt/CeO ₂	29.7	49.5	3.3	11.4	11.4	24.4	7.2	68.0
2	5wt% Pt/TiO ₂	29.1	31.9	19.8	9.0	12.3	27.0	7.9	68.7
3	5wt% Pt/SiO ₂	23.9	77.4	0.0	15.3	7.3	0.0	0.0	0.0
4 ^a	5wt% Pt/TiO ₂	42.4	15.6	7.8	37.7	11.7	27.2	11.5	69.8
5 ^b	5wt% Pt/TiO ₂	11.5	35.8	25.6	traces	traces	38.7	4.5	100.0
6 ^d	5wt% Pt/TiO ₂	15.9	0.9	25.9	18.1	26.4	28.6	4.5	52.0
7 ^e	5wt% Pt/TiO ₂	12.2	25.5	22.4	15.0	traces	37.1	4.5	100.0
8 ^f	5wt% Pt/TiO ₂	44.7	5.8	1.6	38.1	5.9	7.6	3.4	56.5
9 ^c	5wt% Pt/TiO ₂	19.3	29.8	16.9	10.6	10.1	32.6	6.3	76.4

Reaction conditions: catalyst = 200 mg, 170 ° C, 2-EEMPA-5g (CO₂ loaded 2-EEMPA was used, 6 wt.% CO₂ loading), initial P(H₂) = 60 bar, time = 12 h, ^aethanol(10.6 g) ^b3h, ^c10wt% CO₂, ^d30bar H₂, ^e150 ° C, ^f30 wt% MEA was used as a capture solvent; mostly MEA-formate and MEA-N-formamide species were observed; MEA decomposition products were also observed under the reaction conditions, C-N cleavage selectivity= (moles of methanol)*100/(moles of 2-EEMPA-N-CH₃ + moles of methanol).

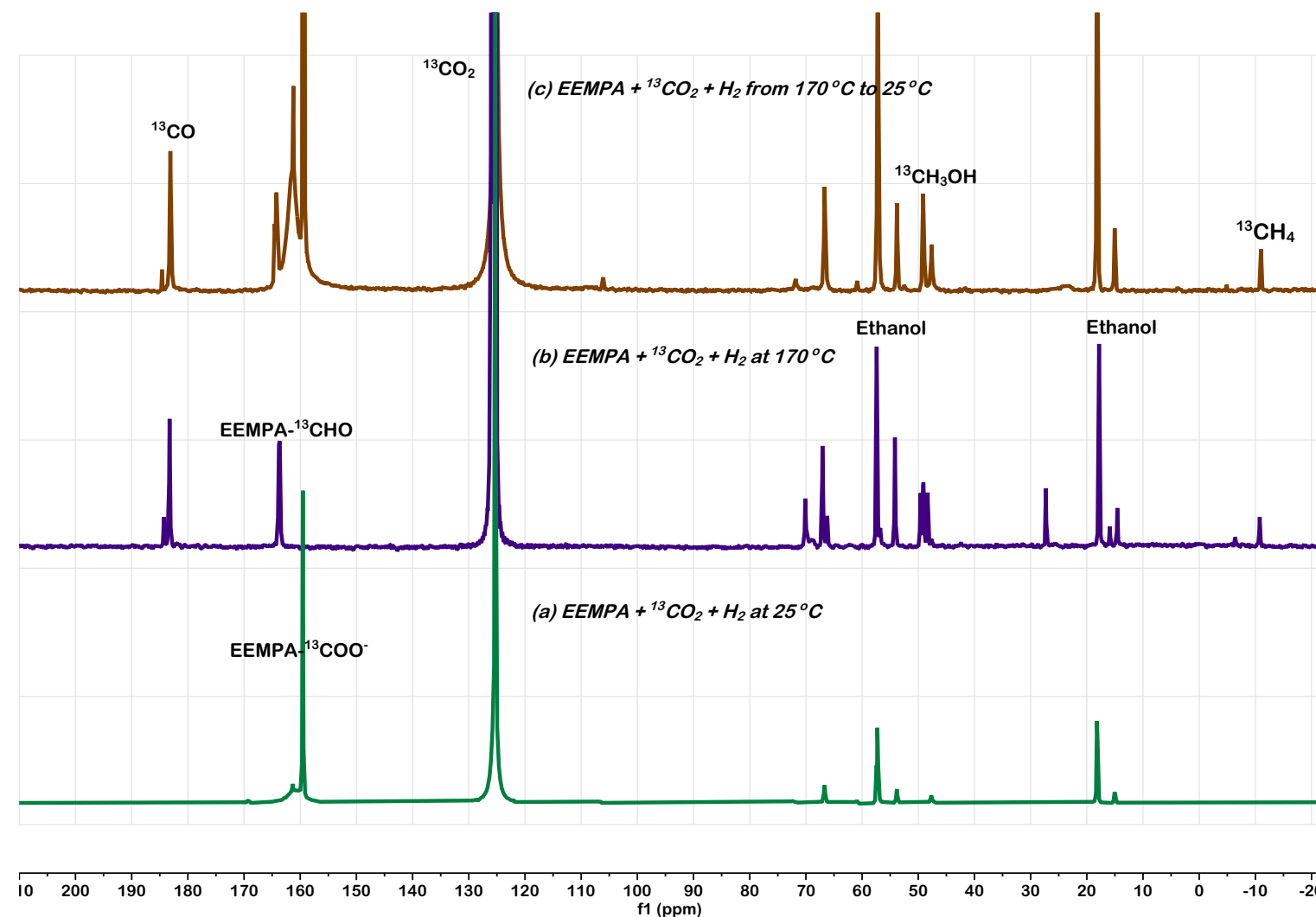
New Heterogeneous Catalysts Selective for C-N Cleavage Identified



Catalysts with acidic supports are selective for methanol.

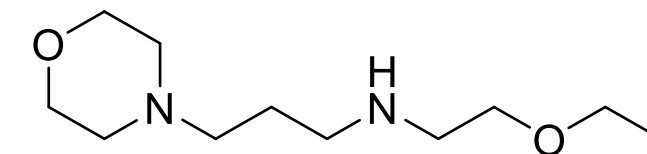


High-Temperature/Pressure WHiMS MAS Rotors
400 bar @ 20 °C ; 300 bar @ 250 °C – limit of
most H. temp VT

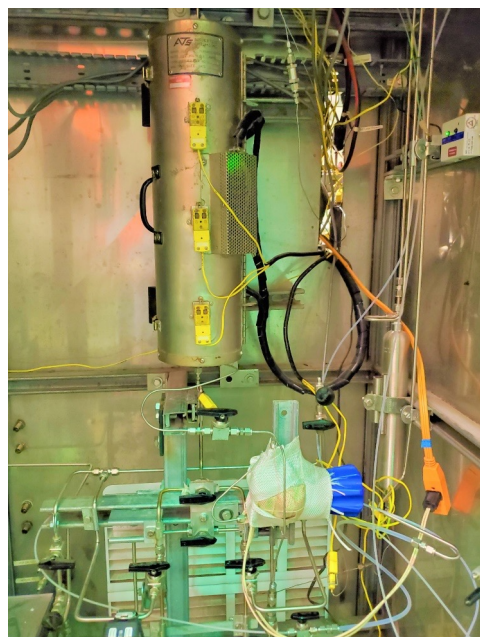


$^{13}\text{CO}_2$ in the presence of 2-EEMPA and a 5 wt % Pt/TiO₂ catalyst at 170 °C under 60 bar H₂ (initial pressure) in an ethanol co-solvent, 2-EEMPA: EtOH=1:10 (molar ratio).

Continuous Flow Hydrogenation in EEMPA



Catalyst screening shows methanol formation is sensitive to temperature and space velocity.



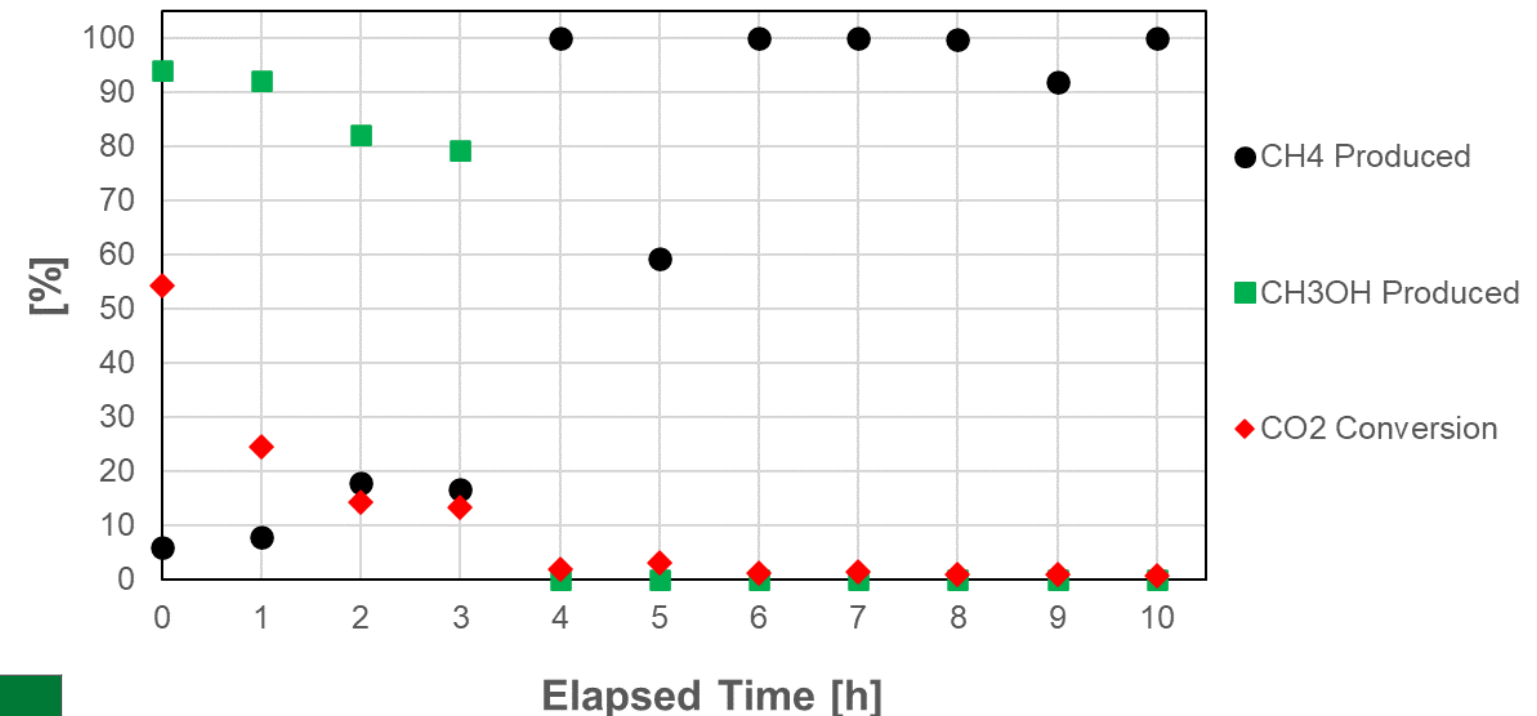
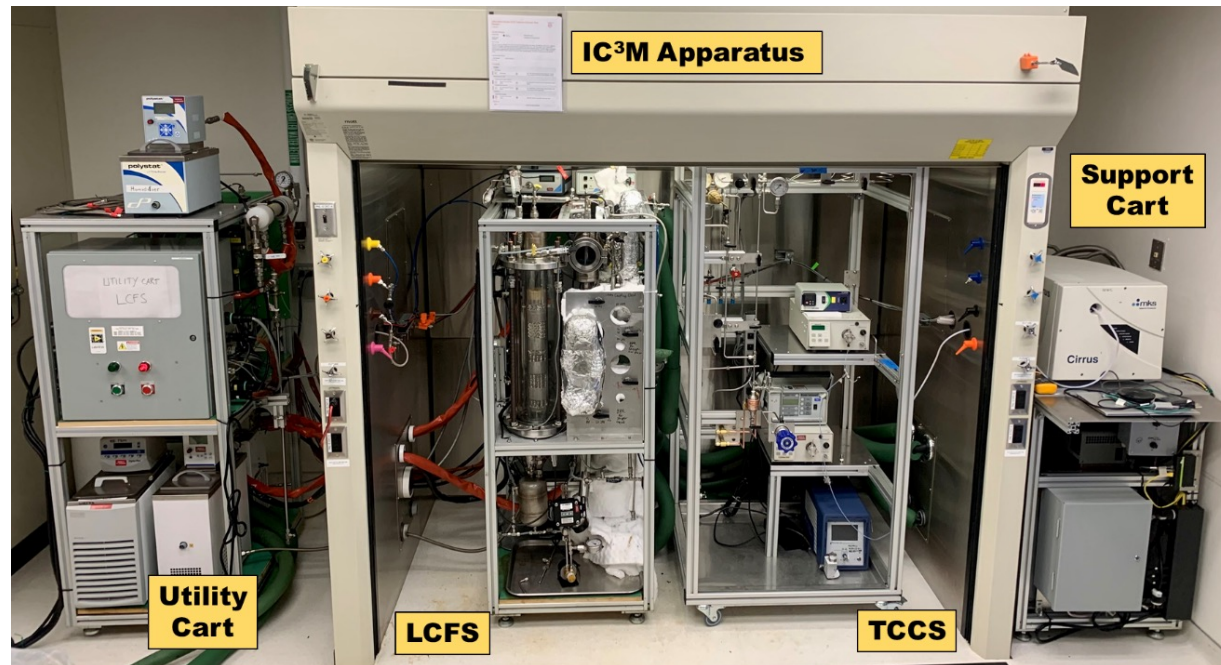
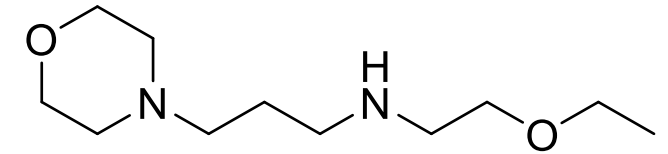
Entry	Reaction T (°C)	CO ₂ Conv (%)	WHSV g _{CO2} /g _{cat} /h	TOS (h)	Selectivity (mol C%)					
					MeOH	EtOH	PrOH	BuOH	CH ₄	C ₂ H ₆
1	140	2.2	0.15	-	92.7	0.0	7.3	0.0	0.0	0.0
2	170	7.7	0.15	-	66.5	4.3	2.5	0.7	26.0	0.0
3	170	29.1	0.015	-	57.0	4.5	0.8	1.4	26.7	8.7
4	190	11.8	0.15	-	78.0	4.3	0.0	2.5	15.1	0.0
5	190	26.9	0.075	-	63.6	4.6	0.2	1.9	26.4	3.3
6	190	85.7	0.015	40	51.5	9.7	0.6	1.9	27.1	9.3
7	190	75.9	0.015	60	50.2	8.6	0.7	2.0	29.2	9.3
8	190	65.2	0.015	80	46.0	8.0	1.1	4.7	29.8	10.5

Liquid feed: captured CO₂ in EEMPA solvent (5 wt.% CO₂) Reaction conditions: 1.0 g catalyst D1, 870 psig; Gas feed: 38 sccm H₂, 5 sccm N₂. Change in WHSV is achieved by changing the liquid feed flow (0.05, 0.025, 0.005 mL/min).

- Catalyst identified highly selective towards **methanol** with **93% selectivity** at **140 °C**.
- At 190 °C, the **CO₂ conversion** increased from **12%** to **86%** when space velocity was decreased by a factor of 10.
- Conversion decreased from 86% to 65% over a span of approximately 80 hours.

Semi-Batch CO₂ Capture and Catalytic Conversion to Methanol

Single-pass; 10-hours on simulated coal-derived flue gas (CO₂, N₂, H₂O).



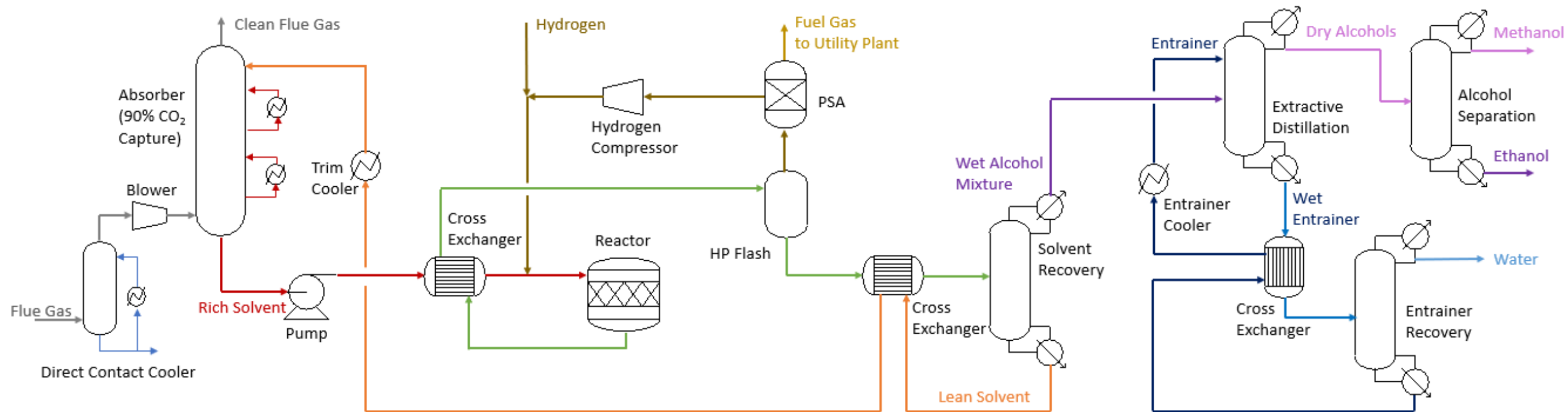
CO ₂ Capture - LCFS			
Feed	CO ₂ /N ₂ [dry basis]	15 / 85	[mol%]
	Dew Point	15.6	[°C]
Absorber	Avg. Temperature	32.3	[°C]
	Avg. Pressure	0.08	[psig]
Stripper	Avg. Temperature	95.1	[°C]
	Avg. Pressure	14.39	[psig]
Reboiler	Temperature	114.9	[°C]
Flow	Liquid	15.3	[kg/h]
	Gas	0.61	[kg/h]
	L/G	25.2	[-]
CO ₂ Capture Efficiency		88.9	[%]

CO ₂ Conversion - TCCS			
Gas Feed	H ₂ /N ₂	93 / 7	[mol%]
	Flowrate	6.7 E-3	[kg/h]
Liquid Feed	2-EEMPA/CO ₂ /H ₂ O	78 / 5 / 17	[mol%]
	Flowrate	5.9 E-4	[kg/h]
Reactor	Temperature	170	[°C]
	Pressure	865	[psig]
	Catalyst: 5wt% Pt on TiO ₂	2.5	[g]
CO ₂ Conversion		55 → 0.8	[%]
Methanol Yield		94 → 0	[%]

- High conversion for ~4 hours
- Catalyst deactivated due to CO poisoning
- Repeat with catalyst re-activation completed

Process Configuration for the IC³M Technology- CH₃OH Slipstream

Exploits exothermic hydrogenation to drive solvent regeneration, operates in the condensed phase.

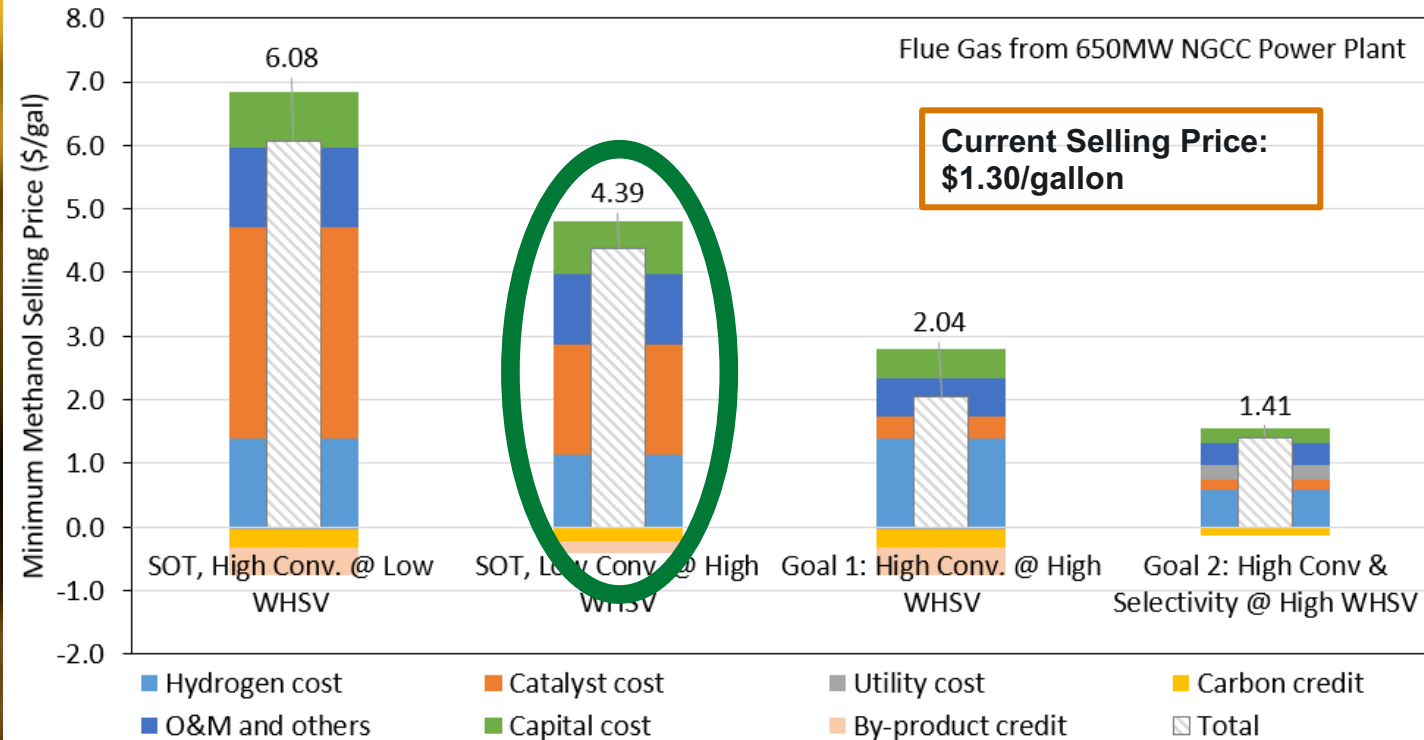


Energy saving features of the IC³M process:

- Exothermic hydrogenation offsets some regeneration of the carbon capture solvent
- Heat recovered is used to generate low-pressure steam to be used in other parts of the process
- No mechanical compression of CO₂ is required for the subsequent reaction.

Current Techno-Economic Assessment

IC³M has potential to achieve cost parity assuming reaching targeted performance.



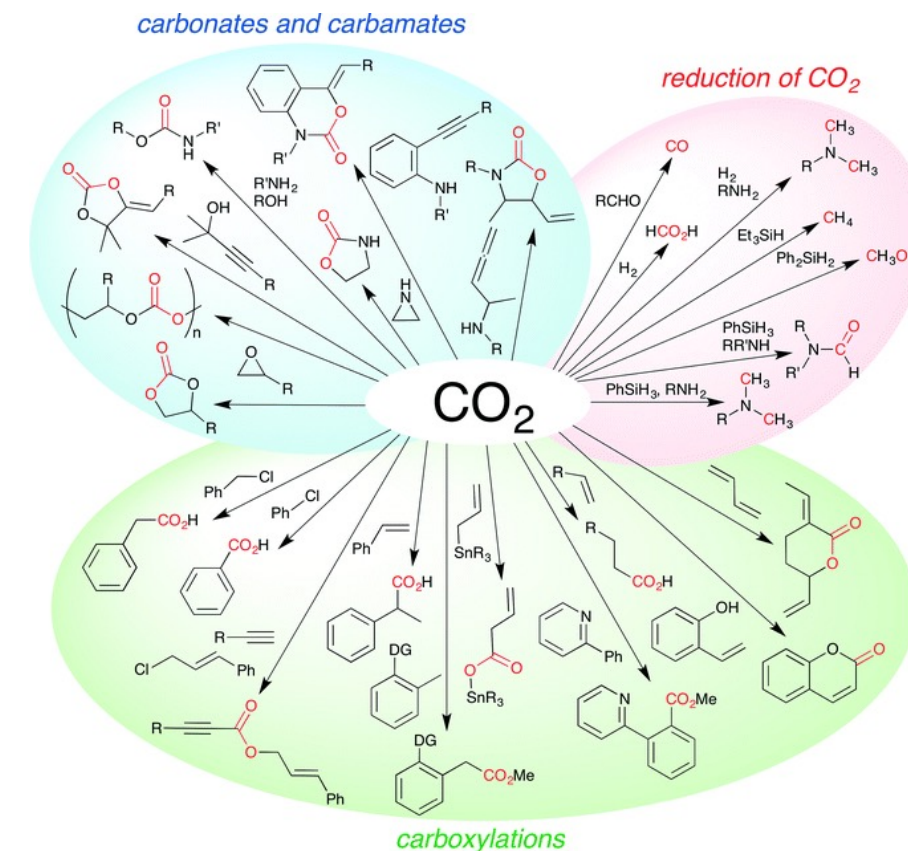
Compared with the optimistic case (High Conv. w/o Alcohol in 2021, the 2022 SOT shows:

- Increase in hydrogen consumption due to the production of by-products (i.e. CH₄)
- \$1/kg H₂
- Increase in capital cost for product separation
 - Extractive distillation to break azeotrope between methanol-ethanol-water
 - PSA to separate CH₄ from H₂

	SOT @ Low WHSV	SOT @ High WHSV	Goal 1 High Conversion	Goal 2 High Conversion and Selectivity
WHSV (gCO ₂ /gCat/hr)	0.015	0.075	0.15	0.15
Single-pass CO ₂ conversion (%)	85.7	26.9	85.7	85.7
Methanol selectivity (C %)	51.5	63.6	51.5	100
Methane selectivity (C %)	27.1	26.4	27.1	0
Source	Experiment	Experiment	R&D Target	R&D Target

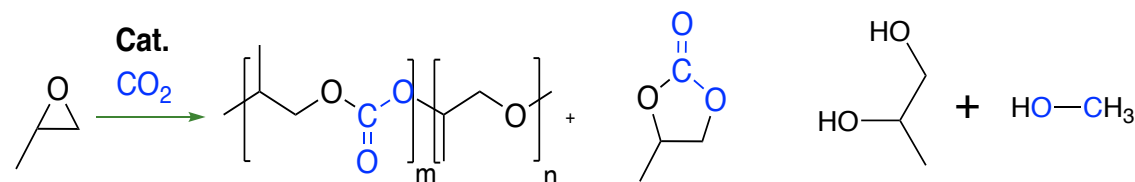
What's Next for IC³M?

Continued development to make new materials from CO₂.



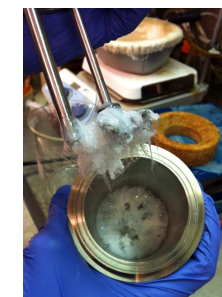
Near term targets

carbon-neutral fuels and chemicals:
CH₃OH, CH₄, carbonates, glycols



Intermediate term targets

carbon-negative building materials:
CO₂LIG





Acknowledgements



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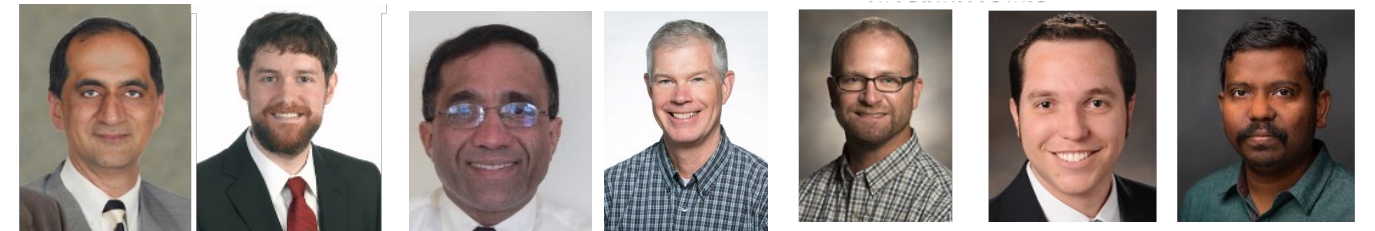
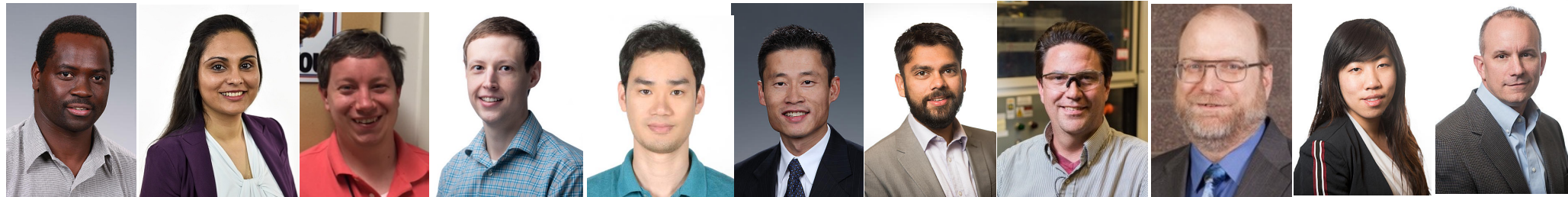
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