PNWD-3303 WTP-RPT-081, Rev. 0

Large Tank Experimental Data for Validation of the FLUENT CFD Model of Pulsed Jet Mixers

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June 2003

WTP Project Report

Battelle – Pacific Northwest Division Richland, Washington, 99352

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June 2003

Prepared for Bechtel National, Inc. under Contract 24590-101-TSA-W000-0004

Test specification: None Test plan: TP-RPP-WTP-051 Test exceptions: 24590-WTP-TEF-RT-02-057 24590-WTP-TEF-RT-02-089 R&T focus area: Pretreatment Test Scoping Statement(s): B-55

Battelle - Pacific Northwest Division Richland, Washington 99352

Completeness of Testing

This report describes the results of work and testing specified by TP-RPP-WTP-051. The work and any associated testing followed the quality assurance requirements outlined in the Test Specification/Plan. The descriptions provided in this test report are an accurate account of both the conduct of the work and the data collected. Test plan results are reported. Also reported are any unusual or anomalous occurrences that are different from expected results. The test results and this report have been reviewed and verified.

Approved:

Gordon H. Beeman, Manager WTP R&T Support Project Date

Summary

Battelle–Pacific Northwest Division (PNWD) was contracted to provide Bechtel National Incorporated (BNI) with simulant mixing tests results for the validation of the FLUENT CFD (computational fluid dynamics) model of the pulsed jet mixing (PJM) systems. Several hundred of these PJMs are expected to be used in the U.S. Department of Energy (DOE) River Protection Project (RPP) Waste Treatment Plant (WTP). Section 5 of the Research and Technology Plan (BNI 2002) identifies the research needs for pulsed jet mixers. The generation of experimental data for CFD model validation is addressed in Scoping statement B-55, which is included in Appendix C of the Research and Technology Plan.

Objectives

The three objectives of the work performed included:

- 1. Reconfiguring the large tank test stand to be as geometrically symmetric as possible and determining the as-built dimensions of the test system
- 2. Conducting hydrodynamic tests to check for symmetry of the fluid flow in the tank
- 3. Performing mixing tests to generate concentration and velocity data using glass-bead/water simulants with a nominal volume mean particle size of 10 and 35 µm at varying solids loading and/or modes of PJM operation.

All of the objectives have been met.

Conduct of Test

This report summarizes the modifications made to be the large tank test configuration to make it geometrically symmetric and presents the experimental data generated after the modifying the test system. Specifically, the data presented in this report includes: 1) as-built dimensions of the test configuration after PJM realignment, 2) hydrodynamic velocity data, and 3) velocity and density data with a simulant consisting of glass-beads in water with a nominal volume mean particle size of 10 and 35 μ m.

Results and Performance against Objectives

In order to locate the PJMs symmetrically within the tank, the following adjustments were made: 1) squaring the PJMs along the mounting structure near the top of the tank and 2) adding two additional tie beams and squaring the PJMs at the tie-beams which connect the pulse tubes at ~ 72 in from the tank floor. All attempts to square the PJMs within the tank were made to within a tolerance of \pm 0.5 in (\pm 0.0127 m). In addition to squaring the PJMs in the tank, the Atomic Energy Agency (AEA) staff adjusted the drive and suction pressures of the jet pump pair (JPP) control module and fine tuned the PRESCONTM controller programming to operate the PJMs in an as close to a synchronous and prototypical manner as possible.

Hydrodynamic velocity profiles measured in the tank indicated that despite a significant improvement, some asymmetries in the flow field are still present. These asymmetries were found to be

due to both geometric dissimilarities and the differences in the individual pulse tubes operation. With BNI's concurrence, further improvements in the symmetry were not pursued due to budget and time constraints.

Simulant mixing data (i.e., concentration and velocity profiles) were determined using glass-beads with nominal volume mean particle size of 10 and 35 μ m at varying solids loading and/or modes of PJM operation. Because of the large size of the data files containing the results, they are presented as the Excel spreadsheets on a CD included with this report.

Quality Requirements

PNWD implemented the RPP-WTP quality requirements by performing work in accordance with the quality assurance project plan (QAPjP) approved by the RPP-WTP Quality Assurance (QA) organization. This work was conducted to the quality requirements of NQA-1-1989 and NQA-2a-1990, Part 2.7 as instituted through PNWD's Waste Treatment Plant Support Project (WTPSP) Quality Assurance Requirements and Description Manual.

PNWD addressed verification activities by conducting an independent technical review of the final data report in accordance with procedure QA-RPP-WTP-604. This review verified that the reported results were traceable and that inferences and conclusions were soundly based.

Issue

There were no design or operations issues associated with the testing and/or the results presented in this report. However, care must be exercised in using the data presented in this report to draw broad conclusions regarding the PJM performance in vessels with significantly larger dimensions than the test vessel. Extrapolation of these results to actual waste behavior is also not recommended as some of these slurries exhibit non-Newtonian rheology. Such conclusions should be supported by additional data such as those obtained experimentally with validated simulants and from a validated CFD model.

Acknowledgements

The authors would like to thank Mike White and Bill Combs for all their help with the test system configuration, simulant preparation, and assistance during all phases of the testing. In addition, we would like to thank Cameron Bates and Franz Nigl for their support in putting the data packages together. Finally, we wish to acknowledge Perry Meyer for his thorough review of the data presented in this report.

Terms and Abbreviations

AEA	Atomic Energy Agency
BNFL	British Nuclear Fuel Limited, Inc.
BNI	Bechtel National Inc.
CFD	computational fluid dynamics
DACS	Data Acquisition and Control Software
DAS	Data Acquisition System
DOE	U.S. Department of Energy
E	east
EM	electromagnetic
FY	fiscal year
JPPs	jet pump pairs
LTTS	large-tank test stand
Ν	north
PJM	pulsed jet mixer
PNWD	Battelle-Pacific Northwest Division
PVC	polyvinyl chloride
QAPjP	quality assurance project plan
QA	Quality Assurance
RPP	River Protection Project
S	south
SS	stainless steel
W	west
WTP	Waste Treatment Plant
WTPSP	Waste Treatment Plant Support Project

Unit Abbreviations

°C	degrees Centigrade
CFM	cubic feet per minute
cm	centimeter
D	diameter
deg	degree
ft	feet
g	gram
gal	gallon
Н	height
hr	hour
ID	internal diameter
in	inch
L	liter
lb	pound
μm	micrometer
m	meter
min	minute
OD	outer diameter
PSD	particle size distribution
psi	pounds per square inch
psia	pounds per square inch, absolute
psig	pounds per square inch, gauge
s or sec	second
SP GR	specific gravity
wt%	weight percent

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1.0 Introduction

1.1 Background

During FY 01, experiments were performed by Battelle–Pacific Northwest Division (PNWD) in the large 12.75-ft (3.8862 m) internal diameter (ID) x 15-ft (4.572 m) H, four pulsed jet mixer (PJM) test system available in the 336 Test Facility. The objective of those tests was to generate hydrodynamic and simulant mixing data for the validation of the TEMPEST^(a) computational fluid dynamics (CFD) model for the pulsed jet mixing systems. Analysis of the data revealed the existence of large asymmetries in the fluid flow due to protrusions along the floor of the tank made the data unsuitable for validation of the CFD model^(b).

During early to middle of FY 02, attempts were made to improve the quality of the experimental data within the constraints of the task budget. This included: 1) operating the PJMs under gravity refill to keep the cycle time constant and 2) removing protrusions in the tank that caused asymmetries in the flow fields. However, there were certain other variables that still affected the flow symmetry in the tank. For example, the four PJMs were not situated exactly in the center of each quadrant of the tank (one was closer to the wall than the others). Also, the pulse tube nozzles were not exactly at the same distance from the tank floor. In addition, since the jet pump pairs (JPPs) regulating the airflow to the pulse tubes were not identical, the drive times were not identical. Finally, there were two tie beams located midway between the top and bottom of the tank, which were used to provide additional support to the pulse tubes. All of these factors still contributed to asymmetries in the fluid flow patterns within the tank. Also, after the initial modifications, only the hydrodynamic tests, but not the simulant mixing tests, were repeated due to budget constraints.

During the end of FY02, Bechtel National Inc. (BNI) requested PNWD to repeat the simulant mixing tests after reconfiguring the test stand to as geometrically symmetric as possible because of the importance of the simulant mixing data to the code validation. This included: 1) aligning the PJMs in order to maintain the same off-wall and off-floor distances, 2) adding equal length tie beams to connect the PJMs at approximately the tank mid section, and 3) enabling adjustment of the air pressure to the JPPs to minimize asymmetric firing of the PJMs. In addition to the above modifications, BNI has also requested the modification of the test system to fire the PJMs under vacuum refill in order to maintain prototypical operation. Finally, BNI has requested that the simulant mixing tests be conducted with glassbeads simulants of ~10 and 35 μ m volume mean particle size and different solids loading and PJM operation conditions.

The information regarding the modifications made to the large tank test configuration and the experimental data generated after the modifying the test system are presented in this report.

⁽a) TEMPEST (which stands for Transient Energy Momentum and Pressure Equations Solution in Three Dimensions) is a CFD model developed by the Pacific Northwest National Laboratory to address the complex multiphase fluid flow phenomena encountered with highly radioactive waste at the Hanford Site.

⁽b) Geometric similarity is important because time varying transients are very difficult and extremely time consuming to model since they require full 3D simulations.

1.2 Scope of the Project

The scope of the work presented in this report involves the large-tank experimental testing conducted after the test system has been modified to minimize asymmetries of the flow patterns in the tank. The data presented in this report includes: 1) as-built dimensions of the test configuration after PJM realignment, 2) hydrodynamic velocity data, and 3) velocity and density data with glass-beads of nominal volume mean particle size of 10 and 35 μ m.

2.0 Large Tank Test Stand Modifications

In this section, a description of the large tank test stand (LTTS) and the work done to modify the PJM location in the tank to improve the geometric similarity of the test system are presented.

2.1 Large Tank and PJM Test Stand Description

The description of the large tank test system has been presented before (Bontha et al. 2000 and 2002) but for continuity sake is presented again.

The tank (generally referred to as the supernate tank), in which the PJM system is located, is one of the three large-scale tanks available for PNWD clients to evaluate their test equipment and processes. The LTTS tank is a cylindrical steel vessel of 12.75 ft (3.87 m) internal diameter (ID) and 15 ft (4.57 m) depth and is shown in Figure 2.1. The bottom of the tank is elliptically (2:1) shaped with minimum and maximum radii of 3.2 ft (0.971 m) and 12.75 ft (3.87 m), respectively.

The PJM system consisted of four pulse tubes each with a cylindrical section of 10 ft (3.05 m) length, 2 ft (0.610 m) internal diameter, and 0.25 inch (6.35E-03 m) wall thickness. Each tube is elliptically (2:1) rounded at the top end with an opening for a 2 inch (5.10E-02 m) flange connection. The bottom end of the pulse tube was tapered down at an included angle of 60° to a 4 inch (0.102 m) nozzle. The overall height of the pulse tube was approximately 12 ft (3.66 m) and is shown in Figure 2.2.

The pulsed-jet tubes are held in place using cross beams, which traverse the diameter of the tank and are welded to the tank sides (see Figure 2.3). In addition to the support beams on the top on the tank, there are two tie beams connecting the pulse tubes (in pairs). These beams provide additional support to the tubes and prevent their vibration during the PJM operation. These tie beams are situated at ~ 6 ft (1.83 m) from the tank floor (as measured from the center). The pulsed jet tubes were positioned approximately at the center of the four quadrants of the supernate tank at ~ 9 inch (0.229 m) from the floor of the tank. The pulse tubes are connected to 2-inch (0.0508 m) pipe couplings that enable the insertion of level gauges and attachment of the air/vacuum lines that are required for the PJM operation.

A catwalk or observation bridge was present at a height of 3 ft (0.914 m) from the top of the tank. The bridge contained a 2 ft x 2.5 ft (0.610 m x 0.762 m) port (covered) for the installation of test equipment. Another catwalk (not shown in Figure 2.1) was present at an elevation of ~ 40 ft (12.19 m) from the top of the tank and was used to support the air hoses to the pulse tubes.

Transfer pipes (also not shown in the figures) at the top and at the bottom of the tank enable the addition or removal of material to and from the tank during loading or disposal operations. The supernate tank is positioned on three load gauges, which can be used to determine the weight of the tank and its contents.

Though all the testing and in the results presented in this report, the pulse tubes were labeled using the alphabetical letters A, B, C, and D and their positions located in the tank based on an approximate geographical North direction perpendicular to the catwalk on top of the tank. This labeling with respect to the catwalk on top of the tank and the North direction are shown in Figure 2.4.

2.2 Initial Estimate of PJM Locations in the Tank

Prior to the start of any realignment of the PJMs in the tank, an estimation of the symmetric locations of the PJMs within the tank was made based on the existing configuration. This is schematically shown in Figure 2.5. This was used as the target for the realignment of the pulse tubes in the tank.

In all of the sketches presented in this section a mark was made along the rim of the tank near pulse tube B in order to locate all measurements to a common reference point. The location of the reference point was determined by drawing a string between the pipe couplings (securing the level probes as discussed in the next section) on pulse tubes B and D. The string line passed on the NW side of pulse tube D pipe coupling and the SE side of the pulse tube B pipe coupling securing the level probes to the 2-inch (0.0508 m) pipe crosses at the top of the pulse tubes. A laser guide was directed along the string line, and the laser projection point on the tank wall was marked. A carpenter square was used to transfer the point marked on the wall to the rim of the tank. The location of the reference mark with respect to the tank wall is shown in Figure 2.6.

In Figure 2.6, based on circumferential measurements (average tank diameter = 153.7 inches [3.90398 m]), the angles θ_{AB} and θ_{BC} were calculated to be 90.6° and 89.4°, respectively. However, based on dimensions from tank drawings (tank diameter assumed = 153 inches [3.8862 m]): $\theta_{AB} = 90.9^{\circ}$ and $\theta_{BC} = 89.8^{\circ}$. These slight differences are within *the accuracy of the measurements, which unless otherwise noted for all the distance measurements presented in this section, was within* ± 0.25 inches (± 6.35E-03 m).

2.3 Realignment of the Pulse Tubes

In order to locate the PJMs symmetrically within the tank, the following adjustments were made: 1) squaring the PJMs along the mounting structure near the top of the tank and 2) adding two additional tie beams and squaring the PJMs at the tie-beams which connect the pulse tubes at ~ 72 inches (1.8288 m) from the tank floor. All attempts to square the PJMs within the tank were made to within a *tolerance of* \pm 0.5 *inches* (\pm 0.0127 m).

2.4 As-Built Dimensions of the LTTS

After the modifications to the LTTS were made, the as-built dimensions of the LTTS were measured in terms of: 1) the wall to wall distances between the PJMs and 2) the distances between the tank wall and the walls of the PJM. These measured distances and a pulse tube outer diameter (OD) of 24.5 inches (0.6223 m) were then used to calculate the distances between: 1) the center to center of the PJMs and 2) tank wall to center of the PJMs. These distances are shown schematically in Figures 2.7 to 2.8 at two elevations corresponding to: 1) the top flanges to the PJMs and 2) the beginning of the nozzle section of the PJMs.

The distances of the spans between the PJM nozzles are shown in Figure 2.9. Here the spans were calculated based on the measured average internal diameters of the nozzles of 3.937, 3.958, 3.884, and 3.967 inches [0.0999998, 0.1005332, 0.0986536, and 0.1007618 m] for pulse tube A, B, C, and D, respectively. Note the nozzle diameters were measured using a micrometer.

The location of the as-built nozzle from the as-built body of the PJMs was measured using a plumb line dropped from the top center of each of the PJMs and through the nozzles at the bottom. These measurements are shown in Figure 2.10. In this figure, the crosses represent the location of the plumb line from the edge of the nozzle closest to the string. The distances shown in this figure are the distance from the closest edge of the nozzle to the string. The information in Figure 2.10 was overlaid on the "ideal"^(a) location of the PJM nozzles as shown in Figure 2.11. Here the "X" and "Y" distances represent the deviation of the measured nozzle center (represented by dashed circles) from "ideal" nozzle center location (represented by solid circles).

The as-built measurements made on the PJMs pertaining to the conical section of the pulse tubes as shown in Figure 2.12 and 2.13. The measured distances and angles referred to in these figures are listed in Tables 2.1 and 2.2. The measurements made involving the height of the center of the nozzle from the floor of the tank as shown in Figure 2.14 are summarized in Table 2.3.

PJM Tube Designation	Direction from Tube	Horizontal distance	Vertical Distance	Hypotenuse "H"	Measured Angle θ
	Center	(in)	(in)	(in)	(deg)
Α	North	10 1⁄4	$17^{-1}/8$	20	61
А	East	10 ¼	$17^{-1}/8$	20	60
А	South	10 ¼	$17^{-1}/8$	20	60
А	West	10	$17^{-1}/8$	19 7/8	61
В	North	10 1/4	17 ¼	20	61
В	East	10 ¹ /8	17 ¹ /8	20	61
В	South	10 1⁄4	$17^{-1}/8$	20	59
В	West	10 1/4	17 ¹ /8	20	60
C	North	10 ½	17 ¼	20 ¹ /8	61
C	East	10 1/4	17 ³ /8	20	60
C	South	10 1⁄4	17 ¼	20 ¹ /8	60
C	West	10 1⁄4	17 ¼	20	60
D	North	10 1⁄4	16 7/8	19 7/8	59
D	East	10 1/4	17 ¹ /8	19 7/8	60
D	South	10 1/2	17 ¹ /8	20	61
D	West	10 1/2	17	19 7/8	61

Table 2.1. PJM Measured Cone Dimensions and Taper Angles as defined in Figure 2.12 and 2.13(All Distances Were Measured to a Tolerance of ± 0.25 inches [± 0.00635 m])

(a) Here the ideal location is based on the assumption that all PJMs are vertically aligned and free from fabrication defects.

PJM Tube	Diameter	Elevated	Measured Angle α
Designation	Orientation	Side	(deg)
А	East/West	N/A	0
А	North/South	N/A	0
В	East/West	N/A	0
В	North/South	South	1
С	East/West	N/A	0
С	North/South	N/A	0
D	East/West	West	1
D	North/South	N/A	0
N/A = not app	olicable.		

Table 2.2. Orientation of the Plane of the Discharge Nozzle As defined in Figure 2.13 (All DistancesWere Measured to a Tolerance of ± 0.25 inches [± 0.00635 m])

Table 2.3. PJM Nozzle Heights from the Tank Floor as Defined in Figure 2.14 (All Nozzle Heights Were
Measured to a Tolerance of ± 0.1 inches [± 0.00254 m])

Pulse Tube	Distance from
Designation	Tank Floor (inches)
А	8 9/16
В	9 1/16
С	9 1/16
D	9 3/8



Figure 2.1. Photograph of the Tank Containing the Pulsed Jet Mixers



Figure 2.2. Photograph of the One of the Pulse Tube Included in the Large Tank Test System



Figure 2.3. Photograph of the Top View of the LTTS Showing the Structure Used to Support the PJMs



Figure 2.4. Schematic Showing the PJM Location in the Tank With Respect to the Labeling Use in the Present Testing



Figure 2.5. Initial Estimated Location of the PJMs in the LTTS



Figure 2.6. Positions of PJM Tubes with Respect to Tank Rim (* Measurements taken from inside of tank rim; ** 1 inch [0.00254 m] Threaded Fitting on Level Probe Rod for Securing to Access T in Head Cap)



Figure 2.7. Distances of the PJM Center to PJM Center and PJM Center to Tank Wall at the Top of the PJM Flange Connections @~ 166 inches [~ 4.2164 m] Elevation (All Distances are Reported to a Tolerance of ± 0.25 inches [± 0.00635 m])



Figure 2.8. Distances of the PJM Center to PJM Center and PJM Center to Tank Wall at the Bottom of the PJMs Just above the Weld to the Cone @ ~ 30 inches [~ 0.762 m] Elevation (All Distances are Reported to a Tolerance of ± 0.25 inches [± 0.00635 m])



Figure 2.9. Distances of the Spans between the PJM Nozzles (All Distances are Reported to a Tolerance of ± 0.25 inches [± 0.00635 m])



Figure 2.10. Measurement of PJM "As-Built" Nozzle With Respect To PJM "As-Built" Tube Bodies (All Distances are Reported to a Tolerance of ± 0.25 inches [± 0.00635 m])



Figure 2.11. Measurement of "As-Built" to "Ideal" Nozzle Locations (All Distances are Reported to a Tolerance of \pm 0.25 inches [\pm 0.00635 m])



Figure 2.12. Measurements Made Relative to the PJM Cone



Figure 2.13. Measurements Made Relative to the PJM Cone Orientation



Figure 2.14. Nozzle Height Measurement from Tank Bottom Head

3.0 Experimental Approach

As discussed in Section 1.0, the primary data needed to support the validation of the FLUENT CFD model of the pulsed jet mixing systems included: 1) velocity measurements during the hydrodynamic (water only) tests and 2) velocity and density data measurements with nominal 10 and 35 μ m volume mean particle size glass-beads at different solids loading and/or PJM operation conditions. In addition to the velocity and/or density measurements, additional data such as the liquid level changes in the pulse tube were also essential for computing the fluid velocities out of the nozzles of the PJMs. Finally, the pressure inside the pulse tubes and in the drive/suction lines of the JPPs were needed for operating the PJMs in a symmetric and prototypical manner.

In this section, the experimental approaches used to measure the various items discussed above are presented.

3.1 Velocity Measurement

The local velocity values in the large tank during the PJM operation were measured using 3.2 cm (1.259 inches) disc-shaped Valeport 802 electromagnetic (EM) flow sensors. The Valeport EM flow sensors were chosen for this application primarily because of the ruggedness of the probes and their applicability for measuring velocities in the presence of solids in the test system (i.e., for fluid velocity measurement during the simulant tests conducted in the LTTS). In addition, Valeport sensors also had the advantage of measuring the flow in two dimensions. In this application, the local velocity changes were measured vertically and azimuthally.

During the hydrodynamic (water only) tests, velocity measurements were made at 5 verticals, collecting 25 velocity measurements at each elevation (1 at the tank center line and 24 around a core with a 12.5 inches (0.3175 m) radius in increments of 15°). This was done primarily to check for symmetry of the fluid flow in the tank after the PJM realignment. During the simulant tests, however, velocity measurements were focused primarily at the tank centerline at the same five elevations as used in the hydrodynamic tests.

The velocity mapping was achieved by horizontally mounting the velocity probes (which are located at the end of a 12.5-inch [0.3175 m] extension rod) to a 0.75-inch (0.01905 m) stainless steel (SS) pipe approximately 20 ft long. The spacing between each velocity probe was 24 inches (0.6096 m), and the lowest probe was located at an elevation of 30 inches (0.762 m) as measured from the floor of the tank at the tank centerline. This is schematically shown in Figure 3.1. The probes were numbered 1 to 5 starting with 1 at the top (126 inch [3.2004 m] elevation) and 5 at the lowest point (30 inch [0.762 m] elevation). In order to stabilize the probe support and the probes in the tank, the probe support was anchored at the bottom of the tank and at the top to the tank-bridge. The arrangement was such that the velocity probe could be slid radially-outward (by 12 inches [0.3048 m]) to bring the velocity sensor heads to the tank centerline or rotated to map the velocity at different angular positions around a circle of 12.5 inch (0.3175 m) radius.



Figure 3.1. Schematic of the Velocity Probe Support Used in the Large Tank Test Stand

Figure 3.2, which shows the top view of the velocity probe assembly, illustrates the how the velocity probe angle is measured. Here the reference 0 deg plane is located in the East direction with the center of the mast located at the center of the tank or 12 inches (0.3048 m) westward from the tank center. This creates a bias of +3.4° inches (+0.08636 m) the angles presented in this report when measured from the center of the sensor head.



Figure 3.2. Top View of the Velocity Probe Holder Assembly

3.2 Density Measurement

During the simulant tests, the density of the slurry at various locations within the tank was monitored continuously during the PJM operation using a set of three MicroMotion Coriolis mass flow meters. The continuous slurry density monitoring equipment, shown schematically in Figure 3.3, consists of three recirculation pumps and three MicroMotion sensors. Slurry from the tank enters a pump inlet through one of the three 20 ft (6.096 m) long, 1 inch (2.54E-02 m) SS tubes located at the radial positions of 0, 3, and 5.75 ft (0, 0.914, and 1.753 m), respectively.

Each sample line had a provision so the height at which the sample is collected can be adjusted upward from a minimum of 3 inches (7.62E-02 m) from the floor of the tank. After the circulating sample stream was analyzed by the MicroMotion sensor, it was returned back to the tank. Using this configuration, density measurements were made at various depths and lateral positions to obtain a topographical representation of the slurry concentration profiles within the tank during the mixer operation.

Each MicroMotion sample loop had a 3-way valve assembly which enabled diverting the sample into a receiver vessel. Such an arrangement enabled the collection of grab samples which can be used to confirm the MicroMotion sampler readouts or to determine the PSD for assessing effectiveness of mixing and determining solids stratification.

3.3 Pulse Tube Liquid Level Measurement

The change of the liquid height in each pulse tube was individually measured using 12-ft (3.6576 m) long Teflon coated capacitance liquid level sensors (fabricated by DrexelBrook Inc.). These sensors were


Figure 3.3. Schematic of the Sampling System Used to Continuously Monitor the Density in the Tank During the Large Tank Simulant Testing

mounted in the center of each pulse tube through one end of a "T"-fitting attached to the 2-inch flange connector at the top of the pulse tube.

During the PJM operation, liquid/slurry completely fills the pulse tubes with the liquid/slurry entering ~15 ft into the air/vacuum lines. This was done by the AEA engineers to ensure that all PJMs fire at the same time. Once the liquid/slurry enters the air/vacuum line, the level probe reading gets saturated at the maximum value of 140 inches^(a) (3.556 m). This should however make negligible contribution to the nozzle velocities since the liquid volume is relatively small fraction of the total pulse tube volume (2.5 gal vs. 250 gal or ~ 1%).

3.4 Pulse Tube and JPP Pressure Measurements

In order to ensure that all the PJMs are operated (as close as possible) in an identical manner, the pressure inside each PJMs/JPP was individually measured using pressure transducers mounted on top of the pulse tube and at the air inlets to the drive and suction sides of the JPPs. Although independent pressure measurements within the PJMs and the JPP control module were made during the testing, the control of the PJMs was done using AEA proprietary PRESCONTM control system. In other words, the drive, vent, and suction times were set in the PRESCON controller to cycle the PJMs repeatedly at a period of 45 seconds.

3.5 PJM Operation

The large tank PJMs were operated using prototypical systems, i.e., using a combination of JPPs and solenoid valves to regulate the suction and discharge of the liquid to and from the pulse tubes. The JPPS were connected to the pulse tubes using 2 inch (5.08E-02 m) ID, wire reinforced, polyvinyl chloride (PVC) tubing.

A compressor/accumulator combination was used to regulate the airflow to the jet pump pairs. The compressor chosen for the present study based on the requirements for the airflow to the JPPs was a diesel powered compressor capable of delivering 1300 CFM at an operating pressure of 100 psig (8 bar). The accumulator was an ASME standard 240 gal (1000 L) Brunner vertical air receiver tank with pressure relief valves and timed electronic drain valve. Both the compressor and the accumulator were located outside the 336 Building.

The sequence of operation and cycle frequency of the PJMs was controlled by a PRESCONTM controller; an Atomic Energy Agency (AEA) Technology proprietary control system. PRESCONTM monitors pressure signals using pressure transmitters, which are a part of the JPP control module. PRESCONTM enables various combinations of pulse tube operation (i.e., all four at a time, two at a time, or one at a time) and cycle times. Prior to the start of the testing, AEA staff reprogrammed the

⁽a) This is less than the 144 inch (3.6576 m) size of the level probes since 4 inches (0.1016 m) of the level probe sensor is concealed behind the fittings used to fasten the probe to the PJMs.

PRESCONTM and in addition adjusted the air pressures to the drive/vent sides of the JPP to: 1) set cycle times close to prototypical operation conditions^(a) and 2) drive/refill the four PJMs in a "near" identical manner^(b).

3.6 Data Acquisition and Storage

All data from the experiments, which included date, time, liquid levels, pressures, velocities^(c,d), densities^(e), mass flow rates^(f), and temperature, were monitored continuously and recorded digitally on a computer using DASYLab, Version 5.5 data acquisition software installed on a Micron Millennia XRU PC running Windows 98.

The Data Acquisition System (DAS) sampled all channels at 32 Hz frequency and averaged the data over one second intervals. These one-second averages were electronically recorded in the data log files. The electronic data files were saved as ASCII or text files. Each electronic entry in the file included a date/time stamp and the file also included a header which at a minimum contains information regarding the test objective and the location of the velocity and density probes.

All data from the experiments were transferred on to zip disks and stored in duplicate. For data examination and "reasonableness" checks, data files were then copied into separate Excel spreadsheets. These Excel spreadsheets are presented on the CD included as an attachment to this report.

The Excel spreadsheets have the same header information and data label information as the data log files which are listed in Rows 1 to 11 of each file. Row 12 of the Excel files contains the labels of the various items recorded in each column. A description of the various column labels used in the Excel spreadsheets containing the experimental data from the present testing is listed in Table 3.1.

3.7 Data Quality

Of the various sensors used in the present testing, some measurements were made for helping the experimentalists operate the equipment in as near a symmetric manner as possible while other

⁽a) A cycle time of 45 s (~10 s drive and 35 s of vent/refill) was used during all testing.

⁽b) It was found to be extremely difficult to tune the PRESONTM to operate the PJMs in a truly identical manner due to the different performance characteristics of the JPPs and the difficulty in balancing the pressure/air flow conditions in air/vacuum lines of the PJMs. The tuning eventually achieved was the best possible with the current equipment.

⁽c) Of the five velocity sensors, the one present at the 126-inch (3.2004 m) elevation (Probe 1) was of an earlier model of the Valeport unit which had a built-in signal lag time of 6 seconds before the signal was transmitted to the data acquisition board. Therefore, all vertical and azimuthal velocity data for this sensor should be shifted back by 6 s to directly correlate the measured velocities to the pulse tube operation cycle.

⁽d) The vertical velocities in the downward direction and azimuthal velocities in the counter clockwise direction are treated and logged as positive values.

⁽e) It should be noted that the calibrations of the MicroMotion density meter included at the 5.75 ft (1.7526 m) radial position (Sensor 1) indicated a 0.002 specific gravity offset, thus 0.002 should be added to all raw values measured by this sensor.

⁽f) In addition to the density of the sample, the MicroMotion sensors also measure the mass flow rates in each density sampling loops. This information was also recorded in the data log files.

data/information was collected in accordance with the project/task requirements. The former set of data is classified as "Data for Information Only" and the later is defined as "Reportable Data". The difference between the two classifications is that:

- The sensors/instruments for "Reportable Data" were calibrated or performance checked in accordance to the WTP project QA requirements ^(a,b)
- The sensors for "Data for Information Only" utilized only the vendor provided calibration certificates (these calibrations do not necessarily meet the WTP project QA requirements)

The various instruments, functions, quality of the data (i.e., reportable/For Information only), service or organization performing the calibration or performance check, range of validity of the instrument output are listed in Table 3.2. It can be seen from Table 3.2 that the calibration of MicroMotion density^(c) and the DrexelBrook Level^(d) sensors were performed by the users (i.e., the PNWD staff involved in the PJM testing).

After the performance check of the level sensors and during the subsequent hydrodynamic testing, it was realized that the level sensor span drifted by ~ +6 inches (0.1524 m). The cause of the span drift is not known but it is speculated that this was due to the change in the liquid conductivity resulting from the decrease in pH due to the solubilization of CO_2 from the atmosphere during the PJM operation. For this reason, the reading of each level probe and the stationary height of the liquid/slurry in the tank was recorded prior to the start of each days test. Based on this information, the average span drift in the level probes in pulse tube A, B, C, and D over the duration of the testing was determined to be +4.3, +4.3, +4.6, and +4.4 inches (0.10922, 0.10922, 0.11684, and 0.11176 m), respectively. On the other hand, the maximum drift for the four level probes was +7.2, +7.5, +8.5, and +8.1 inches (0.18288, 0.1905, 0.2159, and 0.20574 m), respectively.

3.8 Measurement Uncertainties, Noise Levels, and Scale Factor/Bias Errors

The DAS software has a feature allowing input scaling to be directly entered, individually and uniquely, for each channel. Each analog input channel to the DAS uses an industry-standard 5B module that converts the applied input signal (whether it be 4-20 mA, \pm 5 V, thermocouple) to an analog voltage in the range of 0-5 V, which the analog input channel "sees". As an example, the scaling for one of the Valeport 802 velocity sensor/signal conditioner units is illustrated in Table 3.3.

The Valeport 802 signal conditioner outputs over a nominal range of \pm 5 Volts. From the tow tank calibration performed by Northwest Research Associates in Bellevue, WA, it was determined that for this

⁽a) PNWD implemented the RPP-WTP quality requirements by performing work in accordance with the quality assurance project plan (QAPjP) approved by the RPP-WTP Quality Assurance (QA) organization. This work was conducted to the quality requirements of NQA-1-1989 and NQA-2a-1990, Part 2.7 as instituted through PNWD's Waste Treatment Plant Support Project (WTPSP) Quality Assurance Requirements and Description Manual.

⁽b) List of project approved calibration services is available at http://bss-ams.pnl.gov/quality/esl.

⁽c) User calibration was necessary for the MicroMotion density sensors due to the fact that there was no QA service that met the project requirements to calibrate the sensors.

⁽d) The DrexelBrook capacitance level probes required a user calibration since the sensitivity of the probes was dependent on the capacitance characteristics of the medium/environment in which the measurements were made.

particular sensor this corresponds to a linear variation between -5.4997 m/s to + 5.2003 m/s^(a). These two extreme velocity points are linearly^(b) translated to 0V and + 5V, respectively, by the 5B module as inputted to the DAS analog input channel. This analog input scaling, set for each individual channel's unique calibration, tends to greatly eliminate scale factor and bias errors.

Excel Col.	Variable Label	Description Mea			
Α	Date	Date the Experiment was Conducted	Day/Month/Year		
В	Time	Time at which the data was logged	Hr: Min: Sec		
С	Velo. 1-X	Azimuthal Velocity Component of Probe 1 at 126 inch Elevation	m/s		
D	Velo. 1-Y	Vertical Velocity Component of Probe 1 at 126 inch Elevation	m/s		
E	Velo. 2-X	Azimuthal Velocity Component of Probe 2 at 102 inch Elevation	m/s		
F	Velo. 2-Y	Vertical Velocity Component of Probe 2 at 102 inch Elevation	m/s		
G	Velo. 3-X	Azimuthal Velocity Component of Probe 3 at 78 inch Elevation	m/s		
Н	Velo. 3-Y	Vertical Velocity Component of Probe 3 at 78 inch Elevation	m/s		
Ι	Velo. 4-X	Azimuthal Velocity Component of Probe 4 at 54 inch Elevation	m/s		
J	Velo. 4-Y	Vertical Velocity Component of Probe 4 at 54 inch Elevation	m/s		
K	Velo. 5-X	Azimuthal Velocity Component of Probe 5 at 30 inch Elevation	m/s		
L	Velo. 5-Y	Vertical Velocity Component of Probe 5 at 30 in Elevation	m/s		
M ^(a)	Q 1	Mass Flow Rate of MicroMotion Sensor 1 @ $R = 5.5$ -ft	L/min		
N ^(a)	S.G. 1	Density of MicroMotion Sensor 1 $@$ R = 5.5-ft	g/cm ³		
O ^(a)	Q 2	Mass Flow Rate of MicroMotion Sensor 2 $@$ R = 3-ft	L/min		
P ^(a)	S.G. 2	Density of MicroMotion Sensor 2 $@$ R = 3-ft	g/cm ³		
Q ^(a)	Q 3	Mass Flow Rate of MicroMotion Sensor 3 $@$ R = 0-ft	L/min		
R ^(a)	S.G. 3	Density of MicroMotion Sensor 3 $@$ R = 0-ft	g/cm ³		
S	Level A	Level of the Liquid in Pulse Tube A	Inches		
Т	Level B	Level of the Liquid in Pulse Tube B	Inches		
U	Level C	Level of the Liquid in Pulse Tube C	Inches		
V	Level D	Level of the Liquid in Pulse Tube D	Inches		
W	P.T. P. A	Pressure in Pulse Tube A	psia		
Х	P.T. P. B	Pressure in Pulse Tube B	psia		
Y	P.T. P. C	Pressure in Pulse Tube C	psia		
Z	P.T. P. D	Pressure in Pulse Tube D	psia		
AA	Manif. P. A	Manifold Drive Pressure on JPP for Pulse Tube A	psia		
AB	Manif. P. B	Manifold Drive Pressure on JPP for Pulse Tube B	psia		
AC	Manif. P. C	Manifold Drive Pressure on JPP for Pulse Tube C	psia		
AD	Manif. P. D	Manifold Drive Pressure on JPP for Pulse Tube D	psia		
AE	Temp. 1	Temperature in Tank	°C		
AF	Temp. 2	Ambient Temperature	°C		
AG	S.N. Tank Wt.	Gross Weight of Tank and its Contents	lbs		
(a) Density and mass flow rate data recorded in these columns during the hydrodynamic tests are irrelevant to the tests.					

 Table 3.1. Description of the Various Column Labels Used in the Excel Spreadsheets Containing the Experimental Data from the Present Testing

⁽a) Note – Although the calibration data was extrapolated to ~ ± 5 m/s (the full range of the velocity probes), the velocity data is only applicable to ± 2.5 m/s, which is the range over which the probes were calibrated.

⁽b) Note – A linear translation was utilized since the Valeport calibration was linear. The DAS system also allows for non-linear calibration curves.

The Measurement Computing PCI-DAS6402/16 analog input board used in the DAS has 16 bit resolution (.001526% resolution). Based on this, the resolutions for the inputs from the various sensors are shown in Table 3.4. The actual system resolution/accuracy is, however, limited by the sensors and signal conditioning, which are summarized in Table 3.5. See Appendix A for more details about the different sensors used to measure the reportable data.

Manufacturer	Function/Measured	Data Quality	Calibrated or Performance	Range
	Variable		Checked By	
Valeport	Velocity (Vertical	Reportable Data	Calibrated/Northwest Research	± 2.5 m/s
	and Azimuthal)		Associates, Bellevue, WA ^(a)	
MicroMotion	Density	Reportable Data	Performance Check/User ^(b)	$0.99 - 1.5 \text{ g/cm}^{3 (c, d)}$
DrexelBrook	Level	Reportable Data	Performance Check/User ^(b)	0 - 140 in ^(e)
Type K T/C	Ambient	Reportable Data	Calibrated/Battelle Calibration	0 – 50 °C
	Temperature		Services	
Туре К Т/С	Slurry/Liquid	Reportable Data	Calibrated/Battelle Calibration	0 – 50 °C
	Temperature		Services	
Sartorius	Weighing Balance ^(f)	Reportable Data	Calibrated/Quality Control Services,	0 – 200 g
			Portland, OR	
Inscale	Platform Scale ^(g)	Reportable Data	Calibrated/Quality Control Services,	0 – 5000 lbs
			Portland, OR	
Measurement	DAS - Analog Input	Reportable Data	Calibrated/Battelle Calibration	All Channels
Computing	Board PCI-		Services	
	DAS6402/16			
MicroMotion	Flow Rate	Data For Info Only	Calibrated/Fischer Rosemount ^(h)	0 – 100 L/min
Cecomp	Pulse Tube Pressure	Data For Info Only	Calibrated/Cecomp ^(h)	0 – 100 psi
Cecomp	JPP Module Pressure	Data For Info Only	Calibrated/Cecomp ^(h)	0 – 100 psi
Hardy	Tank Weight	Data For Info Only	Calibrated/Hardy Instruments ^(h)	0 – 300,000 Lbs
Instruments				

Table 3.2. Data Quality, Mechanism of Calibration/Performance Checking, and Range of Applicability of Data Obtained from the Various Sensors Used in the Testing

(a) Project approved calibration service.

(b) All user calibrations were performed using procedures or test instructions that were determined to meet the project QA requirements by PNWD QA personnel

(c) The MicroMotion sensors performance was checked using three density standards of specific gravities of 0.99, 1.07, and 1.12 g/cm^3 . The sensor output which varies linearly with density is valid over the range of 0 to 5 g/cm³.

(d) The MicroMotion sensors density readings during the testing were also check periodically using grab samples collected from each sampling system bypass line.

(e) Performance check of the level probe sensors was done to $\pm 1/4$ in. with each probe installed in the pulse tube system.

(f) Sample weights and volumes determined using standard laboratory glassware were used to determine the density of the samples used for MicroMotion density sensors performance check.

(g) This balance was used to determine the mass of glass beads added to the tank. This along with the volume determined from the dimensions of the tank and height of fill were used to determine the concentration of the solids in tank.

(h) Vendor provided calibration.

Instrument Signal	DA	S Channel Sca	ling	
Conditioner Output	Ser	Hardware		
	Low	High	Low	High
± 5 V	-5.4997 m/s	+5.2003 m/s	0 V	5 V

Table 3.3. Instrument Output and DAS Channel Scaling of One of the Valeport Sensors

Table 3.4. DAS Resolution for Inputs from Various Sensors

Sensor	Input Range to DAS	DAS Resolution
Valeport Velocity Sensors	$\pm 5 \text{ m/s}$	7.63E-05 m/s
MicroMotion Density	$0.9 - 1.5 \text{ g/cm}^3$	$2.29E-05 \text{ g/cm}^3$
MicroMotion Flow Rate	0 – 100 L/min	0.001526 L/min
DrexelBrook Level Sensor	0 – 140 in	2.20E-03 in
Cecomp Pressure Sensor	0 – 100 psia	1.53E-03 psia
Туре К Т/С	0 – 50 °C	7.63E-04 °C
Load Gages for Tank Weight	0 – 300K lbs	5 lbs

Table 3.5 .	Accuracy of the Sensors and the Corresponding Signal Conditioning Equipment Used in the
	Large Tank Testing

Variable	Manufacturer	Sensor Model	Transmitter	Accuracy
			Model	
Velocity	Valeport	3.2 cm Discus	802	± 5.0 E-03 m/s + 1% of Each
				Axis
Density (Sensor 1)	MicroMotion	D100	RFT 9739	$\pm 0.001 \text{ g/cm}^3$
Density (Sensors 2	MicroMotion	CMF 100	RFT 9739	$\pm 0.0005 \text{ g/cm}^3$
& 3)				
Level Probes	DrexelBrook	700-0002-057	408-8232-001	0.25% of Span = 0.35 inches
				for the 140 inch span
Pulse Tube Pressure	Cecomp	DPG100	F4DR	$\pm 0.25\%$ of Full Scale = 0.25
	Electronics			psi for a span of 100 psi
Temperature	Omega	Type K T/C	-	± 2.2 °C

4.0 Results: Hydrodynamic Tests

The primary focus of the hydrodynamic tests was to determine the symmetry of the velocity flow fields in the tank after the PJMs realignment and fine tuning the PRESCONTM programming for control of the PJMs operation. These results are presented as Excel spreadsheets in the CD included along with this report.

In this section, the nomenclature used in the description of the files containing the data and a brief discussion of the results in terms of the flow field symmetry are presented.

4.1 Nomenclature Used

The Excel spreadsheets containing the hydrodynamic test data is stored in the folder "021108 DATA". The file list is summarized in Table 4.1.

File Name	ime Clock Time		Velocit	y Probe Position		
	Start	Finish	Direction	Radial Position (in)		
021108A.xls ^(a)	09:09:59	09:19:50	0° (East)	12		
021108B.xls ^(a)	09:29:26	09:50:09	0° (East)	12		
021108C.xls ^(a)	09:52:45	10:34:15	30°	12		
021108D.xls ^(a)	10:36:50	11:16:50	60°	12		
021108E.xls ^(a)	11:18:36	12:01:45	90° (South)	12		
021108F.xls ^(a)	12:02:45	12:25:20	120°	12		
021108G.xls ^(a)	12:30:30	12:52:30	150°	12		
021108I.xls ^(a)	13:14:50	13:36:55	180° (West)	12		
021108J.xls ^(b)	13:49:20	14:04:35	210°	12		
021108K.xls	14:06:40	14:29:40	240°	12		
021108L.xls ^(c)	14:31:00	14:59:55	270° (North)	12		
021108M.xls	15:01:50	15:26:05	300°	12		
021108N.xls	15:34:05	15:56:10	330°	12		
021108O.xls	16:12:30	16:36:50	0° (East)	12		
021108P.xls	16:39:40	17:29:15	45°	12		
021108Q.xls	17:33:30	17:55:00	135°	12		
021108R.xls	17:56:45	18:18:03	225°	12		
021108S.xls	18:21:35	18:43:28	315°	12		
021108T.xls	18:52:20	19:14:40	0° (East)	0		
021108U.xls	19:16:30	19:38:10	180° (West)	24		
(a) Valasity make No. 1 data invalid wina waa kaakan						

Table 4.1. Summary of the Files Containing the Hydrodynamic Test Data

(a) Velocity probe No. 1 data invalid, wire was broken.

(b) Velocity probe wire repaired; data valid from here onwards.

(c) Data for Columns S through AG missing.

During each run, a minimum of 25 cycles of data was collected to enable computation of the cycle average velocity profiles in the tank. However, during several measurements, more than 25 cycles of data was collected due to repeated shutdown/restart of the PRESCONTM controller as a result of clogged air regulators on the JPP control module^(a).

4.2 Velocity Profiles and Flow Field Symmetry

The cycle averaged vertical velocities at the tank center line region, and the five elevations where the measurements were made are shown in Figure 4.1. It can be seen from this figure that as the elevation increases and the magnitude of the velocity decreases.

Although the data in Figure 4.1 shows the general trends of the velocity profiles, it does not provide any information regarding the symmetry of the flow field in the tank. This effect is illustrated in Figures 4.2 through 4.5 showing the contour maps of the cycle averaged vertical velocities in the tank at 8 s after the start of a typical pulse and at elevations of 30, 54, 78, and 102 inches (0.762, 1.3716, 1.9812, and 2.5908 m), respectively. In all of these figures, the pulse tubes A, B, C, and D are located in the NW, SW, SE, and NE directions, respectively, at a radial position of ~4.25 ft (~1.2954 m).

It can be seen from Figure 4.2 that although the flow is slightly skewed towards pulse tubes A and B, the velocities are reasonably symmetric and peak velocities occur at the tank center. However as the velocity fields are examined at higher elevations (see Figures 4.3 to 4.5), the asymmetric behavior becomes more pronounced. However, in all cases, the peak velocities are still close to the tank center regions.

Although the geometric dissimilarity (presented in Section 3.0) still causes some asymmetry in the flow, the differences in the individual pulse tubes operation also contributes to the asymmetric flow. This is illustrated in Figure 4.6 in terms of the cycle averaged liquid levels in the pulse tubes. It can be seen from this figure that pulse tubes B and D drive much harder than pulse tubes A and C. Although AEA staff attempted to minimize the differences in the liquid level changes in the pulse tubes, inherent system and PRESCONTM controller limits did not enable further improvements in the synchronous firing of the PJMs.

At this point, BNI decided that further improvements in the symmetry are not possible within the budget and time constraints and gave the go ahead for the simulant tests. These results are presented in the next section.

⁽a) Cleaning the air regulators after the completion of the hydrodynamic tests essentially eliminated the controller shutdown problem during the simulant runs.



Figure 4.1. Time Averaged Vertical Velocity Profiles at the Tank Centerline



Figure 4.2. Contour Map Showing the Fluid Velocities in a 2-ft Diameter Core Around the Center of the Tank and an Elevation of 30 inches (0.762 m)



Figure 4.3. Contour Map Showing the Fluid Velocities in a 2-ft Diameter Core Around the Center of the Tank and an Elevation of 54 inches (1.3716 m)



Figure 4.4. Contour Map Showing the Fluid Velocities in a 2-ft Diameter Core Around the Center of the Tank and an Elevation of 78 inches (1.9812 m)



Figure 4.5. Contour Map Showing the Fluid Velocities in a 2-ft Diameter Core around the Center of the Tank and an Elevation of 102 inches (2.5908 m)



Figure 4.6. Cycle Averaged Liquid Level Changes in the Pulse Tubes

5.0 Results: Simulant Tests

The primary focus of the simulant tests was to determine the startup transients and steady state concentration profiles in the tank after the PJM realignment and fine tuning of the PRESCONTM controller programming of the PJM operation. These results are presented as Excel spreadsheets in the CD included along with this report.

In this section, the tests performed, simulants used, nomenclature used in the description of the files containing the data, and a brief discussion of the results is presented.

5.1 Simulant Used

The simulant used in the mixing tests was Spheriglass[®] glass-beads (specific gravity 2.49) of either 10 or 35 µm nominal volume mean particle size.^(a, b) Spheriglass[®] is a registered trademark of Potters Industries Inc., Valley Forge, PA, is supplied under the trade names of A5000 and A3000 for the nominal volume mean particle sizes of 10 and 35 µm, respectively.

The choice of glass-beads of nominal volume mean particle sizes of 10 and 35 μ m was driven by: 1) extremely poor mixing results obtained in FY01 with the larger (~75 μ m volume mean) particle size glass-beads (Bontha et al 2003)^(c) and 2) some preliminary settling tests performed with the A3000 and the A5000 grade materials. The latter indicated that the settling rates with the nominal 10 μ m volume mean particle size material (A5000 grade)^(d) were a factor of 3 greater than those of some typical Hanford type wastes (which are typically on the order of 10 cm/hr).

For the testing, 20,000 lbs each of the A3000 and A5000 grade materials were procured from Potters (packaged in 500 or 1000 lbs bags) to make up a simulant of a maximum solids loading of 20 wt%. Because of the sifting of the samples in the bags during shipping from the vendor, it was difficult to obtain representative samples to precisely determine the average particle size distribution (PSD). Also, since there was variability in the vendor supplied minimum, mean, and maximum values of the particle sizes between bag to bag of the same grade materials, homogenizing a single bag was deemed to not produce representative sample of the entire lot. Therefore, it is recommended that homogeneously^(e) mixed slurry samples collected during the mixing tests be used to determine the representative particle size distribution of the simulant. This data for the different solid loading tests performed is listed in Appendix B.

⁽a) The particle sizes presented here and through out this report are the volume based particle size distribution. The area (or Sauter's) based particle size distribution are included in Appendix A.

⁽b) The PSD distribution of the two simulants grade materials is presented in Appendix A.

⁽c) During these tests, no solids were observed above ~ 60 inches (1.524 m) from the bottom of the tank.

⁽d) It was difficult to determine the settling rate with the 35 μm nominal volume mean particle size (A3000 grade) material due to the lack of a clear solid/liquid interface during the settling tests.

⁽e) Here homogeneity is based on the density of the slurry in the tank at the top, middle and bottom regions of the tank being within ± 0.002 g/cm³ of each other.

5.2 Tests Performed

A variety of PJM mixing tests were performed with the two different types of simulant at different solids loading and PJM operation conditions. The tests performed and their scope is summarized in Table 5.1.

Test ID	Simulant	Wt%	Average SP GR ^(a)	PJMs Operating Mode	Test Scope
1	A5000 Grade -	5	1.029	A, B, C, & D	Start Up Transient and Steady
	10 µm Glass-beads				State Profiles
2	A5000 Grade -	20	1.113	A, B, C, & D	Start Up Transient and Steady
	10 µm Glass-beads				State Profiles
3	A5000 Grade -	20	1.113	B & D	Settling Transient after
	10 µm Glass-beads				Achieving Steady State
4	A5000 Grade -	20	1.113	B & D	Start Up Transient and Steady
	10 µm Glass-beads				State Profiles
5	A3000 Grade -	5	1.029	A, B, C, & D	Start Up Transient and Steady
	35 µm Glass-beads				State Profiles
6	A3000 Grade -	5	1.029	B & D	Settling Transient after
	35 µm Glass-beads				Achieving Steady State
7	A3000 Grade -	5	1.029	B & D	Start Up Transient and Steady
	35 µm Glass-beads				State Profiles
8	A3000 Grade -	20	1.134	A, B, C, & D	Start Up Transient and Steady
	35 µm Glass-beads				State Profiles
9	A3000 Grade -	20	1.134	B & D	Settling Transient after
	35 µm Glass-beads				Achieving Steady State
10	A3000 Grade -	20	1.134	B & D	Start Up Transient and Steady
	35 µm Glass-beads				State Profiles
(a) D	etermined from the act	ual mass o	of solid and l	iquid phases in the ta	ank.

Table 5.1. List of Simulant Mixing Test Performed and their Scope

In all tests, the tank was filled up to 36 inches (0.9144 m) from the top rim and the PJM cycle time was maintained at 45 s. The difference in the PJM operation modes was with respect to the number of PJMs operated at a time, e.g., all four or two at a time. This was driven by the extent of mixing observed after steady state was achieved. For example, for Tests #1, #2, #5, and #8, it was observed that the tank contents, except for some slight variations, were nearly completely mixed. Although these slight variations are important from considerations of the PJMs ability to mix, they are not appreciable for code validation since it is generally very difficult to predict such small changes. By switching two of the PJMs off, the amount of mixing energy added to the system was reduced and this resulted in increased solids stratification in the tank. Such data is considered to be more relevant to code validation efforts.

5.3 Nomenclature Used

The Excel spreadsheets containing the results of Test # 1 (Table 5.1) are stored in the folder "021115 DATA" on the CD accompanying this report and the file list is summarized in Table 5.2.

	Clock	Time	Vel. Probes (2	Vel. Probes (1 to 5) Pos.		MicroMotion Sensor Elevation	
File Name	Start	End	Angular	Radial	Sensor 1	Sensor 2	Sensor 3
			(deg)	(in)	(in)	(in)	(in)
021115B.xls ^(a)	12:57:44	13:50:00	0°	0	54	54	N/A
021115C.xls ^(b)	13:53:29	14:16:24	0°	0	54	54	N/A
021115D.xls ^(b)	15:23:00	15:41:56	180°	24	126	36	24
021115E.xls ^(b)	15:49:46	16:10:17	180°	24	90	9	12
021115F.xls ^(b)	16:22:39	16:43:58	135°	24	24	90	54
021115G.xls ^(b)	16:48:40	17:10:31	135°	17	36	126	90
021115H.xls ^(b)	17:13:50	17:35:57	135°	17	72	12	36
021115I.xls ^(b)	17:40:10	18:02:49	135°	17	108	24	3
021115J.xls ^(b)	18:14:36	18:36:27	0°	0	54	54	N/A
(a) Contains the startup transient data.							
(b) Files containing the velocity and concentration data after steady state or a periodic condition in							

Table 5.2. Summary of Files Containing the Startup Transient and Steady State Data for the Simulant Test #1 (5 wt%, 10 μm nominal volume mean glass-beads, 4 PJMs) Data

(b) Files containing the velocity and concentration data after steady state or a periodic condition in concentration have been reached.

In all the data tables presented in this section, the radial position of the MicroMotion sensors sampling tubes and the vertical positions of the velocity probes (1 through 5) are listed in Tables 5.3 and 5.4.

 Table 5.3.
 Radial Position of the MicroMotion Sensors During All Simulant Tests

MicroMotion Sensor	Radial Position (in) ^(a)			
Sensor 1	69			
Sensor 2	36			
Sensor 3	0			
(a) As measured from the tank center				

Table 5.4 .	Vertical Position of	the Velocity	Probes During	All Simulant Tests
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Velocity Probe	Vertical Position (in) ^(a)			
Probe #1	126			
Probe #2	102			
Probe #3	78			
Probe #4	54			
Probe #5	30			
(a) As measured from the tank floor and the center of the drain pipe.				

At the completion of Test #1, an additional amount of the nominal 10 μ m volume mean particle size glass-beads was added to increase the solids loading up to 20 wt% and prepare for Test #2. The Excel spreadsheets containing the results of Test #2 (Table 5.1) are stored in the folder "021121 DATA" on the CD accompanying this report and the file list is summarized in Table 5.5.

	Clock Time		Velocity Prob	Velocity Probe Position		MicroMotion Sensor Elevation		
File Name	Start	End	Angular	Radial	Sensor 1	Sensor 2	Sensor 3	
			(deg)	(in)	(in)	(in)	(in)	
021121A.xls ^(a)	10:31:45	11:48:35	0°	0	126	54	N/A	
021121B.xls ^(b)	12:00:45	12:56:25	0°	0	126	54	N/A	
021121C.xls ^(b)	13:05:20	13:28:12	180°	24	90	24	12	
021121D.xls ^(b)	13:33:45	13:00:08	180°	24	54	18	3	
021121E.xls ^(b)	14:03:50	14:26:00	180°	24	24	9	54	
021121F.xls ^(b)	14:31:30	14:33:00	135°	17	36	108	90	
021121G.xls ^(b)	14:34:50	14:54:00	135°	17	36	126	90	
021121H.xls ^(b)	15:01:30	15:20:50	135°	17	72	90	24	
021121I.xls ^(b)	15:26:40	15:47:40	0°	0	126	54	N/A	
(a) Contains the	startup trans	ient data.		· · · · · ·				

Table 5.5. Summary of Files Containing the Startup Transient and Steady State Data for the Simulant Test #2 (20 wt%, 10 μm nominal volume mean glass-beads, 4 PJMs)

(b) Files containing the velocity and concentration data after steady state or a periodic condition in concentration have been reached.

At the completion of Test #2, the settling transient data with PJMs B and D running were determined. The Excel spreadsheets containing the results of the settling transient (Tests #3 of Table 5.1) are also stored in the folder "021121 DATA" on the CD accompanying this report. The file list is summarized in Table 5.6.

Table 5.6. Summary of Files Containing the Settling Transient Data for the Simulant Test #3(20 wt%, 10 µm nominal volume mean glass-beads, 2 PJMs)

	Clock	Clock Time		e Position	MicroMotion Sensor Elevation		
File Name	Start	End	Angular	Radial	Sensor 1	Sensor 2	Sensor 3
			(deg)	(in)	(in)	(in)	(in)
021121K.xls ^(a)	16:25:40	19:23:45	0°	0	126	54	N/A
021121L.xls	19:31:10	19:51:55	180°	24	90	54	90
021121M.xls ^(b)	19:58:30	20:21:09	180°	24	138	54	90
021121O.xls	20:37:15	21:15:22	180°	24	134	54	126
021121P.xls	21:22:30	21:37:55	180°	24	126	9	36
(a) PJMs A & C running initially and at 16:47 PJMs A & C turned off and PJMs B & D turned on.							
(b) At 20:04 Mic	croMotion se	ensor 1 samp	ling tube raised t	to 134 inch	es (3.4036 m).	

After the completion of the simulant Test #3, the contents of the tank were allowed to settle overnight before the simulant Test #4 was started. The Excel spreadsheets containing the results of simulant Test #4 (Table 5.1) are stored in the folder "021122 DATA" on the CD accompanying this report. The file list is summarized in Table 5.7.

Table 5.7. Summary of Files Containing the Startup Transient Data for the Simulant Test #4 (20 wt%, 10 μm nominal volume mean glass-beads, 2 PJMs)

	Clock Time		Velocity Probe Position		MicroMotion Sensor Elevation		
File Name	Start	End	Angular	Radial	Sensor 1	Sensor 2	Sensor 3
			(deg)	(in)	(in)	(in)	(in)
021122A.xls	14:07:00	15:15:00	0°	0	136	54	N/A

After the completion of simulant Test #4, the tank contents were emptied and the nominal 35 μ m volume mean glass-bead simulant at 5 wt% solids loading was prepared. The Excel spreadsheets containing the results of simulant Test #5 (Table 5.1) are stored in the folder "021204 DATA" on the CD accompanying this report. The file list is summarized in Table 5.8.

After completion of the Test #5, the PJMs A and B were turned off, and the settling transient with PJMs B and D operating (Test #6) were collected. The Excel spreadsheets containing the results of Test #6 (Table 5.1) are also stored in the folder "021204 DATA" of the CD accompanying this report. The file list is summarized in Table 5.9.

After the completion of Test #6, the simulant was allowed to settle for 6 days, and the startup transient with just PJMs B and D operating was determined. The Excel spreadsheets containing these results of Test #7 (Table 5.1) are stored in the folder "021210 DATA" on the CD accompanying this report. The file list is summarized in Table 5.10.

After the completion of Test #7, additional amount of the nominal 35 μ m volume mean particle size glass-beads was added to increase the solids loading up to 20 wt%. The Excel spreadsheets containing the results of Tests #8 (Table 5.1) are stored in the folder "021212 DATA" on the CD accompanying this report. The file list is summarized in Table 5.11.

After the completion of Test #8, the PJMs A and C were turned off and the settling transient was determined with only PJMs B and D operating. The Excel spreadsheets containing the results of Test #9 (Table 5.1) are also stored in the folder "021212 DATA" on the CD accompanying this report. The file list is summarized in Table 5.12.

After the completion of Test #9, the simulant was allowed to settle for 3 days, and the startup and steady state data with only PJMs B and D operating was recorded. The Excel spreadsheets containing the results of Test #10 (Table 5.1) are stored in the folder "021216 DATA" on the CD accompanying this report. The file list is summarized in Table 5.13.

	Clock Time		Velocity Probe	e Position	MicroMo	tion Sensor	Elevation
File Name	Start	End	Angular	Radial	Sensor 1	Sensor 2	Sensor 3
			(deg)	(in)	(in)	(in)	(in)
021204A.xls ^(a)	11:14:00	11:38:00	0°	0	126	54	N/A
021204B.xls ^(b)	11:38:00	13:07:30	0°	0	126	54	N/A
021204C.xls ^(c)	13:09:40	13:46:05	0°	0	126	54	N/A
021204D.xls ^(c)	13:58:10	14:12:55	180°	24	108	24	3
021204E.xls ^(c)	14:20:50	14:39:55	135°	17	90	36	6
021204F.xls ^(c)	14:48:45	15:08:40	180°	24	72	90	12
021204G.xls ^(c)	15:15:10	15:36:40	225°	17	54	9	24
021204H.xls ^(c)	15:44:50	16:03:20	180°	24	24	136	54
021204I.xls ^(c)	16:07:00	16:28:50	180°	24	36	126	90
021204J.xls	16:36:20	17:09:15	0°	0	126	54	N/A
021204J.xls	16:36:20	17:09:15	0°	0	126	54	N/A

Table 5.8. Summary of Files Containing the Startup Transient and Steady State Data for the SimulantTest #5 (5 wt%, 35 μm nominal volume mean glass-beads, 4 PJMs)

(a) First log file of the startup transient data.

(b) Second log file of the startup transient data.

(c) Files containing the velocity and concentration data after steady state or a periodic condition in concentration have been reached.

Table 5.9. Summary of Files Containing the Settling Transient Data for the Simulant Test #6 (5 wt%, 35 μm nominal volume mean glass-beads, 2 PJMs)

	Clock Time		Velocity Probe Position		MicroMotion Sensor Elevation		
File Name	Start	End	Angular (deg)	Radial (in)	Sensor 1 (in)	Sensor 2 (in)	Sensor 3 (in)
021204N.xls	19:16:30	19:35:35	180°	24	108	12	3
021204P.xls	19:42:35	20:01:20	180°	24	72	36	6
021204Q.xls	20:17:35	20:38:40	180°	24	126	90	24
021204R.xls	20:48:15	21:07:05	0°	0	24	54	N/A

Table 5.10. Summary of Files Containing the Startup Transient and Steady State Data for the SimulantTest #7 (5 wt%, 35 μm nominal volume mean glass-beads, 2 PJMs)

	Clock Time		Velocity Probe Position		MicroMotion Sensor Elevation		
File Name	Start	End	Angular	Radial	Sensor 1	Sensor 2	Sensor 3
			(deg)	(in)	(in)	(in)	(in)
021210A.xls	09:59:37	11:49:12	180°	24	126	54	30
021210B.xls	11:54:15	12:29:25	180°	24	126	54	3
021210C.xls	12:38:00	13:33:00	0°	0	126	54	N/A

	Clock Time		Velocity Probe	Velocity Probe Position		tion Sensor	Elevation
File Name	Start	End	Angular	Radial	Sensor 1	Sensor 2	Sensor 3
			(deg)	(in)	(in)	(in)	(in)
021212A.xls ^(a,b)	11:57:40	12:19:00	0°	0	126	54	N/A
021212B.xls ^(c)	12:22:06	15:04:00	180°	24	126	54	36
021212C.xls ^(d)	15:10:46	15:29:15	0°	0	126	54	N/A
021212D.xls ^(d)	15:40:20	15:59:45	180°	24	54	90	12
021212E.xls ^(d)	16:10:15	16:30:45	180°	24	24	108	3
021212F.xls ^(d)	16:43:40	17:02:51	180°	24	72	9	24
021212G.xls ^(d)	17:09:55	17:29:05	180°	24	90	24	54
021212H.xls ^(d)	17:36:45	17:55:45	180°	24	136	36	90
021212I.xls ^(d)	18:18:15	18:37:45	0°	0	126	54	N/A

Table 5.11.Summary of Files Containing the Startup Transient and Steady State Data for the Simulant
Test #8 (20 wt%, 35 μm nominal volume mean glass-beads, 4 PJMs)

(a) First log file of the startup transient data.

(b) PJMs started at 12:00:10.

(c) Second log file of the startup transient data.

(d) Files containing the velocity and concentration data after steady state or a periodic condition in concentration have been reached.

Table 5.12. Summary of Files Containing the Settling Transient Data for the Simulant Test #9(20 wt%, 35 μm nominal volume mean glass-beads, 2 PJMs)

	Clock Time		Velocity Prob	Velocity Probe Position		MicroMotion Sensor Elevation		
File Name ^(a, b)	Start	End	Angular	Radial	Sensor 1	Sensor 2	Sensor 3	
			(deg)	(in)	(in)	(in)	(in)	
021212J.xls	18:52:30	20:31:09	180°	24	126	54	36	
021212K.xls	20:38:20	20:42:30	180°	24	126	54	36	
021212L.xls	20:43:15	22:22:56	180°	24	126	54	36	
021212M.xls	22:27:56	22:36:30	180°	24	126	54	36	
021212N.xls	23:12:50	23:36:30	180°	24	78	72	36	
(a) Started w/4 PJMs running, @19:05:45 PJMs A & C shut down, leaving only B & D running.								
(b) Files are con	secutive log	files contain	ing the settling t	ransient dat	ta			

	Clock Time		Velocity Probe Position		MicroMotion Sensor Elevation		
File Name	Start	End	Angular	Radial	Sensor 1	Sensor 2	Sensor 3
			(deg)	(in)	(in)	(in)	(in)
021216A.xls ^(a)	07:41:45	09:18:10	180°	24	72	54	36
021216B.xls ^(b)	09:19:40	10:38:00	180°	24	72	54	36
021216C.xls ^(c)	10:39:35	12:14:28	180°	24	72	78	36
021216D.xls ^(d)	12:15:45	12:44:00	180°	24	72	78	36
021216E.xls ^(d)	12:50:10	13:54:00	180°	24	126	90	24
021216H.xls ^(d)	15:59:30	16:18:00	0°	0	36	54	N/A
021216I.xls ^(d)	16:29:20	16:49:20	135°	17	72	78	36

Table 5.13.Summary of Files Containing the Startup Transient and Steady State Data for the Simulant
Test #5 (20 wt%, 35 μm nominal volume mean glass-beads, 2 PJMs)

(a) First log file of the startup transient data.

(b) Second log file of the startup transient data.

(c) Third log file of the startup transient data.

(d) Files containing the velocity and concentration data after steady state or a periodic condition in concentration have been reached.

5.4 Concentration Profiles and Mixing Effectiveness

The results of the simulant mixing tests were reviewed for consistency, and some of the data was partially analyzed to determine the average, maximum, and minimum values of the specific gravity, and the corresponding standard deviations^(a). These averages and standard deviations in the measured specific gravities at different elevations are summarized in Tables 5.14 through 5.17. In all of these tables, the elevation of the MicroMotion sampling line is measured from the tank floor at the center of the inlet to the drain pipe. It can be seen from the data in these tables that the repeat measurements made at several of the elevations confirm the reproducibility of the data and that a "near" steady state was achieved.

The effect of increasing the solids loading from 5 to 20 wt% is shown in Tables 5.14 and 5.15. In these two cases, the nominal volume mean particle size was 10 μ m and all four PJMs were operated at a cycle time of 45 seconds. It can be seen from the data in theses tables, that with the nominal mean 10 μ m volume mean particle size glass-beads, the tank is nearly homogenously mixed from top to bottom for both the 5 and 20 wt% solids loading cases.

The effect of all four PJMs versus only two PJMs operating is shown in Tables 5.16 and 5.17. In these two cases, the nominal volume mean particle size was \sim 35 µm, and the solids loading was 20 wt%. For the case of the four PJMs operating all the time, it can be seen from the data in Table 5.16, that except for the very top of the tank, the tank contents are nearly homogeneously mixed. For the two PJM case, it can be seen from the data in Table 5.17 that the majority of the solids are suspended at elevations below 72 inches (1.8288 m).

⁽a) Complete analysis of the data was beyond the scope of the testing activity.

Elevation ^(a)		Radial Position	
(in)	Tank Center	Radius = 3 ft	Radius = 5.75 ft
3	Average: 1.029		
	Std. Dev.: 0.001		
9		Average: 1.029	
		Std. Dev.: 0.000	
12	Average: 1.029	Average: 1.029	
	Std. Dev.: 0.000	Std. Dev.: 0.000	
24	Average: 1.029	Average: 1.029	Average: 1.029
	Std. Dev.: 0.000	Std. Dev.: 0.000	Std. Dev.: 0.001
36	Average: 1.029	Average: 1.029	Average: 1.029
	Std. Dev.: 0.000	Std. Dev.: 0.000	Std. Dev.: 0.001
54	Average: 1.029	Average: 1.029	Average: 1.028
Initial Measurement	Std. Dev.: 0.000	Std. Dev.: 0.000	Std. Dev.: 0.001
54		Average: 1.029	Average: 1.029
Final Measurement		Std. Dev.: 0.000	Std. Dev.: 0.0005
72			Average: 1.028
			Std. Dev.: 0.001
90	Average: 1.029	Average: 1.029	Average: 1.028
	Std. Dev.: 0.000	Std. Dev.: 0.000	Std. Dev.: 0.000
108			Average: 1.028
			Std. Dev.: 0.000
126		Average: 1.029	Average: 1.028
		Std. Dev.: 0.004	Std. Dev.: 0.000
(a) All elevations are	e measured from the	floor of the tank at	the centerline.

Table 5.14. Average Specific Gravity Measurements for Test #1 (5 wt%, 10 μmnominal volume mean glass-beads, 4 PJMs)

Elevation ^(a)		Radial Position	
(in)	Tank Center	Radius = 3 ft	Radius = 5.75 ft
3	Average: 1.132		
	Std. Dev.: 0.001		
9		Average: 1.131	
		Std. Dev.: 0.000	
12	Average: 1.131		
	Std. Dev.: 0.001		
18		Average: 1.131	
		Std. Dev.: 0.000	
24	Average: 1.131	Average: 1.131	Average: 1.131
	Std. Dev.: 0.000	Std. Dev.: 0.000	Std. Dev.: 0.001
36			Average: 1.130
			Std. Dev.: 0.001
54	Average: 1.131	Average: 1.130	Average: 1.130
	Std. Dev.: 0.000	Std. Dev.: 0.001	Std. Dev.: 0.001
54		Average: 1.130	
2 nd Measurement		Std. Dev.: 0.001	
54		Average: 1.131	
Final Measurement		Std. Dev.: 0.001	
72			Average: 1.130
			Std. Dev.: 0.000
90	Average: 1.131	Average: 1.130	Average: 1.130
	Std. Dev.: 0.000	Std. Dev.: 0.001	Std. Dev.: 0.000
126		Average: 1.130	Average: 1.130
		Std. Dev.: 0.000	Std. Dev.: 0.000
126			Average: 1.130
2 nd Measurement			Std. Dev.: 0.000
126			Average: 1.130
Final Measurement			Std. Dev.: 0.000
(a) All elevations ar	e measured from the	e floor of the tank at	the centerline.

Table 5.15. Average Specific Gravity Measurements for Test #2 (20 wt%, 10μmnominal volume mean glass-beads, 4 PJMs)

Elevation ^(a)		Radial Position	
(in)	Tank Center	Radius = 3 ft	Radius = 5.75 ft
3	Average: 1.152		
	Std. Dev.: 0.008		
9		Average: 1.146	
		Std. Dev.: 0.001	
12	Average: 1.148		
	Std. Dev.: 0.003		
24	Average: 1.147	Average: 1.145	Average: 1.144
	Std. Dev.: 0.003	Std. Dev.: 0.001	Std. Dev.: 0.001
36		Average: 1.143	
		Std. Dev.: 0.001	
54	Average: 1.146	Average: 1.140	Average: 1.142
	Std. Dev.: 0.002	Std. Dev.: 0.001	Std. Dev.: 0.001
54		Average: 1.144	
		Std. Dev.: 0.001	
72			Average: 1.141
			Std. Dev.: 0.001
90	Average: 1.142	Average: 1.140	Average: 1.138
	Std. Dev.: 0.003	Std. Dev.: 0.001	Std. Dev.: 0.002
108		Average: 1.137	
		Std. Dev.: 0.002	
126			Average: 1.120
Initial Measurement			Std. Dev.: 0.009
			Average: 1.121
126			Std. Dev.: 0.007
Final Measurement			
136			Average: 1.071
			Std. Dev.: 0.029
(a) All elevations are	e measured from the	floor of the tank at	the centerline.

Table 5.16.Average Specific Gravity Measurements for Test #8 (20 wt%, 35μmnominal volume mean glass-beads, 4 PJMs)

Elevation ^(a)	Radial Position			
(in)	Tank Center	Radius = 3 ft	Radius = 5.75 ft	
24	Average: 1.272			
	Std. Dev.: 0.005			
36	Average: 1.278		Average: 1.280	
Initial Measurement	Std. Dev.: 0.003		Std. Dev.: 0.002	
36	Average: 1.279			
Final Measurement	Std. Dev.: 0.003			
54		Average: 1.274		
		Std. Dev.: 0.003		
72			Average: 1.176	
Initial Measurement			Std. Dev.: 0.051	
72			Average: 1.173	
Final Measurement			Std. Dev.: 0.054	
78		Average: 1.044		
		Std. Dev.: 0.021		
90		Average: 1.018		
		Std. Dev.: 0.008		
126			Average: 0.999	
			Std. Dev.: 0.000	
(a) All elevations are measured from the floor of the tank at the centerline.				

Table 5.17. Average Specific Gravity Measurements for Test #11 (20 wt%, 35μmnominal volume mean glass-beads, 2 PJMs)

6.0 References

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Appendix A: Vendor Specifications of Instruments Used

Valeport Velocity Sensors

Direct Reading Electromagnetic Current Meters Model 802



FEATURES

- High Accuracy
- High Stability
- Low Noise
- Low Power Consumption
- Choice of Sensor Shapes
- Choice of Configurations
- Digital or Analogue Output
- Wide Measurement Range
- Corrosion resistant materials

APPLICATIONS

- Sediment Transport Studies
- Hydraulic Modelling
- Open Channel Current Measurement
- Ship's Log
- ROV/AUV Speed
- Fixed Site Current Measurement

INTRODUCTION

The Model 802 is the latest version of Valeport's successful 800 Series of electromagnetic current meters. Using state of the art electronics design techniques, we have produced a highly accurate, stable, solid state instrument that is greatly reduced in size and power consumption from earlier versions. These improvements, together with a selection of sensor shapes and a versatile range of electronics packages ensure that the Model 802 is the instrument of choice in a variety of applications, from sediment transport studies to modelling flow patterns or real time monitoring of current flow.

Output from the Model 802 is strictly in the format of X and Y velocity components only. If a compass or other additional parameters are required, please refer to the Model 808 data sheet.



Direct Reading Electromagnetic Current Meters Model 802

DESCRIPTION

Electromagnetic Current Meters work on Faraday's principle that a conductor (water in this case) moving through a magnetic field (produced by the sensor) generates a voltage (measured by a pair of electrodes). By having 2 orthogonally positioned electrodes, 2 axis flow can be measured by a single sensor.

Each Model 802 system comprises a sensing head, and a set of electronics to produce the magnetic field and measure the resultant voltage. Valeport offers a range of different sensing heads and electronics assemblies to suit different applications. Any of the listed sensors may be fitted to any of the electronics packages to provide a Model 802 system. The standard output of all systems is RS232 of X and Y components of the flow speed, relative to the mounting position of the head. 2 channel analogue outputs are also available as an option.

Heads

Annular Sensor: The 17cm annular sensor measures flow in the open space inside the ring, and therefore has excellent response to off axis flow. It is therefore most suitable for use in applications where off axis flow is expected, or for use in pairs to measure 3 dimensional changes.

Spherical Sensor: Available in either 3.2cm or 5.5cm sizes, the spherical sensors have

reasonable response to tilt and azimuth flow variations, but are hydrodynamically noisier than the other sensors. Spatial resolution requirements determine the choice of sensor size.

Discus Sensor: The discus sensor is available in 3 sizes; 3.2cm, 5.5cm and 11cm diameter. Since the flow is measured on one face of the discus, tilt response is as good as the other sensors ,but azimuth response is excellent, with low hydrodynamic noise. These sensors are therefore suited to any applications where two dimensional flow is expected. Again, choice of sensor size depends on spatial resolution required.

Electronics

Control Display Unit: This package consists of an IP67 (10secs at 0.3m) display unit, and 3m signal cable to the sensor of choice. The display has an integral battery compartment making it ideal for field use, or can be powered using external DC for laboratory applications. Features of the display include real time and averaged X & Y velocities and Standard Deviation of X & Y velocities. The user may choose the type of sampling required – fixed time, moving average, or free running, and the length of the average. In addition, the control unit has an optional internal memory, which can hold up to 999 records of the above information, together with date and time stamp. Recorded data can be viewed on screen or downloaded to PC in ASCII text format.

Integral Underwater Housing: Driving electronics and preamplifiers are contained in a stainless steel underwater housing, with the chosen sensor mounted on a stem protruding from one end. A single connector allows power in (12 to 24vDC) and RS232 signal out at 1Hz update rate. Output signal is in the format X=sn.nnn Y=sn.nn<cr><lf>, where s indicates the flow direction + or -, and n.nnn signifies the flow speed in m/s. 0-5v analogue output option is available for X & Y channels

Remote Underwater Housing: Exactly as Integral Underwater System, but flow sensor is supplied on a 3m length of signal cable, rather than attached to the electronics housing.

OEM Package: Driving electronics are supplied as OEM parts, for interface to customers' existing systems. Electronics require power in (12 to 24vDC) and give RS232 digital signal out. Sensor is supplied on 3m signal cable, with free end. Again, analogue output is available as an option.

ORDERING AND SPECIFICATIONS

Sensor	Characteristics				
501301	Accuracy	Depth Rating	Tilt Response	Azimuth Response	Hydrodynamic Noise
17cm Annular	±1% + 5mm/s	1000m	\checkmark	<i>」 」 」 」 」</i>	\checkmark
11cm Discus	±1% + 5mm/s	5000m	<i>JJJ</i>	ノノノノ	$\int \int \int \int \int \int$
5.5cm Discus	±1% + 5mm/s	3000m	<i>JJJ</i>	<i></i>	$\int \int \int \int \int \int$
3.2cm Discus	(<u>±</u> 1% + 5mm/s)	(3000m)		$\checkmark \checkmark \checkmark \checkmark \checkmark \checkmark$	
5.5cm Spherical	±1% + 5mm/s	3000m	\checkmark	\checkmark	$\int \int \int$
3.2cm Spherical	±1% + 5mm/s	3000m	J J J J	\checkmark	$\int \int \int$

Package	Specification (may vary slightly according to sensor selection)				
luonago	Size	Power Consumption	Depth Rating		
Sensor on spar with pre-amp housing and 3m cable to Control Display Unit	CDU: 250 x 170 x 100mm	240mA	IP67 (10s at 0.3m)		
Underwater housing with integral sensor on spar, and 3m power in/signal out cable	525mm long x 76mmØ (inc sensor)	130mA	3000m		
Underwater housing with remote sensor on spar/pre-amp housing, 3m sensor cable, and 3m power in/signal out cable	350mm long x 76mmØ	130mA	3000m		
Sensor on spar with pre-amp, 3m sensor cable to OEM board set with wiring loom.	54mm x 205mm	130mA	N/A		

Also Available

2 channel 0-5v analogue output option for any package.

Extra Sensor cable (maximum 50m) Extra Power in/Signal out cable (maximum 100m) Alternative Signal ranges (standard ±5m/s for each axis)

Valeport manufactures a wide range of oceanographic and hydrometric instruments including self-recording and direct reading multi-parameter current meters, CTD probes, electromagnetic current meters, tide gauges, open channel flow meters, optical instruments, water and plankton samplers, winches, sinker weights, connectors and accessories.

As part of our policy of continuing development, we reserve the right to alter, without notice, all specifications, designs, prices and conditions of supply of all equipment. Data Sheet Reference No. 802/1

For more detailed specification, please refer to additional sheet.



Valeport Limited Townstal Industrial Estate Dartmouth, Devon TQ6 9LX United Kingdom Tel: +44 (0)1803 834031 Fax: +44 (0)1803 834320 e-mail: sales@valeport.co.uk Web Site: http://www.valeport.co.uk **MicroMotion Transmitter and Sensors**

Product Data Sheet PS-00024 March 2002

Micro Motion Model RFT9739

Mass Flow and Density Transmitter







EMERSON. Process Management

www.micromotion.com

RFT9739 transmitter

The RFT9739 transmitter works with Micro Motion[®] sensors to provide precision fluid measurement in a wide variety of fluid applications. The RFT9739 has modular, microprocessor-based electronics, incorporating ASIC digital technology with a choice of digital communication protocols.

Combined with a Micro Motion sensor, the RFT9739 provides accurate mass flow, density, temperature, and volumetric measurements of process fluids. With a pressure transmitter properly installed in the flow loop, the transmitter also indicates pressure.

The RFT9739 simultaneously transmits four output signals. Two independently configured analog outputs can each indicate flow rate, density, temperature, or pressure. A frequency/pulse output indicates flow rate or total. A control output indicates flow direction, a fault, or flowmeter zero in progress.

The RFT9739 is available in field-mount and rackmount versions. The field-mount transmitter is housed in a NEMA 4X (IP65) explosion-proof enclosure that provides easy access to the electronics module, and allows the transmitter and sensor to be installed in the same hazardous area. The rack-mount transmitter's compact housing is ideal for control room installations.

The RFT9739 features user-selected Bell 202 or RS-485 serial standard for HART® or Modbus® communication protocol. For configuration in the field, use Micro Motion ProLink® software, Fisher-Rosemount AMS software, or a Rosemount® Model 275 HART Communicator.

An integral liquid crystal display (LCD) is standard on the rack-mount model, optional with the fieldmount version. Use the display to set communication parameters, read process variables, reset flow totalizers, and view diagnostic messages.

Choose from a wide range of sensors to suit your application. The RFT9739 is compatible with Micro Motion ELITE[®] sensors, the most accurate Coriolis meters available today. Or choose Micro Motion F-Series sensors, standard or high-pressure Model D sensors, Model DT high-temperature sensors, or Model DL sanitary sensors.



Model RFT9739 transmitters support PlantWeb[®] field-based
 architecture, a scalable way to use open and interoperable
 devices and systems to build process solutions of the future.

RFT9739 performance specifications

Sensor model		Flow accuracy*
ELITE®	liquid gas	$\pm 0.10\% \pm$ [(zero stability/flow rate) x 100]% of rate $\pm 0.50\% \pm$ [(zero stability/flow rate) x 100]% of rate
F-Series	liquid gas	$\pm 0.20\% \pm$ [(zero stability/flow rate) x 100]% of rate $\pm 0.70\% \pm$ [(zero stability/flow rate) x 100]% of rate
D (except DH38), DL and DT	liquid gas	$\pm 0.15\% \pm$ [(zero stability/flow rate) x 100]% of rate $\pm 0.65\% \pm$ [(zero stability/flow rate) x 100]% of rate
DH38	liquid gas	$\pm 0.15\% \pm$ [(zero stability/flow rate) x 100]% of rate $\pm 0.50\% \pm$ [(zero stability/flow rate) x 100]% of rate
Sensor model		Flow repeatability*
Sensor model ELITE	liquid gas	Flow repeatability* $\pm 0.05\% \pm [\frac{1}{2}$ (zero stability/flow rate) x 100]% of rate $\pm 0.25\% \pm [$ (zero stability/flow rate) x 100]% of rate
Sensor model ELITE F-Series	liquid gas liquid gas	Flow repeatability* $\pm 0.05\% \pm [\frac{1}{2}$ (zero stability/flow rate) x 100]% of rate $\pm 0.25\% \pm [($ zero stability/flow rate) x 100]% of rate $\pm 0.10\% \pm [\frac{1}{2}$ (zero stability/flow rate) x 100]% of rate $\pm 0.35\% \pm [($ zero stability/flow rate) x 100]% of rate
Sensor model ELITE F-Series D (except DH38), DL and DT	liquid gas liquid gas liquid gas	Flow repeatability* $\pm 0.05\% \pm [\frac{1}{2}(\text{zero stability/flow rate}) \times 100]\% \text{ of rate}$ $\pm 0.25\% \pm [(\text{zero stability/flow rate}) \times 100]\% \text{ of rate}$ $\pm 0.10\% \pm [\frac{1}{2}(\text{zero stability/flow rate}) \times 100]\% \text{ of rate}$ $\pm 0.35\% \pm [(\text{zero stability/flow rate}) \times 100]\% \text{ of rate}$ $\pm 0.05\% \pm [\frac{1}{2}(\text{zero stability/flow rate}) \times 100]\% \text{ of rate}$ $\pm 0.30\% \pm [(\text{zero stability/flow rate}) \times 100]\% \text{ of rate}$

Sensor model		Density acc <i>g/cc</i>	curacy <i>kg/m</i> ³	Density rep <i>g/cc</i>	beatability kg/m ³
ELITE (except high-pressure CMF010P)	(liquid) gas	±0.0005 ±0.002	±0.5 ±2.0	±0.0002 ±0.001	±0.2 ±1.0
ELITE high-pressure CMF010P	liquid gas	$_{\pm 0.002}^{\pm 0.002}$	±2.0 ±8.0	±0.001 ±0.004	±1.0 ±4.0
F-Series	liquid only	±0.002	±2.0	±0.001	±1.0
D6, D12, D25, D40, DH100, DH150	liquid only	±0.002	±2.0	±0.001	±1.0
DH6, DH12, DH25, DH38	liquid only	±0.004	±4.0	±0.002	±2.0
D65, DL65, DT65, D100, DT100, D150, DT150, DH300	(liquid only)	±0.001	(±1.0)	±0.0005	±0.5
DL100, DL200, D300, D600	liquid only	±0.0005	±0.5	±0.0002	±0.2
Sensor model		Temperature accuracy		Temperature repeatability	
All models		$\pm 1^\circ C$ \pm 0.5% of reading in $^\circ C$		±0.2°C	

* Flow accuracy includes the combined effects of repeatability, linearity, and hysteresis. All specifications are based on reference conditions of water at 68 to 77°F (20 to 25°C), and 15 to 30 psig (1 to 2 bar) unless otherwise noted. For gas measurement specifications, refer to product specifications for each sensor. For values of zero stability, refer to product specifications for each sensor.
RFT9739 functional specifications

Output signals

Analog

Two independently configured analog outputs, designated as primary and secondary, can represent mass or volumetric flow rate, density, temperature, event 1 or event 2. These outputs cannot be changed from active to passive. With a pressure transmitter, outputs can also provide indication for pressure. Internally powered, can be selected as 4-20 mA or 0-20 mA current outputs. Galvanically isolated to \pm 50 VDC, 1000 ohm load limit. Out-of-range capability: 0-22 mA on 0-20 mA output; 3.8-20.5 mA on 4-20 mA output.

Milliamp (mA) output rangeability

Flow

Maximum span determined by sensor specifications Range limit determined by sensor maximum rate

Minimum recommended span (% of nominal flow range):

F-Series sensors		10%					
D, DL, and DT sen	D, DL, and DT sensors						
D300 and D600 s	5%						
High-pressure (DH	High-pressure (DH) sensors						
Density							
Range limit:	0 to 5 g/cc	(0 to 5000 kg/m ³)					
Minimum span:	0.1 g/cc (100 kg/m ³)						
Temperature	400 1- 04						
Rande limit:	-400 to 84	42°F (-240 to 450°C)					

 Range limit:
 -400 to 842°F (-240 to 450°C)

 Minimum span:
 36°F (20°C)

Frequency

One frequency/pulse output can be configured to indicate mass flow rate, volumetric flow rate, mass total (inventory), or volume total (inventory), independent of analog outputs. Internally powered, 0-15 V square wave, unloaded; 2.2 kohm impedance at 15 V, galvanically isolated to ±50 VDC. In open collector configuration: sinking capability, 0.1 amps in "on" condition (0 volt level), 30 VDC compliance in "off" condition. Signal can be scaled up to 10,000 Hz. Out-of-range capability to 15,000 Hz. Programmable pulse width for low frequencies.

Dual-channel frequency (rack-mount transmitter only)

Approved for custody transfer applications, a dual-channel frequency output, referred to as frequency A and frequency B. Phase shift between channels is 90 degrees. Output derived from the primary frequency, and represents the same process variable as the frequency/pulse output, but with half the frequency. All specifications match frequency/ pulse output except: Signal can be scaled up to 5000 Hz; out-of-range capability to 7500 Hz. The output complies with VDE/VDI 2188.

Optocoupler (rack-mount transmitter only)

The optocoupler is an externally powered output. Signal voltage: low level 0-2 VDC, high level 16-30 VDC. Maximum signal current 0.01 amp. Maximum capacitive load 150 nF at 10 kHz. Output is derived from the primary frequency, and represents the same process variable as the frequency/pulse output. The output complies with VDE/VDI 2188.

Control

One control output can represent flow direction, fault alarm, zero in progress, event 1 or event 2. Internally powered, digital level, 0 or 15 V, 2.2 kohm pull-up, galvanically isolated to ± 50 VDC. In open collector configuration: sinking capability, 0.1 amps in "on" condition (0 volt level), 30 VDC compliance in "off" condition.

Digital

Switch allows selection of Bell 202 and/or RS-485 serial standard.

Bell 202 signal is superimposed on primary variable mA output, and available for host system interface. Frequency 1.2 and 2.2 kHz, amplitude 0.8 V peak-to-peak, 1200 baud. Requires 250 to 1000 ohms load resistance.

RS-485 signal is a ± 5 V square wave referenced to transmitter ground. Baud rates between 1200 baud and 38.4 kilobaud can be selected.

Drexelbrook Level Sensors



A Leader in Level Measurement

Universal Lite[™]

509-15 Series RF Level Transmitter



Easy Calibration Saves Time

Push button calibration is menu-driven through a full 4-digit LCD display that resides integral to the electronic unit. No hand-held calibration/ configuration terminals are required for a fast basic setup.

Consistent Accuracy

Microprocessor-based circuitry means precise level indication along the entire sensing element. Internal circuitry provides ambient temperature compensation.

Reliability

Drexelbrook's exclusive circuitry ensures dependable level indication in applications with light or moderate coatings.

Eliminate Routine Maintenance

No moving parts to break or wear out. No need for routine maintenance or recalibration.

Digital Display

An optional full 4-digit LCD display can be set up to read in percent or engineering units.

The Drexelbrook Universal Lite RF Level indicating transmitter provides a low-cost solution to most level applications and is superior in reliability and performance.

AMETEK Drexelbrook's 509-15 Series two-wire RF Level transmitter provides dependable, low-cost level indication and control that is suitable for all liquid, and interface applications that do not leave a severe build-up on the sensing element. For applications where heavy build-up is expected, Drexelbrook offers the Universal Admittance transmitter.

A convenient integrally mounted package (or remote up to 50 feet) comes with optional local indication through a full 4-digit LCD display. Calibration and configuration is quick and easy through menu-driven push button selection.

Each system is available with:

- User definable display. (percent or engineering units).
- Easy 2-point calibration.
- Adjustable time delay provides signal damping.
- Meter trim to adjust the output signal to a known plant standard.
- Real-time View of input capacitance values.
- Optional display/keypad for quick and easy setup and local indication.

The Universal Lite can also be configured with the HART® Model 275 Communicator or optional AMETEK Drexelbrook PC software for more detailed setup and diagnostics.

Specifications

Application	Process Pressure and Temperature	Sensing Element Dimensions	Standard Mounting	Materials of Construction	System Model # (Sensing Element)	
(Water Based) (Liquids)	(100°F @ 1000 psi) 38°C @ 69 BAR) 300°F @ 500 psi (149°C @ 34 BAR)	3/8-inch (10 mm) OD (TFE Rod) (Max. 20 feet (6 m) (engin	(3/4-inch NPT) (or Flange)	(316 SS and TFE)	509 -15- X09 ((700-1-22))	
Water Based Liquids in Tall Vessels¹	300°F @ 500 psi 149°C @ 34 BAR	0.093-inch (2mm) OD PFA Flex. Cable Max. 100 feet (30m) length	3/4-inch NPT or Flange	316 SS and PFA	509-15-X25 (700-5-54)	
Conducting/ Insulating Interface	100°F @ 1000 psi 38°C @ 69 BAR 300°F @ 500 psi 149°C @ 34 BAR	0.56-inch (14mm) OD TFE Rod Max. 19 feet (5.8m) length	3/4-inch NPT or Flange	316 SS and FEP	509-16-X02 (700-2-27)	
Conducting/ Insulating Interface	100°F @ 1000 psi 38°C @ 69 BAR 250°F @ 500 psi 121°C @ 34 BAR	0.84-inch (21mm) OD "X" Rod Max. 19 feet (5.8m) length	1-inch NPT or Flange	316 SS and X ²	509-16-X06 (700-2-57)	
Hydrocarbon & Organic Liquids	Hydrocarbon & 100°F @ 1000 psi 1.66-inc Organic Liquids 38°C @ 69 BAR F 149°C @ 34 BAR Max :		1 1/2-inch NPT or Flange	316 SS and TFE	509-17-X16 (700-1-26)	
Water Based Liquids in Non-Metallic Vessels	200°F @ 200 psi 93°C @ 14 BAR	0.185-inch (5 mm) OD FEP Flex. Cable with Integral Ground Max. 100 feet (30 m) length	3/4-inch NPT or Flange	316 SS and TFE	509-15-X85 (700-5-85)	

¹Applications that produce significant coating build-up may require the Universal Admittance transmitter. ²X is a fluorocarbon-type insulation.

Power Requirement: 18 to 30 VDC, HART® 13 to 30 VDC, Analog

Output: 4-20mA Analog, 4-20mA HART Protocol, Digital HART Protocol

Maximum Load Resistance: 550 ohms, HART® with modem/gateway 650 ohms @ 24 VDC, Analog

Minimum Resistance: 250 ohms for HART® protocol

Supply Voltage Effect: 0.05% / 10VDC

Linearity: 0.25% of span

Specifications subject to change.

Electronic Housing: Meets Nema 1-5 & 12 including Nema 4X. Suitable for Class I, Groups A, B, C, D, Class II, Groups E, F, G, Div. 1 & 2, Class III Div. 2. Intrinsically Safe for Div. 1 when supplied from an approved power source

Response Time: Less than 1 second with no damping time 1-90 seconds programmable damping time

Spark Protection: 10A standard (100A optional)

Fail Safe: Direct Acting/Reverse Acting

Ambient Temperature Limits: -40°F to 185°F (-40°C to 85°C)

Maximum Cable Length: 50 feet (15 m) Span Range (Typical): 3" (76 mm) to 100' (30 m) on water-based materials. 3' (914 mm) to 100' (30 m) on organic materials

Calibration: Three button keypad, PC-based software, or Model 275 calibrator

Display: Integral 4-digit LCD

Minimum Resistance Sensing Element to Ground: 100,000 ohms (with less than a 1.0% effect on output signal)

Temperature Stability: 0.15% per 30°F (17°C)

Approvals: CE Mark, KEMA (CENELEC), FM, CSA



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Digital Pressure Gauges

Falcon Digi Pro⁴ NEMA 4X Digital Pressure Gauges

F4DR 4-Wire Indicating Transmitter F4DRBL 4-Wire Indicating Transmitter with Backlit Display

ELECTRICAL SPECIFICATIONS

Ranges and Resolution

Bold indicates standard ranges, price adder for all others

"abs" indicates absolute reference, gauge will read atmospheric pressure with no connection and zero under full vacuum.

"vac"	indicates	vacuum	gauge	

Consult factory	150.0 mmHg	±1000 mbar	14.00 MPa		
for other	250 mmHg	1000 mbar	19.99 MPa		
	760 mmHg abs	1999 mbar abs	35.0 MPa		
engineering units	760 mmHg vac	1999 mbar	1000 g/cm ² abs		
3.00 psig	760 mmHg	1.000 bar abs	1000 g/cm ²		
5.00 psig	1500 mmHg abs	1.000 bar	1999 g/cm ² abs		
15.00 psi abs	1500 mmHg	1.999 bar abs	1999 g/cm ²		
15.00 psig vac	50.0 oz/in ²	1.999 bar	±1.000 kg/cm ²		
±15.00 psig	80.0 oz/in ²	4.00 bar	1.000 kg/cm ² abs		
15.00 psig	240 oz/in ²	7.00 bar abs	1.000 kg/cm ²		
30.0 psia	85.0 inH ₂ O	7.00 bar	1.999 kg/cm ² abs		
30.0 psig	140.0 inH ₂ O	14.00 bar	1.999 kg/cm ²		
60.0 psig	400 inH ₂ O abs	19.99 bar	4.00 kg/cm ²		
100.0 psi abs	400 inH ₂ O vac	35.0 bar	7.00 kg/cm ² abs		
100.0 psig	±400 inH ₂ O	70.0 bar	7.00 kg/cm ²		
199.9 psig	400 inH ₂ O	140.0 bar	14.00 kg/cm ²		
300 psig	850 inH ₂ O	199.9 bar	19.99 kg/cm ²		
500 psig	7.00 ftH ₂ O	350 bar	35.0 kg/cm ²		
1000 psig	12.00 ftH ₂ O	19.99 kPa	70.0 kg/cm ²		
1999 psig	35.0 ftH ₂ O	35.0 kPa	140.0 kg/cm ²		
6.00 inHg	70.0 ftH ₂ O	100.0 kPa abs	199.9 kg/cm ²		
10.00 inHg	140.0 ftH ₂ O	100.0 kPa vac	350 kg/cm ²		
30.0 inHg abs	230 ftH ₂ O	100.0 kPa	1.000 atm		
30.0 inHg vac	500 ftH ₂ O	199.9 kPa abs	4.00 atm		
±30.0 inHg	1999 mmH ₂ O	199.9 kPa	7.00 atm		
30.0 inHg	199.9 cmH ₂ O	400 kPa	14.00 atm		
60.0 inHg abs	350 cmH ₂ O	700 kPa abs	19.99 atm		
60.0 inHg	1000 cmH ₂ O	700 kPa	35.0 atm		
120.0 inHg	1999 cmH ₂ O	1500 kPa	70.0 atm		
199.9 inHg abs	199.9 mbar	1999 kPa	135.0 atm		
199.9 inHg	350 mbar	3.50 MPa	199.9 atm		
760 torr abs	1000 mbar abs	7.00 MPa	340 atm		

Resolution is fixed as indicated in table below

Accuracy (linearity, hysteresis, repeatability)

Standard: ±0.25% of full scale ±1 least significant digit

"-HA" option: $\pm 0.1\%$ FS ± 1 LSD (most ranges) or "-4A" option $\pm 0.4\%$ FS ± 1 LSD NIST traceable test report and data optional

Temperature Stability (relative to 77°F or 25°C)

 \pm 1% FS for offset and span, 32 to 158°F (0 to 70°C) typical \pm 2% FS for offset and span, 32 to 158°F (0 to 70°C) typical for 3 and 5 psi ranges

Display (update rate, type, size)

3 readings per second nominal display update rate DR in ranges up to 1999: 3¹/₂ digit LCD, ¹/₂" digit height DRBL ranges up to 1999: 3¹/₂ digit LCD, ¹/₂" digit height, red LED backlighting

Controls

Non-interactive zero and span, ±10% range Test calibration level: 0-100% range Retransmission zero and span: internal potentiometers

Retransmission Output

True analog output, 50 milliseconds typical response time. Current output: "-I" option, 4-20 mA DC, output drive (compliance) determined by power source. See graph.

Voltage output: "-V" option, 0-2 VDC into 5K Ohm or greater

Test Function

Front panel TEST button, when depressed sets display and retransmission output to "test calibration" level, independent of pressure input to allow testing of system operation. Test level is set by top-accessible multiturn potentiometer to any value from 0 to 100% of full scale.

Power

Any AC source of 8 to 24 VAC 50/60 Hz or any DC source of 9 to 32 VDC 30 mA maximum, 40 mA for DRBL model with backlighting 3 ft long, 4-conductor 22 AWG shielded cable

Order optional WMPSK 12 VDC wall mount power supply kit to operate on 115 VAC

- ±0.25% Test Gauge Accuracy
- 316 Stainless Steel Wetted Parts
- Low-Voltage AC/DC-Powered
- 4-20 mA or 0-2 V Analog Output
- 4-20 mA Models Power Current Loop
- Output Test Function
- Polycarbonate Display Window



MECHANICAL SPECIFICATIONS

Size

 $3.5"W \times 3.0"H \times 2.0"D$ (not including pressure fitting) Add approximately 0.75" to height for pressure fitting and 1" to depth for strain relief and wire clearance

Weight (approximate) Gauge: 9 ounces

Shipping weight: 1 pound

Housing NEMA 4X

UV stabilized polycarbonate/ABS case, light gray color Clear polycarbonate window to protect display Gasketed rear cover, six captive stainless steel screws

Pressure/Vacuum Connection & Material

1/4" NPT male, 316 stainless steel

Media Compatibility

All wetted parts are 316 SS Compatible with most liquids and gases

Overpressure

5000 psig for metric ranges equivalent to 3000 psig 7500 psig for metric ranges equivalent to 5000 psig All others 2x rated pressure minimum

Burst Pressure

4x rated pressure minimum or 10,000 psi, whichever is less

ENVIRONMENTAL SPECIFICATIONS

Storage temperature	40 to 203°F (-40 to 95°C)
Operating temperature	4 to 185°F (-20 to 85°C)
Compensated temperature	32 to 158°F (0 to 70°C)



Phone:**888-763-4884** 847-918-3520 Fax: 888-763-4892 847-327-9697 www.cecomp.com 1220 American Way Libertyville, Illinois 60048 USA

Installation and Precautions

Install or remove the gauge using wrench on hex fitting only. Do not attempt to tighten by turning housing or any other part of the gauge. Use fittings appropriate for the pressure range of the gauge. Do not apply vacuum to gauges not designed for vacuum operation. Due to the hardness of 316 stainless steel, it is recommended that a thread sealant be used to ensure leak-free operation. **NEVER** insert objects into the gauge port or blow out with compressed air. Permanent damage not covered by warranty will result to the sensor.

Electrical Connection

NEVER connect the gauge wires directly to 115 VAC or permanent damage not covered by warranty will result.

The **F4DR** and **F4DRBL** can be powered by any 9 to 32 VDC or 8 to 24 VAC 50/60 Hz power source. An inexpensive unregulated low voltage source can be used. The magnitude of the supply voltage has negligible effect on the gauge calibration as long as it is within the stated voltage ranges. Do not allow the gauge supply voltage fall below 9 VDC or 8 VAC RMS. Operation below these values may cause erratic or erroneous readings or output. Models with 4-20 mA output power the current loop. Use a power source with sufficient voltage to operate the current loop.

Connection is made with the 4-conductor cable at the gauge rear. This cable accommodates both the gauge power supply and retransmission output. This cable has one RED and one BLACK lead. If using a 9 to 32 VDC power source, connect the (+) supply to the RED lead and the (-) supply to the BLACK lead. If using a 8 to 24 VAC 50/60 Hz power source, connect to the RED and BLACK leads. When using low voltage AC power, there is of course, no polarity consideration.

The (+) retransmission output appears on the WHITE lead, and the (–) retransmission output appears on the GREEN lead. Use of the shield (drain) wire of the retransmission output is optional. It is not generally needed for 4-20 mA current loops unless very long cable lengths are used in electrically noisy environments.

The output is a continuous analog signal based on the transducer output rather than the display. This output is filtered to improve noise immunity and has a response time of about 50 milliseconds.

The power supply (-) lead is tied to the retransmission output ground. Therefore, if a DC supply is used, the power supply (-) lead should be considered common with regard to the retransmission output (-) connection.

Using the Retransmission Output

NEVER connect retransmission output wires together or to an external power source or permanent damage not covered by warranty will result.

For 4-20 mA output models, be sure to observe the output compliance (voltage drive) capabilities of the gauge. The compliance, and therefore the maximum loop resistance the output can drive, is a function of the supply voltage to the gauge. Consult the graph below for maximum loop resistance vs. gauge supply voltage. Too large a loop resistance will cause the gauge output to "limit" or saturate before reaching its full 20 mA output.

When using the 0-2 volt retransmission output, do not allow the resistive load on the output to fall below 5K ohms. Also, avoid large capacitive loads (greater that 1000 pF) such as those caused by long runs of shielded cable. For long retransmission runs, use the 4-20 mA output model instead.

Operation

The gauge is powered on whenever a supply voltage is applied. Warm-up time is negligible. In normal operation, the system pressure is displayed on the gauge LCD and an output signal will be present. **F4DRBL** model display backlighting will be on whenever power is applied.



TEST Button

When the front-panel TEST button is held depressed, the display and retransmission output are switched, independent of the system pressure, to a test level determined by the setting of the Test potentiometer. This test mode will allow setup and testing of the output and any external device(s) connected to it by switching to this test level whenever desired without having to alter the system pressure.

To set the test output level, see gauge label for location of Test potentiometer. Press and hold the front-panel TEST button and adjust the Test potentiometer to set the display and retransmission output to the desired test level.

Calibration

See gauge label for location of controls to adjust the zero and span of the display.

GAUGE reference units may be re-zeroed without affecting the span calibration. The gauge port must be open to the ambient with no pressure/vacuum applied. Adjust the Zero control until the gauge reads zero with the minus (–) sign occasionally flashing.

Span calibration should only be attempted if the user has access to a pressure reference of known accuracy. The quality of the calibration is only as good as the accuracy of the calibration equipment and ideally should be at least four times the gauge accuracy. Zero calibration must be done before span calibration. Record readings at three to five points over the range of gauge and adjust span control to minimize error and meet specifications.

ABSOLUTE reference gauges require vacuum generation and atmospheric pressure measurement equipment for accurate calibration and thus are more difficult to calibrate in the field. Gauges may be returned to Cecomp Electronics for factory certified recalibration. N.I.S.T. traceability is available.

Internal potentiometers adjust the agreement between the displayed value and the analog output. These are set at the factory and should not normally be adjusted. If adjustment is required, consult factory. Accurate pressure generation and measurement and current measurement equipment are required to successfully complete this calibration.



Example: F4DR100PSIG-I = F4DR, 100.0 psig, Current (4-20 mA) retransmission

Cecomp Electronics maintains a constant effort to upgrade and improve its products, therefore specifications are subject to change.

Appendix B: Particle Size Distribution Data

Appendix B: Particle Size Distribution Data

During the simulant mixing tests discussed in this report, several grab samples were collected after a steady sate was observed in the slurry densities. A subset of the samples collected was analyzed using a MICROTRAC S3000 Particle Size Analyzer to determine the particle size distribution. The various samples analyzed are listed in Table B.1.

Simulant ^(a)	# of PJM	Location of Sam	ple Extraction	Sample ID
Simulant	Operating	Radial (in)	Vertical (in)	Sample ID
10 um 5 ut9/	4	69	126	Smp021119-2
10 μIII, 3- wt76	4	36	54	Smp021119-4
10 um 20 xxt%	4	69	126	Smp021121-1
10 μIII, 20-wt/0	4	0	3	Smp021121-3
25 um 5 utl	4	69	126	Smp021204-1
55 μm, 5-wt76	4	0	3	Smp021204-3
	4	0	3	Smp021212-4
35 µm, 20-wt%	4	69	126	Smp021212-5
	4	69	136	Smp021212-7
(a) Particle sizes	listed here are	e the nominal volum	e mean diameters	

Table B.1. List of the Various Samples Analyzed for the Particle Size Distribution.

In this section, the approach used to determine the PSD data, and the measurements are included in terns of the volume based and area (Sauter's mean) based distribution data.

Test Instructions for Measuring PSD

ę,

RPP-WTP Support Project Test Instruction

Unique Numerical Designation: TI-RPP-WTP-228 Revision number: 0 Effective Date: Upon final signature Controlling Procedure No: [TPR-RPP-WTP-222]

TITLE: Particle Size Distribution Analyses of B-55 Large Scale test Samples

Perform PSD analysis on the following 9 slurry samples:

ł

Smp021119-2 Smp 021119-4 Smp 021121-1 Smp 021204-1 Smp 021204-3 Smp021212-4 Smp021212-5 Smp021212-7

Reference the sample numbers when recording LRB entries and transmitting the results.

The samples were obtained from testing conducted according to TPR-RPP-WTP-214. For each 4-PJM test, single samples from the top and bottom of the tank are to be analyzed. Four 4-PJM tests were conducted. Three samples are supplied from the 4-PJM test conducted on 12/12/02. Refer to LRB BNW-14248 for a description of each sample. The corresponding logbook page is listed on each sample container.

Using Procedure TPR-RPP-WTP-222, "S3000 Microtrac Particle Size Analyzer", APEL 109:

- Perform analysis on *Duke Scientific* 10 µm and 100 µm standards, lot numbers 24616 and 24343 respectively. Certificates of Calibration and Traceability are retained in Project files.
 - a. Use 1 to 4 drops of dispersant for each standard
 - b. Dilute with deionized water (DIW) as required to achieve measurable results
 - c. Use the ultrasonic horn to de-agglomerate the standard slurry
 - d. Agitate the standard slurry with a magnetic stirrer before drawing the aliquot for analysis
 - e. Analyze each standard and printout the results. The mean standard particle size must fall between 9 μ m and 11 μ m for the 10 μ m standard, and between 95 μ m and 105 μ m for the 100 μ m standard. If the results do not fall within these

ranges, contact Carl Enderlin (375-2141) or Jim Bates (375-2539) before proceeding.

- Agitate each slurry sample with a magnetic stirrer before drawing the aliquot for 2) analysis.
- Use 1 to 4 drops of dispersant for each aliquot. 3)
- Dilute with DIW as required to achieve measurable results. 4)
- Use the ultrasonic horn to de-agglomerate each aliquot. 5)
- Agitate the sample aliquot with a magnetic stirrer before transferring into the 6) Microtrac S3000 for analysis.
- Print out the results and record the appropriate LRB number and corresponding LRB 7) page numbers on the printout.
- Sign, and date each printout (to include the sample number reference), and attach the 8) printouts to this test instruction along with the standards analysis results. Return all information to Jim Bates (5-2539).

Approvals:

12/18/02

Carl Enderlin

Technical Reviewer: Bill Buchmiller

Calibration Standard Certificates



September 25, 2001

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1-800-334-3883 1-650-424-1177 Fax 1-650-424-1158

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PARTICLE SIZE STANDARDS NIST Traceable Mean Diameter

1. DESCRIPTION. These particle size standards provide accurate and traceable size calibration values for particle size analysis. They are part of a series of uniform glass microspheres with calibrated mean diameters traceable to the Standard Meter through the National Institute of Standards and Technology (NIST). Uniform glass microspheres are widely used as calibrants and controls for instruments requiring a higher density than polymer microspheres. Made of borosilicate or soda lime glass, diameters from 2 to 2000 micrometers (µm) are available as dry spheres, calibrated by optical microscopy. Other values are for information only and should not be used as calibration values.

2. PHYSICAL DATA. Certified Mean Diameter: Standard Deviation: Coefficient of Variation: Microsphere Composition: Microsphere Density: Index of Refraction: **Dielectric Constant:** Approximate Number:

Catalog Number: 9010, Nominal 10µm $10.0 \mu m \pm 1.0 \mu m$ 1.0µm 10% Borosilicate Glass 2.50g/cm³ 1.56 @ 589nm 5.8 @ 1MHz and 22°C 7.6 x 10⁸ per gram

- Continued on page 2

VALUABLE CERTIFICATE - KEEP ON FILE

CERTIFICATE OF CALL	BRATION AND TRACEABILITY
This certifies that the calibrated mean microscopy from a stage micrometer ca Technology (Calibration Report #5524). 1960, and 1961 were used to validate methods.	diameter dimension was transferred by optical librated by the National Institute of Standards and NIST Standard Reference Materials 1690, 1692, the accuracy and traceability of the calibration
Catalog Number: 9010, Partic Certified Mean Diameter: 10.0µm Uncertainty: ± 1.0µm	cle Size Standards - Borosilicate Glass Material Batch: 9010-004 Certification Date: September 25, 2001
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Philip L. Warren, President Duke Scientific Corporation	Void without seal
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Packaging Lot # 24616

OCT '05

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May 9, 2002

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PARTICLE SIZE STANDARDS NIST Traceable Mean Diameter

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2. PHYSICAL DATA. Certified Mean Diameter: Standard Deviation: Coefficient of Variation: Microsphere Composition: Microsphere Density: Index of Refraction: Dielectric Constant: Approximate Number:

Catalog Number: 9100, Nominal 100µm 99.8µm ± 5.0µm 3.2µm 3.2% Soda Lime Glass 2.45g/cm³ 1.51 @ 589nm 7.3 @ 1MHz and 22°C 7.8 x 10⁵ per gram

- Continued on page 2

VALUABLE CERTIFICATE - KEEP ON FILE

CERTIFICATE OF CALIBRATION AND TRACEABILITY

This certifies that the calibrated mean diameter dimension was transferred by optical microscopy from a stage micrometer calibrated by the National Institute of Standards and Technology (Calibration Report #5524). NIST Standard Reference Materials 1690, 1692, 1960, and 1961 were used to validate the accuracy and traceability of the calibration methods.

Catalog Number: 9100, Particle Size Standards - Soda Lime Glass Certified Mean Diameter: 99.8µm Uncertainty: ± 5.0µm Material Batch: 9100-004 Certification Date: May 9, 2002

Philip L. Warren, President Duke Scientific Corporation

Packaging Lot # 24343

Expiration Date:

JUL '05 – Over for more data

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STAND Void without seal

Instrument Performance Checks

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1408 1291 1186 995.6 995.6 995.6 995.6 995.6 952.0 542.9 497.8 456.5 592.0 542.9 497.8 456.5 322.8 296.0 352.0 352.0 352.0 352.0 352.0 352.2 209.3 176.0 161.4 195.7 176.0 161.4 195.7 176.0 161.4 195.7 176.0 161.4 195.7 176.0 161.4 195.7 176.0 161.4 195.7 176.0 161.4 195.7 195	$\begin{array}{c} 100.00\\$	0.00 0.00	74.00 67.86 62.23 57.06 52.33 47.98 44.00 33.93 31.11 28.53 26.16 23.99 22.00 20.17 18.50 15.56 15.56 14.27 13.08 12.00 11.009 9.250 8.482 7.778 7.133 6.541 5.998 5.500 5.044 4.625 4.241	100.00 100.00 100.00 100.00 99.88 99.46 99.15 98.21 97.52 96.64 95.55 94.24 92.70 90.96 89.04 86.96 84.76 82.44 80.00 77.41 74.63 71.62 68.32 64.72 68.32 64.72 60.83 55.51 48.33 44.37 40.71 37.41	0.00 0.00 0.00 0.12 0.19 0.23 0.31 0.41 0.53 0.88 1.09 1.54 1.74 1.74 1.74 2.08 2.20 2.32 2.44 2.59 2.78 3.30 3.60 3.30 3.66 3.30 2.95	3.889 3.566 3.270 2.999 2.750 2.522 2.121 1.945 1.783 1.499 1.375 1.499 1.375 1.499 1.375 1.060 0.972 0.892 0.818 0.630 0.530 0.486 0.446 0.409 0.375 0.344 0.315 0.289 0.265 0.223	34.3 31.3 225.2 20.0 20.0	46 855 51 93 43 85 90 7 65 95 7 20 14 84 11 11 10000000000000000000000000	$\begin{array}{c} 2.61\\ 2.34\\ 2.12\\ 1.85\\ 1.77\\ 1.74\\ 1.71\\ 1.71\\ 1.71\\ 1.71\\ 1.71\\ 1.70\\ 1.68\\ 1.65\\ 1.59\\ 1.49\\ 1.37\\ 1.25\\ 1.12\\ 0.99\\ 0.87\\ 0.76\\ 0.64\\ 0.53\\ 0.40\\ 0.30\\ 0.20\\ 0.11\\ 0.00\\$	0.204 0.187 0.172 0.158 0.145 0.133 0.122 0.111 0.102 0.086 0.079 0.072 0.066 0.061 0.047 0.043 0.043 0.030 0.033 0.036 0.028 0.023	$\begin{array}{c} 0.00\\$	0.00 0.00
Distrib Progre	ution: Volume ssion: Geomet	tric Root8	RunTime: Run Num	30 second ber Avg of	is 3 runs	Fluid: W Fluid Ref	ater ractive	Index	1.33	Analysis Sample	Mode: S300 Cell Id: 0084	0
Upper Lower Residu Numbe	Edge: 1408 Edge: 0.021 Ials: Disabled er Of Channels:	128	Particle: Particle T Particle R Particle S	active anoc ransparency efractive Inc hape: N/A	le powder y: Absorb dex: N/A	Loading Transmis Above Re Below Re	Factor: sion: sidual sidual	0.02 0.91 : 0.0 : 0.0	0 0			
Filter:	On		Database	Path: C:\	MTWIN\1217	PJM.DB	-	-				

Serial	Number: S3177	7	M		OTR	AC	- 53	000)				Vor:9 0a
Itange	. 0.021-1400 0	12180	2PJM			SMP02	21119-2			Date	e: 12/18/0	2 Meas Pres	#: 11 #: 1
						Sum mv = mn = cs = sd =	mary 7.866 0.878 3.178 1.888 2.440	5% = 20% = 30% = 40% = 50% =	Percenti 0.550 6 0.834 7 1.046 8 1.305 9 1.664 9	$\frac{les}{0\%} = 2.264$ $\frac{0\%}{0\%} = 3.344$ $\frac{0\%}{0\%} = 4.873$ $\frac{0\%}{0\%} = 7.244$ $\frac{0\%}{0\%} = 10.17$	Dia Dia 4 4.710 1 1.024 3 4 7 7	Area% 42% 58%	Width 6.100 0.980
%PA	SS			-		-					-	%	CHAN
100.0	, <u> </u>		TIT			1	TTT	III	TT			TIIIT	10.0
90.0													9.0
80.0	+ + +												8.0
70.0	-												7.0
60.0													6.0
50.0													5.0
40.0	+ ++												4.0
30.0	+ ++												3.0
20.0	-					-							2.0
10.0	+ + +		+++/				++++		+++				1.0
0.0	0.010	0.100	1.0	000	10.0	0		100.0		1000		10000	0.0
0175		N CHIAN	0175 0	B400	- Size (m	icrons)	-		0/01144	Lours			
1408 1291 1184 1086 913.0 837.2 767.7 704.0 645.6 592.0 542.9 497.8 456.5 418.6 383.9 352.0 352.0 352.0 352.0 352.0 352.2 209.3 176.0 161.4 148.0 135.7 7124.5 114.1 104.7 95.96 88.00	$\begin{array}{c} 100.00\\$	0.00 0.00	0.121 74.00 10 74.00 10 67.86 10 67.86 10 67.86 10 67.86 10 57.06 11 57.06 11 57.06 11 57.06 11 57.06 11 44.00 9 44.035 9 37.00 9 33.93 9 31.11 9 28.53 9 22.00 9 22.00 9 22.00 9 22.00 9 16.96 9 15.56 9 14.277 9 14.277 9 12.00 9 12.00 9 9.250 9 9 7.778 9 7.133 8 6.541 8 5.998 8 5.998 8 5.004 8 4.625 7	00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 99.98 99.93 99.96 99.93 99.84 99.77 99.53 99.35	0.00 0.00 0.00 0.00 0.01 0.02 0.03 0.04 0.05 0.07 0.10 0.14 0.23 0.29 0.34 0.40 0.47 0.62 0.71 0.62 0.71 0.62 0.71 0.62 0.71 0.62 0.71 0.62 0.71 0.62 0.71 0.62 0.71 0.62 0.71 0.62 0.71 0.62 0.71 0.62 0.71 0.62 0.71 0.62 0.71 0.62 0.71 0.62 0.71 0.63 0.64 0.65 0.53 0.64 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.54 0.54 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53	3.566 3.270 2.522 2.522 2.522 2.121 1.945 1.783 1.635 1.499 1.375 1.261 1.156 1.060 0.892 0.818 0.630 0.578 0.630 0.578 0.630 0.578 0.630 0.578 0.630 0.578 0.630 0.578 0.315 0.289 0.263 0.223	7771697655200000000000000000000000000000000000	88 88 65 47 59 15 92 59 11 43 55 60 95 .36 .95 .31 .55 .60 .89 .19 .29 .11 .36 .95 .31 .55 .60 .89 .11 .52 .36 .95 .31 .55 .60 .31 .55 .60 .89 .11 .52 .36 .95 .31 .55 .60 .89 .19 .29 .11 .36 .95 .31 .55 .60 .89 .19 .19 .29 .11 .36 .55 .60 .89 .19 .29 .11 .36 .55 .60 .89 .19 .19 .29 .11 .36 .55 .60 .89 .19 .20 .00 .00 .00 .00 .00 .00 .00	2.23 2.18 2.15 2.23 2.33 2.48 2.91 3.44 3.93 3.95 3.90 3.55 3.90 3.55 3.92 3.55 3.12 2.78 3.55 3.12 2.78 3.55 3.12 2.78 3.55 3.12 2.78 3.41 3.64 3.93 3.95 0.355 0.00 0.00 0.00 0.00 0.00 0.00 0.	Olizie 0.204 0.187 0.172 0.158 0.145 0.133 0.122 0.111 0.102 0.094 0.096 0.072 0.066 0.051 0.0433 0.0330 0.036 0.028 0.023			0.00 0.00
Distrib Progre Upper Lower Residu	ution: Area ession: Geome Edge: 1408 Edge: 0.021 uals: Disabled	etric Root8	RunTime: 30 Run Number Particle: acti Particle Trans Particle Refra	second Avg of ive anod sparency ictive Ind	ts 3 runs le powder /: Absorb dex: N/A	Fluid: Fluid R Loading Transm Above	Water efractiv g Facto iission: Residua	e Index r: 0.02 0.91 al: 0.0	: 1.33 297 0	Analys Sample	is Mode: S Cell Id: 0	3000 084	
Numbe	on On	128	Particle Shap	e: N/A	MTWIN(4247	Below I	Residua	al: 0.0	0				
inter.	UII		Database Fat	0.1		L OIN DB	-						

Serial	Number: \$3177 2: 0.021 -1408 um	MICR	OTR	AC -	\$300	0			Ver:8.0a
	1218	02PJM		SMP021	119-4		Date: Time:	12/18/02 Me 21:11 Pre	as #: 10 s #: 1
				<u>Summ</u> mv = 7 mn = 0 ma = 3 cs = 1 sd = 5	ary 7.393 5% = 0.928 20% 3.158 30% 1.900 40% 5.608 50%	Percentile = 0.918 60% = 2.088 70% = 3.242 80% = 4.413 90% = 5.532 95%	6 = 6.779 6 = 8.466 6 = 11.26 6 = 16.42 6 = 21.19	Dia Vol9 5.532 100	<u>% Width</u> % 11.22
%PA 100.0	NSS		1 1 1 1 1 1 1						%CHAN
90.0				X					- 9.0
80.0									- 8.0
70.0			/						- 7.0
60.0									- 6.0
50.0									- 5.0
40.0						_			- 4.0
30.0								_	- 3.0
20.0	-								- 2.0
10.0									- 1.0
0.0	0.010 0.100	1000	10.0		100.0		1000	100	L 0.0
	0.010	1.000	- Size (m	icrons) -	100.0	100	1000	100	
1408 1291 1291 1184 1086 995.6 913.0 837.2 767.7 704.0 645.6 592.0 592.0 542.9 497.8 456.5 592.0 592.0 542.9 497.8 456.5 592.0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	On Let On Action 74.00 100.00 67.86 100.00 67.86 100.00 57.06 100.00 57.06 100.00 47.98 100.00 44.00 100.00 44.00 100.00 44.00 100.00 44.00 99.86 37.00 99.86 37.00 99.86 37.00 99.86 37.00 99.86 37.00 99.86 37.00 99.86 37.00 99.86 37.00 99.86 37.00 99.82 33.11 98.92 28.53 98.38 26.16 97.66 23.99 96.73 22.00 95.58 20.17 94.19 18.50 92.57 16.96 90.75 15.56 88.75 14.27 86.61 13.08 84.32	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.24 0.24	3.889 3.566 3.270 2.999 2.750 2.522 2.312 1.945 1.635 1.499 1.375 1.261 1.156 1.060 0.972 0.892 0.892 0.892 0.892 0.892 0.630 0.530 0.688 0.630 0.530 0.486 0.409 0.375 0.344 0.315 0.289 0.265 0.223	35.41 32.68 30.23 28.00 25.94 24.00 22.14 20.33 18.55 16.78 15.03 13.30 11.61 9.99 8.46 7.05 5.77 4.63 3.62 2.73 1.97 1.32 0.79 0.37 0.10 0.02 0.00 0.00 0.00 0.00 0.00 0.00	$\begin{array}{c} 3.001144\\ 2.73\\ 2.45\\ 2.23\\ 2.06\\ 1.94\\ 1.86\\ 1.81\\ 1.77\\ 1.75\\ 1.75\\ 1.73\\ 1.69\\ 1.62\\ 1.53\\ 1.41\\ 1.28\\ 1.14\\ 1.28\\ 1.14\\ 1.01\\ 0.89\\ 0.76\\ 0.65\\ 0.53\\ 0.42\\ 0.27\\ 0.08\\ 0.02\\ 0.00\\ 0$	0.204 0.187 0.172 0.158 0.145 0.133 0.122 0.111 0.102 0.094 0.086 0.079 0.072 0.066 0.061 0.051 0.047 0.043 0.039 0.036 0.033 0.036 0.028 0.028 0.023	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00
Distrit Progre Upper	bution: Volume ession: Geometric Root8 Edge: 1408	RunTime: 30 second Run Number Avg of Particle: active anod Particle Transport	ds 3 runs le powder	Fluid: W Fluid Ref Loading	ater ractive Inde Factor: 0.22	ex: 1.33 0270	Analysis Sample (Mode: S3000 Cell Id: 0084)
Reside	uals: Disabled er Of Channels: 128	Particle Refractive Inc Particle Shape: N/A	dex: N/A	Above Re Below Re	esidual: 0 esidual: 0	.00 .00			
Filter:	On	Database Path: C:\	MTWIN\1217	PJM.DB				Salar	

Serial	Number: S317 : 0.021 -1408 u	7		MICE	OTR	AC -	S 3	000)			Ver:8.0a
		12180	2PJM			SMP02	1119-4			Date Time	: 12/18/02 Me : 21:11 Pr	eas #: 10 es #: 1
						Sumr mv = mn = cs = sd =	nary 7.393 0.928 3.158 1.900 2.412	5% = 20% = 30% = 40% = 50% =	Percenti 0.582 6 0.864 7 1.078 8 1.340 9 1.708 9	les 0% = 2.320 0% = 3.376 0% = 4.863 0% = 7.173 5% = 9.930	<u>Dia Area</u> 1.708 100	Width 0% 4.823
%PA 100.0	ss 0	Ì I IIIII	111	11111 1	1 1 1111		1111		TTT	T1111-		%CHAN
90.0	+ + +								+++			9.0
80.0			-						+++			8.0
70.0	-								+++			7.0
60.0					4				+++			6.0
50.0												5.0
40.0	+++								+++			4.0
30.0	+++								+++			3.0
20.0												2.0
10.0	-			1								- 1.0
0.0	0.010	0.100		1.000	10.0	00		100.0	+ + + +	1000	100	0.0
CI7E	P/DACC	0/ CHAN	0175	N/DACC	- Size (m	nicrons) -		400	0/ 01100	Loize		
1408 1291 1186 995.6 995.6 995.6 995.6 995.6 995.6 995.6 992.0 592	$\begin{array}{c} 100.00\\$	0.00 0.00	74.00 67.86 62.23 57.06 52.33 47.98 44.00 40.35 37.00 33.93 31.11 28.53 26.16 23.99 22.00 20.17 18.50 16.96 15.56 14.27 13.08 12.00 10.09 9.250 8.482 7.778 7.133 6.541 5.998 5.500 5.044 4.625 4.241	100.00 100.00 100.00 100.00 100.00 100.00 100.00 99.99 99.97 99.94 99.90 99.84 99.64 99.64 99.64 99.64 99.64 99.64 99.64 99.64 99.61 98.69 98.30 97.85 97.32 96.71 96.71 96.71 96.71 96.71 98.69 94.16 94.16 94.16 94.16 94.16 94.15 95.78 83.85 83.45	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	3.889 3.566 3.270 2.999 2.750 2.522 2.121 1.945 1.635 1.499 1.375 1.261 1.156 1.060 0.972 0.892 0.818 0.630 0.530 0.486 0.446 0.409 0.375 0.289 0.243 0.223	73. 71. 69. 664. 62. 59. 57. 54. 57. 54. 33. 29. 25. 21. 148. 44. 44. 44. 44. 44. 44. 44. 44. 44.	7.73 .42 .15 .63 .31 .30 .54 .55 .55 .55 .55 .55 .52 .23 .22 .23 .22 .24 .24 .24 .24 .24 .24 .24 .24 .24	2.31 2.27 2.25 2.27 2.32 2.43 2.58 2.76 2.99 3.29 3.49 3.71 3.99 4.00 3.98 3.73 3.73 3.57 3.57 2.42 1.68 0.57 0.14 0.00 0.00 0.00 0.00 0.00 0.00	0.204 0.187 0.172 0.158 0.145 0.133 0.145 0.145 0.145 0.145 0.145 0.145 0.145 0.145 0.094 0.094 0.086 0.079 0.072 0.066 0.051 0.047 0.043 0.039 0.036 0.033 0.030 0.028 0.023	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.000 0.00
Distrib Progre Upper Lower Residu Numbu	Distribution: Area RunTime: 30 seconds Progression: Geometric Root8 Run Number Avg of 3 runs Upper Edge: 1408 Particle: active anode powder Lower Edge: 0.021 Particle Transparency: Absort Residuals: Disabled Particle Refractive Index: N/A Number Of Channels: 128 Particle Shape: N/A					Fluid: A Fluid Re Loading Transmi Above F Below R	Water efractive Factor ission: Residua Residua	e Index :: 0.02 0.92 I: 0.0 I: 0.0	: 1.33 270 0	Analysis Sample	Mode: S300 Cell Id: 0084	0
Filter:	On		Database	Path: C:\	MTWIN\1217	PJM.DB						

 $\mu\text{m},$ 20 wt% PSD Data

Serial N	lumber: S3177	'n		MICR	OTR	40 -	S 3	000)			v	er:8.0a
- terringer	1100 01	12180	2PJM			SMP021	121-1			Date: Time:	12/18/02 20:51	Meas # Pres #:	: 8
						<u>Summ</u> mv = mn = cs = sd =	ary 9.012 0.857 3.170 1.893 6.887	5% = 20% = 30% = 40% = 50% =	Percentil 0.886 60 2.096 70 3.308 80 4.549 90 5.760 95	es 0% = 7.160 0% = 9.177 0% = 12.94 0% = 21.34 5% = 30.34	<u>Dia V</u> 5.760 1	/ <u>ol%</u> 100%	Width 13.77
%PAS	S							-				%C	HAN
100.0			TIT		TITI		HT						10.0
90.0												+++	9.0
80.0	-					/							8.0
70.0					////								7.0
60.0													6.0
50.0													5.0
40.0	-											+++-	4.0
30.0	+ + +								+++			+++	3.0
20.0	+++											+++	2.0
10.0				£1/								+++-	1.0
0.0	0.010	0,100		1.000	10.0	00		00.0	+ + + + +	1000		0000	0.0
					- Size (m	icrons) -	_						
Size 1408 1291 1184 1086 995.6 913.0 837.2 767.7 704.0 645.6 592.0 542.9 497.8 456.5 418.6 383.9 352.0 322.8 296.0 271.4 248.9 228.2 209.3 176.0 161.4 135.7 114.1 104.7 95.96 88.000 80.70	$\begin{array}{c} \underline{bb} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	0.001 0.000	74.00 67.86 62.23 57.06 52.33 47.98 44.00 33.93 37.00 33.93 31.11 28.53 26.16 23.99 22.00 20.17 18.50 16.96 15.56 14.27 13.08 12.00 11.00 9.250 8.482 7.778 7.133 6.541 5.500 5.044 4.625 4.241	100,00 99.85 99.63 99.63 99.63 99.69 98.69 98.23 96.99 96.20 94.26 93.12 91.87 90.51 89.05 87.50 85.86 84.11 82.26 78.11 75.76 75.76 75.78 75.78 75.78 59.83 55.886 47.91 44.14 40.63 37.45	0.15 0.22 0.25 0.38 0.46 0.57 0.91 1.03 1.44 1.25 1.46 1.554 1.75 1.46 1.75 1.46 1.75 2.35 2.35 2.38 3.49 3.77 3.51 3.25 3.25 3.25 3.25 3.25 3.25 3.25 3.25	3.889 3.566 3.270 2.999 2.750 2.522 2.312 2.121 1.945 1.783 1.635 1.499 1.375 1.261 1.156 1.060 0.892 0.892 0.892 0.818 0.630 0.688 0.630 0.688 0.630 0.486 0.446 0.409 0.375 0.344 0.315 0.289 0.265 0.243 0.223	33299275231018611111887.65.44.321110.000.000.0000.0000000000000000000	7.59 5.02 7.70 5.61 7.75 8.61 5.75 7.75 7.75 7.75 7.75 7.75 7.75 7.7	$\begin{array}{c} 2.57\\ 2.32\\ 2.12\\ 1.97\\ 1.86\\ 1.78\\ 1.70\\ 1.69\\ 1.67\\ 1.65\\ 1.62\\ 1.56\\ 1.62\\ 1.56\\ 1.62\\ 1.38\\ 1.26\\ 1.38\\ 1.26\\ 1.38\\ 1.26\\ 0.57\\ 0.43\\ 0.23\\ 0.13\\ 0.00\\$	0.204 0.187 0.172 0.158 0.145 0.133 0.122 0.111 0.102 0.094 0.086 0.079 0.072 0.066 0.051 0.047 0.047 0.043 0.030 0.038 0.033 0.038 0.028 0.023	$\begin{array}{c} 0.00\\$		
Distrib Progre Upper	Distribution: Volume RunTime: 30 seconds Progression: Geometric Root8 Run Number Avg of 3 runs Jpper Edge: 1408 Particle: active anode powder Lower Edge: 0.021 Particle Transparency: Absor					Fluid: V Fluid Re Loading Transmi	Vater fractiv Facto ssion:	e Index r: 0.0	:: 1.33 272	Analysis Sample	Mode: S3 Cell Id: 00	3000 84	
Residu Numbe	als: Disabled r Of Channels:	128	Particle R Particle S	efractive In hape: N/A	dex: N/A	N/A Above Residual: 0.00 Below Residual: 0.00							
Filter:	On		Database	Path: C:\	MTWIN\1217	PJM.DB			a company and a	and the second second			

Serial	Number: S3177	7	M	ICROT	RAC	- 5	3000)		1	Veril 0a
Kange	. 0.021 - 1408 01	12180	2PJM		SM	P021121-	1		Date:	12/18/02 Mea	ver:8.0a as #: 8 s #: 1
					SL mv mr ma cs sd	immary = 9.012 = 0.857 = 3.170 = 1.893 = 2.377	$\begin{array}{c} 5\% = \\ 20\% = \\ 30\% = \\ 40\% = \\ 50\% = \end{array}$	Percentil 0.538 60 0.807 70 1.011 80 1.261 90 1.607 95	es)% = 2.175)% = 3.188)% = 4.716)% = 7.101 5% = 9.964	Dia Area% 1.607 1009	6 Width 6 4.755
%PA	SS				-						%CHAN
100.0	,]										- 10.0
90.0	-										- 9.0
80.0											- 8.0
70.0	-										- 7.0
60.0	-										- 6.0
50.0											- 5.0
40.0											- 4.0
30.0											- 3.0
20.0											- 2.0
10.0											- 1.0
0.0	0.010	0 100	1.0		10.00		100.0		1000	1000	- 0.0
	0.010	0.100	1.00	- Size	e (micron	s) -	100.0		1000	1000	
1408 1291 1291 1184 1086 913.0 837.2 767.7 704.0 645.6 592.0 542.9 497.8 456.5 418.6 383.9 352.0 542.9 497.8 456.5 418.6 383.9 352.0 542.9 228.2 209.3 176.0 161.4 148.0 135.7 176.0 161.4 148.0 135.7 124.5 114.1 104.7 95.96 88.00	$\begin{array}{c} 100.00\\$	0.00 0.00	Size 70 74.00 10 67.86 99 62.23 99 57.06 96 52.33 99 47.98 99 40.35 99 37.00 99 33.93 99 28.53 99 22.00 99 22.00 99 22.00 99 22.00 99 22.00 99 22.00 96 15.56 97 14.27 97 12.00 96 11.00 95 9.250 94 8.482 93 7.778 91 7.133 90 6.541 86 5.500 84 5.044 81 4.625 79 4.241 77	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	SIZE 3.88 3.88 3.86 3.277 2.99 2.75 2.52 2.31 1.94 1.78 1.49 1.37 1.06 0.97 0.89 0.81 0.63 0.44 0.31 0.28 0.24 0.24 0.24 0.24	27777666665555443333222211117776666655554443333222211117776666655554459533	4.97 4.97 2.78 0.62 8.47 1.73 9.26 6.61 1.73 9.26 6.61 3.74 0.64 7.30 3.73 9.96 6.07 2.15 8.21 4.35 0.58 6.93 3.44 0.14 7.16 2.56 0.90 0.00	2.19 2.19 2.16 2.15 2.17 2.24 2.33 2.47 2.65 2.87 3.10 3.34 3.57 3.77 3.65 3.92 3.94 3.89 3.92 3.94 3.86 3.77 3.65 3.49 3.30 2.98 2.54 2.06 1.60 0.96 0.00 0.00 0.00 0.00 0.00	SIZE 0.204 0.187 0.172 0.158 0.145 0.133 0.122 0.111 0.102 0.094 0.086 0.079 0.066 0.061 0.047 0.043 0.036 0.033 0.028 0.023	0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
Distribution: Area RunTime: 30 seconds Progression: Geometric Root8 Run Number Avg of 3 runs						: Water Refracti	ve Index	1.33	Analysis Sample	Mode: \$3000 Cell Id: 0084	
Lower Residu Numbe	Edge: 1408 Edge: 0.021 als: Disabled er Of Channels:	128	Particle: activ Particle Trans Particle Refrac Particle Shape	parency: Abs stive Index: N// N/A	orb Tran A Abov Belo	ing Facto smission /e Residu w Residu	or: 0.02 : 0.92 ual: 0.00 ual: 0.00	0			
Filter:	On		Database Path	: C:\MTWIN\1	217PJM.	DB				in the second second	



Filter: On Database Path: C:\MTWIN\1217PJM.DB

Serial Bange	Number: S317	7	1	MICH	ROTR	40.	- 53	000	0				Vor:8 0a
Trange	. 0.021-1400 0	12180	2PJM			SMP02	1121-4				Date: Time:	12/18/02 Me 20:59 Pr	es #: 9
						Sumi mv = mn = cs = sd =	mary 7.375 0.878 3.070 1.954 2.351	5% = 20% = 30% = 40% = 50% =	Percent 0.550 0.831 1.041 1.297 1.646	tiles 60% = 70% = 80% = 90% = 95% =	2.217 3.230 4.715 7.001 9.666	<u>Dia Area</u> 1.646 100	% Width 0% 4.703
%PA	SS												%CHAN
100.0) 1					1	TTT			TIII			T ^{10.0}
90.0	+++												9.0
80.0	+++												8.0
70.0										++++			- 7.0
60.0													6.0
50.0													- 5.0
40.0	-												4.0
30.0	-			1									- 3.0
20.0	-			/									2.0
10.0	+++												- 1.0
0.0	0.010	0.100	++-//	.000	10.0	0		00.0	+++	100	0	100	L 0.0
0175			0.75		- Size (m	icrons)	-						
1408 1291 1184 995.6 995.6 995.6 995.6 995.6 952.0 542.9 497.8 456.5 418.6 383.9 352.0 322.8 296.0 322.8 296.0 322.8 296.0 352.2 209.3 352.0 352.2 209.3 176.0 161.0 135.7 124.5 114.1 104.7 95.96.0 88.00 80.70	$\begin{array}{c} 100.00\\$	0.00 0.00	74.00 67.86 62.23 57.06 52.33 47.98 44.00 40.35 37.00 33.93 31.11 28.53 26.16 23.99 22.00 20.17 18.50 16.96 15.56 14.27 13.08 12.00 11.00 9.250 8.482 7.778 7.133 6.541 5.998 5.500 5.044 4.625 4.241	$\begin{array}{c} 100.00\\ 100.00\\ 100.00\\ 100.00\\ 100.00\\ 100.00\\ 100.00\\ 99.99\\ 99.97\\ 99.94\\ 99.90\\ 99.94\\ 99.90\\ 99.84\\ 99.75\\ 99.63\\ 99.48\\ 99.28\\ 99.28\\ 99.28\\ 99.28\\ 99.28\\ 99.28\\ 99.48\\ 99.28\\ 99.48\\ 99.28\\ 99.48\\ 99.48\\ 99.48\\ 99.48\\ 99.28\\ 99.48\\ 99.28\\ 99.48\\ 99.28\\ 99.48\\ 99.28\\ 99.48\\ 99.28\\ 99.48\\ 99.28\\ 99.48\\ 99.28\\ 99.48\\ 99.28\\ 99.48\\ 99.28\\ 99.48\\ 99.28\\ 99.28\\ 99.48\\ 99.28\\ 99$	0.00 0.00 0.00 0.00 0.00 0.00 0.01 0.02 0.03 0.04 0.09 0.12 0.25 0.25 0.30 0.36 0.42 0.49 0.57 0.66 0.79 0.57 0.66 0.79 0.94 1.14 1.85 2.08 2.35 2.39 2.32	3.889 3.566 3.270 2.750 2.522 2.121 1.945 1.499 1.3751 1.499 1.3751 1.1560 0.8922 0.818 0.6888 0.6808 0.5300 0.4866 0.409 0.375 0.2895 0.2433 0.223	74 72 708 655 633 655 552 462 428 334 306 223 195 152 95 64 20 01 00 01 00 00	79 53 31 89 60 221 667 94 97 76 62 277 82 82 83 60 331 36 22 82 03 31 36 22 42 07 20 88 1 00 00 00 00 00 00 00 00	2.26 2.22 2.22 2.29 2.39 2.54 2.73 2.97 3.246 3.68 3.95 3.85 3.95 3.84 3.95 3.84 3.95 3.84 3.95 3.84 3.95 3.84 3.95 3.84 3.72 3.57 3.38 3.14 2.80 2.35 3.14 0.00 0.00 0.00 0.00 0.00		122 187 172 145 145 121 121 102 0946 0079 0079 0079 0079 0079 0079 0079 007	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00
Progression: Geometric Root8 Upper Edge: 1408 Run Time: 30 seconds Run Number Avg of 3 runs Particle: active anode powder					Fluid: Fluid Re Loading	Water efractive g Factor	e Index	t: 1.33 259	An Sa	mple C	Mode: S300 Cell Id: 0084	0	
Residu Numbe	Edge: 0.021 als: Disabled er Of Channels:	128	Particle Tra Particle Ref Particle Sha	ractive Ir ape: N/	cy: Absorb ndex: N/A A	Above I Below F	Ission: Residua Residua	0.92 1: 0.0 1: 0.0	00				
Filter:	On		Database P	ath: C:	MTWIN\1217	PJM.DB	0						

 $\mu\text{m},$ 5 wt% PSD Data

Serial Range	Ver:8.0a											
		12180	2PJM			SMP0212	204-1		Date: Time:	12/18/02 N 18:01 P	leas #: 6 res #: 1	
						<u>Summa</u> mv = 3 mn = 1 ma = 1 cs = 0 sd = 1	ary 35.28 5% = 1.194 20% 12.94 30% 0.464 40% 19.75 50%	Percentile = 2.855 60° = 16.39 70° = 23.90 80° = 29.18 90° = 33.57 95°	<u>s</u> % = 37.86 % = 42.65 % = 49.01 % = 60.39 % = 74.35	Dia Vo 33.57 10	00% Width 00% 39.50	
%PA	SS								2		%CHAN	
100.0	1	ППП	TTT	TTTT			TIT	TTT	TIII I		10.0	
90.0	+++										9.0	
80.0	+++										8.0	
70.0											7.0	
60.0	+++						/				6.0	
50.0	-										5.0	
40.0											.4.0	
30.0	-					1					3.0	
20.0											2.0	
10.0	-		+++								1.0	
0.0	0.010	0.100	+ + + + +	1.000	10.0	0	100.0		1000	10	0.0	
SITE	0/ DASS	%CHAN	SIZE	%DASS	- Size (m	icrons) -	%DASS	%CHAN	SIZE	%DASS	%CHAN	
1408 1291 1184 995.6 995.6 995.6 995.6 995.6 995.6 592.0 542.9 497.8 456.5 418.6 383.9 352.0 352.0 352.0 352.0 352.0 352.2 209.3 176.0 161.4 148.0 135.7 124.5 114.1 104.7 95.960 88.070	100.00 10	0.00 0.24 0.44 0.55 0.70 0.91 1.23	74.00 67.86 62.23 57.06 52.33 47.98 44.00 33.93 31.11 28.53 26.16 23.99 22.00 20.17 18.50 15.56 14.20 11.009 9.250 8.482 7.778 7.133 6.541 5.500 5.644 4.625 4.241	94.93 93.27 91.00 87.92 83.87 78.68 72.49 65.44 58.05 50.65 44.25 38.61 33.91 30.13 27.09 24.59 22.50 20.67 19.03 17.52 16.13 14.84 13.65 10.79 10.06 9.42 8.85 8.34 7.87 7.44 7.03 6.64	1.66 2.27 3.08 4.05 5.19 6.19 7.39 7.19 6.61 5.64 4.70 3.74 2.50 2.09 1.83 1.64 1.51 1.29 1.19 1.095 0.84 0.57 0.51 0.57 0.51 0.57 0.51 0.57 0.51 0.57 0.53 0.54 0.57 0.51 0.57 0.51 0.57 0.51 0.55 0.54 0.55 0.55 0.55 0.55 0.55 0.55	$\begin{array}{r} \hline 3.889\\ 3.566\\ 3.270\\ 2.999\\ 2.750\\ 2.522\\ 2.312\\ 2.121\\ 1.945\\ 1.783\\ 1.499\\ 1.375\\ 1.499\\ 1.375\\ 1.499\\ 1.375\\ 1.261\\ 1.156\\ 0.972\\ 0.892\\ 0.818\\ 0.750\\ 0.688\\ 0.630\\ 0.530\\ 0.486\\ 0.409\\ 0.375\\ 0.344\\ 0.315\\ 0.289\\ 0.265\\ 0.243\\ 0.223\\ \end{array}$	$\begin{array}{r} 6.27\\ 5.91\\ 5.55\\ 5.85\\ 4.85\\ 4.51\\ 4.51\\ 3.81\\ 3.46\\ 3.11\\ 2.75\\ 2.39\\ 2.04\\ 1.37\\ 1.07\\ 0.55\\ 0.33\\ 0.13\\ 0.00\\$	$\begin{array}{c} 0.36\\ 0.36\\ 0.35\\ 0.35\\ 0.35\\ 0.35\\ 0.35\\ 0.35\\ 0.35\\ 0.35\\ 0.36\\ 0.36\\ 0.36\\ 0.36\\ 0.36\\ 0.32\\ 0.24\\ 0.22\\ 0.20\\ 0.13\\ 0.00\\$	0.204 0.187 0.172 0.158 0.145 0.133 0.122 0.111 0.102 0.086 0.079 0.066 0.061 0.051 0.047 0.043 0.033 0.036 0.033 0.028 0.028 0.023	$\begin{array}{c} 0.00\\$	$\begin{array}{c} 0.00\\$	
Distribution: Volume RunTime: 30 seconds Progression: Geometric Root8 Run Number Avg of 3 runs					Fluid: W Fluid Ref	ater fractive Inde	x: 1.33	Analysis Sample (Mode: S30 Cell Id: 008	00		
Upper Lower Residu Numbe	Upper Edge: 1408 Lower Edge: 0.021 Residuals: Disabled Number Of Channels: 128			active and Transparen Refractive I Shape: N	ode powder cy: Absorb ndex: N/A /A	Loading Transmis Above Re Below Re	Factor: 0. ssion: 0.93 esidual: 0 esidual: 0	0732 .00 .00				
Filter:	On		Database	e Path: C	MTWIN\1217	PJM.DB	-					

Serial N	Number: S3177	7		MICE	OTR	4C -	S 3	000)				Ver:8 0a
Trainge.	0.021-1400 01	12180	2PJM			SMP021	204-1			Date: Time:	12/18/02 18:01	Meas Pres #	#: 6 #: 1
						Summ mv = mn = ma = cs = sd =	35.28 1.194 12.94 0.464 15.02	5% = 20% = 30% = 40% = 50% =	Percenti 0.804 6 1.173 7 1.522 8 2.138 9 3.630 9	les 60% = 7.911 70% = 15.50 80% = 26.89 90% = 37.96 95% = 46.43	Dia An 20.27 1.303	rea% 52% 48%	Width 34.32 1.333
%PAS	SS											%0	CHAN
100.0	1						IH	Ш	TT			TT	10.0
90.0											++++	+++	9.0
80.0	-					/							8.0
70.0	-					1							7.0
60.0	-												6.0
50.0												+++-	5.0
40.0												+++	4.0
30.0									-			+++-	3.0
20.0				1								+++-	2.0
10.0	-			-/					+++			+++	1.0
0.0	0.010	0.100		1.000	10.0	0	1 1 11	00.0	+++	1000		0000	0.0
					- Size (m	icrons) -		CTID-644			-		-
1408 1291 1184 995.6 913.0 767.7 704.0 645.6 592.0 542.9 497.8 456.5 418.6 383.9 352.0 322.8 296.0 322.8 296.0 322.8 296.0 322.8 296.0 322.8 296.0 322.8 296.0 322.8 296.0 322.8 296.0 352.0 352.0 10.6 148.0 135.7 124.5 114.1 104.7 95.96 88.00 80.70	$\begin{array}{c} 100.00\\$	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	74.00 67.86 62.23 57.06 52.33 47.98 44.00 33.93 31.11 28.53 26.16 23.99 22.00 20.17 18.50 16.96 15.56 15.56 14.27 13.08 12.00 10.09 9.250 8.4822 7.778 7.133 6.598 5.500 5.500 5.500 4.625 4.241	99.32 99.02 98.57 97.91 96.96 95.63 93.90 91.74 89.28 86.02 81.56 79.33 75.66 74.13 75.66 74.13 75.73 75.73 75.73 75.73 75.75 67.44 66.10 63.45 62.17 60.978 58.66 57.58 55.47 55.52 55.47 54.41 53.32 52.19	0.30 0.45 0.66 0.95 1.33 1.73 2.46 2.46 2.23 1.92 2.46 2.23 1.92 1.53 1.44 1.31 1.34 1.31 1.34 1.31 1.34 1.32 1.34 1.32 1.28 1.28 1.28 1.33 1.73 1.44 1.31 1.34 1.34 1.28 1.22 1.05 1.05 1.05 1.05 1.05 1.05 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.1	3.889 3.566 3.270 2.522 2.750 2.522 2.121 1.945 1.783 1.635 1.499 1.375 1.261 1.156 1.060 0.972 0.892 0.818 0.630 0.486 0.486 0.409 0.375 0.344 0.315 0.289 0.265 0.243 0.223	51.1 49.2 46.1 45.4 45.4 45.4 45.4 45.4 39.3 37.3 35.2 29.2 26.2 29.2 26.2 29.2 20.2 29.2 20.2 20.2 20.2 20.2 20	00 74 39 37 568 37 568 37 568 38 30 57 12 33 43 368 30 57 12 33 43 368 30 57 12 33 43 368 30 57 12 33 44 36 4 36 4 36 4 36 4 37 56 8 30 4 37 56 8 30 4 37 56 8 30 4 37 56 8 30 4 37 56 8 30 4 37 56 8 30 4 37 56 8 30 4 37 56 8 30 4 37 56 8 30 4 37 56 8 30 4 37 56 8 30 57 56 8 30 57 56 8 30 57 57 56 8 30 57 57 57 57 57 57 57 57 57 57 57 57 57	$\begin{array}{c} 1.26\\ 1.35\\ 1.45\\ 1.57\\ 1.69\\ 1.85\\ 2.23\\ 2.45\\ 2.95\\ 3.18\\ 3.57\\ 3.52\\ 3.35\\ 3.57\\ 3.52\\ 3.38\\ 3.35\\ 2.33\\ 0.00\\$	0.204 0.187 0.172 0.158 0.145 0.133 0.122 0.111 0.102 0.094 0.086 0.079 0.072 0.066 0.061 0.056 0.061 0.047 0.043 0.039 0.036 0.033 0.030 0.028 0.026 0.023	$\begin{array}{c} 0.00\\$		0.00 0.00
Distribution: Area RunTime: 30 seconds Progression: Geometric Root8 Run Number Avg of 3 runs Upper Edge: 1408 Particle: active anode powder Lower Edge: 0.021 Particle Transparency: Absorb Residuals: Disabled Particle Refractive Index: N/A					Fluid: V Fluid Re Loading Transmi Above R	Vater fractive Factor ssion: esidual	Index 0.07 0.93 : 0.0	: 1.33 '32 0	Analysis Sample C	Mode: S3 Cell Id: 00	000 84		
Numbe Filter:	or Of Channels:	128	Particle SI Database	Path: C:\	MTWIN\1217	Below R	esidual	: 0.0	0				



Range	: 0.021 -1408 u	m 12180	2PJM			SMP021	204-3			Date:	12/18/02	2 Meas	Ver:8.0
		12100	21 010			Summ mv = mn = ma = cs = sd =	39.86 1.190 13.36 0.449 15.30		801 60° .166 70° .511 80° .104 90° .507 95°	Time: 5 % = 7.620 % = 15.10 % = 27.16 % = 39.01 % = 48.48	18:16 Dia / 20.37 1.303	Pres Area% 51% 49%	#: 1 Width 35.78 1.337
%PA	SS							_				%	CHAN
100.0		ПШ	TTT				IH	11				TIT	10.0
90.0												++++	9.0
80.0	-												8.0
70.0	+++					\wedge							7.0
60.0	+++												6.0
50.0	-												5.0
40.0	-												4.0
30.0	-												3.0
20.0				+ / *									2.0
10.0	+++			-/	1 Bearing	un II							1.0
0.0	0.010	0.100		1.000	10					1000		10000	0.0
	0.010	0.100		1.000	- Size (m	nicrons) -		0.0		1000		10000	
SIZE 1408 1291 1184 1086 995.6 913.0 837.2 7704.0 645.6 592.9 497.8 456.5 645.9 497.8 456.5 6383.9 352.0 8296.0 271.4 228.2 209.3 176.0 161.4 135.7 124.5 114.1 7 95.96 880.70	%PASS 100.00 100	%CHAN 0.00 0.01 0.02 0.03 0.05 0.06 0.07 0.08	SIZE 74.00 67.86 62.23 57.06 52.33 47.98 44.00 40.35 37.00 33.93 31.11 28.53 26.16 23.99 22.00 20.17 18.50 16.96 15.56 14.27 13.08 12.00 11.00 9.250 8.482 7.7133 6.541 5.998 5.500 5.044 4.625 4.241	98.87 98.87 97.97 97.23 96.20 94.81 93.05 90.91 88.51 86.53 86.52 86.53 86.52 86.52 86.52 86.53 86.52 86.53 86.52 86.53 86.52 86.53 86.52 86.53 86.52 86.53 86.52 86.53 86.52 86.53 86.52 86.53 86.52 86.53 86.53 86.53 86.52 86.53 85.56 85.500 85.500 85.500 85.500 85.500 85.500 85.500 85.5000 85.5000 85.5000 85.5000 85.5000 85.5000 85.50000 85.50000 85.50000000000	%CHAN 0.37 0.53 0.74 1.39 1.76 2.14 2.40 2.53 2.49 2.30 2.07 1.81 1.60 1.43 1.32 1.33 1.31 1.27 1.21 1.32 1.33 1.31 1.27 1.21 1.51 1.007 1.05 1.04 1.06 1.09 1.13	SIZE 3.889 3.566 3.270 2.999 2.750 2.522 2.312 1.945 1.783 1.635 1.499 1.375 1.261 1.156 1.060 0.892 0.818 0.750 0.486 0.446 0.409 0.375 0.344 0.315 0.265 0.243 0.223	%PL 51.5 50.2 50.2 48.4 44.1 442.2 37.9 35.4 329.7 265.5 233.6 162.6 9.2 5.8 2.4.0 0.00	155 53 53 53 53 53 53 53 53 54 53 54 54 54 54 55 15 15 17 20 00 00 00 00 00 00 00 00 00	1.27 1.35 1.45 1.57 1.72 1.88 2.07 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.74 2.51 2.51 2.51 2.51 2.51 2.51 2.51 2.51	SIZE 0.204 0.187 0.172 0.158 0.145 0.133 0.122 0.011 0.094 0.094 0.094 0.079 0.072 0.066 0.061 0.051 0.043 0.039 0.036 0.033 0.030 0.028 0.023	70PA 0.000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.000000 0.00000000		0.00 0.00
Distrib Progre Upper Lower Residu	istribution: Area rogression: Geometric Root8 pper Edge: 1408 ower Edge: 0.021 esiduals: Disabled Run Time: 30 seconds Run Number Avg of 3 runs Particle: active anode powder Particle Transparency: Absorl Particle Refractive Index: N/A				Fluid: Water Analysis Mode: S3000 Fluid Refractive Index: 1.33 Sample Cell Id: 0084 Loading Factor: 0.0859 rb Transmission: 0.92 Above Residual: 0.00								
Numbe	on On	: 128	Particle S	Shape: N//	MTWIN(121)	Below R	esidual	0.00					

 $\mu m,$ 20 wt% PSD Data



Serial I	Number: S317	7		MICE	OTR	AC -	53	00	0	1				Ver:8.0a
Trange.	. 0.021-1400 0	12180	2PJM			SMP02	1212-4			1	Date:	12/18/02	2 Meas	#: 3 #: 1
						Sumr mv = mn = cs = sd =	37.89 1.191 13.18 0.455 14.45	5% = 20% = 30% = 40% = 50% =	Percent 0.802 = 1.170 = 1.517 = 2.116 = 3.580	tiles 60% = 7 70% = 1 80% = 2 90% = 3 95% = 4	7.823 6.86 26.32 6.79 6.76	Dia / 21.22 1.303	51% 49%	Width 33.50 1.330
%PA	SS	-											%	CHAN
100.0								HT					TIT	10.0
90.0	-													9.0
80.0	+++						1						++++	8.0
70.0						/								7.0
60.0	+++										-			6.0
50.0	+++													5.0
40.0														4.0
30.0														3.0
20.0	+++													2.0
10.0	+ ++			+/		and it i							++++	1.0
0.0	0.010	0.100		1.000	10.0	00	• • • •	100.0		1000			10000	0.0
SITE	0/ DACC	%CHAN	SIZE	0/ DACC	- Size (n	nicrons) -	9/ 0	ACC	9/ CHA	N Leiz	76	9/ DAG		CHAN
1408 1291 1184 1086 995.6 913.0 837.2 767.7 704.0 645.6 592.0 542.9 497.8 497.8 497.8 497.8 497.8 296.0 271.4 228.2 209.3 191.9 228.2 209.3 191.9 176.0 161.4 148.0 135.7 124.5 114.1 104.7 95.96 88.00 80.70	100.00 100.00	0.00 0.01 0.02 0.03 0.04 0.06 0.021 0.16	012L 74.00 67.86 62.23 57.06 52.33 47.98 44.00 40.35 37.00 33.93 31.11 28.53 26.16 23.99 22.00 20.17 18.50 16.96 15.56 14.27 13.08 12.00 11.00 9.250 8.482 7.778 7.133 6.541 5.998 5.0044 4.625 4.4241	98.89 98.52 98.03 97.38 96.52 95.41 94.00 92.25 90.17 87.77 85.77 82.48 79.84 77.38 75.16 73.23 71.56 70.10 68.80 67.61 66.48 65.38 64.29 63.20 62.11 61.01 59.92 58.84 57.76 56.69 55.63 54.56 53.47	0.37 0.49 0.65 0.86 1.11 1.41 1.75 2.40 2.60 2.69 2.64 2.46 2.22 1.93 1.67 1.46 1.30 1.19 1.13 1.10 1.09 1.09 1.09 1.09 1.09 1.08 1.07 1.08 1.07 1.08 1.07 1.09 1.13 1.17	3.889 3.566 3.270 2.999 2.750 2.522 2.312 1.945 1.783 1.635 1.499 1.375 1.261 1.156 1.060 0.972 0.818 0.630 0.578 0.630 0.446 0.409 0.375 0.243 0.243 0.223	549 48 47 432 40 37 352 226 239 152 20 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	17 .94 .62 .17 .94 .62 .93 .07 .29 .255 .40 .58 .402 .51 .964 .93 .004 .79 .55 .402 .51 .964 .90 .00 .00 .90 .94 .95 .58 .402 .94 .964 .900 .900 .900 .900 .900 .910 .920 .944 .930 .900 .900 .900 .910 .920 .930 .944 .944 .945 <t< td=""><td>1.23 1.32 1.43 1.56 2.03 2.50 2.50 2.50 2.74 2.97 3.18 3.35 3.55 3.52 3.35 3.55 3.52 3.36 3.28 3.41 2.39 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0</td><td>July 0.2 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0</td><td>004 004 007 004 007 004 004 004</td><td></td><td></td><td>0.00 0.00</td></t<>	1.23 1.32 1.43 1.56 2.03 2.50 2.50 2.50 2.74 2.97 3.18 3.35 3.55 3.52 3.35 3.55 3.52 3.36 3.28 3.41 2.39 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	July 0.2 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	004 004 007 004 007 004 004 004			0.00 0.00
Distribution:AreaRunTime: 30 secondsProgression:Geometric Root8Run Number Avg of 3 runsUpper Edge:1408Particle: active anode powderLower Edge:0.021Particle Transparency: AbsoResiduals:DisabledParticle Refractive Index: N/ANumber Of Channels:128Particle Shape: N/A				ds 3 runs de powder y: Absorb dex: N/A	Fluid: N Fluid Re Loading Transmi Above F Below F	Water efractiv Facto ission: Residua Residua	e Inde: r: 0.0 0.93 al: 0.1 il: 0.1	x: 1.33 1725 00 00	Ana San	alysis nple C	Mode: S cell Id: 0	3000 084		






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