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**Pacific Northwest  
National Laboratory**

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# **Borehole Data Package for Four CY 2003 RCRA Wells 299-E27-4, 299-E27-21, 299-E27-22, and 299- E27-23 at Single-Shell Tank, Waste Management Area C, Hanford Site, Washington**

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June 2004



Prepared for the U.S. Department of Energy  
under Contract DE-AC06-76RL01830

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Pacific Northwest National Laboratory  
Richland, Washington 99352

## Summary

Four new Resource Conservation and Recovery Act (RCRA) groundwater monitoring wells were installed at the single-shell tank farm Waste Management Area (WMA) C in fiscal year 2003 to fulfill commitments for well installations proposed in the *Hanford Federal Facility Agreement and Consent Order* milestone M-24-57. Well 299-E27-22, installed upgradient, was drilled through the entire uppermost unconfined aquifer to the basalt and wells 299-E27-4, 299-E27-21 and 299-E27-23 were drilled approximately 40 feet into the uppermost unconfined aquifer and installed downgradient of the WMA. Specific objectives for these wells include monitoring the impact, if any, that potential releases from inside the WMA may have on current groundwater conditions (i.e., improved network coverage) and differentiating upgradient groundwater contamination from contaminants potentially released at the WMA.

This report supplies the information obtained during drilling, characterization, and installation of the four new groundwater monitoring wells. This document also provides a compilation of hydrogeologic and well construction information obtained during drilling, well development, aquifer testing, and sample collection/analysis activities.

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# 1.0 Introduction

Four new Resource Conservation and Recovery Act (RCRA) groundwater monitoring wells were installed at single-shell tank Waste Management Area (WMA) C in fiscal year 2003 to fulfill commitments for well installations proposed in *Hanford Federal Facility Agreement and Consent Order* (Tri-Party Agreement; Ecology et al. 2003) Milestone M-24-57 (Murphy-Fitch 2003).<sup>(a)</sup> The need for increased monitoring capability at this WMA was identified in Narbutovskih and Horton (2001) and during a data quality objectives process for establishing a RCRA/Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA)/Atomic Energy Act of 1954 (AEA) integrated 200 West and 200 East Area Groundwater Monitoring Network (Byrnes and Williams 2003).

Four wells have been installed; one located upgradient and three downgradient of the WMA (Figure 1). Specific objectives for these wells are monitoring the impact, if any, that potential releases from the WMA may have on current groundwater conditions (i.e., improved network coverage) and differentiating upgradient groundwater contamination from contaminants potentially released at the WMA. This report provides the information obtained during drilling, characterization and installation of these four new groundwater monitoring wells at the single-shell tank WMA C.

## 1.1 New Groundwater Monitoring Wells

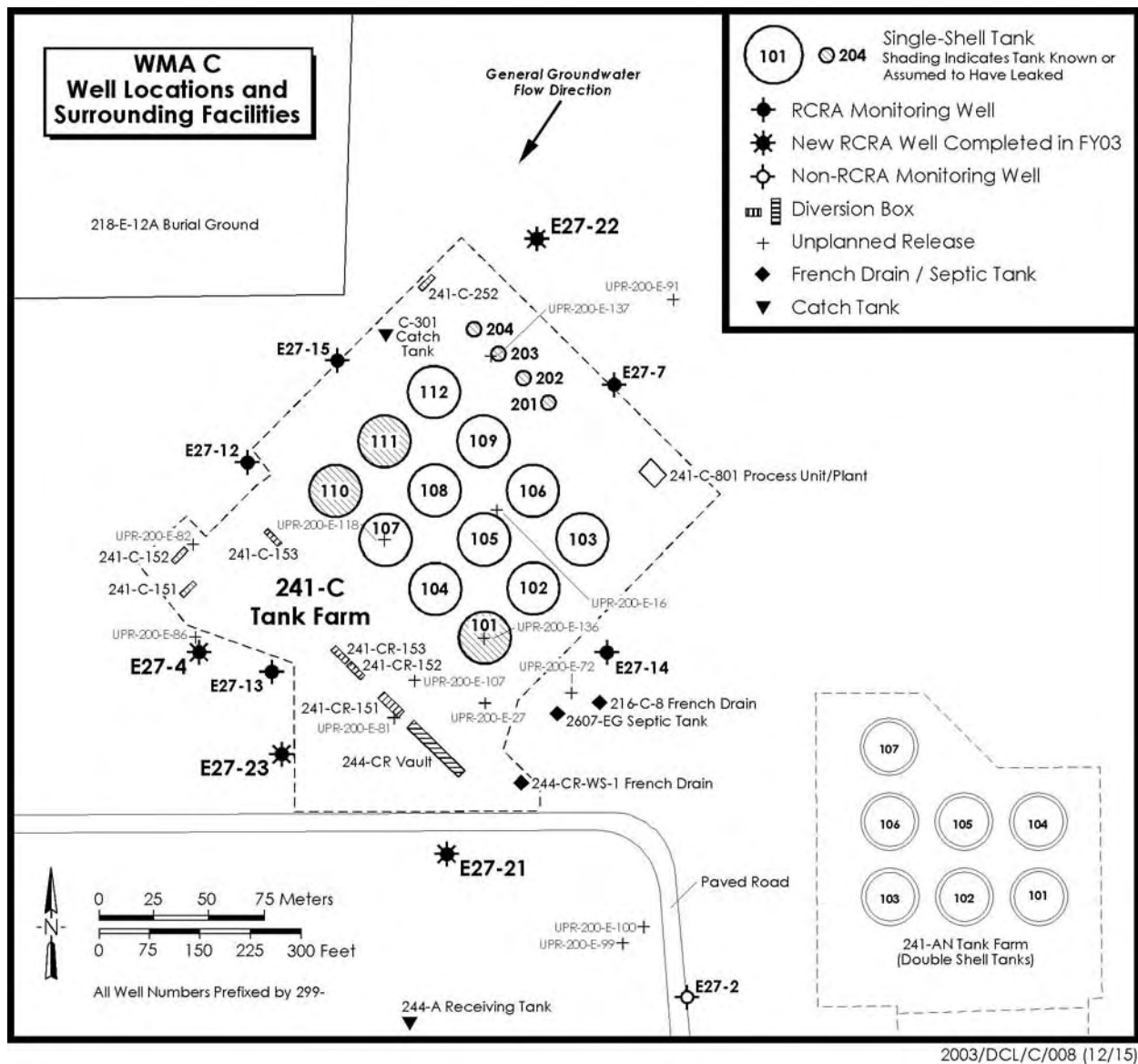
Four groundwater monitoring wells were installed between July and September 2003. The wells are identified as 299-E27-4 (well ID C4125), 299-E27-21 (well ID C4127), 299-E27-22 (well ID C4124) and 299-E27-23 (well ID C4190) and are shown on the location map in Figure 1. Well 299-E27-20 (C4126) was abandoned due to drilling problems and replaced with 299-E27-23 (C4190), which is located approximately 10 feet to the south from well 299-E27-20. The new wells were constructed to the specifications and requirements described in Washington Administrative Code (WAC) 173-160, the groundwater monitoring description of work for drilling and installation (Williams 2003) and specifications used by Fluor Hanford, Inc. (FHI), Richland, Washington. During drilling and construction of the wells, sampling and analysis activities were conducted to support field screening for radiological and chemical contaminants, to collect sediment grab samples for geologic descriptions, digital photography, and for archival in the Hanford Geotechnical Sample Library (HGSL).

Additional characterization was conducted by the CH2M Hanford Group in borehole 299-E27-22 (C4124), which was drilled through the aquifer to the top of basalt. Intact vadose zone core samples were collected. Although the results of tests on these cores are not reported in this document, depth-discrete aquifer testing and groundwater analyses performed during drilling are included in Sections 6.2 and 9.4.

This document provides a compilation of all available geologic data, spectral gamma ray logs, hydrogeologic data and well information obtained during drilling, well construction, well development, pump installation, aquifer testing, and sample collection/analysis activities. Appendix A contains the

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(a) Letter from EJ Murphy-Fitch (Fluor Hanford Inc., Richland, Washington) to Distribution, "Tentative Agreement on Tri-Party Agreement Negotiations on the Overall Strategy and Approach for Hanford Groundwater Protection, Monitoring, and Remediation (M-024)," dated September 22, 2003.



**Figure 1. Map of Single-Shell Tank Waste Management Area C and Locations of New and Existing Wells in the Groundwater Monitoring Network**

Well Summary Sheets, the Well Construction Summary Report, the geologist's borehole log, well development and pump installation records, well survey results, and a construction variance report. Appendix B contains sediment sieve analysis results, core sample chain of custody forms, the core log for 299-E27-22 (C4124), and selected core sample digital photographs. Appendix C contains complete spectral gamma ray logs and borehole deviation surveys while Appendix D contains the hydrologic test report for well 299-E27-22 (C4124).

Additional well construction documentation is on file with FHI. Drilling, geologic and geophysical logs, and well construction/completion data are presented in Martinez (2003). The Records Management

Information System (RMIS) and the Hanford Well Information System (HWIS) [<http://apweb02/cfroot/rapidweb/phmc/cp/hwisapp/>] are two electronic databases that also contain drilling and construction records for these four wells.

English units are used in this report to describe drilling and well completion activities because that is the system of units used by drillers to measure and report depths and well construction measurements. Conversion to metric can be done by multiplying feet by 0.3048 to obtain meters or by multiplying inches by 2.54 to obtain centimeters.

## **2.0 Well 299-E27-22**

Well 299-E27-22 is located to the northeast of the WMA C tank farm. The well is upgradient of WMA C and will help differentiate upgradient groundwater contamination from contaminants potentially released at the WMA.

### **2.1 Drilling and Sampling**

Well 299-E27-22 (well ID C4124) was drilled with a dual-wall percussion drill rig (Becker-hammer) from surface to a total depth of 268 feet below ground surface (bgs). The borehole was drilled through the unconfined aquifer to the top of basalt. Temporary 9-inch outside diameter (OD), dual-wall casing was used during drilling to total depth. Drilling began on July 10, 2003 and total depth was reached on September 5, 2003.

Grab samples of sediment for geologic description, digital photography and archives were collected at approximately 5-foot intervals from ground surface to total depth. Sixty-nine continuous split spoon samples were collected from approximately 19 feet bgs to 111.5 feet bgs. The samples were sealed in one-foot long lexan liners and transferred to Pacific Northwest National Laboratory (PNNL) for analysis. These samples were used to define lithology and for physical and chemical characterization of the vadose zone. An additional 45 split spoon samples were collected at approximately 5-foot intervals at two samples per interval from ~114 bgs to ~231.5 feet bgs near the water table, which was located at 230.5 feet bgs. The borehole log in Appendix A provides the sample depths while the composite log in Section 9.5 (Figure 6) summarizes the sampled intervals and graphic results of core descriptions. The chain of custody forms for transfer of the core samples and selected digital photographs of several cores are contained in Appendix B. Two grab samples were collected from drill depths of 233 feet bgs and 268 feet bgs and evaluated for physical property analysis (sieve analysis) to confirm screen selection. The sieve analysis data and distribution curves are in Appendix B.

Sediments encountered during drilling were predominantly unconsolidated sand to gravelly sand of the Hanford formation from ~5 feet bgs to a depth of 185 feet bgs. Above the Hanford formation are recent deposits. The sandy gravel to gravel of the lower Hanford H3 unit comprises the sediments from approximately 185 feet bgs to 268 feet bgs. Although, the Cold Creek unit (CCU), as defined in Wood et al. (2003), may be present, there is no contact within this gravel unit that can be identified between the lower Hanford formation Unit 3 and the CCU. If the CCU is present, it is not clearly defined.



Furthermore hydrologic testing produced hydraulic conductivities ranging from 6,200 to 22,600 feet per day for the gravels in the aquifer. These high values are indicative of the open, highly permeable lower Hanford gravels of the H3. This interpretation is in agreement with Martinez (2003) and Narbutovskih and Horton (2001). There is no indication that Ringold Formation sediments were encountered. The top of basalt is at total borehole depth at 268 feet bgs. The field geologist's detailed borehole log, along with the well construction summary report, as-built diagram, well development and pump installation records, and well survey results are included in Appendix A. A more detailed hydrogeologic interpretation of the borehole sediments is included in Section 9.0.

The borehole and drill cuttings were monitored regularly for organic vapors, ammonia, and radionuclide contaminants (i.e., alpha, beta, and gamma). Radionuclide monitoring indicated the presence of background levels. Ammonia was detected at several intervals (see borehole log in Appendix A). Spectral gamma ray logs were run on September 8, 2003, by Stoller Corporation. A slight amount of cesium-137, near the minimum detection level (MDL, 0.3 pCi/g), was found sporadically throughout the borehole (Appendix C). Section 7.0 provides more details of this logging.

## **2.2 Well Completion**

The permanent casing and screen were installed in well 299-E27-22 in September 2003. A 40-foot long, 4-inch inside diameter (ID), stainless steel, continuous wire-wrap 20 slot (0.02-inch slot) screen was set from 268.02 feet to 228.05 feet bgs. There is no sump below the screen in this well because the design required the screen to be placed directly on top of the basalt to maximize the length of the sample interval. The permanent well casing is 4-inch ID, stainless steel from 228.05 feet bgs to 2 feet above ground surface.

The screen filter pack is composed of 10-20 mesh silica sand placed from 268 to 225.8 feet bgs, and 4-8 mesh filter pack sand placed from 225.8 to 222.5 feet bgs. The annular seal is composed of 1/4-inch bentonite pellets from 222.5 feet to 217.2 feet bgs and granular bentonite crumbles from 217.2 feet to 10 feet bgs. The surface seal is composed of Portland cement grout from 10 feet bgs to ground surface. A 4-foot by 4-foot by 6-inch concrete pad was placed around the well at the surface. A protective well head casing with locking cap, four protective steel posts, and a brass marker stamped with the well identification number and Hanford well number were set into the concrete pad.

Approximately 170 feet of 1/4-inch galvanized carbon steel tremie pipe was lost between the borehole wall and the casing during installation of the bentonite seal material. The well was constructed with the tremie pipe left in the borehole annulus, located from 47 to 217 feet bgs, and sealed in the bentonite. The bottom end of the pipe is approximately 13 feet above the water table. The Washington State Department of Ecology was informed of the nonconformance (NCR # WMP-GPP-03NCR-010) and approved the design. The Well Construction Summary Report, Well Summary Sheet (as-built), construction variance and nonconformance report are included in Appendix A.

A vertical borehole survey was conducted using a downhole gyroscope in the completed well to determine the bottom location relative to the vertical projection. Survey results are discussed in Section 8.0 and located in Appendix C.

The vertical and horizontal coordinates of the well were surveyed by Fluor Federal Services on October 31, 2003. The horizontal position of the well was referenced to horizontal control stations established by the U.S. Army Corps of Engineers (USACE). The coordinates are Washington Coordinate System, South Zone, NAD83(91) datum. Vertical datum is NAVD 1988 and is based on existing USACE bench marks. Survey data are included in Table 1 and Appendix A. The static water level was 230.46 feet bgs on September 10, 2003.

**Table 1. Survey Data for Four New RCRA Wells at WMA C**

Well Name (Well ID)	Easting (meters)	Northing (meters)	Elevation (meters)	Comments
299-E27-22 (C4124)	575185.10	136685.33		Center of casing
			193.383	Top of casing, N. edge
			192.604	Brass survey marker
			193.389	Top pump base plate, N. edge
299-E27-4 (C4125)	575032.02	136497.92		Center of casing
			205.569	Top of casing, N. edge
			204.685	Brass survey marker
			205.575	Top pump base plate, N. edge
299-E27-21 (C4127)	575145.03	136407.21		Center of casing
			205.728	Top of casing, N. edge
			204.995	Brass survey marker
			205.734	Top pump base plate, N. edge
299-E27-23 (C4190)	575069.46	136452.23		Center of casing
			206.563	Top of casing, N. edge
			205.661	Brass survey marker
			206.569	Top pump base plate, N. edge
NOTES: Horizontal Datum is NAD83 (91); Vertical Datum is NAVD88; Washington State Plane Coordinates (South Zone); surveyed October 31, 2003.				

## 2.3 Well Development and Pump Installation

Well 299-E27-22 was developed on September 12, 2003 at three different intervals using a temporary, 5-horsepower submersible pump. The depth to water was measured at 233.69 feet below top of casing (btc) prior to development. A pressure transducer was installed above the pump and connected to a Hermit datalogger to monitor water level during development. A total of 3521 gallons of water were pumped. Table 2 contains the well development results, including pump intake depth, pump rate, pump run time, drawdown, recovery time, final turbidity (NTU) and stabilized conductivity and temperature readings.

A dedicated Redi-Flo-2, 0.5-horsepower Grundfos™ submersible sampling pump was installed in well 299-E27-22 on September 19, 2003. The sampling pump intake was set at 240.96 feet (btc), approximately 7.3 feet below the water table, and connected to the surface with 3/4-inch diameter stainless steel riser pipe.

**Table 2. Well Development Information for Well 299-E27-22**

Pump Rate	Pump Intake Depth (ft btc)	Pumping Run Time	Drawdown (ft)	Final Turbidity Readings	Recovery Test Time
25 gpm	264.5	60 min	0.27	1.08 NTU, 504 $\mu$ s/cm, 20.7 C	NA
24 gpm	255.5	43 min	0.39	0.97 NTU, 490 $\mu$ s/cm, 20.3 C	9 min (100%)
23 gpm	243.3	43 min	0.44	2.31 NTU, 476 $\mu$ s/cm, 20.2 C	12 min (100%)
ft btc = Feet below top of casing. gpm = Gallons per minute. NTU = Nephelometric turbidity unit. $\mu$ s/cm = micro siemens per centimeter.					

### **3.0 Well 299-E27-4**

Well 299-E27-4 (C4125) is located to the southwest of the 241-C tank farm. The well is downgradient of WMA C and will help differentiate upgradient groundwater contamination from potential contaminants released at the WMA.

#### **3.1 Drilling and Sampling**

Well 299-E27-4 (well ID C4125) was drilled with a hollow stem auger from 0 to 30 feet bgs and with a Becker-hammer rig from ~30 feet bgs to a total depth of 311 feet bgs. Temporary 9-inch outside diameter (OD), dual-wall casing was used below the 30-foot temporary casing for drilling throughout the borehole to total depth. Drilling began on August 12, 2003, and total depth was reached on August 14, 2003.

Grab samples of sediment for geologic description, digital photography and archives were collected at approximately 5-foot intervals from ground surface to total depth. Also, two grab samples were collected from the proposed screen interval at ~270 feet bgs and ~302 bgs for sieve analysis to confirm screen selection. The sieve analysis data and distribution curves are in Appendix B.

Sediments encountered during drilling were predominantly unconsolidated sands to gravelly sands of the Hanford formation beginning at ~22 feet bgs to about 239 feet bgs. Above the Hanford formation are recent deposits. The sandy gravel to gravel of the lower Hanford H3 unit and possibly the CCU comprise the sediments from approximately 239 feet bgs to 311 feet bgs at total depth. Neither Ringold Formation sediments nor basalt were encountered. The field geologist's detailed borehole log, along with the well construction summary report, as-built diagram, well development data, pump installation records and well survey results are included in Appendix A.

The borehole and drill cuttings were monitored regularly for organic vapors, ammonia, and radionuclide contaminants (i.e., for alpha, beta, and gamma). Radionuclide monitoring indicated that alpha, beta and gamma readings were below background levels but ~2 parts per million (ppm) of ammonia were detected at 19 feet bgs (see borehole log in Appendix A). A spectral gamma ray log, run on August 15

and 16, 2003, by Stoller Corporation indicate that a slight amount of cesium-137 near the MDL (0.3 pCi/g) was detected sporadically throughout the borehole (Appendix C). Section 7.0 provides more details of this logging.

### **3.2 Well Completion**

The permanent casing and screen were installed in well 299-E27-4 in August 2003. A 35-foot, 4-inch ID stainless steel, continuous wire-wrap 20 slot (0.02-inch slot) screen was set from 305.33 feet to 270.32 feet bgs with a 2-foot long stainless steel sump placed from 307.76 to 305.33 feet bgs. The permanent well casing is 4-inch ID, stainless steel from 270.32 feet bgs to 1.9 feet above ground surface.

The screen filter pack is 10-20 mesh silica sand placed from 309 to 264.4 feet bgs. The annular seal is composed of 1/4-inch bentonite pellets from 264.4 to 259 feet bgs and bentonite crumbles from 259 to 9.9 feet bgs. The surface seal is composed of Portland cement grout from 9.9 feet bgs to ground surface. A 4-foot by 4-foot by 6-inch concrete pad was placed around the well at the surface. A protective well head casing with locking cap, four protective steel posts, and a brass marker stamped with the well ID number and Hanford well number were set into the concrete pad. During well construction, a stainless steel weight used for tagging and measuring the fill level in the annulus was lost in the borehole at approximately 309 feet bgs. The weight was not recovered and remains in the annulus. The Well Construction Summary Report and Well Summary Sheet (as-built) are included in Appendix A. A borehole deviation survey using a gyroscope was conducted in the completed well to determine the bottom hole location relative to the vertical borehole projection. Survey results are discussed in Section 8.0 and located in Appendix C.

The vertical and horizontal coordinates of the well were surveyed by Fluor Federal Services on October 31, 2003. The horizontal position of the well was referenced to horizontal control stations established by the USACE. The coordinates are Washington Coordinate System, South Zone, NAD83(91) datum. Vertical datum is NAVD 1988 and is based on existing USACE bench marks. Survey data are included in Table 1 and Appendix A. The static water level was 270.65 feet bgs on August 20, 2003.

### **3.3 Well Development and Pump Installation**

Well 299-E27-4 was developed on September 11 and 12, 2003. Development was performed at three different intervals using a temporary, 5-hp submersible pump. The depth to the water was 274.29 feet btc prior to development. A pressure transducer was installed above the pump and connected to a Hermit datalogger to monitor water level during development. Table 3 contains the results of final well development, including pump intake depth, pump rate, pump run time, drawdown, recovery time, final turbidity and stabilized conductivity and temperature readings. A total of 5,100 gallons of water were pumped.

A dedicated Redi-Flo-3, 0.7 hp, Grundfos™ submersible sampling pump was installed in well 299-E27-4 on September 19, 2003. The sampling pump intake was set ~6.9 feet below the water table at 281.11 feet btc and connected to the surface with 3/4-inch diameter stainless steel riser pipe.

**Table 3. Well Development Information for Well 299-E27-4**

Pump Rate	Pump Intake Depth (ft btc)	Pumping Run Time	Drawdown (ft)	Final Turbidity Readings	Recovery Test Time
27 gpm	304.4	70 min	<0.1	3.20 NTU, 516 $\mu$ s/cm, 19.5 C	10 min (100%)
26 gpm	295.4	50 min	<0.1	0.74 NTU, 452 $\mu$ s/cm, 20.1 C	10 min (100%)
28 gpm	283.3	70 min	<0.1	1.16 NTU, 403 $\mu$ s/cm, 18.4 C	15 min (100%)
ft btc = Feet below top of casing. gpm = Gallons per minute. NTU = Nephelometric turbidity unit. $\mu$ s/cm = micro siemens per centimeter.					

## **4.0 Well 299-E27-21**

Well 299-E27-21 (well ID C4127) is located south of the WMA C tank farm. The well is down-gradient of WMA C and will help differentiate upgradient groundwater contamination from potential contaminants released at the WMA.

### **4.1 Drilling and Sampling**

Well 299-E27-21 (well ID C4127) was drilled with a Becker-hammer rig from surface to a total depth of 318 feet bgs. Temporary 9-inch OD, dual-wall casing was used for drilling throughout the borehole to total depth. Drilling began on July 10, and total depth was reached on July 21, 2003.

Grab samples of sediment for geologic description, digital photography and archives were collected at approximately 5-foot intervals from ground surface to total depth. Also, two grab samples were collected from the proposed screen interval from 277 to 280 feet bgs and from 312 to 315 feet bgs for sieve analysis to confirm screen selection. The geologist's borehole log is included in Appendix A. Sieve analysis results and distribution curves are located in Appendix B.

Sediments encountered during drilling were predominantly unconsolidated sand to gravelly sand of the Hanford formation from ~1 feet bgs to about 246 feet bgs. Above the Hanford formation are recent deposits. The sandy gravel to gravel of the lower Hanford H3 unit and possibly the CCU comprises the sediments from approximately 246 feet bgs to 318 feet bgs at total depth. Neither Ringold Formation sediments nor basalt were found in this borehole. The field geologist's detailed borehole log, along with the well construction summary report, as-built diagram, well development and pump installation records, and well survey results are included in Appendix A.

The borehole and drill cuttings were monitored regularly for organic vapors, ammonia and gamma-emitting radionuclides. Radionuclide monitoring indicated that gamma readings were at background levels, and no organics or ammonia was detected (see borehole log in Appendix A). The well was logged with a spectral gamma ray tool on July 21 and 22, 2003, by Stoller Corporation. Logging results showed

a slight amount of cesium-137 near the MDL sporadically throughout the borehole (Appendix C). Section 7.0 provides information on the spectral gamma data collected in the borehole.

## **4.2 Well Completion**

The permanent casing and screen were installed in well 299-E27-21 in July 2003. A 35-foot, 4-inch ID stainless steel, continuous wire-wrap 20 slot (0.02-inch) screen was set from 306.43 feet to 271.37 feet bgs. Below the screen interval there is a 2-foot stainless steel sump extending from 308.83 to 306.43 feet bgs. The permanent well casing is 4-inch ID, stainless steel from 271.37 feet bgs to 2 feet above ground surface.

The screen filter pack is 4-8 mesh silica sand placed from 318 to 314 feet bgs, and 10-20 mesh silica sand placed from 314 to 265.5 feet bgs. The annular seal is composed of 1/4-inch bentonite pellets from 265.5 to 260.4 feet bgs and bentonite crumbles from 260.4 to 10.1 feet bgs. The surface seal is composed of Portland cement grout from 10.1 feet bgs to ground surface. A 4-foot by 4-foot by 6-inch concrete pad was placed around the well at the surface. A protective well head casing with four protective steel posts and a brass marker were set into the concrete pad. The brass marker is stamped with the well identification number and the Hanford well number. The well head has a locking cap. The Well Construction Summary Report and Well Summary Sheet (as-built) are included in Appendix A.

A borehole deviation survey, using a downhole gyroscope, was conducted in the completed well to determine the bottom hole location relative to a vertical borehole projection. Survey results are discussed in Section 8.0 and located in Appendix C.

The vertical and horizontal coordinates of the well were surveyed by Fluor Federal Services on October 31, 2003. The horizontal position of the well was referenced to horizontal control stations established by the USACE. The coordinates are Washington Coordinate System, South Zone, NAD83(91) datum. The vertical datum is NAVD 1988 and is based on existing USACE bench marks. Survey data are included in Table 1 and Appendix A. The static water level was 271.38 feet bgs on July 25, 2003.

## **4.3 Well Development and Pump Installation**

Well 299-E27-21 was developed on August 28, 2003 at three different intervals using a temporary, 5-hp submersible pump. The depth to water was 274.56 feet btc prior to development. A pressure transducer, installed above the pump and connected to a Hermit datalogger, monitored the water level during development. Table 4 contains the data from the well development, including pump intake depth, pump rate, pump run time, drawdown, recovery time, final turbidity and stabilized conductivity and temperature readings. A total of 3,879 gallons of water were pumped.

A dedicated Redi-Flo-3, 0.7 hp, Grundfos™ submersible sampling pump was installed in well 299-E27-21 on September 18, 2003. The sampling pump intake was set at 281.10 feet btc, which is ~6.6 feet below the water table. It was connected to the surface with a 3/4-inch diameter stainless steel riser pipe.

**Table 4. Well Development Information for Well 299-E27-21**

Pump Rate	Pump Intake Depth (ft btc)	Pumping Run Time	Drawdown (ft)	Final Turbidity Readings	Recovery Test Time
23 gpm	306.7	63 min	<0.1	1.24 NTU, 376 $\mu$ s/cm, 20.0 C	7 min (100%)
23.5 gpm	297.7	48 min	<0.1	1.64 NTU, 363 $\mu$ s/cm, 20.2 C	<5 min (100%)
21 gpm	285.6	62 min	<0.1	1.83 NTU, 353 $\mu$ s/cm, 20.7 C	<5 min (100%)
ft btc = Feet below top of casing. gpm = Gallons per minute. NTU = Nephelometric turbidity unit. $\mu$ s/cm = micro siemens per centimeter.					

## 5.0 Well 299-E27-23

Well 299-E27-23 (well ID C4190) is located southwest of the WMA C tank farm and south of existing well 299-E27-13. Located downgradient of WMA C, this well will help differentiate upgradient groundwater contamination from potential contaminants released at the WMA. This well was drilled as an offset replacement to the originally proposed well 299-E27-20 (C4126) that was decommissioned after drilling refusal occurred at 278.5 feet bgs. Drilling information on this decommissioned borehole is included in Appendix A.

### 5.1 Drilling and Sampling

Well 299-E27-23 (well ID C4190) was drilled with a Becker-hammer rig from surface to a total depth of 318 feet bgs. The borehole was drilled approximately 45 feet into the unconfined aquifer. Temporary 9-inch OD, dual-wall casing was used during drilling to total depth. Drilling was completed in one day on August 5, 2003.

Grab samples of sediment for geologic description, digital photography and archives were collected at approximately 5-foot intervals from ground surface to total depth. Also, two grab samples were collected from the proposed screen interval for sieve analysis to confirm screen selection. One sample was from decommissioned borehole 299-E27-20 at ~275 feet bgs, and one was from 299-E27-23 at ~310 bgs. The field geologist's detailed borehole log, along with the well construction summary report, as-built diagram, well development and pump installation records, and well survey results are included in Appendix A. A more detailed hydrogeologic interpretation of the borehole sediments is included in Section 9.0. Sieve analysis results and distribution curves are located in Appendix B.

Sediments found during drilling were predominantly unconsolidated sand to gravelly sand of the Hanford formation from 10 feet bgs to about 245 feet bgs. Above the Hanford formation are recent deposits. The sandy gravels to gravels of the lower Hanford H3 unit and possibly the CCU comprise the sediments from approximately 245 feet bgs to 318 feet bgs, which is the total well depth. Neither Ringold Formation sediments nor basalt were encountered.

The borehole and drill cuttings were monitored regularly for organic vapors, ammonia, and radionuclide contaminants (alpha, beta, gamma). Ammonia was detected to a depth of ~110 feet bgs ranging from 0 to 5 ppm. No man-made radiological contamination was detected. The well was logged with a spectral gamma tool on August 7 and 8, 2003, by Stoller Corporation (see Section 7.0 and Appendix C).

## **5.2 Well Completion**

The permanent casing and screen were installed in well 299-E27-23 in August 2003. A 35-foot, 4-inch ID stainless steel, continuous wire-wrap, 20 slot (0.02-inch) screen was set from 308.54 feet to 273.51 feet bgs. Below the screen interval there is a 2-foot stainless steel sump from 310.97 to 308.54 feet bgs. The permanent well casing is 4-inch ID, stainless steel from 273.51 feet bgs to 1.8 feet above ground surface.

The screen filter pack is 10-20 mesh silica sand placed from 318 to 267.8 feet bgs. The annular seal is composed of 1/4-inch bentonite pellets from 267.8 to 263 feet bgs and granular bentonite from 263 to 9.9 feet bgs. The surface seal is composed of Portland cement grout from 9.9 feet bgs to ground surface. A 4-foot by 4-foot by 6-inch concrete pad was placed around the well at the surface. A protective well head casing with a locking cap, four protective steel posts, and a brass marker stamped with the well ID number and Hanford well number were set into the concrete pad. The Well Construction Summary Report and Well Summary Sheet (as-built) are included in Appendix A.

A vertical borehole survey using a gyroscope was conducted in the completed well to determine the bottom hole location relative to a vertical borehole projection. Survey results are discussed in Section 8.0 and located in Appendix C.

The elevation and location coordinates of the well were surveyed by Fluor Federal Services on October 31, 2003. The horizontal position of the well was referenced to horizontal control stations established by the USACE. The coordinates are Washington Coordinate System, South Zone, NAD83(91) datum. Vertical datum is NAVD 1988 and is based on existing USACE bench marks. Survey data are included in Table 1 and Appendix A. The static water level was 273.1 feet bgs on August 12, 2003.

## **5.3 Well Development and Pump Installation**

Well 299-E27-23 was developed on September 2, 2003 at three different intervals using a temporary, 5-hp submersible pump. Depth-to-water level was measured at 276.52 feet btc prior to development. A pressure transducer was installed above the pump and connected to a Hermit datalogger to monitor water level during development. Table 5 contains the results of final well development, including pump intake depth, pump rate, pump run time, drawdown, and recovery time. Final turbidity, electrical conductivity, dissolved oxygen content, pH and temperature readings are also reported. A total of 3,624.5 gallons of water were pumped.

A dedicated Redi-Flo-3, 0.7 hp, Grundfos™ submersible sampling pump was installed in well 299-E27-23 on September 18, 2003. The sampling pump intake was set at 281.11 feet btc, which is about 4.7 feet below the water table. The riser pipe is 3/4-inch diameter stainless steel.



**Table 5. Well Development Information for Well 299-E27-23**

Pump Rate	Pump Intake Depth (ft btc)	Pumping Run Time	Drawdown (ft)	Final Turbidity Readings	Recovery Test Time
26 gpm	311.3	57 min	0.14	3.93 NTU, 4.46 mg/L DO, 409 $\mu$ s/cm, 7.86 pH, 20.2 C	15 min (99.6%)
26 gpm	301.3	30 min	0.03	0.74 NTU, NA DO, NA $\mu$ s/cm, NA pH, NA C	8 min (100%)
6 gpm	291.3	78 min	0.63	3.00 NTU, 3.23 mg/L DO, 381 $\mu$ s/cm, 7.91 pH, 22.1 C	NA
ft btc = Feet below top of casing. DO = Dissolved Oxygen. gpm = Gallons per minute. NA = Not available. NTU = Nephelometric turbidity unit. C = temperature in degrees centigrade. $\mu$ s/cm = micro siemens per centimeter.					

## 6.0 Sampling and Analysis During Drilling

This section describes the collection and analysis of sediment and water samples collected during drilling from wells 299-E27-22, 299-E27-4, 299-E27-23, 299-E27-21, and 299-E27-20, which is the decommissioned well.

### 6.1 Field Screening

The drill cuttings from all the wells were screened in the field for volatile organic and combustible and/or hazardous gas contamination, beta-gamma activity and alpha activity by radiation control technicians (RCT) and site safety staff. Subsurface spectral gamma logs were also evaluated for gamma-emitting contaminants, and details are discussed in Section 7.0.

Radiation screening of drill cuttings from well 299-E25-93 revealed beta and gamma readings slightly above background in a few intervals. Alpha radiation was also detected but determined to be radon. Radiation screening of cuttings from the other wells revealed only background levels. No actions were required. The cuttings were also screened for volatile organics and other potential hazardous gases using an Organic Vapor Monitor (OVM) photo-ionization detector, an Ammonia Monitor, and a Multi Gas / Combustible Gas Monitor. Ammonia was detected sporadically up to 25 ppm in wells 299-E27-22, 299-E27-4 and 299-E27-23. No action was required. Results of field screening for radiation and gases during drilling are indicated on the geologist's borehole logs in Appendix A.

### 6.2 Sediment and Groundwater Sampling

Sediment samples were collected for geologic description, digital photography, and the soil archives from all four boreholes at 5-foot intervals from ground surface to total depth. The geologic descriptions of these samples are contained in the wellsite geologist's borehole logs in Appendix A. The archive grab samples are contained in 1-pint glass jars, labeled by depth and well number. These jars are stored in the HGSL, which is located at Building 3718A/B in the 300 Area. In addition to the archived jars, sediment

grab samples from each 5-foot depth interval were placed in 1-inch by 2-inch plastic sample trays to create a digital photographic log for each well. These small trays do not include the coarser grain size from the gravels. These digital photographic logs are with the composite logs in Section 9.5. All sediment sample depths and/or intervals are documented in the geologist's borehole logs, located in Appendix A.

Continuous or near continuous core samples were recovered from the vadose zone in borehole 299-E27-22 to provide baseline sediment chemistry data for comparison to potentially contaminated boreholes located inside WMA C tank farm. The core was recovered using a 4-inch ID split spoon sampler that is approximately 2.25 feet long. One hundred and fifteen core samples were collected in one-foot long lexan liners then sealed and labeled. These samples were delivered to the Radiochemical Processing Laboratory in the 325 Building for storage and analysis. The core interval is documented in the borehole log in Appendix A and on the composite log (Figure 6) for well 299-E27-22 in Section 9.5. Chain of custody forms for core transfer to the lab, the detailed core log and selected digital photographs of several cores are located in Appendix B.

Prior to well completion two sediment grab samples were collected from the proposed screen interval in each borehole except for well 299-E27-23. One sample was taken from well 299-E27-23 and another from well 299-E27-20, the nearby well that was not completed because of bit refusal. All of these samples were sieved for particle size distribution to provide data for screen slot size confirmation/selection. Sieve data and distribution curves are available in Appendix B.

Groundwater samples were collected in borehole 299-E27-22 from five intervals to coincide with depth-discrete aquifer testing as the borehole was drilled below the water table. Water was circulated to the surface for collection from the cuttings return line. Each sample interval was isolated below a packer to isolate the sample interval from the shallower saturated zone within the borehole. The samples were analyzed in the field for conductivity, nitrate (TNT Hach Kit method), technetium-99 (3-M filter disk screening method), and pH. Samples from the same depths were also analyzed by inductively coupled plasma-mass spectroscopy (ICP-MS) for technetium-99 and uranium. Technetium-99 levels for all depths, using the ICP-MS method, were below the lower limit of quantitation of 426 pCi/L (0.025 µg/L). Values less than 80.1 pCi/L were identified with the 3-M filter method. The uranium values for all depths were below the natural background value of 3.43 µg/L reported in Johnson (1993). The analytical results are presented in Table 6 below. The water sample depths are also provided on the composite log of 299-E27-22 in Section 9.0.

**Table 6. Depth-Discrete Water Sample Results for Well 299-E27-22 (C4124)**

Sample No.	Sample Date	Depth bgs (ft)	Cond µS/cm	pH	nitrate mg/L	Tc-99 (3-M) pCi/L	Tc-99 (ICP-MS) pCi/L	Uranium µg/L
E22-27-22	9/3/2003	239.5-242.5	447	ND	14.2	10.9	U	BG
E36-27-22	9/4/2003	247-250	412	8.11	16.2	U	U	BG
E12-27-22	9/4/2003	252-254	429	7.95	18.4	14	U	BG
E33-27-22	9/5/2003	260	439	7.98	20.1	38.5	U	BG
E14-27-22	9/5/2003	268	563	8.01	31.1	80.1	U	BG
U = undetected.								
BG = below uranium natural background level of 3.43 µg/L.								

## 7.0 Spectral Gamma Ray Logging

A high resolution spectral gamma-ray survey was conducted in each borehole by Stoller Corporation to determine the presence and concentration of man-made and naturally occurring gamma-emitting radionuclides in the surrounding sediments. Survey measurements were made at a “move-stop-acquire” mode at a rate of 100 seconds per foot. Neutron-moisture logging was not completed because a dual-wall casing was used during drilling which has a casing thickness that is too large for the calibrated neutron moisture tool. The geophysical logs have been evaluated and correlated to the geologic log data for each borehole and the results are presented in the composite logs in Section 9.5. The full suite of geophysical logs for each well, including the detailed log data reports are provided in Appendix C. The log reports describe calibration requirements, data processing, and log plots.

Well 299-E27-22 (C4124) was logged on September 8, 2003 using the gamma-ray tool from ground surface to 266.45 feet bgs inside temporary dual-wall carbon steel casing with an approximate outside diameter of 9 inches. A repeat section was run from 31.45 to 4.45 feet bgs. As reported by Stoller Corporation, cesium-137 was the only gamma-emitting man-made radionuclide detected during geophysical logging. The cesium-137 was detected at a few sporadic locations in the borehole near the 0.2 pCi/g MDL.

In well 299-E27-4 (C4125), logged on August 15 and 16, 2003, the gamma-ray tool was run from below the 11-inch diameter temporary surface casing from 25 feet bgs to a depth of 301 feet bgs within the nominal 9-inch diameter dual-wall temporary carbon steel casing. A repeat section was run from 121 to 90 feet bgs. As reported by Stoller Corporation, cesium-137 was the only gamma-emitting manmade radionuclide detected during geophysical logging. The cesium-137 was detected at a few sporadic locations in the borehole near the 0.2 pCi/g MDL.

In well 299-E27-21 (C4127), logged on July 21 and 22, 2003, the gamma ray tool was run from ground surface to a depth of 316 feet bgs within the nominal 9-inch diameter dual-wall temporary carbon steel casing. A repeat section was run from 142 to 110 feet bgs. As reported by Stoller Corporation, cesium-137 was the only gamma-emitting man-made radionuclide detected during geophysical logging. The cesium-137 was detected at a few sporadic locations in the borehole near the 0.2 pCi/g MDL.

In well 299-E27-23 (C4190), logged on August 7 and 8, 2003, the gamma ray tool was run from ground surface to a depth of 319 feet bgs within the nominal 9-inch diameter dual-wall temporary carbon steel casing. A repeat section was run from 147 to 115 feet bgs. As reported by Stoller Corporation, cesium-137 was the only gamma-emitting man-made radionuclide detected during geophysical logging. The cesium-137 was detected at 2 feet bgs and from 11 through 13 feet bgs with a maximum concentration of 0.6pCi/g. Cesium-137 was also detected from a few deeper intervals in the borehole near the 0.3 pCi/g MDL.

## **8.0 Borehole Gyroscope Survey**

Downhole deviation surveys using a borehole gyroscope were performed in each well following construction to determine how plumb or vertical the well is and to determine the vertical and horizontal location coordinates of the total depth relative to the borehole surface location. These data are used to determine the extent of borehole deviations created during drilling. For this tool, depths are measured from the top of casing to the top of the tool when it is sitting on the bottom of the well. Three dimensional plots showing a hypothetical vertical well and the true attitude of each deviated well are provided in Figures 2 through 5 below. Further gyroscope information can be found in Appendix C.

In well 299-E27-22 (C4124), results show that at a measured cable depth of 257 feet, the true vertical depth of the well is 256.24 feet, a difference of 0.76 feet. In well 299-E27-4 (C4125), the measured cable depth is 297 feet while the true vertical depth of the well is 295.5 feet, a difference of 1.5 feet. In well 299-E27-21 (C4127), results indicate a measured cable depth of 297.5 feet and a true vertical depth of the well is 296.5 feet, a difference of 1.0 foot. In well 299-E27-23 (C4190), results indicate that at a measured cable depth of 300.5 feet, the true vertical depth of the well is 300.3 feet, a difference of 0.2 feet. Thus deviations from vertical result in depth errors ranging from 1.5 feet to 0.2 feet. These data may be used to correct depths to water levels.

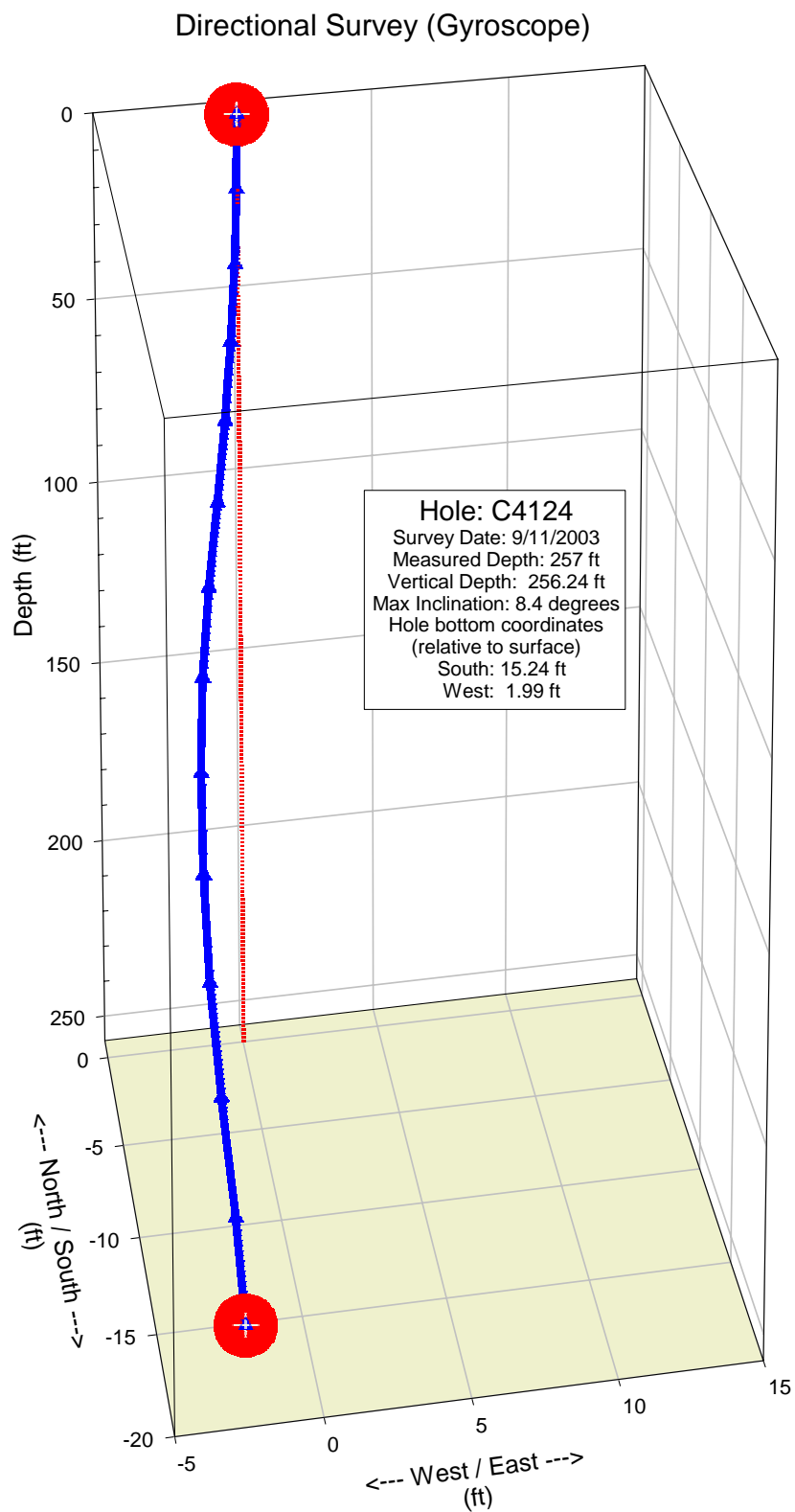
## **9.0 Subsurface Characterization Results**

Results from sediment and water sampling, physical property analysis, geologic logs, spectral gamma logs, well development and aquifer testing for each borehole are correlated to provide an interpretation of the geology at each borehole. This section includes a discussion of the criteria used to evaluate and interpret the data. The composite logs in Figures 6 through 9 illustrate the interpreted hydrogeology developed for each well. These interpretations are consistent with Martinez (2003), Narbutovskih and Horton (2001) and Williams et al. (2000).

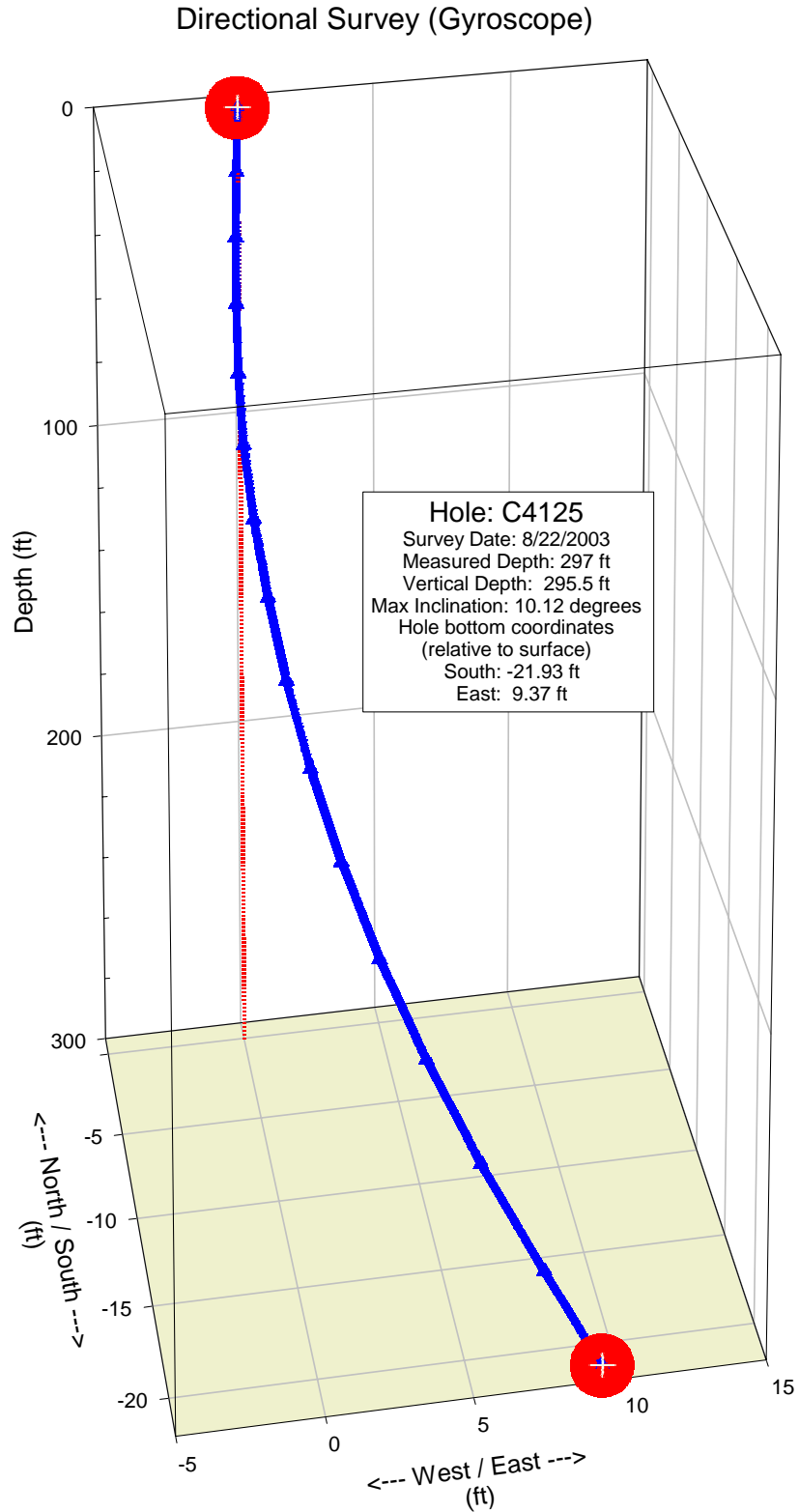
### **9.1 Physical Properties**

There was no analysis for physical properties conducted on samples from these wells except sieve analysis for particle size distribution from either grab or split spoon samples collected from the screen interval. Particle size distribution results are provided in Appendix B.

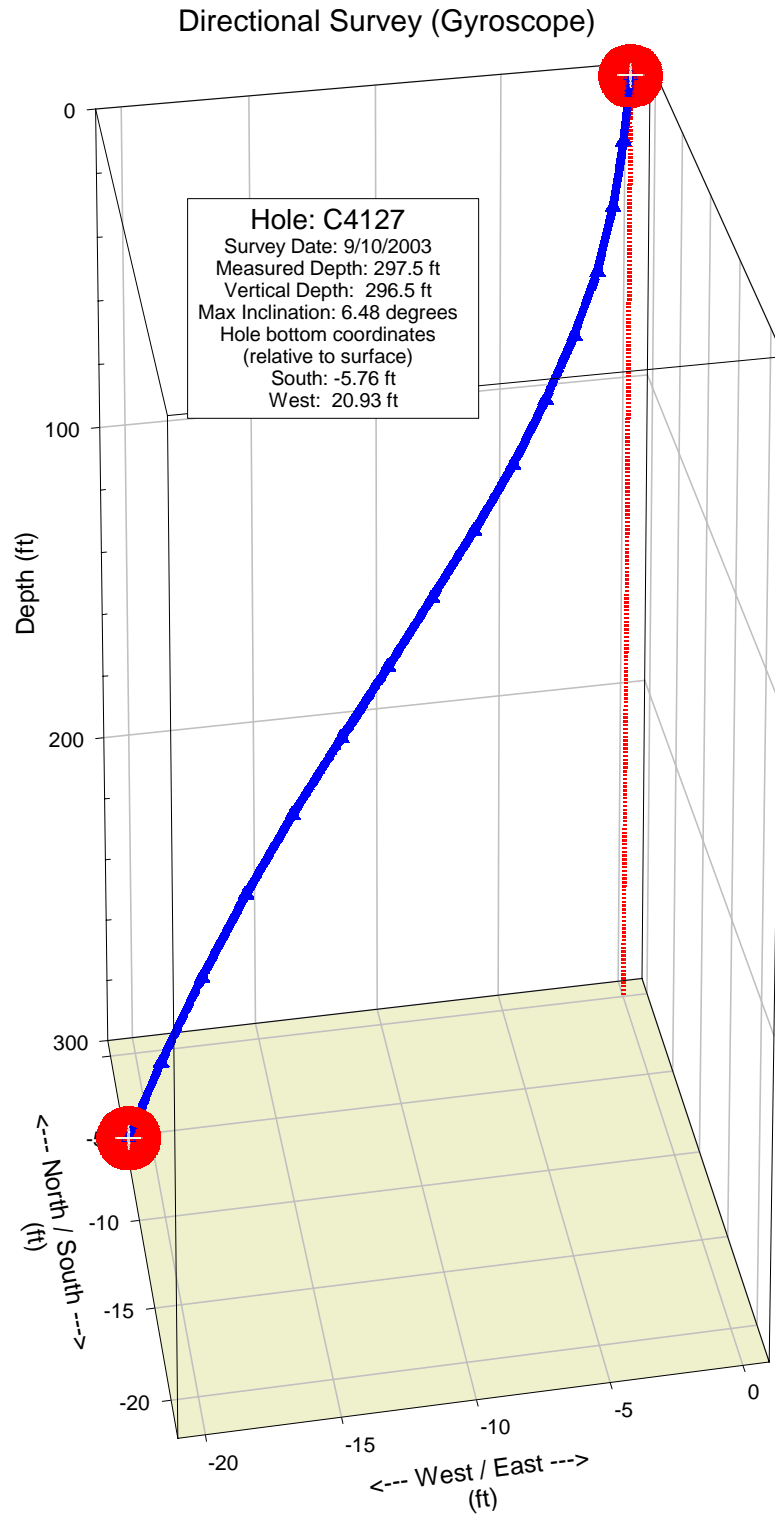
Grab samples collected at 5-foot-depth intervals are described on the geologist's borehole log located in Appendix A. The wellsite geologist's graphic representation of the borehole logs for the four wells are illustrated in composite logs (Figures 6 through 9). The sample quality and formation representativeness of the grab samples, and thus the borehole log descriptions, are limited due to the nature of the drilling. At greater than 250 feet per day, drilling rates were fast. Thus the airlifted return process for cuttings causes gravity separation of sediments based on grain size and density. This process may have mixed the sediment cuttings from different depth intervals before the cuttings reached the surface. When thin beds or sharp contacts were drilled, the returned sediments that were collected could not be completely



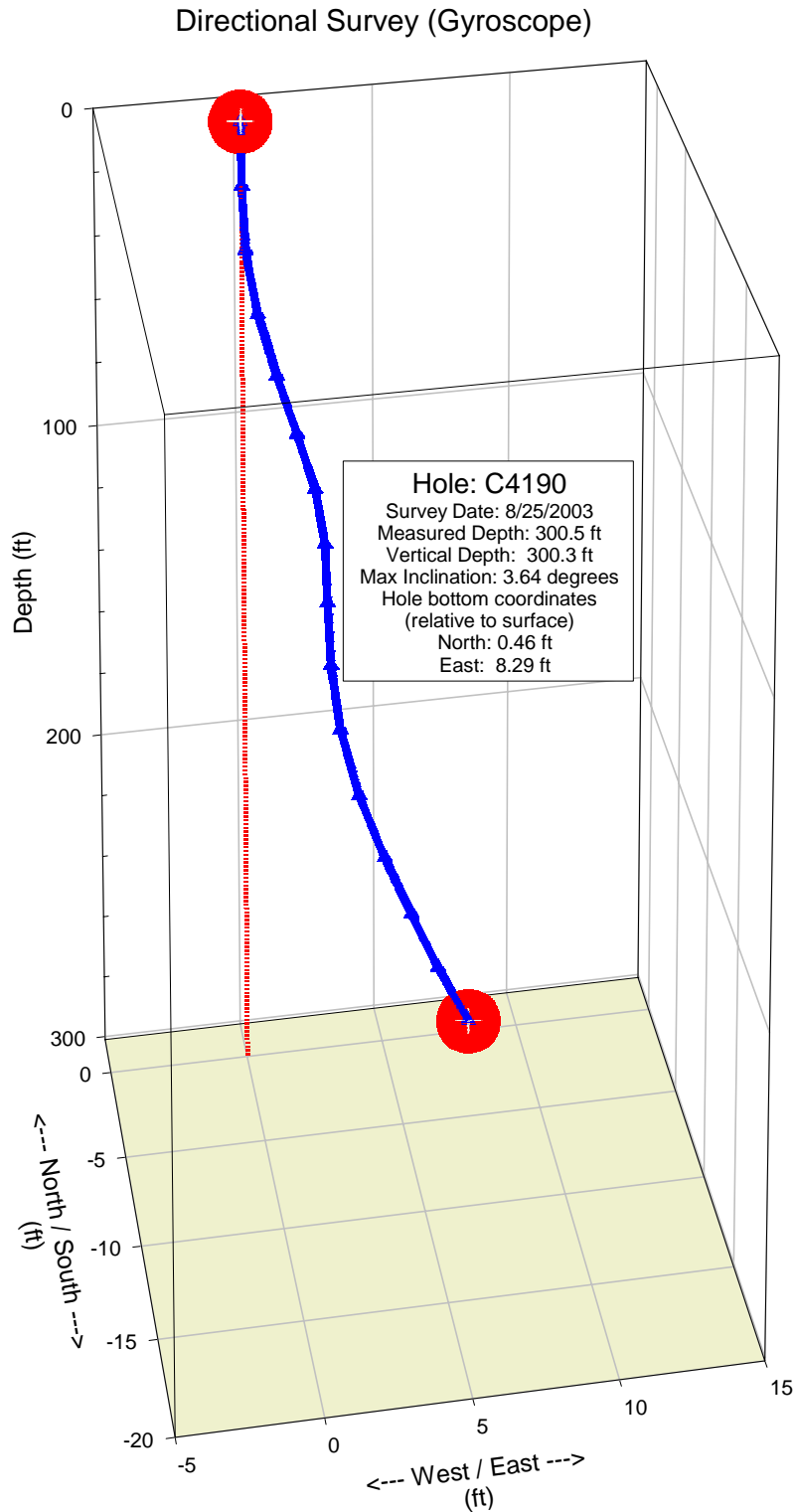
**Figure 2. Vertical Profile and Bottom Hole Projections of Well 299-E27-22**



**Figure 3. Vertical Profile and Bottom Hole Projections of Well 299-E27-4**



**Figure 4. Vertical Profile and Bottom Hole Projections of Well 299-E27-21**



**Figure 5. Vertical Profile and Bottom Hole Projections of Well 299-E27-23**



correlated to their representative depth intervals. However, near-continuous cored intervals in well 299-E27-22 provide an accurate record of lithology and contacts.

The spectral gamma logs indicate the presence of sharp contacts and/or thin bed intervals that may not have been differentiated in the grab samples from the returned cuttings. Consequently lithologic changes are not always documented in the geologic borehole log for these wells. However, evidence they exist can be seen when comparing data from the vadose zone core recovered from well 299-E27-22 to the spectral gamma ray logs. Figure 6 is the composite log for 299-E27-22. The detailed core description, close-up digital core photographs and a detailed geologist's graphic log of the core illustrate these contacts and thin, or sharp lithologic changes. Detailed core log and digital core photographs are also in Appendix B. These changes are not visible on the graphic log or sample photographs that were generated from evaluating the grab samples from the drill cuttings. The spectral gamma ray logs have proven to be an important tool for identifying and accurately locating contacts and subtle lithologic changes that are important for stratigraphic correlations both within and between boreholes.

## **9.2 Sediment Digital Photographic Log**

A digital photographic log of drill cuttings is included in each composite log for the wells (Figures 6 through 9). Grab samples from the cuttings return line were collected for lithologic descriptions documented in the borehole log in Appendix A, for sediment archives, and for digital photography. These photographic log presentations, compiled from 1-inch by 2-inch chip tray samples, collected at 5-foot depth intervals, provide a qualitative visual tool that reveals changes in major lithologic intervals (i.e., grain size, color, and relative moisture). The digital photographic logs provide a means to illustrate subsurface lithology and related hydrogeologic features. The interpretative value of these logs is limited by the sample collection technique, discussed earlier, and sample container size.

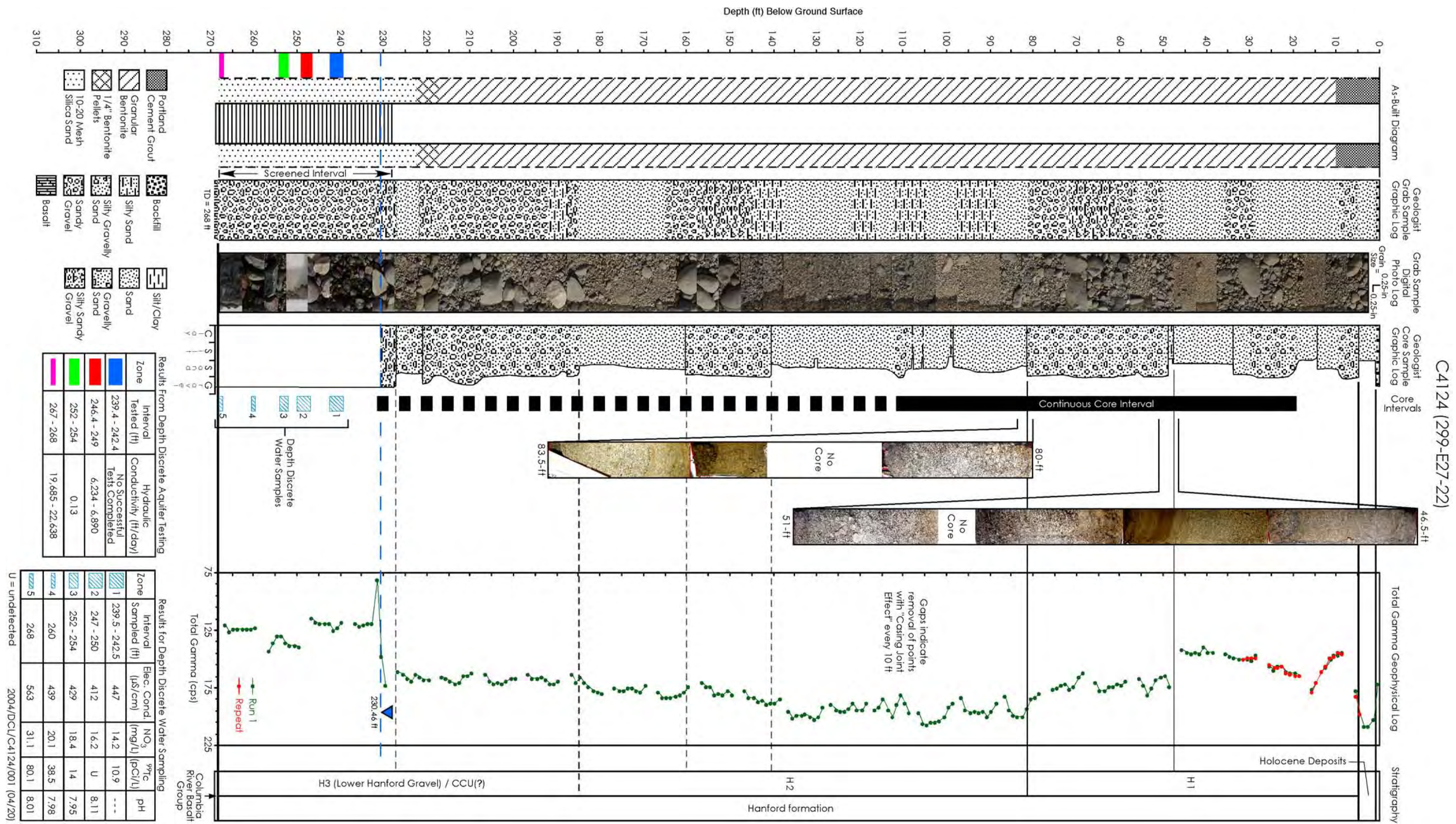
## **9.3 Spectral Gamma Ray Logging**

Based on processing by Stoller Corporation, cesium-137 was the only man-made gamma-emitting radionuclide detected in the four wells (details in Appendix C). This contaminant is mainly near the surface in the boreholes but there are a few sporadic detections, near the MDL of 0.3 pCi/g deeper in the boreholes. In borehole 299-E27-23 (C4190), cesium-137 was detected with a maximum concentration of 0.6 pCi/g at 12 feet bgs. Appendix C provides more details about the cesium-137 detected in the boreholes.

These data are used in the geology interpretation presented in Section 9.5. No discussion of the shallow gamma ray inflections at less than 30 feet bgs is included because these inflections are difficult to correlate, reflecting dramatic changes due to shallow contamination, backfill materials, multiple casing strings, and/or recently deposited loose sediments.

For well 299-E27-22 (C4124), the gamma log plots of the naturally occurring gamma-emitting radionuclides (potassium, uranium, and thorium) indicate there are several distinct activity changes marked by inflection points at depths of ~48, 81, 141, 160, 185, 226, and 230 feet bgs. These major changes correlate to either lithologic features such as bedding contacts and/or thin contrasting lithologic intervals or the water table (Figure 6). The inflections at ~48, 81, 141, 160, 185, and 226 feet bgs







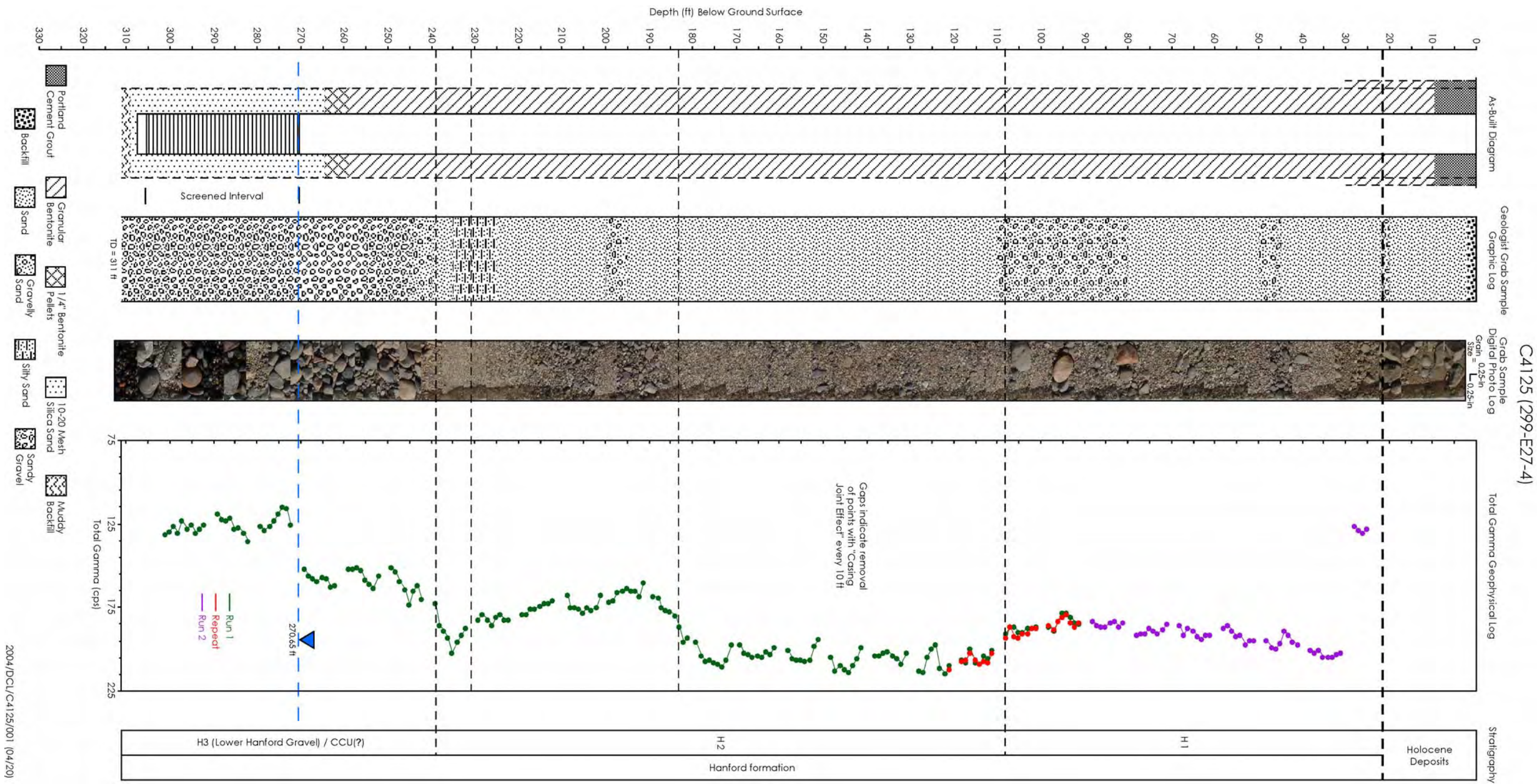


Figure 7. Hydrogeologic Interpretation for Well 299-E27-4 near Single-Shell Tank Farm WMA C



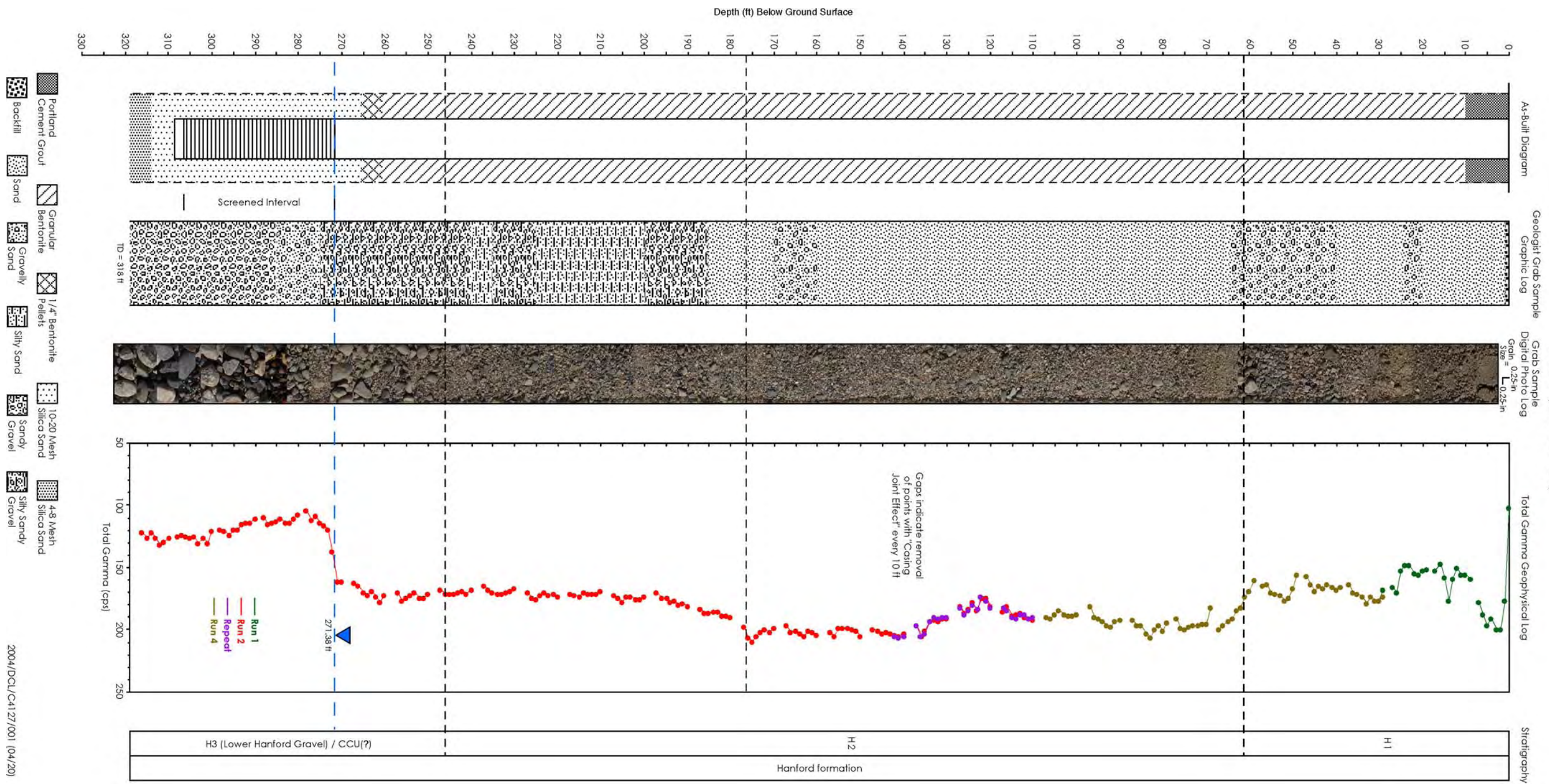


Figure 8. Hydrogeologic Interpretation for Well 299-E27-21 near Single-Shell Tank Farm WMA C



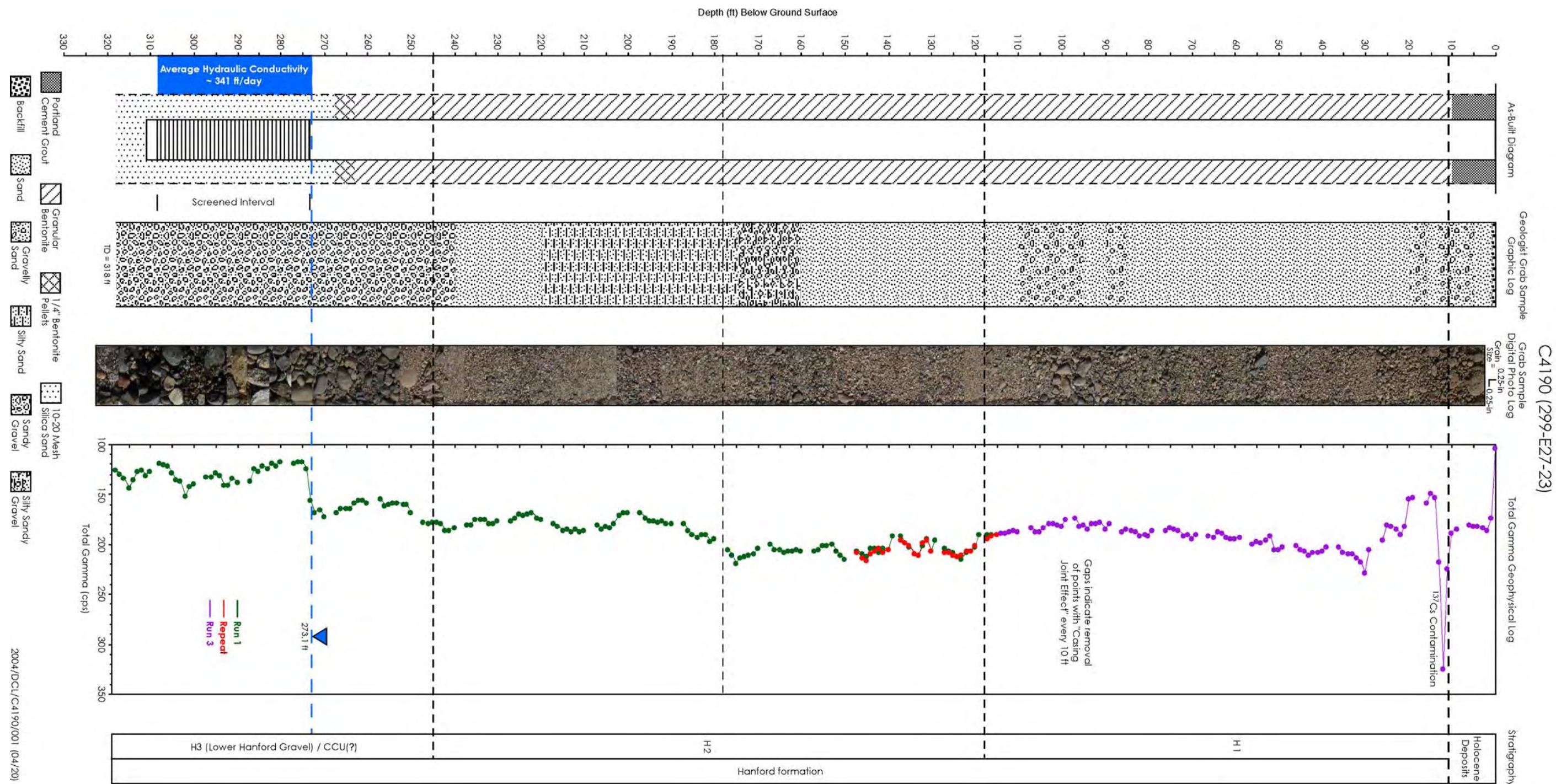


Figure 9. Hydrogeologic Interpretation for Well 299-E27-23 near Single-Shell Tank Farm WMA C

correspond to distinct lithologic changes identified in core samples from the borehole. For example, digital photographs of intact core samples collected from this well are included in the composite log to illustrate the nature of two of the inflections at ~48 and 81 feet bgs (Figure 6 and Appendix B). The cored contact at 48 feet is described as several inches of well-laminated, brown, silty, fine sand between gravelly sand below and grayish sand above. The upper and lower contacts on the finer-grained layer are sharp and distinct. In contrast, the 81-foot contact consists of 0.5 feet of weakly laminated, fine sand between layers of coarser, gravelly sand above and fine to coarse sand below. The upper contact is sharp while the lower contact is gradational. The inflections at 141, 160, 185, and 226 feet bgs reflect other lithologic changes that are visible on the composite log (Figure 6). A graphic log developed from the detailed core descriptions provides an additional comparison to the grab sample derived graphic log.

For well 299-E27-4 (C4125), geophysical log plots of naturally occurring radionuclides indicate several distinct inflection points at depths of ~108, 183, 231, 236, and 270 feet bgs. The inflections at 108 and 183 bgs correspond to changes in lithology similar to those discussed in the paragraph above. The inflections at 231 and 236 feet bgs and a high total gamma peak found at about 238 feet bgs correspond to a thick, fine sand/silt interval approximately 5 feet thick that is recognized in the digital photographic logs at those depths (Figure 7). The water table is located at the inflection at 270 feet bgs.

In the data for well 299-E27-21 (C4127), geophysical log plots of naturally occurring radionuclides indicate several distinct inflection points at depths of ~61, 178, and 271 feet bgs (Figure 8). The inflections at 61 and 178 feet bgs correspond to changes in lithology. The water table is seen at 271 feet bgs. Similarly for well 299-E27-23 (C4190), log plots of naturally occurring radionuclides indicate several distinct inflection points at depths of ~118, 178, and 273 feet bgs. The inflections at 118 and 178 feet bgs correspond to subtle changes in lithology that are not readily apparent in the geology log or digital photographic log (Figure 9). The inflection at 273 feet bgs corresponds to the water table. When details of the geology are correlated to spectra gamma ray logs, it is possible to further define lithologic character within a given well and provide more confidence in correlating geologic units between wells.

## 9.4 Aquifer Tests

Slug testing was performed in well 299-E27-23 (C4190) following construction and development, and at several different depth intervals during drilling in borehole 299-E27-22 (C4124). The slug tests are performed to provide semi-quantitative estimates of hydraulic conductivity in the unconfined aquifer (i.e., the screen interval). The slug testing results provide an objective method to evaluate the hydraulic properties of the formation. Results also support interpretation of the aquifer system lithology. During slug testing, the aquifer in both wells exhibited highly permeable intervals comparable to other wells completed in the Hanford formation.

Highly permeable conditions are also indicated from well screen development drawdown data collected during constant rate pumping in the wells. Each well was developed at three different depth intervals within the well screen to remove excess sediment and to increase hydraulic communication with the surrounding aquifer. Drawdowns ranged from less than 0.03 to 0.63 feet with pumps rates greater than 20 gallons per minute in all but one interval in all four wells.

#### **9.4.1 Well 299-E27-23**

A total of three standard slug tests, one low and two high stress, were conducted on October 7, 2003. Because of the high permeability in the test intervals, no usable test responses were observed for the low stress test where the test response is less than 0.03 feet, with a recovery of less than 3 seconds. As a result, no repeat of the low-stress test was attempted. Consequently, hydraulic conductivity (K) was estimated from high-stress test results. As indicated, similar under-damped, oscillatory responses with rapid recoveries to static conditions within ~7 seconds were exhibited for both tests. The under-damped behavior and rapid recovery are indicative of highly permeable conditions. Slug tests, exhibiting this type of response behavior, cannot be analyzed using standard, over-damped response-based analytical methods such as the Bouwer and Rice or the type-curve methods. The High-K analysis method presented in Butler and Garnett (2000) and Butler et al. (2003) was used to analyze the slug tests at well 299-E27-23. Because the under-damped test responses were very similar, results obtained from the High-K analysis method are quite comparable. Estimates for K ranged between 328 and 354 feet per day for the two tests.

#### **9.4.2 Well 299-E27-22**

Multi-stress slug tests were performed at four specific test/depth intervals within well 299-E27-22. Results from testing and analysis are reported in Spane (2003). This letter report is included in Appendix D. The reported hydraulic conductivities have been incorporated into the composite log for well 299-E27-22 (Figure 6). The estimated hydraulic conductivities, ranging from 6,200 to 22,600 feet per day, are well within the permeability range of 3,300 to 1,600,000 feet per day assigned to the Hanford formation (Wurstner et al. 1995). These data support the interpretation that the basalt is overlain by H3 gravels of the Hanford formation at this waste management area. In a small zone from 252 to 254 feet, a low hydraulic conductivity of 0.13 feet per day was estimated. This low value may be related to hole instability since the open hole was not screened during the testing. Alternatively the low conductivity may reflect the in situ conditions in the aquifer at this level or be the result of an artifact left from the drilling process. At this time, the cause of this low value is not known.

### **9.5 Composite Logs**

Composite logs have been assembled for each well using the well as-builts, well development and aquifer testing results, the geologic descriptions of the sediments and representative graphic logs, the digital photographic logs, and the geophysical logs. Stratigraphic contacts and key lithologic changes are identified where possible. The composite logs for the new wells are illustrated in Figures 6 through 9. These interpretations are also consistent with Martinez (2003), Narbutovskih and Horton (2001) and Williams et al. (2000). Recent surficial sediments composed of reworked Hanford, eolian deposits and/or tank farm backfill sediments overlie the area and range in thickness from one foot up to approximately 20 feet bgs.

The Hanford formation comprises most of the thick (~230 to 270 feet) vadose zone in the WMA C, and is composed of unconsolidated sediments ranging in grain size from cobble to pebble gravel, coarse to fine grained sand, silty sand and silt. There are several distinct contacts and thin, fine grain intervals, either silts or soil horizons that separate thicker Hanford formation sedimentary packages or intervals

such as the upper coarse grained gravelly sequence (H1 unit), the sand sequence (H2 unit), and the lower or basal gravelly sequence (H3 unit). More detailed descriptions of these units are in Narbutovskih and Horton (2001). The selection of these contacts is based on dominant grain size intervals and differences identified by the geologist sample descriptions. These changes in lithology are illustrated by the digital photographic logs. Contacts are also identified by the inflections and general curve fitting from the spectral gamma ray logs. For each borehole, the inflections are dashed on the respective composite logs to imply a unit boundary or contact. The contact between H1 unit and H2 unit is readily identified but the H2 and H3 unit contact is more complicated because of large, discontinuous changes in sediment grain size across the lower interval beneath the WMA C. The contact between the Hanford H2 unit and the H3 unit also appears gradational in places and is approximately located on each composite log (Figures 6 through 9).

The thickness of the uppermost unconfined aquifer beneath WMA C ranges from about 37.5 feet in the north to 61 feet in the south based on water levels from the new wells and on regional mapping of the top of basalt (Williams et al. 2000). The unconfined aquifer beneath the WMA C is composed mostly of basaltic, uncemented, loose, clean, sandy- to silty-sandy gravels that appears characteristic of the permeable lower Hanford formation gravel (H3 unit). Although the CCU may be present based on Wood et al. (2003), there is not a contact with this gravel unit that can be identified between the lower Hanford formation H3 and the CCU. If the CCU is present, it is not clearly defined.

Ringold sediments have not been identified in these boreholes. Criteria used for determining the presence of Ringold Formation sediments and differentiating them from the younger, overlying H3 gravel include dominantly consolidated silty-sandy gravel, composed of less than 25% basalt, the presence of cementation, including iron staining, micaceous material and comparatively low hydraulic conductivities (< 55 feet per day) in the range of published results for known Ringold Formation sediments (Spane 2002). Sediments of this description were not found in the samples from these wells. Only well 299-E27-22 (C4124) was drilled to basalt, which was encountered in at approximately 268 feet bgs. The top of basalt is defined as the base of the uppermost unconfined aquifer which in well 299-E27-22 is ~37.5-feet thick.



## 10.0 References

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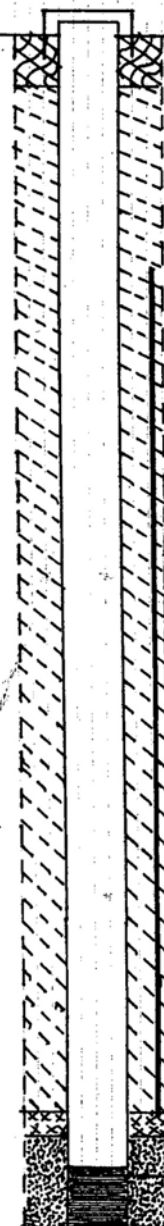

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## **Appendix A**

### **Geologic Logs, Well Construction and Completion Documentation**

#### **Well 299-E27-22**

WELL SUMMARY SHEET		Start Date: 08/21/03		Page 1 of 2	
		Finish Date: 09/10/03			
Well ID: C4124		Well Name: 299-E27-22			
Location: East of C-Tank Farm		Project: C403 RCRA drilling			
Prepared By: Charlene Martinez	Date: 09/11/03	Reviewed By: L.D. Walker	Date: 9/15/03		
Signature: <i>Charlene Martinez</i>		Signature: <i>L.D. Walker</i>			
CONSTRUCTION DATA		GEOLOGIC/HYDROLOGIC DATA			
Description	Diagram	Depth in Feet	Graphic Log	Lithologic Description	
9" OD dual-wall temporary casing used.		0		0'-1' Backfill (crushed gravel)	
				1'-5' SAND(S)	
6" ID protective casing set + 1.0' above permanent.				5'-10' gravelly SAND(gS)	
				10'-29' SAND(S)	
4" ID 53304 sch 10 riser: + 2.2' → 228.05'				29'-36' sandy GRAVEL(sG)	
				36'-50' SAND(S)	
				50'-54' sandy GRAVEL(sG)	
				54'-56' SAND(S)	
				56'-60' sandy GRAVEL(sG)	
Portland Cement Grout: 0' → 10.0'				60'-72' silty sandy GRAVEL(msG)	
				72'-81.5' silty gravelly SAND(msS)	
				81.5'-89' SAND(S)	
Granular Bentonite: 10.0' → 217.2'				89'-98' silty SAND(ms)	
				98'-105' SAND(S)	
				105'-112' silty SAND(ms)	
1/4" Bentonite Pellets: 217.2' → 222.5'				112'-116' SAND(S)	
				116'-122' silty SAND(ms)	
10-20 mesh silica sand: 222.5' → 248.0'				122'-138' SAND(S)	
				138'-145' silty SAND(ms)	
				145'-153' gravelly silty SAND(gms)	
		153'-157' silty sandy GRAVEL(msG)			
		157'-165' sandy GRAVEL(sG)			
		165'-185' SAND			
		185'-188' silty sandy GRAVEL(msG)			
		188'-192' silty SAND(ms)			
		192'-215' sandy GRAVEL(sG)			
		215'-219' gravelly SAND(gS)			
		219'-222' silty sandy GRAVEL(msG)			
		222'-227' SAND(S)			
		227'-233' silty sandy Gravel (msG)			
All depths in feet below ground surface:					
All temporary casing removed from ground.					
170' of 1/4" OD pipe remain in ground (bentonite seal) from 47'-217'					

A-6003-643 (03/03)



WELL CONSTRUCTION SUMMARY REPORT				Start Date: 08/21/03			
				Finish Date: 09/12/03			
				Page 1 of 1			
ID: C-4124		Well Name: 299-E27-22		Approximate Location: East of C-Tank Farm			
Project: C403 RCRA drilling		Other Companies: F.A., C.H.G.					
Drilling Company: Layne Christensen		Geologist(s): C. Martinez, M.S. Hocking					
Driller: Paul ("Derry") Loader License #: 1628							
TEMPORARY CASING AND DRILL DEPTH			DRILLING METHOD	HOLE DIAMETER (in.) / INTERVAL (ft)			
*Size/Grade/Lbs. Per Ft.	Interval	Shoe O.D./I.D.	Auger:	Diameter _____ From _____ to _____			
Dual-wall, carbon steel,	0' - 268'	9"	Cable Tool:	Diameter _____ From _____ to _____			
F.S. 9" OD (outer)	_____ - _____		Air Rotary:	Diameter _____ From _____ to _____			
7" (6" inner)	_____ - _____		A.R. w/Sonic:	Diameter _____ From _____ to _____			
	_____ - _____		Becker Hammer	Diameter 9" From 0' to 268'			
	_____ - _____		(Reverse Air)	Diameter _____ From _____ to _____			
*Indicate Welded (W) - Flush Joint (FJ) Coupled (C) & Thread Design				Diameter _____ From _____ to _____			
			Drilling Fluid: none				
Total Drilled Depth: 268'		Hole Dia @ TD: 9"	Total Amt. Of Water Added During Drilling: _____				
Well Straightness Test Results: Passed using a 20.4' long, 4.5" tool on 09/09/03			Static Water Level: 230.46'		Date: 09/10/03		
GEOPHYSICAL LOGGING							
Sondes (type)	Interval	Date	Sondes (type)	Interval	Date		
Spectral Gamma	0' - 268'	09/08/03		_____ - _____			
	_____ - _____			_____ - _____			
	_____ - _____			_____ - _____			
COMPLETED WELL							
Size/Wt./Material	Depth	Thread	Slot Size	Type	Interval Annular Seal/Filter Pack	Volume	Mesh Size
4" to 55304 sch. 10 riser	+2.2' - 228.05'	8480	N/A	Portland Cement (94" bag)	0' - 10.0'	5 bags	N/A
4" to 55304 sch. 10 well screen	228.05' - 268.02'	"	0.020"	Granular Bentonite (50" bag)	10' - 217.2'	102.5 bags	N/A
4" to 55304 sch. 10 endcap	268.02' - 268.1'	"	N/A	Bentonite Pellets (50")	217.2' - 222.5'	2 buckets	1/4"
	_____ - _____			Colorado silica sand (50")	222.5' - 225.8'	3.5 bags	4-8
	_____ - _____			Colorado silica sand (50")	225.8' - 268.0'	82 bags	10-20
OTHER ACTIVITIES							
Aquifer Test: well development		Date: 09/12/03		Well Decommission:		Yes:	No:
Description: Franklin 5 HP submersible pump, 3 stages				Description:			
Intake @ 264.5' / 355.5' / 243.3'. 23-25 gpm.							
Final turbidity: 1.08 / 0.97 / 2.31 (NTU's.)							
WELL SURVEY DATA (If applicable)							
				Protective Casing Elevation:			
Washington State Plane Coordinates:				Brass Survey Marker Elevation:			
COMMENTS / REMARKS							
Vol. calcs: P.C. => 5 bags * 1.285 <sup>ft<sup>3</sup></sup> /bag = 6.43 <sup>ft<sup>3</sup></sup> ; Granules => 102.5 bags * 0.71 <sup>ft<sup>3</sup></sup> /bag = 72.78 <sup>ft<sup>3</sup></sup> ; pellets => 2 buckets * 0.62 <sup>ft<sup>3</sup></sup> /bucket = 1.24 <sup>ft<sup>3</sup></sup> ; 10-20 sand => 82 bags * 0.535 <sup>ft<sup>3</sup></sup> /bag = 43.87 <sup>ft<sup>3</sup></sup> ; 4-8 sand => 3.5 bags * 0.663 <sup>ft<sup>3</sup></sup> /bag = 2.32 <sup>ft<sup>3</sup></sup> .							
Reported By:		Title:		Signature:		Date:	
Charlene Martinez		Geologist		Charlene Martinez		09/18/03	

A-6003-658 (04/03)

BOREHOLE LOG						Page <u>1</u> of <u>7</u>
						Date: <u>08/21/03</u>
Well ID: <u>C4124</u>		Well Name: <u>299-G27-22</u>		Location: <u>n.e. of C-Tank Farm</u>		
Project: <u>C403 RCPA Drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample Type No.	Blows Recovery	Graphic Log	Sample Description	Comments	
				Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method, Method of Driving Sampling Tool, Sampler Size, Water Level	
0	BH #1	N/A		0'-1' Backfill material. Crushed gravel.	Becker Hammer using 9" OD dual-wall casing	
5	Grab BH #1			1'-5' SAND(S). 100% sand, r. v. well sorted, vfn-fn, non basaltic. micaceous. 2.5Y5/3 light olive brown (moist) no rxn HCl.	Collect 5' archive	
10	Grab BH #1			5'-10' gravelly SAND(S) 20% gravel, 75% sand, 5% silt. Gravel med. sorted, SR-R, 45% basalt, 35% qtz/other. Sand, poorly sorted, prod. v. coarse grained, vfn-v. coarse, SR-SA, 80% basalt, 20% qtz/other. 10YR3/1, v. dark gray. moist. no rxn HCl.	Collect 10' archive @ 10' NH <sub>3</sub> = 25 ppm	
15	Grab BH #1			10'-20' SAND, 95% sand, 5% silt. Sand, SR-SA, v. poorly sorted, SR-SA, 80% basalt, 20% qtz/other, vfn-v. coarse, prod. v. coarse grained. 10YR3/1 v. dark gray (moist) no rxn HCl.	Collect 15' archive @ 20' NH <sub>3</sub> = 17 ppm	
20	Grab BH #1	100% recovery		@ 15' sand graded to vfn-fn, v. well sorted, micaceous, 40% basalt, 60% qtz/other no rxn HCl. 2.5Y4/2, dark grayish brown. Rounded	ss #1 19.5'-21.5' bgs collect 20' archive ss #2 21.5'-24.0' bgs	
25	Grab BH #1	100% recovery		@ 20' sand graded to v. poorly sorted vfn-v. coarse, 40% basalt, 60% qtz/other SR-SA	ss #3 24.0'-26.5' bgs Collect 25' archive. L.O.S. @ 26.5' bgs (08/21/03) start 08/22/03	
30	Grab BH #1	95% recovery		@ 22' trace poorly sorted gravel (< 8/16) mps ~ 4". Basaltic, SR-R	ss #4 26.5'-29.0' bgs 4 ppm NH <sub>3</sub> ss #5 29.0'-31.5' bgs 5 ppm NH <sub>3</sub>	
35	Grab BH #1	100% recovery		@ 24.5' basalt cobbles w/ poorly sorted gravel. Sand grading to poorly sorted, SR-SA, vfn-v. coarse	ss #6 31.5'-34.0' bgs	
36	Grab BH #1	100% recovery		29'-36' Sandy Gravel (26) 30% gravel, 65% sand, 5% silt. Gravel, med. sorted, pea-size-med cobbles, basaltic. Sand, poorly sorted	Collect 35' archive ss #7 34.0'-36.5' bgs ss #8 36.5'-39.0' bgs	

Reported By: <u>Charlene Martinez</u>	Reviewed By: <u>L.D. Walker</u>
Title: <u>Geologist</u>	Title: <u>Geologist</u>
Signature: <u>Charlene Martinez</u>	Signature: <u>L.D. Walker</u>
Date: <u>08/21/03</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

BOREHOLE LOG						Page 2 of 7
						Date: 08/22/03
Well ID: C4124		Well Name: 299-E27-22		Location: N.E. of C-Tank Farm		
Project: C403 RCRA drilling				Reference Measuring Point: Ground Surface		
Depth (Ft.)	Sample Type No.	Blows Recovery	Graphic Log	Sample Description	Comments	
				Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method, Method of Driving Sampling Tool, Sampler Size, Water Level	
40	3H9" 6mb 8H9"	SS#9 100% recovery		(29' cent.) sand, SR-SA, vfn-vcse, 50% basalt, 50% gtz/other.	Becker Hammer using 9" OD dual wall casing	
		SS#10 100% recovery		10YR4/2 dark grayish brown, moist	collect 40' archive	
				No rxn HCl.	SS#9 39'-41.5' bgs	
					SS#10 41.5'-44.0' bgs	
45	6mb 8H9"	SS#11 100% recovery		36'-50' SAND(S) 95% sand, 5% silt. Sand, vfn-fn, R.	collect 45' archive	
		SS#12 100% recovery		well sorted, non-basaltic	SS#11 44.0'-46.5' bgs	
				No rxn HCl. 2.5Y4/3, light olive brown (moist)		
					SS#12 46.5'-49.0' bgs	
50	6mb 8H9"	SS#13 100% recovery		48'-48.5' compact sand lens.	collect 50' archive	
		SS#14 100% recovery		laminar bedding, vfn-fn grain, rounded, non-basaltic.	SS#13 49.0'-51.5' bgs	
				@ 48.5' vcse - vfn grain sand.	SS#14 51.5'-54.0' bgs	
				poorly sorted, basaltic.	SS#15 54.0'-56.5' bgs	
					collect 55' archive	
55	6mb 8H9"	SS#15 100% recovery		50'-54' sandy GRAVEL (SG) 50% gravel, 40% sand, 10% silt. Gravel, poorly sorted, med. pea-size - sm. cobbles	SS#16 56.5'-59.0' bgs	
		SS#16 100% recovery		SA-R. Sand, poorly sorted SR-SA, 40% basalt, 40% gtz/other, vfn-vcse grain	SS#17 59.0'-61.5' (0% MC)	
				higher % vcse grain. 10YR4/1, dk gray (moist). No rxn HCl.	collect 60' archive	
					SS#18 61.5'-64.0' bgs	
					SS#19 64.0'-66.5' bgs	
60	6mb 8H9"	SS#17 100% recovery				
65	6mb 8H9"	SS#19 50% recovery		54'-56' SAND(S) 90% sand, 10% silt. sand, med-sorted, SR-SA	collect 65' archive	
		SS#20 95% recovery		vfn-med, non-basaltic, 2.5Y4/3 olive brown, moist. No rxn HCl.	SS#20 66.5'-69.0' bgs	
				SS#21 69.0'-71.5' bgs (0% MC)		
				collect 70' archive		
70	6mb 8H9"	SS#21 100% recovery	57'-60' sandy GRAVEL (SG) 45% gravel, 30% sand, 5% silt. Gravel, basaltic, SA-R, poorly sorted, mps - 2" sand, poorly sorted	SS#22 71.5'-74.0' bgs		
			SR-SA, 40% basalt, 40% gtz/other, vfn-vcse, 10YR4/1 dk gray (moist). No rxn HCl.	collect 75' archive		
				SS#23 74.0'-76.5' bgs		
				collect 75' archive		
				SS#24 76.5'-79.0' bgs		
75	6mb 8H9"	SS#23 100% recovery	60'-72' silty sandy GRAVEL (SG) 65% gravel, 25% sand, 10% silt			
		SS#24 100% recovery				

Reported By: Charlene Martinez	Reviewed By: L.D. Walker
Title: Geologist	Title: Geologist
Signature: Charlene Martinez	Signature: L.D. Walker
Date: 08/22/03	Date: 9/30/03

A-6003-642 (03/03)



BOREHOLE LOG					Page 3 of 7
					Date: 08/25/03
Well ID: C4124		Well Name: 299-E27-22		Location: n.e. of C-Tank farm	
Project: C403 RCRA drilling				Reference Measuring Point: Ground surface	
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments
	Type No.	Blows Recovery			
40	BH 21	SS#25 80% recovery	[Graphic Log: Stippled pattern]	6.0' cont.) Gravel, poorly sorted, SA-R, 25% size to med cobbles, 45% basalt, 55% other. Sand, poorly sorted, SE-A, 50% qtz, 50% basalt, fn-vase grained. 10YR 5/3 brown (dry), no rxn HCl.	Becker Hammer using 9" OD dual-wall casing. Collect 80' archive.
85	BH 21	SS#27 85% recovery		72' - 81.5' silty, gravelly SAND (ms), 15% gravel, 73% sand, 12% silt.	SS#25 79.0' - 81.5' bgs. SS#26 81.5' - 84.0' bgs. Collect 85' archive.
90	BH 21	SS#28 100% recovery		Gravel, med-sorted, SA-R, 50% basalt, 50% qtz, other. mps ~ 2" sand, poorly sorted, SE-A, fn-vase grained, 50% basalt, 50% qtz, other, 10YR 5/2, grayish brown (moist). No to weak rxn HCl.	SS#27 84.0' - 86.5' bgs. SS#28 86.5' - 89.0' bgs. SS#29 89.0' - 91.5' bgs. Collect 90' archive.
95	BH 21	SS#30 100% recovery		81.5' - 89' SAND (s) 95% sand, 5% silt, sand, R, v. well sorted, vfn-fn grained, non-basaltic, trace mica, 2.5Y 5/3 light olive brown (moist). Weak rxn HCl.	SS#30 91.5' - 94.0' bgs. SS#31 94.0' - 96.5' bgs. Collect 95' archive.
100	BH 21	SS#32 100% recovery		@ 84' sand grading to v. coarse-vfn grained, basaltic, poorly sorted.	SS#32 96.5' - 99.0' bgs. Collect 100' archive.
105	BH 21	SS#33 100% recovery		@ 85' sand, grading to v. coarse-med grained, med. sorted, basaltic, trace well-sorted gravel, basaltic.	SS#33 99.0' - 101.5' bgs. SS#34 101.5' - 104.0' bgs.
110	BH 21	SS#35 100% recovery		89' - 98' silty SAND (ms) 85% sand, 15% silt. Sand, SE-SA, poorly sorted, fn-vase grained, 35% basalt, 45% qtz, other, 2.5Y 4/3 olive brown (moist), micaceous. No rxn HCl.	SS#35 104.0' - 106.5' bgs. Collect 105' archive.
115	BH 21	SS#36 100% recovery		98' - 105' SAND (s) 95% sand, 5% silt. Sand, R, vfn-fn grain, compact matrix, micaceous, non-basaltic, v. well sorted, 2.5Y 5/2 grayish brown (moist). No rxn HCl.	SS#36 106.5' - 109.0' bgs. SS#37 109.0' - 111.5' bgs. Collect 110' archive.
	BH 21	SS#37 100% recovery		@ 99.5' sand, poorly sorted, vfn-vase, SE-SA, 25% basalt, 75% qtz, other, increase in silt (~10%), unconsolidated.	SS#37 111.5' - 114.0' bgs. Collect 115' archive.
	BH 21	SS#38 100% recovery		@ 101.5' increase in basalt content (45%).	SS#38 114.0' - 116.5' bgs.

Reported By: Charlene Martinez	Reviewed By: L.D. Walker
Title: Geologist	Title: Geologist
Signature: Charlene Martinez	Signature: L.D. Walker
Date: 08/25/03	Date: 9/30/03

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>4</u> of <u>7</u>
						Date: <u>08/26/03</u>
Well ID: <u>C4124</u>		Well Name: <u>299-E27-22</u>		Location: <u>EAST OF <del>299</del> C-Tank Farm</u>		
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample Type No.	Blows Recovery	Graphic Log	Sample Description	Comments	
120	24 9" BH 9"	SS#29 100% recovery		105' - 112' silty SAND (ms) 85% sand, 15% silt, trace gravel. Gravel, basaltic, med. cobbles. Sand, v. poorly sorted, SE-SA, 20% basalt, 80% qtz/other, vfn-vase grained, micaceous 2.5Y 5/3 light olive brown, moist. No rxn HCl.	Rock Hammer using 9" CD dual-wall casing collect 120' archive SS#29 119'-121.6' bgs collect 123' archive SS#40 124'-126.6' bgs collect 125' archive	
125	24 9" BH 9"	SS#40 100% recovery		112' - 118' SAND(S) 95% sand, 5% silt. Sand, SE-SA, med. sorted, pred fn-med grained, vfn-vase grains present, non-basaltic, micaceous, 2.5Y 5/4, light olive brown (moist), No rxn HCl.	Collect 127' archive SS#41 129'-131.6' bgs collect 130' archive	
130	24 9" BH 9"	SS#41 100% recovery		116' - 122' silty SAND (ms) similar to description from 105'-112'.	Collect 133' archive SS#42 134'-136.6' bgs collect 135' archive	
135	24 9" BH 9"	SS#42 100% recovery		122' - 138' SAND(S) 95% sand, 5% silt, sand, vfn-vase, SE-SA, poorly sorted, 45% basalt, 55% qtz/other, micaceous 10YR 5/2, grayish brown, moist. No rxn HCl.	Collect 138' archive SS#43 139.0'-141.6' collect 140' archive	
140	24 9" BH 9"	SS#43 100% recovery		@127' silt increasing to ~10% sand, moderately sorted, SE-SA, pred. med-cse grained. Some fn v vase (small %'s)	@139' 10ppm NH <sub>3</sub> in borshole 9ppm NH <sub>3</sub> in spoils.	
145	24 9" BH 9"	SS#44 100% recovery		@130' sand grading to well-sorted, vfn-med grained.	Collect 143' archive SS#44 144.0'-146.6' bgs collect 146' archive	
150	24 9" BH 9"	SS#45 60% recovery		@135' sand graded to poorly sorted, vfn-vase, silt < 5%.	Start 08/27/03 SS#45 149'-151.5' bgs collect 150' archive	
155	24 9" BH 9"	SS#46 50% recovery		138' - 145' silty SAND (ms) 85% sand, 15% silt, sand, SE-SA, med. sorted, vfn-cse, pred. Med grained, micaceous, 20% basalt, 80% qtz/other, 2.5Y 6/2 light brownish gray (moist), No rxn HCl.	Collect 153' archive	
	24 9" BH 9"	SS#47 50% recovery		145' - 148' gravelly SAND (ms) 15% gravel, 70% sand, 15% silt. Gravel, basaltic, med-sorted, SE-SA, pred-size 40 sm pebbles. Sand poorly sorted, SE-SA, 40% qtz/other, 40% basalt, vfn-vase grained, pred. cse-vase, 10YR 5/3 brown (dry), Non-m	Collect 155' archive collect 157' archive	
Reported By: <u>Charlene Martinez</u>				Reviewed By: <u>L.D. Walker</u>		
Title: <u>Geologist</u>				Title: <u>Geologist</u>		
Signature: <u>Charlene Martinez</u>		Date: <u>08/26/03</u>		Signature: <u>L.D. Walker</u>		
				Date: <u>9/30/03</u>		

A-6003-642 (03/03)



BOREHOLE LOG						Page <u>6</u> of <u>7</u>
						Date: <u>09/02/03</u>
Well ID: <u>C4124</u>		Well Name: <u>299-E27-22</u>		Location: <u>East of C-Tank Farm</u>		
Project: <u>C403 RCR drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample Type No.	Blows Recovery	Graphic Log	Sample Description Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Comments Depth of Casing, Drilling Method, Method of Driving Sampling Tool, Sampler Size, Water Level	
200	BH 911 Grab BH 912 Grab BH 913	SS #55 100% recovery N/A		192'-215' Sandy GRAVEL (SG) 45% gravel, 50% sand, 5% silt. Gravel, SA-S, well sorted, basaltic, pea-size to sm pebbles, sand, SE-SA, poorly sorted, vfn- coarse grained, 40% basalt, 60% qtz/other	Becker Hammer using 9" OD dual-wall casing SS #55 192'-201.5' bgs collect 200' archive	
205	Grab BH 914 Grab BH 915 Grab BH 916	SS #56 100% recovery N/A		trace mica, 2.5 Y 4/2 dk. grayish brown (moist). No rxn HCl. @ 194' gravel increasing to lg. pebbles - sm cobbles poorly sorted.	SS #56 204'-206.5' bgs collect 205' archive collect 207' archive	
210	Grab BH 917 Grab BH 918 Grab BH 919	SS #57 40% recovery N/A		@ 199' gravel content decreasing to ~30% pea-size to med. pebbles, silt increasing to 10%.	SS #57 209'-214.5' bgs collect 210' archive.	
215	Grab BH 920 Grab BH 921 Grab BH 922	SS #58 100% recovery N/A		@ 205' gravel content increasing to ~50% silt decreasing to ~7% Gravel, med-sorted, pea-size to med pebbles.	SS #58 214'-216.5' bgs collect 215' archive	
220	Grab BH 923 Grab BH 924 Grab BH 925	SS #59 10% recovery N/A		@ 209' gravel, v. poorly sorted, pea-size to med cobbles, mps ~ 1", 45% basalt, 55% felsics.	collect 217' archive.	
225	Grab BH 926 Grab BH 927 Grab BH 928	SS #60 75% recovery N/A		215'-219' gravelly SAND (GS) 20% gravel, 92% sand, 8% silt. Gravel, med-sorted, pea-size to med pebbles, SE-A, 40% basalt, 60% qtz/other. Sand, vfn-vsse, SE-A, poorly sorted, pld. 225- vss, 40% basalt, 10% qtz/other, micaceous, 10 YR 5/3, brown (moist). No rxn HCl.	SS #59 219'-228.5' bgs collect 220' archive collect 222' archive SS #60 224'-226.5' bgs collect 225' archive collect 227' archive	
230	Grab BH 929 Grab BH 930 Grab BH 931 Grab BH 932	SS #61 10% recovery Collect sieve sample @ 232'-235' (agglom.)		219'-222' silt, sandy GRAVEL (mg) Gravel 55% sand 35% silt 10% gravel, poorly-sorted, SE-A, 50% basalt, 50% qtz/other. Sand, SE-SA, poorly sorted, vfn-vsse grained, 35-40% basalt, 40-45% qtz/other, trace mica.	E.O.S. @ 229' bgs (09/02/03) Start 09/03/03 SS #61 229'-231.5' bgs collect 230' archive	
235	Grab BH 933 Grab BH 934			2.5 Y 4/2, dk. grayish brown (moist). No rxn HCl.	collect 232' archive sieve sample (232'-235')	
				225'-227' SAND(S). + trace gravel, well sorted, sm. pebbles. Sand, SE-SA, poorly sorted, vfn-vsse trace mica, 50% basalt, 50% qtz/other, no rxn HCl.	collect 235' archive	

Reported By: <u>Charlene Martinez</u>	Reviewed By: <u>L.D. Walker</u>
Title: <u>Geologist</u>	Title: <u>Geologist</u>
Signature: <u>Charlene Martinez</u>	Signature: <u>L.D. Walker</u>
Date: <u>09/02/03</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>7</u> of <u>7</u>
						Date: <u>09/03/03</u>
Well ID: <u>C4124</u>		Well Name: <u>29-E27-23</u>		Location: <u>East of C-Tank Farm</u>		
Project: <u>C403 RCRA Drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments	
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level	
240	BH 9" Grab BH 9"	n/a		227 - 233' silty sandy GRAVEL (mss) 55% gravel, 33% sand, 12% silt. Gravel, v. poorly sorted, SR-A, pea-size to med. cobbles, 20% basalt, 10% quartz. Sand, R-A, v. poorly sorted, vfn-vcs. Grained, 15% basalt, 35% quartz. 2.5/5/2 grayish brown (dry) No rxn HCl.	Beckthammer using 9" OD dual-wall casing. Collect 240' archive	
245	BH 9" Grab BH 9"			233 - 244' Sandy GRAVEL (SG) 40% gravel 55% sand, 5% silt. Gravel, med-sorted, pea-size to sm. pebbles, 55% quartz, 45% basalt, SR-SA. Sand, SR-SA, poorly sorted, vfn-vcs. Grained, med. cse-vcs, 45% basalt, 35% quartz. No rxn HCl.	Collect 245' archive	
250	BH 9" Grab BH 9"			@ 237' gravel increasing in size 4%.	F.O.S. @ 249' bgs (09/03/03)	
255	BH 9" Grab BH 9"			Poorly sorted, sm pebbles - med cobbles, basaltic, Gravel, 60%, sand 35%, silt 5%.	Start 09/04/03. Collect 250' archive	
260	BH 9" Grab BH 9"			263' Basalt. weathered surface, iron oxide staining, vesicular surface, visible fractures, quartz streaks, chloride, "peacock" iridescence	Collect 260' archive	
265	BH 9" Grab BH 9"			TD @ 268' bgs.	Collect 265' archive	
270	BH 9" Grab BH 9"				Collect 268' archive (TD)	
275	BH 9" Grab BH 9"					

Reported By: <u>charlene martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>09/03/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

WELL DEVELOPMENT AND TESTING DATA														
Report # 1: Page 1 of 2														
Well Name: 299-E27-27	Well ID: C4124	Well Location: East of C-Tank Farm	Date: 09/12/03											
Reference Measuring Point (unless otherwise noted): TOP OF OUTER CASING (TOC)														
Has the well been surveyed? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		Does the well have a cement pad? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No												
<b>PART 1</b>		<b>PART 4</b>												
<b>STATIC WATER LEVEL:</b>		<div style="display: flex; justify-content: space-between;"> <div style="border: 1px solid black; padding: 5px; width: 45%;"> Last Recorded Measurements Date: N/A </div> <div style="border: 1px solid black; padding: 5px; width: 45%;"> Current Measurements Date: 09/12/03 </div> </div>												
Start of Job 233.69'		<div style="display: flex; justify-content: space-around; align-items: center;"> <div style="text-align: center;"> C ↑ A B Ground Level </div> <div style="text-align: center;"> </div> <div style="text-align: center;"> C' ↓ A' B' </div> </div>												
End of Job -		A = N/A      A' = 3.3' B = -      B' = 2.3' C = -      C' = 1.0'												
<b>DEPTH TO BOTTOM:</b>		Are there any reference marks on the casing strings? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No												
Start of Job 271.3'		<b>PART 5</b>												
End of Job -		<b>COMMENTS:</b>												
<b>PART 2</b>		1018 Setting up rig.												
<b>WELL DEVELOPMENT DATA</b>		1025 Tagged g.w. @ 233.69' (TOC)												
Pump Model Franklin 5 Hp submersible		Tagged bottom @ 271.3' (TOC) No fill.												
Intake Depth 264.5' 255.5' 243.3'		1100 Tripping in pump & tremmie pipe.												
Starting Turbidity 30.9 24.7 111		1145 Intake set 264.5' TOC												
<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>Pump Start</th> <th>Stop</th> <th>Flow Rate</th> </tr> </thead> <tbody> <tr> <td>(60 min) 1158</td> <td>(1500 gals) 1258</td> <td>25 gpm</td> </tr> <tr> <td>(55 min) 1312</td> <td>(1242 gals) 1355</td> <td>24 gpm</td> </tr> <tr> <td>(43 min) 1412</td> <td>(989 gals) 1455</td> <td>23 gpm</td> </tr> </tbody> </table>	Pump Start	Stop	Flow Rate	(60 min) 1158	(1500 gals) 1258	25 gpm	(55 min) 1312	(1242 gals) 1355	24 gpm	(43 min) 1412	(989 gals) 1455	23 gpm	1157 Ready to run test (#4 on data logger). XD = 26.761'	
Pump Start	Stop	Flow Rate												
(60 min) 1158	(1500 gals) 1258	25 gpm												
(55 min) 1312	(1242 gals) 1355	24 gpm												
(43 min) 1412	(989 gals) 1455	23 gpm												
1500 + 1032 + 989 = 3521 gals.		1158 Begin test. Initial readings: XD = 26.365' TURB												
Total Pumped 3521 gals.		cond = 474 cm T = 20.7°C 25 gpm												
Final Turbidity 1.08 0.97 2.31		see page 2 for readings.												
XD SN/Range (PSI) 20.0		1258 Start recovery test (#5 on data logger)												
<b>PART 3</b>		1306 Stop test. Final XD = 26.698'. 99.8% recovery												
<b>INSTANTANEOUS SLUG TEST</b>		Signature: Charles Martinez												
Static Water Level (TOC)		Date: 09/12/03												
Transducer Depth		Signature: L.D. Walker												
Baseline Start		Date: 9/30/03												
Injection Start														
Baseline Start														
Withdrawal Start														
Slug Volume														
XD SN/Range (PSI)														
Prepared by (print name):														
Reviewed by (print name):														

A-6003-644 (03/03)




FIELD ACTIVITY REPORT - DAILY DRILLING							Page <u>2</u> of <u>2</u>
Continuation Page							Date: <u>09/12/03</u>
Well Name: <u>299-E27-22</u>				Well ID: <u>C4124</u>			
Location: <u>East of CTank Farm</u>				Continuation of Report No.: <u>1 (well development)</u>			
Time/Depth		Description of Activities/Operations with Depth					
From	To	well development					
Readings for 214.5' interval (test #4)							
Time	XD (ft)	NTU	Turb	µS/cm COND	T °C	Drawdown	
1224	26.494	3.37	498	20.6	0.267'		
1235	26.349	2.08	508	20.2	0.417'		
1248	26.470	2.69	509	20.6	0.291'		
1254	26.491	1.08	504	20.7	0.270'		
1307 Resetting intake @ 255.4' TOC. Initial XD = 17.809' (test #6)							
1312 Begin test @ 255.4' TOC. Initial readings: XD = 17.545'; Cond 491; T = 21.1°C							
Turb: 24.7 NTU; 24 gpm.							
Readings for 255.4' interval (test #6) on data logger							
Time	XD (ft)	NTU	Turb	µS/cm COND	T °C	Drawdown	
1322	17.629	2.46	488	20.4	0.18'		
1338	17.605	1.49	490	20.3	0.204'		
1348	17.584	2.06	484	20.8	0.225'		
1354	17.422	0.97	490	20.3	0.387'		
1435 Shut pump off. Begin recovery test (#7) (Purge water truck full)							
1404 Stop recovery test (#7) Final XD = 17.806'; 100% recovery							
1400 2nd purge water truck on site. 1st truck off site.							
1406 move intake to next interval (243.3' TOC). XD = 5.901'							
1412 Begin test @ 243.3' TOC (Test #8) Initial readings: XD = 5.446'; T = 21.4°C; COND = 459 µS/cm; Turb = 111 NTU; 23 gpm.							
Readings for 243.3' TOC (Test #8)							
Time	XD (ft)	NTU	Turb	µS/cm COND	T °C	Drawdown	
1428	5.425	4.26	470	20.9	0.476'	1455 Stop test. Begin recovery test	
1438	5.478	2.64	475	20.1	0.423'	1507 Stop rec. test. Final XD = 5.901'. 100%	
1448	5.583	2.67	475	20.3	0.318'	1500 Drill crew securing site. Purge	
1453	5.457	2.31	476	20.2	0.444'	water truck off site. Generator off site.	
Will pull pump on Monday or Tuesday							
Reported By: <u>Charlene Martinez</u>				Reviewed By: <u>L.D. Walker</u>			
Title: <u>Geologist</u>		Date: <u>09/12/03</u>		Title: <u>Geologist</u>		Date: <u>9/30/03</u>	
Signature: <u>Charlene Martinez</u>				Signature: <u>L.D. Walker</u>			

A-6003-652 (04/03)



FIELD ACTIVITY REPORT WELL SERVICES						Page <u>1</u> of <u>1</u>
Date <u>09/19/03</u>	Well No. <u>C4124</u>	Rig Type/Model <u>Pump setting rig</u>	Rig No.	Contract/Work Order No.	Report No. <u>1</u>	
Purpose <u>Install pumps in C403 RCRA wells</u>				Reference	Location <u>East of C-Tank Farm</u>	
HISTORICAL DATA			PUMP SYSTEM CONFIGURATION			
Construction Depth <u>248.1' bgs</u>					Pre-Maintenance	Post-Maintenance
Casing Size <u>4" ID SS 304, Sch. 10</u>	Type <u>+2.2"</u>	Set At <u>228.05'</u>	Pump Type <u>0.5 HP</u>		Grundfos Rediflo2	
Casing Perforations Schedule Interval			Pump Model <u>model 1A104003</u>			
Well Screen(s) Type <u>4" ID SS Sch 10</u>			Tubing Size/Type			
Interval <u>228.05' - 248.02'</u>			Length-Bottom of Tubing to Pump Intake <u>0.98'</u>			
Last Recorded Depth-to-Water <u>233.69' (TOC)</u>			Tubing Length <u>240.0'</u>			
Last Recorded Depth-to-Bottom <u>271.3' (TOC)</u>			Length-Top of Tubing to Reference Point			
Current Depth-to-Water <u>233.4' (TOC)</u>			Pump Intake Set at (Depth) <u>240.96'</u>			
Current Depth-to-Bottom <u>271.3' (TOC)</u>			Reference/Measuring Point (TOC) <u>TOP of CASING</u>			
Start Time <u>0810</u>		Personnel <u>Layne Christensen</u> <u>Dave DeWitt</u> <u>Ken Jones</u> <u>Fluor Hanford</u> <u>Tim Hotell</u> <u>Cham Hill (CHG)</u> <u>Charlene Martinez</u>		Materials Used <u>24 X 10' long, SS 304, Sch. 40, 0.75" OD tremmie pipe.</u>  <u>0.5 HP Grundfos</u>		
End Time						
Time						
Contract Time						
Total Time						
Description of Operations/Remarks						
<u>0810 On site from C4125. Drill crew dropped off pump setting rig. off site to get 0.75" OD SS 304, schedule 40 tremmie pipe &amp; 0.5 HP Grundfos Rediflo2 pump.</u>						
<u>0848 Drill crew on site. Setting up rig. Prepare to install pump.</u>						
<u>0848 FWS (T. Hotell) off site to get pump.</u>						
<u>0904 Missing an adapter (SS coupler from 3/4" to 1/2") to attach pump to tremmie pipe. FWS (T. Hotell) &amp; driller (B. Newitt) working on problem.</u>						
<u>0910 T. Hotell off site looking for an adapter.</u>						
<u>0918 Drill crew off site looking for an adapter.</u>						
<u>0933 Adapter located, drill crew back.</u>						
<u>0934 Begin installing Rediflo2 pump (0.5 HP Grundfos)</u>						
<u>1022 Done.</u>						
<u>1025 mast down on pump setting rig. Off site to C4122 to begin testing pumps.</u>						
<u>1105 Testing pump. Control box not working. End of shift. off site.</u>						
<u>* Note: Pump tested (09/24/03), worked @ 400Hz on control box.</u>						
Report By <u>Charlene Martinez</u>			Reviewed By <u>L.D. Walker</u>			
Title <u>Geologist</u>			Title <u>Geologist</u>		Date <u>9/30/03</u>	
Signature <u>Charlene Martinez</u>			Signature <u>L.D. Walker</u>			

DISTRIBUTION: White-Field File Custodian Yellow-Group Files Pink-Project Coordinator Goldenrod-Team Leader BC-6000-278 (04/91)

<b>WELL SURVEY DATA REPORT</b>					
<b>Project:</b>			<b>Prepared By:</b> Neil P. Fastabend <b>Company:</b> Fluor Federal Services		
<b>Date Requested:</b> 9/29/03			<b>Requestor:</b> Chris S. Wright (FH)		
<b>Date of Survey:</b> 10/31/03			<b>Surveyor:</b> Fluor Federal Services Survey Dept.		
<b>ERC Point of Contact:</b>			<b>Survey Co. Point of Contact:</b> Grant F. Brazil, P.L.S.		
<b>Description of Work:</b>  Civil Survey of Groundwater Monitoring Well C4124 (299-E27-22).			<b>Horizontal Datum:</b> NAD83(91)		
			<b>Vertical Datum:</b> NAVD88		
			<b>Units:</b> Meters		
			<b>Hanford Area Designation:</b> 200E		
<b>Coordinate System:</b> Washington State Plane Coordinates (South Zone)					
<b>Horizontal Control Monuments:</b> 2E-127 (FFS) and 2E-134 (FFS)					
<b>Vertical Control Monuments:</b> 2E-33 (FFS) and 2E-115 (FFS)					
<b>Well ID</b>	<b>Well Name</b>	<b>Easting</b>	<b>Northing</b>	<b>Elevation</b>	
C4124	299-E27-22	575185.10	136685.33		Center of Casing
				193.383	Top Casing, N. Edge
				192.604	Brass Survey Marker
				193.389	Top Pump Base- plate, N. Edge
<b>Notes:</b>					
<b>Surveyor Statement:</b> I, Grant F. Brazil, a Professional Land Surveyor registered in the State of Washington (Registration No. 22326), hereby certify that this report is based on a field survey performed in October, 2003 under my direct supervision, and that the data contained here is true and correct.					

Original to:  
Distribution by DIS:

<p align="center"><i>Waste Management Project</i></p> <p align="center"><b>NONCONFORMANCE REPORT DISTRIBUTION COVERSHEET</b></p>		
<b>From:</b> Quality Assurance	<b>MSIN:</b> T3-02	<b>Date:</b> 10/1/03
<b>NCR No.:</b> WMP-GPP-03NCR-010	<b>STATUS:</b> Initiation [ ] Disposition [ ] Closure [X]	
<b>TO:</b>		<b>MSIN</b>
<i>Responsible Individual</i>	R. L. Biggerstaff	E6-35
<i>Cognizant QA Engineer</i>	W. R. Thackaberry	E6-35
<i>Originator</i>	W. R. Thackaberry	N/A
<i>QA Manager</i>	D. G. Farwick	T3-02
<i>Facility Manager (if applicable)</i>	N/A	N/A
<i>Facility Department Manager/Lead (if applicable)</i>	N/A	N/A
<i>Authoritative Source</i>	D. B. Wegner	N/A
<i>PAAA Compliance Officer</i>	D. J. Riel	N/A
<i>QA NCR Coordinator</i>	S. L. Day	T3-02
<b>OTHER: (if applicable)</b>		<b>MSIN</b>
<i>FH QA Programs</i>	D. D. Volkman	H7-28
<i>Contract Specialist</i>	J. D. Phillips, FFS	H7-10
	C. S. Wright	E6-35
	T. L. Hottell	R4-02
	R. J. Fabre	R4-02
	B. A. Williams, PNNL	K6-81
	D. A. Myers, CH2M <i>(Closed copy only)</i>	E6-35

# NONCONFORMANCE REPORT

Page 1 of 8

1. P.O./W.O./Job Control No. Contract No. 18618		2. Responsible Program, Project, Facility, or SSC GPP/RCRA/WMA C	
3. Item or Material I.D. No./Catalog No./Other Annular Seal		4. Dwg./Spec./Other No./Rev. SOW for Req 100395	
5. Safety Classification GS		6. Lot/Heat/Serial No. Well C4124/299-E27-22	
7. Lot Size/Sample Size/Quantity Accepted N/A		8. ASME Code Item? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No (If yes, notify authorize inspector.)	
9. Supplier Name/Address Layne Christensen Company 9001 Pacific Ave Bldg B Tacoma, WA 98444		10. Suspect / Counterfeit Item? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No (If Yes, Occurrence Report Required)	
		11. Procurement Related? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No (If Yes, Notify Contract Specialist)	

DESCRIPTION OF NONCONFORMANCE	
1	1. The first nonconformance is related to the lack of a formalized process for the identification and control of nonconformances. The process should include the identification of nonconformances, the assignment of responsibility for their resolution, and the implementation of corrective actions to prevent recurrence.
2	2. The second nonconformance is related to the lack of a formalized process for the control of nonconformances. The process should include the identification of nonconformances, the assignment of responsibility for their resolution, and the implementation of corrective actions to prevent recurrence.
3	3. The third nonconformance is related to the lack of a formalized process for the control of nonconformances. The process should include the identification of nonconformances, the assignment of responsibility for their resolution, and the implementation of corrective actions to prevent recurrence.
4	4. The fourth nonconformance is related to the lack of a formalized process for the control of nonconformances. The process should include the identification of nonconformances, the assignment of responsibility for their resolution, and the implementation of corrective actions to prevent recurrence.
5	5. The fifth nonconformance is related to the lack of a formalized process for the control of nonconformances. The process should include the identification of nonconformances, the assignment of responsibility for their resolution, and the implementation of corrective actions to prevent recurrence.
6	6. The sixth nonconformance is related to the lack of a formalized process for the control of nonconformances. The process should include the identification of nonconformances, the assignment of responsibility for their resolution, and the implementation of corrective actions to prevent recurrence.
7	7. The seventh nonconformance is related to the lack of a formalized process for the control of nonconformances. The process should include the identification of nonconformances, the assignment of responsibility for their resolution, and the implementation of corrective actions to prevent recurrence.
8	8. The eighth nonconformance is related to the lack of a formalized process for the control of nonconformances. The process should include the identification of nonconformances, the assignment of responsibility for their resolution, and the implementation of corrective actions to prevent recurrence.
9	9. The ninth nonconformance is related to the lack of a formalized process for the control of nonconformances. The process should include the identification of nonconformances, the assignment of responsibility for their resolution, and the implementation of corrective actions to prevent recurrence.
10	10. The tenth nonconformance is related to the lack of a formalized process for the control of nonconformances. The process should include the identification of nonconformances, the assignment of responsibility for their resolution, and the implementation of corrective actions to prevent recurrence.

12. Description of Nonconformance	
-----------------------------------	--

(a) Required Condition/Origin of Requirement	(b) Description of Requirement	(c) Date of Requirement	(d) Status of Requirement

Contract 18618 Statement of Work figure 3, The CY03 RCRA Groundwater Monitoring Well Diagram shows bentonite granular seal occupying the annular space between the 4 inch diameter permanent casing and the borehole wall in the interval between the Bentonite pellet seal (above the filterpack) and the cement grout (surface) seal.

(b) Actual Condition

A 170 ft. segment of 1/4" galvanized carbon steel pipe was lost within the granular bentonite annular seal. The bottom of the pipe is reported to be at 217.2 feet below ground surface. This just is above the 5 foot bentonite pellet seal. The top of the lost pipe is 47 feet below ground surface. It is entirely contained within the annular seal and is neither wetted nor in contact with sand pack/screened interval. The 1/4" pipe was being used to measure depth to top of permanent materials being placed in the hole during well completion when a coupling failed and the segment was lost. At the time the pipe was lost the 4 inch permanent casing was encircled by a 6 in ID inner casing and a 9 inch OD outer casing. The presence of these two casings would cause the lost pipe to be isolated from the formation (borehole wall) by at least 2.5 inches of bentonite crumbles. See attached sketch.

Contract Specialist Acknowledgement

Date \_\_\_\_\_

NCR IDENTIFICATION / VALIDATION

13. NCR Initiator *13.11.11*

Date \_\_\_\_\_

14. NCR Validation, Initiating Organization QA Manager or designee.

Date \_\_\_\_\_

## NONCONFORMANCE REPORT (continued)

NCR No. WMP-GPP-03NCR-010

Page 2 of 8

### DISPOSITION

15. Interim Disposition (Check One) ☒ N/A (See Final Disposition) ☐ Conditional Accept/Use ☐ Other

Use only if actions are needed prior to determining final disposition or to facilitate continued work or testing on a conditional and controlled basis

Technical Justification, USQ or CX No. \_\_\_\_\_, required for "Conditional Accept/Use" disposition. Include the extent and any required instructions.

### APPROVAL

15.1 Design Authority or ☐ N/A if not applicable

Print Full Name

Signature

Date

15.2 Responsible Organization's QA Representative or Manager or ☐ N/A if not applicable

Print Full Name

Signature

Date

15.3 ASME Authorized Code Inspector or ☐ N/A if not applicable

Print Full Name

Signature

Date

15.4 Other or ☐ N/A if not applicable

Organization/Discipline Represented \_\_\_\_\_

Print Full Name

Signature

Date

### INTERIM DISPOSITION COMPLETION

16. Interim Disposition Complete (Check One) ☐ Complete ☐ N/A if not applicable

Responsible Organization QA or QC Representative

Print Full Name

Signature

Date

### FINAL DISPOSITION

17. Final Disposition (Check One)

☒ Accept-As-Is ☐ Reject ☐ Repair ☐ Rework

(a) Technical Justification or Engineering Document Change (EDC), Facility Modification Package (FMP), or Design Change Notice (DCN) Number N/A See 17(b) (required for "Accept-As-Is" and "Repair" dispositions.) If EDC, FMP, or DCN Number is not required, explain why and perform USQ screening in accordance with applicable procedure. USQ or CX No. \_\_\_\_\_

Use N/A for "Reject" or "Rework" dispositions.

The 1/4" diameter tube (170 ft long) was encapsulated within bentonite backfill. The conical shape of the shoe of the working string forced the tube to lay up against the 4" SS riser. This resulted in a minimum of 2 1/4" of bentonite sealant between the tube and the formation wall. This is consistent with WAC 173-160 regulations, and was approved by Ecology (oral conversation, followed by E-mail message. Water quality sampling will not be affected by the presence of the tube since the bottom of the tube is 11 ft above the water table.

## NONCONFORMANCE REPORT (continued)

NCR No. WMP-GPP-03NCR-010

Page 3 of 8

(b) Instructions for Completion. For "Repair" and Rework," include Inspection Criteria. For "Reject," identify method of disposal, e.g., scrap, return to vendor or other.

Use N/A for "Accept-As-Is."

This well will be as-built on a Well Summary Sheet which will be entered into RMIS.  
Assure that the presence of the pipe is documented on the Well Summary Sheet for C4124.

### APPROVAL

17.1 Design Authority

Richard L. Biggerstaff

Print Full Name

Signature

9/15/03  
Date

17.2 Responsible Organization's QA Representative or Manager

WR Thackaberry

Print Full Name

Signature

9-15-03  
Date

17.3 ASME Authorized Code Inspector or ☒ N/A if not applicable

Print Full Name

Signature

Date

17.4 Other or ☐ N/A if not applicable

Organization/Discipline Represented Manager Groundwater Remediation

Jane Borghese

Print Full Name

Signature

9-15-03  
Date

### CLOSURE

18. NCR Closure ☒ Approved Disposition Actions Complete and Verified ☐ Follow-on NCR

QA or QC Representative

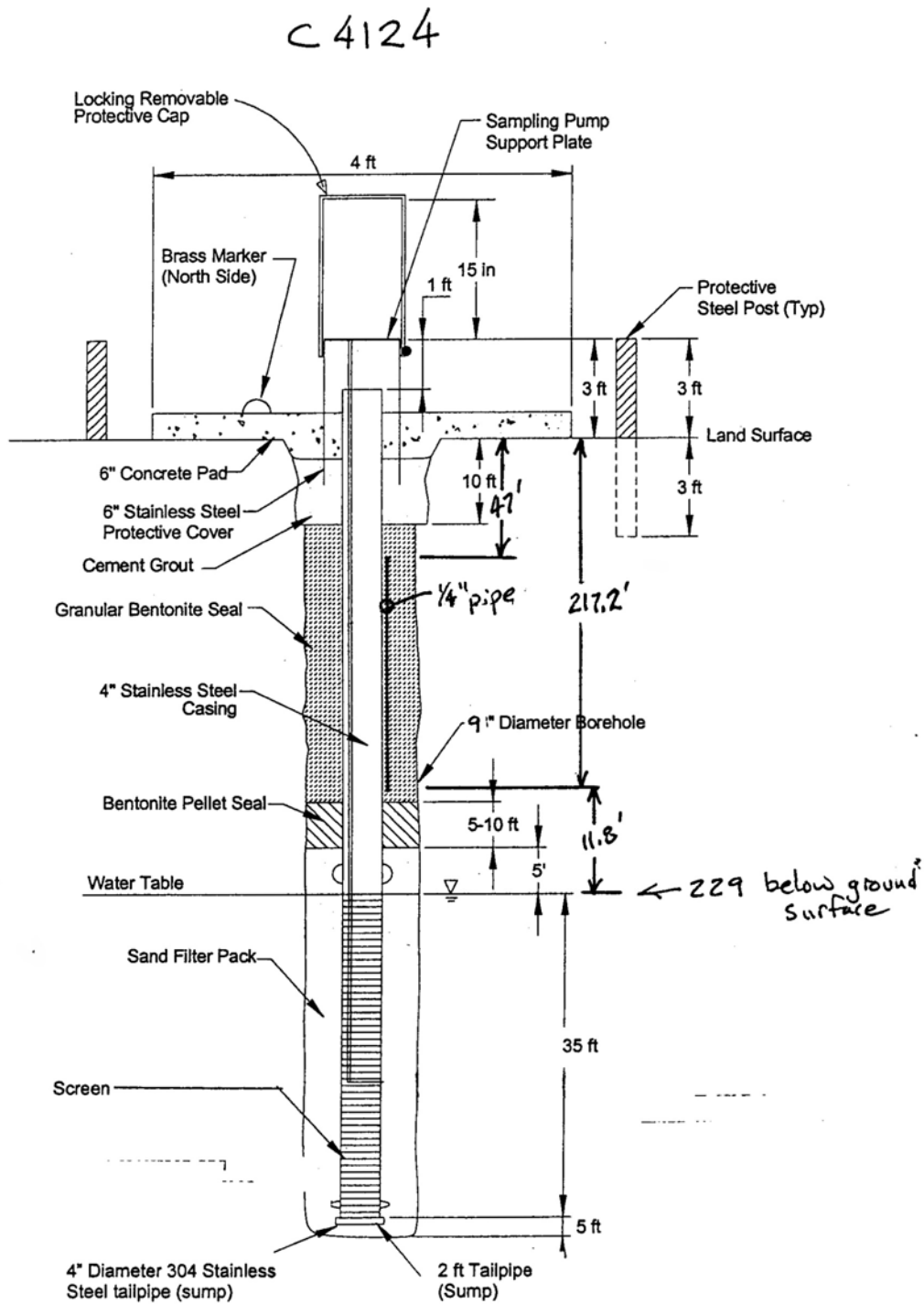
W. R. Thackaberry

Print Full Name

Signature

9-29-03  
Date

Figure 3. CY03 RCRA Groundwater Monitoring Well Diagram.



\* Not To Scale



**Thackaberry, W R (Bill)**

---

**From:** Caggiano, Joseph [Jcag461@ECY.WA.GOV]  
**Sent:** Wednesday, September 10, 2003 3:30 PM  
**To:** 'Biggerstaff, Dick L'  
**Cc:** Wright, Christopher S; Thackaberry, W R (Bill); Fruchter, Jonathan S  
**Subject:** FW: well C4124 lost 1/4" pipe  
**Importance:** High

I copied your message into a Word file, turned on the Track Changes feature, and made a few changes to clarify meaning.

Please proceed as we agreed and as stipulated below. If there are changes from this plan, please contact me. Please be sure to include the tremie pipe in the as-built drawing of the well to be entered into HWIS and, as always, include paper copy of this electronic correspondence in the construction report for this well.

Please conduct an investigation into this accident and correct field procedures to guard against future occurrences of this type.

-----Original Message-----



**From:** Biggerstaff, Dick L [mailto:Dick\_L\_Biggerstaff@RL.gov]  
**Sent:** Wednesday, September 10, 2003 11:32 AM  
**To:** Caggiano, Joseph  
**Cc:** Wright, Christopher S; Thackaberry, W R (Bill); Borghese, Jane V; Williams, Bruce A; Fruchter, Jonathan S  
**Subject:** well C4124 lost 1/4" pipe  
**Importance:** High

Joe—This is to confirm our telecom earlier this morning concerning well 299-E27-22 (C4124). The rig on this well is a dual wall percussion type with limited space between the 4" SS and the 6" ID inner casing. Approximately 170 feet of 1/4" galvanized pipe (being used to tag backfill) was lost (coupling unscrewed) in the hole with the top at ~47 ft and the base at 217.2 ft bgs, just above the 5 ft bentonite pellet seal placed over the sand pack. The groundwater is at 229 ft bgs, or 11.8 ft below the bottom of the pipe. Multiple attempts have been made to fish the pipe out of the hole; however, there is just no annular space to work in, and all attempts have been futile. The plan we discussed is to place bentonite crumbles through the zone and to within 10 ft of the surface, thus encapsulating the pipe within the bentonite crumbles between the 4" SS completion and the formation. Because of the down-hole working system, the 1/4" pipe will be pressed up against the side of the 4" SS as the backfill operation continues. Since the outer temporary casing is 9" OD, there will be sufficient bentonite to provide an adequate seal after it is removed. The upper 10 ft of the hole will be cemented consistent with the prior-approved drilling plan. Please confirm your understanding and approval of this communication by return E-mail

9/10/2003

Joe--This is to confirm our telecom earlier this morning concerning well 299-E27-22 (C4124). The rig on this well is a dual wall percussion type with limited space between the 4" SS and the 6" ID inner casing. Approximately 170 feet of 1/4" galvanized pipe (being used to tag backfill) was lost (coupling unscrewed) in the hole with the top at ~47 ft and the base at 217.2 ft bgs, just above the 5 ft bentonite pellet seal placed over the sand pack. The groundwater is at 229 ft bgs, or 11.8 ft below the bottom of the pipe. Multiple attempts have been made to fish the pipe out of the hole; however, there is just no annular space to work in, and all attempts have been futile. The plan we discussed is to place bentonite crumbles through the zone containing and including the galvanized tremie pipe (i.e., 47 to 217.2 ft. bgs) and to within 10 ft of the surface, thus encapsulating the pipe within the bentonite crumbles between the 4" SS completion and the formation. Because of the down-hole working system, the 1/4" pipe will be pressed up against the side of the 4" SS as the backfill operation continues.

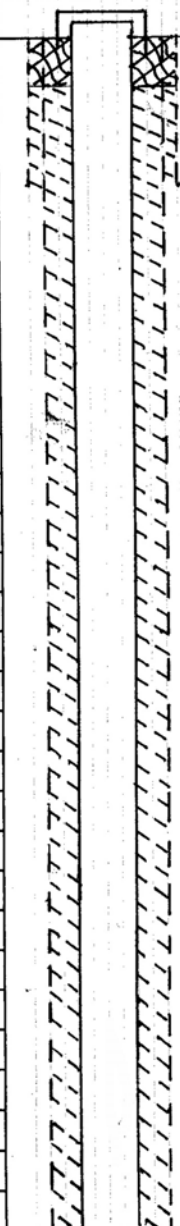
Since the outer temporary casing is 9" OD, there will be sufficient bentonite to provide an adequate annular seal after it is removed. The upper 10 ft of the hole will be cemented consistent with the prior-approved drilling plan. Please confirm your understanding and approval of this communication by return E-mail

WELL SUMMARY SHEET		Start Date: 08/21/03		Page 1 of 2	
		Finish Date: 09/10/03			
Well ID: C4124		Well Name: 299-E27-22			
Location: East of C-Tank Farm		Project: C403 RCRA drilling			
Prepared By: Charlene Martinez	Date: 09/11/03	Reviewed By: L.D. Walker	Date: 9/15/03		
Signature: <i>Charlene Martinez</i>		Signature: <i>L.D. Walker</i>			
CONSTRUCTION DATA		GEOLOGIC/HYDROLOGIC DATA			
Description	Diagram	Depth in Feet	Graphic Log	Lithologic Description	
9" OD dual-wall temporary casing used.		0		0'-1' Backfill (crushed gravel)	
				1'-5' SAND(S)	
6" OD protective casing set + 1.0' above permanent.				5'-10' gravelly SAND(gS)	
				10'-29' SAND(S)	
4" ID 55304 sch 10 riser: + 2.2' → 228.05'				29'-36' sandy GRAVEL(SG)	
				36'-50' SAND(S)	
				50'-54' sandy GRAVEL(SG)	
				54'-56' SAND(S)	
				56'-60' sandy GRAVEL(SG)	
Portland Cement Grout: 0' → 10.0'				60'-72' silty sandy GRAVEL(msG)	
				72'-81.5' silty gravelly SAND(msG)	
				81.5'-89' SAND(S)	
Granular Bentonite: 10.0' → 217.2'				89'-98' silty SAND(ms)	
				98'-105' SAND(S)	
				105'-112' silty SAND(ms)	
1/4" Bentonite Pellets: 217.2' → 222.5'				112'-116' SAND(S)	
				116'-122' silty SAND(ms)	
10-20 mesh Silica Sand: 222.5' → 226.0'				122'-138' SAND(S)	
				138'-145' silty SAND(ms)	
				145'-153' gravelly silty SAND(gms)	
		153'-157' silty sandy GRAVEL(msG)			
		157'-165' sandy GRAVEL(SG)			
		165'-185' SAND			
		185'-188' silty sandy GRAVEL(msG)			
		188'-192' silty SAND(ms)			
		192'-215' sandy GRAVEL(SG)			
		215'-219' gravelly SAND(gS)			
		219'-222' silty sandy GRAVEL(msG)			
		222'-227' SAND(S)			
		227'-233' silty sandy Gravel (msG)			
All depths in feet below ground surface:					
All temporary casing removed from ground.					
170' of 1/4" OD pipe remain in ground (bentonite seal) from 47'-217'					

A-6003-643 (03/03)

A-6003-643 (03/03)

## **Well 299-E27-4**

WELL SUMMARY SHEET		Start Date: 08/12/03		Page 1 of 2	
		Finish Date: 08/20/03			
Well ID: C4125		Well Name: 299-E27-4			
Location: west of C-Tank Farm		Project: C403 RCRA drilling			
Prepared By: Charlene Martinez	Date: 09/05/03	Reviewed By: L.D. Walker	Date: 9/5/03		
Signature: <i>Charlene Martinez</i>		Signature: <i>L.D. Walker</i>			
CONSTRUCTION DATA		GEOLOGIC/HYDROLOGIC DATA			
Description	Diagram	Depth in Feet	Graphic Log	Lithologic Description	
10 5/8" OD casing to 30' bgs		0	AAAA	0'-2' Backfill (Crushed Gravel)	
9" OD dual-wall temporary casing to 311' bgs				2'-20' SAND(S)	
				20'-22' Sandy GRAVEL(SG)	
				22'-45' SAND(S)	
6" ID ss protective casing set + 1.0' above permanent					
			40		45'-50' gravelly SAND(gS)
4" ID SS 304 schedule 10 riser: + 1.9' → 270.32'					50'-80' SAND(S)
Portland Cement Grout: 0' → 9.9'			80		80'-110' gravelly SAND(gS)
Granular Bentonite: 9.9' → 259.0'					110'-195' SAND(S)
			120		
			160		
All temporary casing removed from ground:					
All depths in feet below ground surface.		200		195'-200' Sandy GRAVEL(SG)	
				200'-225' SAND(S)	
				225'-235' silty SAND(mS)	
				235'-240' SAND(S)	

A-6003-643 (03/03)





WELL CONSTRUCTION SUMMARY REPORT						Start Date: 08/12/03	
						Finish Date:	
						Page 1 of 1	
IID: C4125		Well Name: 299-E27-4		Approximate Location: West of C-Tank Farm			
Project: C403 RCRA drilling				Other Companies: F H, CH G			
Drilling Company: Layne Christensen				Geologist(s): C. Martinez, M.J. Hocking			
Driller: Paul "Derry" Loder License #: 16228							
TEMPORARY CASING AND DRILL DEPTH			DRILLING METHOD		HOLE DIAMETER (in.) / INTERVAL (ft)		
*Size/Grade/Lbs. Per Ft.	Interval	Shoe O.D./I.D.	Auger: Hollow Stem		Diameter 9" From 0' to 30'		
Dual-wall carbon steel, FS	0' - 311'	9"	Cable Tool:		Diameter _____ From _____ to _____		
9" OD (outer); 7 1/16" Inner	_____ - _____		Air Rotary:		Diameter _____ From _____ to _____		
	_____ - _____		A.R. w/Sonic:		Diameter _____ From _____ to _____		
10 5/8" (10"), Carbon	0 - 30'	10 5/8" (10")	Becker Hammer		Diameter 9" From 30' to 311'		
steel, FS	_____ - _____		(Reverse Air.)		Diameter _____ From _____ to _____		
*Indicate Welded (W) - Flush Joint (FJ) Coupled (C) & Thread Design					Diameter _____ From _____ to _____		
			Drilling Fluid: none				
Total Drilled Depth: 311'		Hole Dia @ TD: 9"		Total Amt. Of Water Added During Drilling: N/A			
Well Straightness Test Results: Passed using a 20.4' long, 4.5"				Static Water Level: 270.65'		Date: 08/20/03	
ED tool on 08/19/03							
GEOPHYSICAL LOGGING							
Sondes (type)	Interval	Date	Sondes (type)	Interval	Date		
Spectra Gamma	0' - 309'	08/15 & 08/16 2003		_____ - _____			
	_____ - _____			_____ - _____			
	_____ - _____			_____ - _____			
COMPLETED WELL							
Size/Wt./Material	Depth	Thread	Slot Size	Type	Interval Annular Seal/Filter Pack	Volume	Mesh Size
4" 20 22 304 sch. 10 riser	11.9' - 270.32'	F480	N/A	Portland Cement (94#)	0 - 9.9'	6 bags	N/A
4" 20 22 304 sch. 10 well screen	270.32' - 305.33'	"	0.020"	Granular Bentonite (50#)	9.9' - 259.0'	99 bags	N/A
4" 20 22 304 sump	305.33' - 307.76'	"	N/A	Bentonite Pellets (50#)	259.0' - 264.4'	2 buckets	1/4"
	_____ - _____			Colorado Silica Sand (50#)	264.4' - 309.0'	23 bags	10-20
	_____ - _____				_____ - _____		
OTHER ACTIVITIES							
Aquifer Test:		Date:		Well Decommission:		Yes:	No: Date:
Description:				Description:			
WELL SURVEY DATA (if applicable)							
				Protective Casing Elevation:			
Washington State Plane Coordinates:				Brass Survey Marker Elevation:			
COMMENTS / REMARKS							
vol. calcs: P.C. => 6 bags * 1.285 ft <sup>3</sup> /bag = 7.71 ft <sup>3</sup> ; Gravel => 99 bags * 0.71 ft <sup>3</sup> /bag = 70.29 ft <sup>3</sup> . Pellets => 2 buckets * 0.62 ft <sup>3</sup> /bucket = 1.24 ft <sup>3</sup> ; 10-20 sand => 23 bags * 0.535 ft <sup>3</sup> /bag = 12.31 ft <sup>3</sup>							
Reported By:		Title:		Signature:		Date:	
Charlene Martinez		Geologist		Charlene Martinez		09/09/03	

A-6003-658 (04/03)

# WELL ATTRIBUTES REPORT

FIELD ORDER NO

ELL ID

WELL NAME

HOST WELL ID

C 4125  
299-E27-4

DRILL DATE

CONST DATE

CONST DEPTH

08/12/03  
08/12/03  
307.76'

LAST INSPECTION

NORTHING

EASTING

ELEVATION

MEASUREMENT INFORMATION		
	LAST	CURRENT
A DEPTH TO WATER(ft)	274.21'(TOC)	274.19'(TOC)
DEPTH TO WATER DATE	09/19/03	09/29/03
B DEPTH TO BOTTOM(ft)	311.35'(TOC)	n/a
DEPTH TO BOTTOM DATE	09/19/03	n/a
C STICK UP(ft)	2.88'	2.88'
D REFERENCE MARK(ft)		
REFERENCE MARK IS TOC	<input checked="" type="checkbox"/> YES <input type="checkbox"/> NO <input type="checkbox"/> ND*	<input checked="" type="checkbox"/> YES <input type="checkbox"/> NO

PERFORATION INFORMATION			
CASING SIZE	TOP	BOTTOM	CUTS/FT/ROUND

CHANGES

g.w. => 274.21' - 0.02' (landing plate) =  
274.19' TOC

CASING INFORMATION

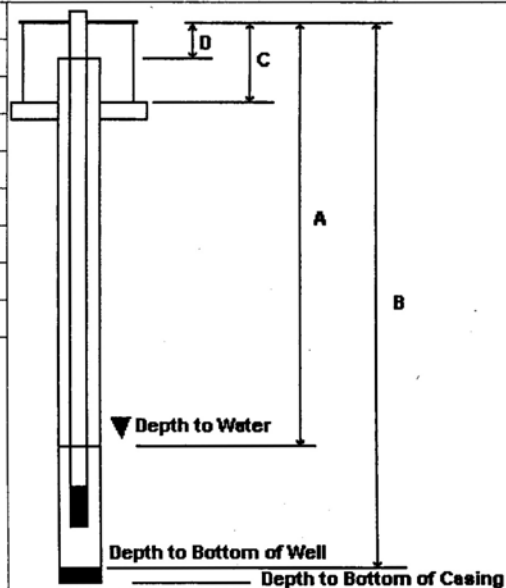
SIZE	TOP	BOTTOM	MATERIAL	TYPE	CONNECTION	THICKNESS
4" ID	41.9'	270.32'	stainless steel	304; sch. 10		

CHANGES

SCREEN INFORMATION

SIZE	TOP	BOTTOM	MATERIAL	TYPE	SLOT SIZE
4" ID	270.32'	305.33'	stainless steel	304; schedule 10	0.020-inch

CHANGES



A DEPTH TO WATER FROM TOP OF CASING  
B DEPTH TO BOTTOM OF WELL FROM TOP OF CASING  
C TOP OF CASING TO GROUND SURFACE/PAD  
D TOP OF CASING TO SURVEY REFERENCE MARKER

BOREHOLE LOG						Page <u>1</u> of <u>2</u>
						Date: <u>08/12/03</u>
Well ID: <u>C4125</u>		Well Name: <u>299-E27-4</u>		Location: <u>West of C-Tank Farm</u>		
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample	Blows Recovery	Graphic Log	Sample Description	Comments	
0	H.S.	N/A	△△△	0'-2' Backfill. Crushed basaltic gravel	med-risk 0-30' bgs.	
5	Grab H.S.		△△△	2'-20' Sand (S) 100% sand, R, v. well sorted, vfn-fn grained, non-basaltic.	Hollow-stem auger used to 30' bgs. 10 9/8" OD	
10	Grab H.S.		△△△	2.5Y4/2 olive brown, moist. Strong rxn HCl.	single-wall casing used to 30' bgs. E.O.S. 08/12/03	
15	Grab H.S.		△△△	20'-22' Sandy GRAVEL (SG) 65% gravel, 35% sand. Gravel, poorly sorted, SR-SA, sm pebbles-sm cobbles basaltic. Sand, vfn-fn grain, R.	Collect 10' archive	
20	Grab H.S.		△△△	Trace mica, non-basaltic, 2.5Y4/3 olive brown, moist. mod rxn HCl.		
25	Grab H.S.		△△△	22'-45' SAND (S) 85% sand, 6% silt, 9% gravel. Gravel, well-sorted, pea-size, SR-R, basaltic. Sand, mod-sorted, vfn-med grain, SR-SA, 2.5Y4/2, dark grayish brown, moist. No rxn HCl trace mica.	Collect 15' archive	
30	Grab 8 1/4"		△△△		Collect 20' archive	
35	Grab 8 1/4"		△△△	@ 35' Sand, poorly sorted, vfn-vcoarse grained, SR-SA, 45% silt/clay, 35% basalt silt content down. No gravel. 2.5Y5/2 grayish brown, moist. No rxn HCl.	Collect 25' archive	
<div style="display: flex; justify-content: space-between;"> <div> <p>Reported By: <u>Charlene Martinez</u></p> <p>Title: <u>Geologist</u></p> <p>Signature: <u>Charlene Martinez</u></p> </div> <div> <p>Reviewed By: <u>L.D. Walker</u></p> <p>Title: <u>Geologist</u></p> <p>Signature: <u>L.D. Walker</u></p> </div> </div>						
		Date:	Date: <u>9/30/03</u>			

A-6003-642 (03/03)

BOREHOLE LOG					Page <u>2</u> of <u>8</u>
					Date: <u>08/13/03</u>
Well ID: <u>C4125</u>		Well Name: <u>299-E27-4</u>		Location: <u>west of C-Tank Farm</u>	
Project: <u>C403 RCEA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>	
Depth (Ft.)	Sample Type No.	Blows Recovery	Graphic Log	Sample Description <small>Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl</small>	Comments <small>Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level</small>
40	8th 9" Grab 8th 9"	N/A		@ 40' trace basaltic gravel. mes ~ 3"	Becker Hammer using 9" OD dual-wall casing Collect 40' archive
45	Grab 8th 9"			@ 45' - 50' GRAVELLY SAND (GS) 15% gravel, 80% sand, 5% silt, Gravel, well-sorted, pea-size to 3m pebbles, basaltic, R-SH. Sand, poorly sorted, fin-vcse grained, micaceous, 55% qtz/other 45% basalt, No rxn HCl.	Collect 45' archive
50	Grab 8th 9"			50' - 55' SAND (S) 95% sand, 5% silt, Sand, poorly sorted, SR-SH, vcn-vcse, 55% qtz/other, 45% basalt, micaceous. No rxn HCl.	Collect 50' archive
55	Grab 8th 9"				Collect 55' archive
60	Grab 8th 9"				Collect 60' archive
65	Grab 8th 9"			@ 65' trace of pea-size basaltic gravel	Collect 65' archive
70	Grab 8th 9"			@ 70' trace of pea-size basaltic gravel	Collect 70' archive
75	Grab 8th 9"			@ 75' ~ 2% pea size basaltic gravel	Collect 75' archive


Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>08/13/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>3</u> of <u>8</u>
						Date: <u>08/13/03</u>
Well ID: <u>C4125</u>		Well Name: <u>299-E27-4</u>		Location: <u>west of C-Tank Farm</u>		
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample	Blows Recovery	Graphic Log	Sample Description	Comments	
	Type No.			Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level	
80	Grab BH 9"	N/A		80'-110' gravelly sand (s) 20% gravel	Becker Hammer using	
	Grab BH 9"			25% sand, 5% silt. Gravelly, well sorted, SR-R, 45% basalt, 35% gtz	9"OD dual-wall casing	
	↓			other, pea-size-sm pebbles. Sand, poorly sorted, SR-SA, vfn-vese, 45% basalt,	Collect 80' archive	
85	Grab BH 9"			55% gtz/other. No rxn HCl, micaceous	Collect 85' archive	
	↓			@ 85' gravel down to 15% pred.		
	↓			pea-size basaltic, SR-R		
90	Grab BH 9"				Collect 90' archive	
	↓					
95	Grab BH 9"			@ 95' gravel increasing to 20% mod sorted, increasing to sm pebbles	Collect 95' archive	
	↓					
100	Grab BH 9"		@ 100' sand mod sorted, basalt content decreasing to 45%. Gravel decreasing to 12%.	Collect 100' archive		
	↓					
105	Grab BH 9"		@ 105' gravel decreasing to 10%	Collect 105' archive		
	↓					
110	Grab BH 9"		110' - 115' SAND(S) 24% sand, 6% silt. Sand, mod sorted, med-vese, SR-SA	Collect 110' archive		
	↓		40% basalt, 60% gtz/other micaceous			
	↓		25% silt grayish brown dry no rxn HCl.			
115	Grab BH 9"		@ 115' sand grading to poorly sorted, vfn-vese, SR-SA.	Collect 115' archive		
	↓					


Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>08/13/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>4</u> of <u>8</u>
						Date: <u>08/13/03</u>
Well ID: <u>C4125</u>			Well Name: <u>299-E27-4</u>		Location: <u>west of C-Tank Farm</u>	
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample		Graphic Log	Sample Description		Comments
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl		Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level
120	BH 9" Grab BH 9"	N/A		@120' sand, v poorly sorted, vfn-vcse grained, pred. cse-vcse. Trace gravel sm pebbles, mps ~ 0.5". silt ~ 6%		Becker Hammer using 9" OD dual-wall casing Collect 120' archive
125	Grab BH 9"			@125' Increase in basaltic, pea-size gravel (~ 8%) sand, 50% basalt, 50% qtz/other. 6-7% silt.		Collect 125' archive
130	Grab BH 9"			@130' pea-size basaltic gravel. Sand, poorly sorted, SR-SA, vfn-vcse. 6-7% silt.		Collect 130' archive
135	Grab BH 9"			@135' still pea-size basaltic gravel		Collect 135' archive
140	Grab BH 9"			@140' pea-size gravel, basaltic. Sand vfn-vcse grain, poorly sorted, SR-SA. silt ~ 6%, 50% qtz/other 50% basalt. No rxn HCl.		Collect 140' archive
145	Grab BH 9"			@145' sand grading to med-sorted med-vcse grain no gravel.		Collect 145' archive
150	Grab BH 9"			@150' ~ 8% basaltic, pea-size gravel. Sand, SR-sh, med-vcse grained, 50% basalt, 50% qtz/other, no rxn HCl.		Collect 150' archive
155	Grab BH 9"					Collect 155' archive

Reported By: <u>Charlene Martinez</u>			Reviewed By: <u>L.D. Walker</u>		
Title: <u>Geologist</u>			Title: <u>Geologist</u>		
Signature: <u>Charlene Martinez</u>	Date: <u>08/13/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>		

A-6003-642 (03/03)

BOREHOLE LOG					Page <u>5</u> of <u>8</u>
					Date: <u>08/13/03</u>
Well ID: <u>C4125</u>		Well Name: <u>29A-E27-4</u>		Location: <u>West of C-Tank Farm</u>	
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>	
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level
160	<u>Grab</u> <u>BH 9"</u>	<u>N/A</u>		@160' trace pea-size gravel (< 5%), basaltic. Sand, SR-SA, poorly sorted, fn-vase, 50% ptzlother, 50% basalt	Becker Hammer using 9" OD dual-wall casing collect 160' archive
165	<u>Grab</u> <u>BH 9"</u>				collect 165' archive
170	<u>Grab</u> <u>BH 9"</u>			@170' trace pea-size basaltic gravel.	collect 170' archive
175	<u>Grab</u> <u>BH 9"</u>			@175' sand grading to med-sorted, SR-SA, 50% ptzlother, 50% basalt, med-vase	collect 175' archive
180	<u>Grab</u> <u>BH 9"</u>			@180' sand grading to poorly-sorted, SR-SA vfn-vase grained, 50% basalt, 50% ptzlother	collect 180' archive
185	<u>Grab</u> <u>BH 9"</u>			@185' pea-size basaltic gravel (~ 8%)	collect 185' archive
190	<u>Grab</u> <u>BH 9"</u>			@190' pea-size to small pebbles (~ 8%) pred. basaltic. Sand, v. poorly sorted, vfn-vase grain, SR-SA. Silt 6-7%.	collect 190' archive
195	<u>Grab</u> <u>BH 9"</u>			195' - 200' Sandy GRAVEL (SG) 45% gravel, 50% sand, 5% silt. Gravel, v. well-sorted, SR-L, basaltic, pea-silt. Sand, med-sorted, m-vase grained, 40% basalt, 60% ptzlother, SR-SA, no rxn HCl	collect 195' archive

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>08/13/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)



BOREHOLE LOG					Page <u>6</u> of <u>8</u>
					Date: <u>08/13/03</u>
Well ID: <u>C4125</u>		Well Name: <u>299-E27-4</u>		Location: <u>west of C-Tank Farm</u>	
Project: <u>CY 03 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>	
Depth (Ft.)	Sample	Blows Recovery	Graphic Log	Sample Description	Comments
	Type No.			Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level
200	Grab BH 9"	n/a		200'-225' SAND (S) 5% gravel, 90% sand, 5% silt. Gravel, SR-SA, basaltic, pea-size, well sorted. Sand, poorly sorted, vfn-vco, SR-SA, 40% Basalt, 60% qtz other. No rxn HCl.	Recker Hammer using 9" OD dual-wall casing collect 200' archive P.M. RCT ok. All okay
205	Grab BH 9"				collect 205' archive
210	Grab BH 9"				collect 210' archive
215	Grab BH 9"			215' no trace gravel. silt content same sand, SR-SA, poorly sorted.	collect 215' archive
220	Grab BH 9"			220' sand, grading to med-sorted, vfn-med grain, few coarse grains. 40% basalt, 60% qtz other.	collect 220' archive
225	Grab BH 9"			225'-235' silty SAND (ms) 85% sand, 12% silt. Sand, SR-SA, med-sorted, vfn-co, 40% basalt, 60% qtz other. No rxn HCl. micaceous	collect 225' archive
230	Grab BH 9"			230' sand grading to well-sorted, vfn-fn, silt same.	collect 230' archive
235	Grab BH 9"			235'-240' SAND (S) 95% sand, 5% silt. Sand, vfn-fn, v. well sorted, R, non-basaltic, micaceous, 2.54/2 light brownish gray (dry) No rxn HCl.	collect 235' archive

Reported By: <u>Charlene Martinez</u>	Reviewed By: <u>L.D. Walker</u>
Title: <u>Geologist</u>	Title: <u>Geologist</u>
Signature: <u>Charlene Martinez</u>	Signature: <u>L.D. Walker</u>
Date: <u>08/13/03</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>7</u> of <u>8</u>
						Date: <u>08/13/03</u>
Well ID: <u>C4125</u>		Well Name: <u>299-E27-4</u>		Location: <u>west of C-Tank Farm</u>		
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample	Blows Recovery	Graphic Log	Sample Description	Comments	
	Type No.			Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level	
240	BA 2" Grab BH 2"	N/A		240' - 245' gravelly sand (gs) 15% gravel, 80% sand, 5% silt. Gravel, well-sorted, basaltic, sm- pebbles. SR-R, sand, poorly sorted SR-SA, vfn-vcse, 40% basalt, 40% qtz/other	Recker Hammer using 9" OD dual-wall casing collect 240' archive	
245	Grab BH 2"			245' - 255' Sandy GRAVEL (SG) Gravel 45% sand 50% silt 5% Gravel well sorted. SR-SA, 45% basalt, 35% qtz/other, sm- pebbles. Sand poorly sorted. SR-SA, vfn-vcse, 45% basalt, 55% qtz/other. No rxn HCl. micaceous.	Collect 245' archive	
250	Grab BH 2"			250' - 255' gravel, med-sorted, mps ~ 2"	Collect 250' archive r.m. I Hcl. N Hg & organics < detect	
255	Grab BH 2"			255' - 272' GRAVEL (G) 85% gravel, 10% sand, 5% silt. Gravel, med-sorted, SR-SA 80% basalt, 20% qtz/other, pea-size. (predominant) occasional med-pebbles. mps ~ 2.5". Sand, poorly sorted, vfn-vcse, SR-SA, 45% basalt, 55% qtz/other. No rxn HCl.	Collect 255' archive	
260	Grab BH 2"				Collect 260' archive	
265	Grab BH 2"			272' - 311' Sandy GRAVEL (SG) 55% gravel, 40% sand, 5% silt. Gravel, med-sorted, SR-R, 45% basalt, 55% qtz/other, mps ~ 3". Sand, poorly sorted, pred. cse-vcse grained. SR-SA, increase in basalt content. 80% basalt, 20% qtz/other	Collect 265' archive RCT performed thorough survey of spoils. @ background (0'-270')	
270	Grab BH 2"	sieve sample			Collect 270' archive collect sieve analysis sample (from cyclone) between 270' - 271' hgs	
275	Grab BH 2"				Collect 275' archive	
Reported By: <u>Charles Martinez</u>				Reviewed By: <u>L.D. Walker</u>		
Title: <u>Geologist</u>				Title: <u>Geologist</u>		
Signature: <u>Charles Martinez</u>		Date: <u>08/13/03</u>		Signature: <u>L.D. Walker</u>		
				Date: <u>9/30/03</u>		

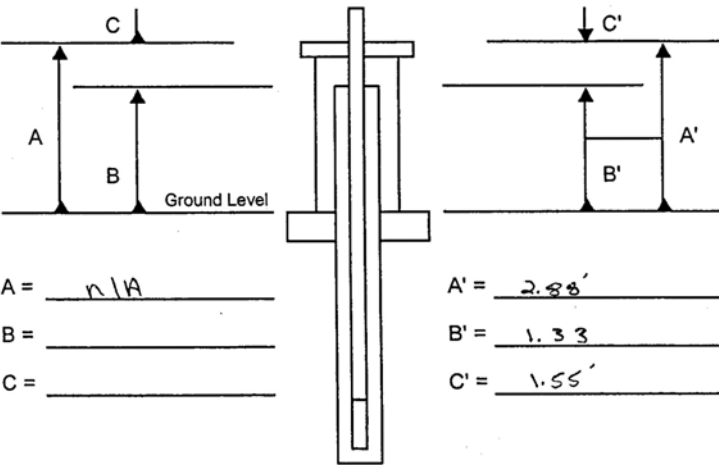
A-6003-642 (03/03)

BOREHOLE LOG					Page <u>8</u> of <u>8</u>
					Date: <u>08/13/03</u>
Well ID: <u>C4125</u>		Well Name: <u>299-E27-4</u>		Location: <u>west - of C-Tank Farm</u>	
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>	
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level
280	BH 9"	NIA			Becker Hammer using 9" OD dual-wall casing collect 280' archive
	Grab BH 9"				
285	Grab BH 9"			@ 285' gravel size decreasing sm-med pebbles, some sm cobbles. Increased basalt content	collect 285' archive
	Grab BH 9"				
290	Grab BH 9"				Collect 290' archive
	Grab BH 9"				
295	Grab BH 9"			@ 295' gravel, poorly sorted, pea-size to med. cobbles. Basalt 60% to 40% to 40%.	Collect 295' archive
	Grab BH 9"				
300	Grab BH 9"				Collect 300' archive
	Grab BH 9"				collect sample for sieve analysis (from cyclone) @ 301'-303' bgs
305	Grab BH 9"		@ 305' gravel, med-sorted, sh-r basaltic.	Collect 305' archive	
	Grab BH 9"				
310	Grab BH 9"			collect 309' archive.	
	TD => 311' bgs			TD => 311' bgs.	
315					

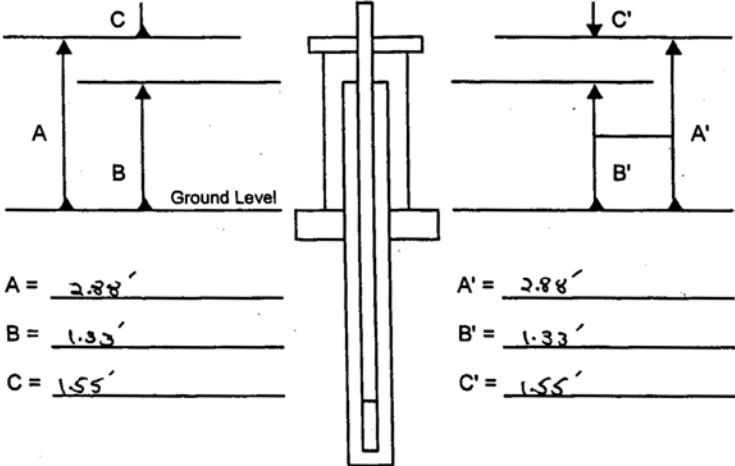
  

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>08/13/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

WELL DEVELOPMENT AND TESTING DATA			
Report 1: Page 1 of 1			
Well Name: <u>299-E27-4</u>	Well ID: <u>C4125</u>	Well Location: <u>West of C-Tank Farm</u>	Date: <u>09/10/03</u>
Reference Measuring Point (unless otherwise noted): TOP OF OUTER CASING (TOC)			
Has the well been surveyed? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		Does the well have a cement pad? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	
<b>PART 1</b>		<b>PART 4</b>	
<b>STATIC WATER LEVEL:</b>		<div style="display: flex; justify-content: space-between;"> <div style="border: 1px solid black; padding: 5px; width: 45%;">           Last Recorded Measurements Date: <u>      </u> </div> <div style="border: 1px solid black; padding: 5px; width: 45%;">           Current Measurements Date: <u>09/10/03</u> </div> </div>	
Start of Job <u>274.29'</u>			
End of Job		<div style="display: flex; justify-content: space-between;"> <div style="width: 45%;">           A = <u>n/A</u>            B = <u>      </u>            C = <u>      </u> </div> <div style="width: 45%;">           A' = <u>2.88'</u>            B' = <u>1.33</u>            C' = <u>1.55'</u> </div> </div>	
<b>DEPTH TO BOTTOM:</b>		Are there any reference marks on the casing strings? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	
Start of Job <u>311.35'</u>		<b>PART 5</b>	
End of Job		<b>COMMENTS:</b>	
<b>PART 2</b>		<u>1200 On site. waiting for drill crew to</u>	
<b>WELL DEVELOPMENT DATA</b>		<u>finish securing C4124.</u>	
Pump Model <u>Franklin 5 HP submersible</u>		<u>1235 Initial measurements =&gt; gw = 274.29' TOC</u>	
Intake Depth <u>272.0'</u>		<u>TD = 311.35' TOC. No fill in well.</u>	
Starting Turbidity		<u>1245 Setting up pump setting rig.</u>	
Pump Start	Stop	Flow Rate	<u>1320 Tripping in pump + tremmie pipe</u>
<u>      </u>	<u>      </u>	<u>      </u>	<u>1330 Calibrating instruments</u>
<u>      </u>	<u>      </u>	<u>      </u>	<u>1415 Pipe in. Lowering transducer.</u>
<u>      </u>	<u>      </u>	<u>      </u>	<u>1430 Goofy readings from Hermit. Pulled transducer up.</u>
<u>      </u>	<u>      </u>	<u>      </u>	<u>Stuck. Trip out tremmie pipe. Tape transducer to above</u>
<u>      </u>	<u>      </u>	<u>      </u>	<u>pump. Trip in pipe. Done. Resume in A.R.</u>
<b>PART 3</b>		<u>1545 Goofy readings from Hermit. will take to office.</u>	
<b>INSTANTANEOUS SLUG TEST</b>			
Static Water Level (TOC)			
Transducer Depth			
Baseline Start			
Injection Start			
Baseline Start			
Withdrawal Start			
Slug Volume			
XD SN/Range (PSI)			
Prepared by (print name): <u>Charlene Martinez</u>		Signature: <u>Charlene Martinez</u>	Date: <u>09/10/03</u>
Reviewed by (print name): <u>L.D. Walker</u>		Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>

A-6003-644 (03/03)

WELL DEVELOPMENT AND TESTING DATA															
Well Name: <u>292-E27-4</u>		Well ID: <u>C4625</u>													
Well Location: <u>West of C-Tank Farm</u>		Date: <u>09/11/03</u>													
Reference Measuring Point (unless otherwise noted): TOP OF OUTER CASING (TOC)															
Has the well been surveyed? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		Does the well have a cement pad? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No													
<b>PART 1</b>		<b>PART 4</b>													
<b>STATIC WATER LEVEL:</b> Start of Job <u>274.29'</u> End of Job <u>274.30'</u>		<div style="display: flex; justify-content: space-between;"> <div style="border: 1px solid black; padding: 5px; width: 45%;">             Last Recorded Measurements              Date: <u>09/10/03</u> </div> <div style="border: 1px solid black; padding: 5px; width: 45%;">             Current Measurements              Date: <u>09/11/03</u> </div> </div>													
<b>DEPTH TO BOTTOM:</b> Start of Job <u>311.35'</u> End of Job <u>n/a</u>															
<b>PART 2</b>		A = <u>2.88'</u> B = <u>1.33'</u> C = <u>1.55'</u>													
<b>WELL DEVELOPMENT DATA</b> Pump Model <u>Franklin 5HP Submersible</u> Intake Depth <u>304.4'</u> <u>295.4'</u> Starting Turbidity <u>26.6</u> <u>4.23</u>		A' = <u>2.88'</u> B' = <u>1.33'</u> C' = <u>1.55'</u>													
<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>Pump Start</th> <th>Stop</th> <th>Flow Rate</th> </tr> </thead> <tbody> <tr> <td><u>0845</u> (70 mins)</td> <td><u>0955</u> (1840 gals)</td> <td><u>26.27 gpm</u></td> </tr> <tr> <td><u>1000</u> (50 mins)</td> <td><u>1050</u> (300 gals)</td> <td><u>26 gpm</u></td> </tr> <tr> <td colspan="3"><u>1840 + 300 = 3140 gals</u></td> </tr> </tbody> </table>		Pump Start	Stop	Flow Rate	<u>0845</u> (70 mins)	<u>0955</u> (1840 gals)	<u>26.27 gpm</u>	<u>1000</u> (50 mins)	<u>1050</u> (300 gals)	<u>26 gpm</u>	<u>1840 + 300 = 3140 gals</u>			Are there any reference marks on the casing strings? <input type="checkbox"/> Yes <input type="checkbox"/> No	
Pump Start	Stop	Flow Rate													
<u>0845</u> (70 mins)	<u>0955</u> (1840 gals)	<u>26.27 gpm</u>													
<u>1000</u> (50 mins)	<u>1050</u> (300 gals)	<u>26 gpm</u>													
<u>1840 + 300 = 3140 gals</u>															
Total Pumped <u>3,140 gals.</u> Final Turbidity <u>3.20</u> <u>0.74</u> XD SN/Range (PSI) <u>n/a</u>		<b>PART 5</b>													
<b>PART 3</b>		<b>COMMENTS:</b> <u>0600 P.O.D. / Safety meeting</u> <u>0615 on site. Prepare to develop well. old-fashioned development</u> <u>0630 Trying to get E-tape into well. Troubles lowering e-tape</u> <u>0651 Raising/lowering pump to try to get e-tape in well.</u> <u>0653 Calibrating instruments.</u> <u>0800 Geologist miscalculated where pump was to be set. Tripped in more tremmie pipe.</u> <u>0830 Running in E-tape. Trying again.</u> <u>0842 Ready to go. Hooking up hoses &amp; valves. XD = 274.29' TOC</u> <u>0845 Turn on pump. Initial measurements: T 19.2°C   COND 1530</u> <u>Turb 26.6; XD = steady @ 274.33' below TOC. 27 gpm.</u> <u>See page 2 for measurements.</u>													
<b>INSTANTANEOUS SLUG TEST</b> Static Water Level (TOC) Transducer Depth Baseline Start <u>0914/03</u> Injection Start <u>Charles Martinez</u> Baseline Start Withdrawal Start Slug Volume XD SN/Range (PSI)		Signature: <u>Charles Martinez</u> Signature: <u>L.D. Walker</u> Date: <u>09/11/03</u> Date: <u>9/30/03</u>													
Prepared by (print name): <u>Charles Martinez</u> Reviewed by (print name): <u>L.D. Walker</u>		Signature: <u>L.D. Walker</u> Date: <u>9/30/03</u>													

A-6003-644 (03/03)



WELL DEVELOPMENT AND TESTING DATA				
Report # 3: Page 1 of 2				
Well Name: <u>299-E27-4</u>	Well ID: <u>C4125</u>	Well Location: <u>West of C-Tank Farm</u>	Date: <u>09/12/03</u>	
Reference Measuring Point (unless otherwise noted): TOP OF OUTER CASING (TOC) <span style="float: right;">(m)</span>				
Has the well been surveyed? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		Does the well have a cement pad? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No		
<b>PART 1</b>		<b>PART 4</b>		
<b>STATIC WATER LEVEL:</b>		<div style="display: flex; justify-content: space-between;"> <div style="border: 1px solid black; padding: 5px; width: 45%;"> Last Recorded Measurements Date: <u>09/11/03</u> </div> <div style="border: 1px solid black; padding: 5px; width: 45%;"> Current Measurements Date: <u>09/12/03</u> </div> </div>		
Start of Job <u>274.29'</u>		<div style="display: flex; align-items: center; justify-content: center;"> <div style="text-align: center;"> C ↑ A B Ground Level </div> <div style="margin: 0 20px;"> </div> <div style="text-align: center;"> C' ↓ A' B' </div> </div>		
End of Job <u>274.35'</u>		A = <u>2.88'</u> A' = <u>2.88'</u> B = <u>1.33'</u> B' = <u>1.33'</u> C = <u>1.55'</u> C' = <u>1.55'</u>		
<b>DEPTH TO BOTTOM:</b>		Are there any reference marks on the casing strings? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		
Start of Job <u>311.35'</u>		<b>PART 5</b>		
End of Job <u>311.35'</u>		<b>COMMENTS:</b>		
<b>PART 2</b>		0600: P.O.D. Safety meeting. Discuss well development.		
<b>WELL DEVELOPMENT DATA</b>		0612 on site. Prepare for stage 3, using Hermit data logger.		
Pump Model <u>Franklin 5 HP</u>		0615 Calibrating instruments		
Intake Depth <u>283.3'</u>		0622 Setting intake. Remove 21 pipe. Add 9 pipe.		
Starting Turbidity <u>35.16</u>		0645 Ready for test #1 (intake @ 283.3'). Initial XD = 8.31 m		
Pump Start	Stop	Flow Rate	(test #2 on data logger)	
(70 m <sup>3</sup> /15) 0647	(1960 gals) 0757	28 gpm	0647 Begin test. Initial readings: XD = 8.233', Cond = 407 μS/cm	
				T = 18.3°C, TURB = 35.6 NTU. measurements listed below
				Time XD (ft) TURB NTU Cond μS/cm T°C 28 gpm => flow rate.
				0658 8.272' 1.46 402 18.2
				0719 8.253' 1.70 403 17.4
				0730 8.247' 1.28 402 18.0
<b>INSTANTANEOUS SLUG TEST</b>				
Static Water Level (TOC)				
Transducer Depth				
Baseline Start				
Injection Start				
Baseline Start				
Withdrawal Start				
Slug Volume				
XD SN/Range (PSI)				
Prepared by (print name): <u>Charlene Martinez</u>		Signature: <u>Charlene Martinez</u>		Date: <u>09/12/03</u>
Reviewed by (print name): <u>L.D. Walker</u>		Signature: <u>L.D. Walker</u>		Date: <u>9/30/03</u>


A-6003-644 (03/03)





FIELD ACTIVITY REPORT WELL SERVICES					Page <u>1</u> of <u>1</u>	
Date <u>09/19/03</u>	Well No. <u>C4125</u>	Rig Type/Model <u>Pump setting rig</u>	Rig No.	Contract/Work Order No.	Report No. <u>1</u>	
Purpose <u>Install pumps in C403 RCR wells</u>				Reference	Location <u>West of C-Tank Farm</u>	
HISTORICAL DATA			PUMP SYSTEM CONFIGURATION			
Construction Depth <u>307.76' bgs</u>					Pre-Maintenance	Post-Maintenance
Casing Size <u>4" ID</u>	Type <u>SS 304 sch 10</u>	Set At <u>+1.9' - 270.33'</u>	Pump Type <u>0.7 HP</u>		Grundfos Rediflo3	
Casing Perforations Schedule <u>Interval</u>			Pump Model <u>Prod # 96030139 model A</u>			
Well Screen(s) Type (4" ID) <u>0.75" OD</u>			Tubing Size/Type <u>0.75" OD SS 304 sch 40</u>			
Interval <u>270.33' - 305.33'</u>			Length-Bottom of Tubing to Pump Intake <u>6.11'</u>			
Last Recorded Depth-to-Water <u>274.29' (TOC)</u>			Tubing Length <u>230.0'</u>			
Last Recorded Depth-to-Bottom <u>311.35' (TOC)</u>			Length-Top of Tubing to Reference Point			
Current Depth-to-Water <u>274.21' (TOC)</u>			Pump Intake Set at (Depth) <u>281.11'</u>			
Current Depth-to-Bottom <u>311.35' (TOC)</u>			Reference/Measuring Point <u>(TOC) Top of Casing</u>			
Start Time <u>0600</u>		Personnel <u>Layne Christensen</u> <u>Dave Dewitt</u> <u>Ken Jones</u> <u>Fluor Hanford</u> <u>Tim Hottell</u> <u>CH2M Hill (CHG)</u> <u>Charlene Martinez</u>		Materials Used <u>28 x 10' long sections SS 304 sch. 40, 0.75" OD tremmie pipe &amp; couplers (ss)</u> <u>0.7 HP Grundfos Rediflo3 pump</u>		
End Time <u>0810</u>						
Time						
Contract Time						
Total Time <u>2.25 hrs</u>						
Description of Operations/Remarks						
<u>0600 P.O.D. / Safety meeting</u>						
<u>0615 Drill crew off to get ss tremmie pipe.</u>						
<u>0630 Drill crew on site. Setting up rig.</u>						
<u>0640 Tagged g.w. =&gt; 274.21' (TOC)</u>						
<u>Tagged TD =&gt; 311.35' (TOC)</u>						
<u>0650 Tripping in 0.7 HP Grundfos Rediflo3 pump &amp; 0.75" OD ss 304, schedule 40 tremmie pipe.</u>						
<u>0906 Done. Lowering mast. Preparing to move to C4124.</u>						
<u>0908 Drill crew + rig off site. Geologist tagging along.</u>						
<u>1122 Pump tested. Works. (cw)</u>						
<u>not used</u>						
<u>Charlene Martinez 09/19/03</u>						
Report By <u>Charlene Martinez</u>			Reviewed By <u>L.D. Walker</u>			
Title <u>Geologist</u>			Title <u>Geologist</u> Date <u>9/30/03</u>			
Signature <u>Charlene Martinez</u>			Signature <u>L.D. Walker</u>			

DISTRIBUTION: White-Field File Custodian Yellow-Group Files Pink-Project Coordinator Goldenrod-Team Leader BC-6000-278 (04/91)

<b>WELL SURVEY DATA REPORT</b>					
<b>Project:</b>			<b>Prepared By:</b> Neil P. Fastabend <b>Company:</b> Fluor Federal Services		
<b>Date Requested:</b> 9/29/03			<b>Requestor:</b> Chris S. Wright (FH)		
<b>Date of Survey:</b> 10/31/03			<b>Surveyor:</b> Fluor Federal Services Survey Dept.		
<b>ERC Point of Contact:</b>			<b>Survey Co. Point of Contact:</b> Grant F. Brazil, P.L.S.		
<b>Description of Work:</b>  Civil Survey of Groundwater Monitoring Well C4125 (299-E27-4).			<b>Horizontal Datum:</b> NAD83(91)		
			<b>Vertical Datum:</b> NAVD88		
			<b>Units:</b> Meters		
			<b>Hanford Area Designation:</b> 200E		
<b>Coordinate System:</b> Washington State Plane Coordinates (South Zone)					
<b>Horizontal Control Monuments:</b> 2E-127 (FFS) and 2E-134 (FFS)					
<b>Vertical Control Monuments:</b> 2E-33 (FFS) and 2E-38 (FFS)					
<b>Well ID</b>	<b>Well Name</b>	<b>Easting</b>	<b>Northing</b>	<b>Elevation</b>	
C4125	299-E27-4	575032.02	136497.92		Center of Casing
				205.569 ✓	Top Casing, N. Edge
				204.685 ✓	Brass Survey Marker
				205.575 ✓	Top Pump Base- plate, N. Edge
<b>Notes:</b>					
<b>Surveyor Statement:</b> I, Grant F. Brazil, a Professional Land Surveyor registered in the State of Washington (Registration No. 22326), hereby certify that this report is based on a field survey performed in October, 2003 under my direct supervision, and that the data contained here is true and correct.					

Original to:  
Distribution by DIS:

**Well 299-E27-20**

**Decommissioned due to bit refusal**

**Not completed**





BOREHOLE LOG						Page <u>1</u> of <u>7</u>
						Date: <u>07/28/03</u>
Well ID: <u>C4126</u>		Well Name: <u>299-E27-20</u>		Location: <u>W. of C-Tank Farm</u>		
Project: <u>CY 03 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample	Blows Recovery	Graphic Log	Sample Description	Comments	
	Type No.			Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method, Method of Driving Sampling Tool, Sampler Size, Water Level	
0	BH 94	0.1A		0-1' Backfill material. Crushed basaltic gravel.	Becker Hammer using 9" OD cast-iron casing	
5	Grab BH 94			1'-5' SAND (s) 95% sand, 5% silt. sand, R, v. well sorted, vfn med grained, non-basaltic. 2.5Y5/3 light olive brown (dry). micaceous No rxn HCl.	Aeolian sand Collect 5' archive	
10	Grab BH 94			5'-13' gravelly SAND (gs) 15% gravel, 80% sand, 5% silt. Gravel, med-sorted. SR-A, basaltic, mps ~ 1.5". Sand, v. well sorted, R, vfn-med, non-basaltic. 2.5Y3/3 dark olive brown (moist). micaceous Strong rxn HCl.	Hanford ftn @ 5' bgs Collect 10' archive Collect 15' archive	
15	Grab BH 94			13'-16' Sand (s) 5% gravel, 87% sand, 8% silt. Gravel, poorly sorted, basaltic, SR-SA, mps ~ 3". Sand, poorly sorted, vfn-v. coarse, 85% basalt, 15% qtz/other, SR-SA 2.5Y3/3, v. dark grayish brown (moist). mod. rxn HCl.	Collect 20' archive NH <sub>3</sub> = 20 ppm in borehole RST surveying spoils Background @ 2200 ppm (Sodium) spoils @ 3000 ppm	
20	Grab BH 94			16'-20' gravelly sand (gs) 10% gravel, 82% sand, 8% silt. Gravel, poorly sorted, SR-SA, sm pebbles-med cobbles, mps ~ 4", basaltic. Sand, poorly sorted, SR-SA vfn-v. coarse grained, 85% basalt, 15% qtz/other, trace mica. 2.5Y3/3 v. dark grayish brown (moist). mod. rxn HCl.	Collect 25' archive Collect 30' archive	
25	Grab BH 94			20'-85' SAND (s) 95% sand, 5% silt. sand, poorly sorted, SR-SA fn-v. coarse grained, 40% basalt, 10% qtz/other. 2.5Y5/2 grayish brown (moist) No rxn HCl.	Collect 35' archive trace gravel @ 35'	
30	Grab BH 94					
35	Grab BH 94					

Reported By: <u>Charles Martinez</u>	Reviewed By: <u>L.D. Walker</u>
Title: <u>Geologist</u>	Title: <u>Geologist</u>
Signature: <u>Charles Martinez</u>	Signature: <u>L.D. Walker</u>
Date: <u>07/28/03</u>	Date: <u>9/30/03</u>









A-6003-642 (03/03)

BOREHOLE LOG						Page <u>2</u> of <u>2</u>
						Date: <u>07/29/03</u>
Well ID: <u>C4126</u>		Well Name: <u>299-E27-20</u>		Location: <u>west of C-Tank Farm</u>		
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample Type No.	Blows Recovery	Graphic Log	Sample Description	Comments	
40	3494 Grab BH 94	n/a		@ 20' sand, cse-vsse, med sorted, basalt increase to 40% to 40% get lother. 2.5 x 413 olive brown (moist) no rxn HCl.	Becker Hammer using 9" dual-use casing. collect 40' archive	
45	Grab BH 94			trace w. sorted gravel (basalt) @ 45' 25'-50' same sand description as 20' interval	Collect 45' archive	
50	Grab BH 94				Collect 50' archive @ 50' NH <sub>3</sub> = 9 ppm	
55	Grab BH 94			@ 55' increase in pea-size basaltic gravel (~10%), well sorted, SR sand same as before.	Collect 55' archive	
60	Grab BH 94				Collect 60' archive @ 60' NH <sub>3</sub> = 18 ppm	
65	Grab BH 94			@ 65' increase in pea-size basaltic gravel (~8%) sand, poorly sorted, fn-vsse grained, pred. cse-vsse, SR-SA, 50% basalt, 50% get lother. no rxn HCl.	Collect 65' archive	
70	Grab BH 94				Collect 70' archive @ 70' NH <sub>3</sub> = 14 ppm	
75	Grab BH 94			@ 75' trace of pea-size gravel (~5%) sand same as above	Collect 75' archive	

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>07/28/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)



BOREHOLE LOG					Page <u>3</u> of <u>7</u>
					Date: <u>07/28/03</u>
Well ID: <u>C4126</u>		Well Name: <u>299-27-20</u>		Location: <u>West of C-Tank Farm</u>	
Project: <u>C403 RCEA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>	
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level
80	BH 94 <u>Grab</u> BH 94	N/A			Becken Hammer using 900 dual-wall casing collect 80' archive NH <sub>3</sub> ≈ 18 ppm (80')
85	BH 94			85'-90' gravelly SAND (s) 12% gravel, 85% sand, 3% silt. gravel, basaltic, SR-R, well-sorted, pea-size-sm pebbles (mps ~ 0.3") sand poorly sorted, fin-verse, SR-SA, 55% basalt, 45% qtz	collect 85' archive
90	BH 94			other 2.5 Y 4/2 dark grayish brown (moist) no rxn HCl.	collect 90' archive NH <sub>3</sub> ≈ 18 ppm (90')
95	BH 94			90'-95' SAND (s) 95% sand, 5% silt, sand, SR-SA, v. poorly sorted, fin-verse grained, 55% basalt, 45% qtz, other 2.5 Y 4/2 dark grayish brown (moist) no rxn HCl.	collect 95' archive
100	BH 94				collect 100' archive @ 100' 20 ppm NH <sub>3</sub> RCT reports slight elevation of SR, but below action levels.
105	BH 94				collect 105' archive
110	BH 94			95'-110' gravelly SAND (s), 15% gravel, 80% sand, 5% silt gravel, well sorted, SR-R, basaltic, pea-size-sm pebbles. Sand, poorly sorted, SR-SA, fin-verse 55% basalt 45% qtz, other 2.5 Y 4/2, dark grayish brown (moist) no rxn HCl.	collect 110' archive
115	BH 94				collect 115' archive
				110' (see next page) SAND (s)	

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>07/28/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>4</u> of <u>7</u>
						Date: <u>07/28/03</u>
Well ID: <u>C4126</u>		Well Name: <u>299-B27-20</u>		Location: <u>West of C-Tank Farm</u>		
Project: <u>CY03 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments	
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level	
120	BHA" Grab BHA"	N/A		110' - 160' SAND(s) 25% sand, 5% silt, sand, 45% basalt, 55% gravel other, poorly sorted, SR-SA, 2.5 x 4 1/2 dark grayish brown (moist), no rxn HCl	Berker Hammer using 9" ID dual-wall casing. collect 120' archive @ 120' O.S.R. levels dropping @ 120' NH <sub>3</sub> = 2.0 ppm	
125	Grab BHA"			@ 120' sand, v. well sorted, non- basaltic, SR-R, v. fn - mod. micaceous 2.5 x 5 1/3, light olive brown (moist) no rxn HCl.	collect 125' archive	
130	Grab BHA"			@ 125' sand as described @ 110' trace basaltic gravel	collect 130' archive @ 130' 19 ppm NH <sub>3</sub>	
135	Grab BHA"			@ 130' sand as @ 125', trace gravel pea-size, basaltic, dry	collect 135' archive	
140	Grab BHA"			@ 135' trace gravel (pea-size) basaltic, dry	collect 140' archive @ 140' NH <sub>3</sub> = 4 ppm. O.S.R. slight elevation between 130' - 140' bgs.	
145	Grab BHA"			@ 145' trace gravel, pea-size basaltic, dry	collect 145' archive	
150	Grab BHA"				collect 150' archive @ 150' NH <sub>3</sub> = 8 ppm. O.S.R. steady (sodium iodide readings between 2400 - 2900 cpm). Background = 2200 cpm.	
155	Grab BHA"			@ 155' trace pea-size gravel	collect 155' archive	

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>07/28/03</u>	Signature: <u>LD Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

BOREHOLE LOG					Page <u>5</u> of <u>7</u>
					Date: <u>07/28/03</u>
Well ID: <u>C4126</u>		Well Name: <u>299-G27-20</u>		Location: <u>west of C-Tank Farm</u>	
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>	
Depth (Ft.)	Sample	Blows Recovery	Graphic Log	Sample Description	Comments
	Type No.			Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method, Method of Driving Sampling Tool, Sampler Size, Water Level
160	Grab BH 9"	N/A		160' - 175' silty sandy GRAVEL (ms) 30% gravel, 60% sand, 10% silt. Gravel, well-sorted, basaltic, pea-size, 3m pebbles, mps ~ 0.2". Sand, med-sorted, SR-SA, 60% qtz/other, 40% basalt, med-vcse grained.	Becker Hammer using 9" o.d. dual-wall casing. Collect 160' archive @ 160' NH <sub>3</sub> = 19 ppm
165	Grab BH 9"			104 RSL, gray, dry. No rxn HCl. micaceous	Collect 165' archive
170	Grab BH 9"				collect 170' archive @ 170' NH <sub>3</sub> = 11 ppm RSL still steady
175	Grab BH 9"			175' - 220' silty SAND (ms) Sand, SR-SA, silt 15%, Sand, 40% basalt, 60% qtz, poorly sorted. SR-SA, vfn-vcse grained, trace mica. dry, 104 RSL, dry (gray) No rxn HCl.	collect 175' archive
180	Grab BH 9"			@ 180' sand grading to well-sorted sand, vfn med grain. No rxn HCl. 40% basalt, 60% qtz/other	Collect 180' archive. @ 180' NH <sub>3</sub> = 9 ppm
185	Grab BH 9"				collect 185' archive
190	Grab BH 9"			@ 190' sand, med-sorted, fn-vcse grain.	collect 190' archive @ 190' NH <sub>3</sub> = 14 ppm RSL steady
195	Grab BH 9"			@ 195' sand, poorly sorted, vfn-vcse, SR-SA, silt decreasing.	Collect 195' archive

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>07/28/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>6</u> of <u>7</u>
						Date: <u>07/28/03</u>
Well ID: <u>C4126</u>			Well Name: <u>299-227-20</u>		Location: <u>West of C-Tank Farm</u>	
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments	
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level	
200	BH 94 <u>Grab</u> BH 94	N/A		@ 200' increase in pea-size basaltic gravel, sand, poorly sorted, vfn-vcse. silt same	Becker Hammer using 9" OD dual-wall casing collect 200' archive @ 200' NH <sub>3</sub> = 12 ppm SR steady SRT off-site.	
205	<u>Grab</u> BH 94			@ 205' sand grading to well-sorted vfn-med grain. 40% basalt, 40% ptz other, dry. no rxn HCl. silt same.	Collect 205' archive	
210	<u>Grab</u> BH 94			@ 210' sand, mod. sorted, med-cse grained, dry. silt same.	collect 210' archive @ 210' NH <sub>3</sub> = 8 ppm	
215	<u>Grab</u> BH 94			@ 215 trace gravel, pea-size, basalt, dry.	Collect 215' archive	
220	<u>Grab</u> BH 94			@ 220' - 240' SAND(S) 95% sand, 5% silt. sand, poorly sorted SR-SA, vfn-vcse. 40% basalt, 60% ptz other.	collect 220' archive @ 220' NH <sub>3</sub> = 21 ppm	
225	<u>Grab</u> BH 94				Collect 225' archive	
230	<u>Grab</u> BH 94			@ 230' sand grading to well-sorted SR-SA, med cse grained, silt increase to ~8%.	Collect 230' archive @ 230' NH <sub>3</sub> = 8 ppm	
235	<u>Grab</u> BH 94				collect 235' archive.	

Reported By: <u>Charlene Martinez</u>			Reviewed By: <u>L.D. Walker</u>		
Title: <u>Geologist</u>			Title: <u>Geologist</u>		
Signature: <u>Charlene Martinez</u>	Date: <u>07/28/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>		

A-6003-642 (03/03)


BOREHOLE LOG						Page <u>7</u> of <u>7</u>
						Date: <u>07/28/03</u>
Well ID: <u>C 4126</u>		Well Name: <u>299-C27-20</u>		Location: <u>West of C-Tank Farm</u>		
Project: <u>CY03 RCR Drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample Type No.	Blows Recovery	Graphic Log	Sample Description	Comments	
240	BH 9"	N/A		@ 240' sand, v. well sorted, vfn-med grained, SR-R, 40% basalt, 40% qtz/other, micaceous, dry, no rxn HCl.	Becker Hammer using 9" dual-wall casing collect 240' archive @ 240' NH <sub>3</sub> = 22 ppm	
245	BH 9"			240' → 245' sandy GRAVEL (36) 35% gravel, 60% sand, 5% silt. Gravel, med-well sorted, SR-SA, 45% basalt, 55% qtz/other. Sand well sorted, SR-SA, med-v. coarse grained, 40% basalt, 40% qtz/other, 10% R512 grayish brown, dry, no rxn HCl.	collect 245' archive	
250	BH 9"				collect 250' archive @ 250' NH <sub>3</sub> = 3 ppm	
255	BH 9"			@ 255' gravel increased to 70%, sand 20%, silt 10%, Gravel, poorly sorted, 3m-pebbles-sm. cobbles.	collect 255' archive	
260	BH 9"			@ 260' gravel, med-sorted, pea-size-sm pebbles. Sand, poorly sorted, vfn-v. coarse. Basalt, 55%, qtz/other 45%, 10% R411 dark gray, dry, no rxn HCl.	collect 260' archive @ 260' NH <sub>3</sub> = 3 ppm	
265	BH 9"			@ 265' gravel, well sorted, trace moisture, 55% gravel, 40% sand, 5% silt.	Collect 265' archive	
270	BH 9"			@ 270' gravel, 60%, 35% sand, 5% silt. Gravel, poorly sorted, SR-SA, basalt, 50%, qtz/other 50%, v. moist. Sand, poorly sorted, SR-SA, vfn-v. coarse, 45% qtz/other, 35% basalt.	Collect 270' archive Collect sample from cyclone (275'-277') sieve analysis Collect 275' archive	
275	BH 9"	sieve analysis sample N/A		@ 275' gravel, increasing in size, med ~ 4", poorly sorted, pea-size-med cobbles. Sand, poorly sorted, SR-SA, same as above.	E.O.S. @ 278' (07/28/03) start 07/29/03 v. hard drilling @ 278' bgs Refusal @ 278.5' bgs.	

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>		TD = <u>278.5'</u>
Title: <u>Geologist</u>		Title: <u>Geologist</u>		
Signature: <u>Charlene Martinez</u>	Date: <u>07/28/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>	

A-6003-642 (03/03)

WELL CONSTRUCTION SUMMARY REPORT				Start Date: 07/28/03			
				Finish Date: 08/04/03			
				Page 1 of 1			
ID: C4126		Well Name: 299-E27-20		Approximate Location: west of C-Tank Farm			
Project: C403 RCRA Drilling		Other Companies: F.H. CHG					
Drilling Company: Layne Christensen		Geologist(s): C. Martinez, M.J. Hocking					
Driller: Chris Dean / Paul Loader		License #: 2554 / 1628					
TEMPORARY CASING AND DRILL DEPTH			DRILLING METHOD	HOLE DIAMETER (in.) / INTERVAL (ft)			
*Size/Grade/Lbs. Per Ft.	Interval	Shoe O.D./I.D.	Auger:	Diameter _____ From _____ to _____			
Dual-wall carbon steel,	0' - 278.5'	9"	Cable Tool:	Diameter _____ From _____ to _____			
FS, 9" OD (outer) 7" ID (inner)			Air Rotary:	Diameter _____ From _____ to _____			
			A.R. w/Sonic:	Diameter _____ From _____ to _____			
			Becker Hammer	Diameter 9" From 0' to 278.5'			
			(Reverse Air)	Diameter _____ From _____ to _____			
*Indicate Welded (W) - Flush Joint (FJ) Coupled (C) & Thread Design				Diameter _____ From _____ to _____			
			Drilling Fluid: n/a				
Total Drilled Depth: 278.5'		Hole Dia @ TD: 9"	Total Amt. Of Water Added During Drilling: -				
Well Straightness Test Results: n/a		Static Water Level: 273.15'		Date: 07/29/03			
GEOPHYSICAL LOGGING							
Sondes (type)	Interval	Date	Sondes (type)	Interval	Date		
	n/a			n/a			
COMPLETED WELL							
Size/Wt./Material	Depth	Thread	Slot Size	Type	Interval Annular Seal/Filter Pack	Volume	Mesh Size
				Quick-Crete Cement (80#)	0' - 10.3'	14 bags	n/a
				Granular Bentonite (50#)	10.3' - 262.8'	141.5 bags	n/a
				Colorado Silica Sand (50#)	262.8' - 278.5'	11 bags	10-20
OTHER ACTIVITIES							
Aquifer Test:		Date:		Well Decommission:		Yes: <input checked="" type="checkbox"/> No: <input type="checkbox"/>	Date:
Description:		n/a		Description: Decommissioned on 08/04/03. Hit refusal @ 278.5' bag $\Rightarrow$ ~ 5' into water table.			
WELL SURVEY DATA (if applicable)							
				Protective Casing Elevation:			
Washington State Plane Coordinates:				Brass Survey Marker Elevation:			
COMMENTS / REMARKS							
Vol. calcs: Quick-crete $\Rightarrow$ $80 \frac{\text{lb}}{\text{ft}^3} / 94 \frac{\text{lb}}{\text{bag}} * 1.285 \text{ ft}^3 \text{ bag} * 14 \text{ bags} = 15.31 \text{ ft}^3$ ; granular bentonite $\Rightarrow$ $141.5 \text{ bags} * 0.71 \frac{\text{ft}^3}{\text{bag}} = 100.47 \text{ ft}^3$ ; 10-20 sand $\Rightarrow$ $11 \text{ bags} * 0.535 \frac{\text{ft}^3}{\text{bag}} = 5.89 \text{ ft}^3$							
Reported By:		Title:		Signature:		Date:	
Charlene Martinez		Geologist		Charlene Martinez		09/08/03	

A-6003-658 (04/03)

<b>WELL SURVEY DATA REPORT</b>					
<b>Project:</b>		<b>Prepared By:</b> Neil P. Fastabend <b>Company:</b> Fluor Federal Services			
<b>Date Requested:</b> 9/29/03		<b>Requestor:</b> Chris S. Wright (FH)			
<b>Date of Survey:</b> 10/31/03		<b>Surveyor:</b> Fluor Federal Services Survey Dept.			
<b>ERC Point of Contact:</b>		<b>Survey Co. Point of Contact:</b> Grant F. Brazil, P.L.S.			
<b>Description of Work:</b>  Civil Survey of Groundwater Monitoring Well C4126 (299-E27-20).		<b>Horizontal Datum:</b> NAD83(91)			
		<b>Vertical Datum:</b> NAVD88			
		<b>Units:</b> Meters			
		<b>Hanford Area Designation:</b> 200E			
<b>Coordinate System:</b> Washington State Plane Coordinates (South Zone)					
<b>Horizontal Control Monuments:</b> 2E-127 (FFS) and 2E-134 (FFS)					
<b>Vertical Control Monuments:</b> 2E-33 (FFS) and 2E-38 (FFS)					
<b>Well ID</b>	<b>Well Name</b>	<b>Easting</b>	<b>Northing</b>	<b>Elevation</b>	
C4126	299-E27-20	575067.36	136455.88		Center of Brass Cap in Concrete
					Top Casing, N. Edge
				205.447	Brass Survey Marker
					Top Pump Base- plate, N. Edge
<b>Notes:</b> <div style="margin-left: 40px;">Brass cap in concrete only. No Well Casing.</div>					
<b>Surveyor Statement:</b> I, Grant F. Brazil, a Professional Land Surveyor registered in the State of Washington (Registration No. 22326), hereby certify that this report is based on a field survey performed in October, 2003 under my direct supervision, and that the data contained here is true and correct.					

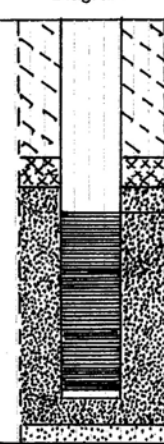

Original to:  
Distribution by DIS:

## **Well 299-E27-21**



WELL SUMMARY SHEET		Start Date: 07/21/03		Page 1 of 2	
		Finish Date: 07/25/03			
Well ID: C4127			Well Name: 299-E27-21		
Location: South of CR-Vault			Project: C403 RCRA drilling		
Prepared By: Charlene Martinez		Date: 08/07/03	Reviewed By: L.D. Walker		Date: 8/11/03
Signature: <i>Charlene Martinez</i>			Signature: <i>L.D. Walker</i>		
CONSTRUCTION DATA		GEOLOGIC/HYDROLOGIC DATA			
Description	Diagram	Depth in Feet	Graphic Log	Lithologic Description	
9" OD Dual-wall temporary casing used		0		0'-1' Backfill (crushed gravel)	
				1'-20' SAND(s)	
				20'-25' gravelly SAND(qs)	
6" ID SS protective casing set 1.0' above permanent				25'-40' SAND(s)	
				40'-65' gravelly SAND(qs)	
4" ID SS 304 sched. 10 riser: + 2.0' → 271.37'				65'-160' SAND(s)	
Portland Cement Grout: 0' → 10.1'					
Granular Bentonite: 10.1' → 260.4'					
1/4" Bentonite Pellets: 260.4' → 265.5'					
		140		140'-170' gravelly SAND(qs)	
				170'-185' SAND(s)	
				185'-200' silty sandy GRAVEL (msG)	
All temporary casing removed from ground:		200		200'-225' silty SAND(ms)	
				225'-235' silty sandy GRAVEL (msG)	
All depths are in feet below ground surface.				235'-240' silty SAND(ms)	

A-6003-643 (03/03)

WELL SUMMARY SHEET			Start Date: 07/21/03		Page 2 of 2
			Finish Date: 07/25/03		
Well ID: C 4127			Well Name: 299-E27-21		
Location: South of CR-Vault			Project: C403 RCRA drilling		
Prepared By: Charlene Martinez		Date: 08/08/03	Reviewed By: L.D. Walker		Date: 8/11/03
Signature: <i>Charlene Martinez</i>			Signature: <i>L.D. Walker</i>		
CONSTRUCTION DATA		Depth in Feet	GEOLOGIC/HYDROLOGIC DATA		
Description	Diagram		Graphic Log	Lithologic Description	
10-20 mesh silica sand: 265.5' → 314.0'		240		240'-275' silty sandy GRAVEL (msg)	
ss 304 (4" ID) schedule 10					
0.020-in. cont. wire-wrap well screen:		275		275'-285' gravelly SAND (gs)	
271.37' → 306.43'		280		285'-318' sandy GRAVEL (sg)	
4" ID ss 304 schedule 10					
sump endcap:		320		TD = 318' bgs	
4-8 mesh silica sand:				Static water 271.38' bgs	
314.0' → 318.0'				(07/25/03)	
		360			
All temporary casing removed from ground:					
All depths are in feet below ground surface.					

A-6003-643 (03/03)

WELL CONSTRUCTION SUMMARY REPORT						Start Date: 07/21/03	
						Finish Date: 08/28/03	
						Page 1 of 1	
IID: C4127		Well Name: 299-627-21		Approximate Location: South of CR-vault			
Project: C403 RCRA drilling				Other Companies: FH, CHG			
Drilling Company: Layne Christensen				Geologist(s): C. Martinez, M.J. Hocking			
Driller: Paul ("Derry") Lodder License #: 1628							
TEMPORARY CASING AND DRILL DEPTH			DRILLING METHOD		HOLE DIAMETER (in.) / INTERVAL (ft)		
*Size/Grade/Lbs. Per Ft.	Interval	Shoe O.D./I.D.	Auger:	Diameter		From to	
Carbon Steel, dual-wall casing, FS.	0' - 318'	9"	Cable Tool:	Diameter		From to	
Outer 9" O.D.			Air Rotary:	Diameter		From to	
Inner 7 1/2"			A.R. w/Sonic:	Diameter		From to	
			Reverse Air	Diameter 9"		From 0' to 318'	
			(Becker Hammer)	Diameter		From to	
*Indicate Welded (W) - Flush Joint (FJ) Coupled (C) & Thread Design					Diameter From to		
Total Drilled Depth: 318'			Hole Dia @ TD: 9"		Drilling Fluid: N/A		
Well Straightness Test Results: Passed using 4.5" O.D., 20.4' long			Total Amt. Of Water Added During Drilling: 0		Static Water Level: 271.38'		
Tool on 07/23/03			Date: (07/25/03)				
GEOPHYSICAL LOGGING							
Sondes (type)	Interval	Date	Sondes (type)	Interval	Date		
Spectral Gamma	0' - 318'	07/21 & 07/22 2003					
COMPLETED WELL							
Size/Wt./Material	Depth	Thread	Slot Size	Type	Interval Annular Seal/Filter Pack	Volume	Mesh Size
4" x 5.31 O.D. sched 10 casing	+2.0' - 271.37'	F480	N/A	Portland Cement (94#)	0' - 10.1'	4 bags	N/A
4" x 5.31 O.D. sched 10 well screen	271.37' - 306.43'	"	2.020"	Granular Bentonite (50#)	10.1' - 260.4'	100 bags	N/A
4" x 5.31 O.D. sched 10 sump	306.43' - 308.83'	"	N/A	Bentonite Pellets (50#)	260.4' - 265.5'	2.5 buckets	1/4"
				Silica Sand (50#)	265.5' - 314.0'	29 bags	10-20
				Silica Sand (50#)	314.0' - 318.0'	2 bags	4-8
OTHER ACTIVITIES							
Aquifer Test: well development		Date: 08/28/03		Well Decommission:		Yes:	No:
Description: 5 HP Franklin submersible pump. Developed 3 stages. Intake @ 306.7'   292.7'   285.6'. Flow rate: 23 gpm.				Description:			
23.5 gpm, 21 gpm. Final turb: (NTU) 1.24   1.44   1.83							
WELL SURVEY DATA (if applicable)							
Washington State Plane Coordinates:				Protective Casing Elevation:			
				Brass Survey Marker Elevation:			
COMMENTS / REMARKS							
Vol. calcs: P.C., 4 bags * 1.485 <sup>ft³</sup> /bag = 5.94 <sup>ft³</sup> ; Granules, 100 bags * 0.71 <sup>ft³</sup> /bag = 71.0 <sup>ft³</sup> ; Pellets, 2.5 buckets * 0.62 <sup>ft³</sup> /bucket = 1.55 <sup>ft³</sup> ; 10-20 sand, 29 bags * 0.535 = 15.52 <sup>ft³</sup> ; 4-8 sand 2 bags * 0.663 <sup>ft³</sup> /bag = 1.33 <sup>ft³</sup> .							
Reported By:		Title:		Signature:		Date:	
Charlene Martinez		Geologist		Charlene Martinez		09/06/03	

A-6003-658 (04/03)

# WELL ATTRIBUTES REPORT

FIELD ORDER NO

WELL ID 04127

WELL NAME 299-E27-21

HOST WELL ID

DRILL DATE 07/21/03

CONST DATE 07/23/03

CONST DEPTH 308.83'

LAST INSPECTION

NORTHING

EASTING

ELEVATION

MEASUREMENT INFORMATION		
	LAST	CURRENT
A DEPTH TO WATER(ft)	274.46' TOC	274.47'(TOC)
DEPTH TO WATER DATE	09/18/03	09/29/03
B DEPTH TO BOTTOM(ft)	311.95' TOC	N/A
DEPTH TO BOTTOM DATE	09/18/03	N/A
C STICK UP(ft)	2.35'	2.35'
D REFERENCE MARK(ft)		
REFERENCE MARK IS TOC	<input checked="" type="checkbox"/> YES <input type="checkbox"/> NO <input type="checkbox"/> ND*	<input checked="" type="checkbox"/> YES <input type="checkbox"/> NO

PERFORATION INFORMATION			
CASING SIZE	TOP	BOTTOM	CUTS/FT/ROUND

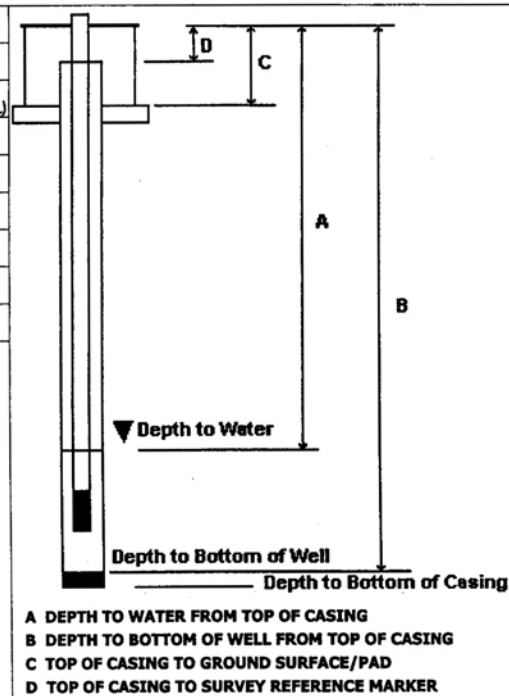
CHANGES g.w. => 274.49' - 0.02' (landing plate) =  
274.47' TOC.

CASING INFORMATION						
SIZE	TOP	BOTTOM	MATERIAL	TYPE	CONNECTION	THICKNESS
4" ID	+2.0'	271.37'	stainless steel	304; sch. 10		

CHANGES

SCREEN INFORMATION					
SIZE	TOP	BOTTOM	MATERIAL	TYPE	SLOT SIZE
4" ID	271.37'	306.43'	stainless steel	304; schedule 10	0.020-inch

CHANGES



BOREHOLE LOG					Page <u>1</u> of <u>8</u>
					Date: <u>07/21/03</u>
Well ID: <u>C4127</u>		Well Name: <u>299-E27-21</u>		Location: <u>S. of CR-vault</u>	
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>	
Depth (Ft.)	Sample	Blows Recovery	Graphic Log	Sample Description	Comments
	Type No.			Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level
0	BH 9" N/A		▲▲▲▲	0'-1' Backfill. Gravel, basalt.	Becker Hammer using 9" OD dual-wall casing
				1'-20' Sand (s), 100% vfn-fn grained, R, v. well sorted, non-basaltic.	2'-5' Aedian sand
				10YR 4/1, dark yellowish brown (moist)	
				weak - no rxn HCl.	Collect 5' archive
5	Grab BH 9"			@ 5' 90% sand, 5% silt, 5% gravel. 5' Hanford ftn.	
				Gravel, pea-size-sm. pebbles, R. well sorted, basaltic. Sand, vfn-cse, mod-sorted.	
				45% basalt, 55% qtz/other, SR-R	collect 10' archive
10	Grab BH 9"			2.5Y 4/3 olive brown (moist) strong rxn HCl. loose matrix.	
15	Grab BH 9"			20'-25' gravelly SAND (s) 15% gravel, 75% sand, 7% silt. Gravel mod-sorted, SR-R, mps ~ 2", basaltic.	collect 15' archive
				Sand, poorly-sorted, SR-SA, vfn-vcse grained, 80% basalt, 20% qtz/other.	
20	Grab BH 9"			10YR 3/3, v. dark grayish brown (moist) mod rxn HCl. Loose matrix	Collect 20' archive
25	Grab BH 9"			25'-40' SAND (s) 93% sand, 7% silt. Sand, poorly sorted, vfn-vcse grained, SR-SA, 80% basalt, 20% qtz/other.	Collect 25' archive
				10YR 3/2, v. dark grayish brown (moist) mod rxn HCl. Loose matrix	
30	Grab BH 9"			@ 30' Sand grading to mod-sorted. fn-cse, grained, non-basaltic, SR-R, trace mica. 2.5Y 5/3 light olive brown (moist), no rxn HCl. Unconsolidated.	collect 30' archive
35	Grab BH 9"			@ 35' sand grading to v. poorly sorted vfn-vcse grained, SR-SA, 80% basalt, 20% qtz/other, silt ~ 5%, trace of pea-size, basaltic gravel (< 5%) 10YR 3/2 v. dark grayish brown. Unconsolidated.	collect 35' archive
Reported By: <u>Charlene Martinez</u>			Reviewed By: <u>L.D. Walker</u>		
Title: <u>Geologist</u>			Title: <u>Geologist</u>		
Signature: <u>Charlene Martinez</u>		Date: <u>07/21/03</u>	Signature: <u>L.D. Walker</u>		Date: <u>9/30/03</u>

A-6003-642 (03/03)

BOREHOLE LOG					Page <u>2</u> of <u>8</u>
					Date: <u>07/21/03</u>
Well ID: <u>C4127</u>		Well Name: <u>299-E27-21</u>		Location: <u>S. of CR-Vault</u>	
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>	
Depth (Ft.)	Sample Type No.	Blows Recovery	Graphic Log	Sample Description <small>Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl</small>	Comments <small>Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level</small>
40	BH 9" Grab	N/A		40'-65' gravelly SAND (gs) 10% gravel, 85% sand, 5% silt. Gravel, well-sorted, SE-R, basaltic, med. pea-size. Sand, SE-SA, v. poorly-sorted, vfn-vcsr grained, 80% basalt, 20% qtz/other. 10% R 3/2, v. dark grayish brown (moist). No rxn HCl.	Becker Hammer using 9" OD dual-wall casing. collect 40' archive
45	BH 9" Grab			65'-160' sand (s) 95% sand, 5% silt. Sand, med-sorted, SE-SA, med-csr grained, 15% basalt, 85% qtz/other. 2.54513 light olive brown (moist), micaceous. No rxn HCl.	collect 45' archive
50	BH 9" Grab				collect 50' archive
55	BH 9" Grab				collect 55' archive
60	BH 9" Grab				collect 60' archive
65	BH 9" Grab				collect 65' archive
70	BH 9" Grab				collect 70' archive
75	BH 9" Grab			@75' sand grading to v. poorly sorted, SE-SA, v. cse-vfn grained, 20% basalt, 30% qtz/other. 2.54513, dark grayish brown. no rxn HCl.	collect 75' archive

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>07/21/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>3</u> of <u>8</u>
						Date: <u>07/21/03</u>
Well ID: <u>C4127</u>		Well Name: <u>299-E27-21</u>		Location: <u>S. of CR-Vault</u>		
Project: <u>403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample Type No.	Blows Recovery	Graphic Log	Sample Description	Comments	
				Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method, Method of Driving Sampling Tool, Sampler Size, Water Level	
80	BHA" 349"	N/A		@80' basalt content decreasing to 60%, qtz/other 40%. Sand continues to be v. poorly sorted, SR-SA, vfn-vase grained.	Baker Hammer using 9" OD dual-wall casing. collect 80' archive	
85	Grab 349"			@85' trace of pea-size, basaltic gravel (< 5 1/8") Sand. same as previous	collect 85' archive	
90	Grab 349"				collect 90' archive	
95	Grab 349"			@95' trace pea-size gravel, msn 0.5" basaltic	collect 95' archive	
100	Grab 349"			@100' trace of gravel (< 0.4") basaltic	collect 100' archive	
105	Grab 349"				collect 105' archive	
110	Grab 349"				collect 110' archive	
115	Grab 349"		@115' gravel increasing to ~ 8%. Pea-size to 3m pebbles, med-sorted, SR-R, basaltic	collect 115' archive		









Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.O. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>07/21/03</u>	Signature: <u>L.O. Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

BOREHOLE LOG					Page <u>4</u> of <u>8</u>
					Date: <u>07/21/03</u>
Well ID: <u>C4127</u>		Well Name: <u>299-E22-21</u>		Location: <u>S. of CR-Vault</u>	
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>	
Depth (Ft.)	Sample Type No.	Blows Recovery	Graphic Log	Sample Description	Comments
120	Grab BH 9"	n/a			Becker Hammer using 9" OD dual wall casing collect 120' archive
125	Grab BH 9"			@ 125' trace gravel, mps ~ 1.5", basaltic. No rxn HCl.	collect 125' archive
130	Grab BH 9"				collect 130' archive
135	Grab BH 9"			@ 135' basaltic gravel (~ 5%) mod-sorted basaltic, mps ~ 2", pred med- pebbles. Sand grading to mod-well sorted, fn- cse grained. SS= SA, 55% qtzl other, 45% basalt. No rxn HCl.	collect 135' archive
140	Grab BH 9"			@ 140' sand grading to vfn- cse, poorly sorted, SS= SA, silt increasing to ~ 7%. No rxn HCl.	collect 140' archive
145	Grab BH 9"				collect 145' archive
150	Grab BH 9"				collect 150' archive
155	Grab BH 9"			@ 155' increase in cse- cse grained sand. Traces of pea-sized gravel.	collect 155' archive
Reported By: <u>Charlene Martinez</u>				Reviewed By: <u>L. D. Walker</u>	
Title: <u>Geologist</u>				Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>		Date: <u>07/21/03</u>		Signature: <u>L. D. Walker</u>	
				Date: <u>9/30/03</u>	

A-6003-642 (03/03)



BOREHOLE LOG						Page <u>5</u> of <u>8</u>
						Date: <u>07/21/03</u>
Well ID: <u>C4127</u>		Well Name: <u>299-E27-21</u>		Location: <u>S. of CR-Vault</u>		
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments	
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level	
160	BHA" Grab BHA"	N/A		160'-170' gravelly SAND (gs) 15% gravel, 75% sand, 10% silt. Gravel, well-sorted, smooth pebbles, max ~1", basaltic, SR-SA. Sand, poorly sorted, SR-SA, vfn-vco grained, 50% basalt, 50% other. 2.545/1 gray (dry), no rxn HCl.	Becker Hammer using 9" on dual-wall casing. collect 160' archive	
165	Grab BHA"				collect 165' archive	
170	Grab BHA"			170'-185' SAND (s) 90% sand, 10% silt, trace gravel. Gravel, pea-size, basaltic. Sand, poorly sorted, SR-SA, vfn-vco grained, 50% basalt, 50% other. 104R5/2, grayish brown (dry) no rxn HCl.	collect 170' archive	
175	Grab BHA"				collect 175' archive	
180	Grab BHA"			185'-200' silty Sandy GRAVEL (msg) 40% gravel, 50% sand, 10% silt. Gravel, well-sorted, SR-SA basaltic, Sand, poorly sorted, SR-SA, 45% basalt, 55% other. 104R5/2, grayish brown (dry) no rxn HCl.	collect 180' archive	
185	Grab BHA"				collect 185' archive	
190	Grab BHA"				collect 190' archive	
195	Grab BHA"				collect 195' archive	

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>07/21/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>6</u> of <u>8</u>
						Date: <u>07/21/03</u>
Well ID: <u>C4127</u>			Well Name: <u>299-627-21</u>		Location: <u>S. of CR-Vault</u>	
Project: <u>CY03 RCRA drilling</u>					Reference Measuring Point: <u>Ground surface</u>	
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments	
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method, Method of Driving Sampling Tool, Sampler Size, Water Level	
200	Grab BH 9"	N/A		200'-225' Silty sand (ms) 88% sand, 12% silt, trace gravel. Sand, med sorted, med-vcse grained. SR-SA, 55% Qtz/other, 45% basalt. 2.5/5/1 gray (dry) no rxn HCl.	Becker Hammer using 9" OD dual-wall casing collect 200' archive	
205	Grab BH 9"			@ 205' sand grading to poorly sorted, fn-vcse grained, trace of pea-sized, basaltic gravel.	collect 205' archive	
210	Grab BH 9"				collect 210' archive	
215	Grab BH 9"			@ 215' trace of mica.	collect 215' archive	
220	Grab BH 9"			@ 220' trace gravel, 1m- pebbles < 0.5"	collect 220' archive	
225	Grab BH 9"			225'-235' silty sandy GRAVEL (ms6) 35% gravel, 55% sand, 10% silt gravel, well-sorted, basaltic, pea-sized. Sand, poorly sorted, ufn-vcse, 55% Qtz/other, 45% basalt. Consolidated silt	collect 225' archive	
230	Grab BH 9"			nodules w/ Fe oxide staining 2.5/5/1 gray (dry) no rxn HCl. micaceous	collect 230' archive	
235	Grab BH 9"			235'-240' silty SAND (ms) 88% sand, 12% silt Sand, poorly sorted, ufn-vcse, SR-SA, 55% Qtz/other, 45% basalt. 2.5/5/1 gray (dry) no rxn HCl. micaceous	collect 235' archive	

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>07/21/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>7</u> of <u>8</u>
						Date: <u>07/21/03</u>
Well ID: <u>C4127</u>		Well Name: <u>299-827-21</u>		Location: <u>S. of CR-Vault</u>		
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground surface</u>		
Depth (Ft.)	Sample	Blows Recovery	Graphic Log	Sample Description	Comments	
	Type No.			Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method, Method of Driving Sampling Tool, Sampler Size, Water Level	
240	Grab BH 9"	n/a		240 - 275' silty sandy GRAVEL (msG)	Becker Hammer using 9" OD dual-wall casing.	
				30% gravel, 60% sand, 10% silt.	Collect 240' archive	
				Gravel, basaltic, well-sorted, pea-size		
				Sand, poorly sorted, vfn-vsse, SR-A		
				45% basalt, 55% qtz/other, 2.5 VSL		
245	Grab BH 9"			gray (drg) no rxn HCl, micaceous	collect 245' archive	
250	Grab BH 9"				collect 250' archive	
					A.m.I.H.C.K. organics < detect.	
255	Grab BH 9"			@ 255' gravel increasing to 55%, sand 35%, silt 10%. Gravel, well-sorted, SR-A, rounded pebbles, 45% basalt, 35% qtz/other, micaceous	collect 255' archive A.m.R.C.T.C. Sodium IODIDE meter used. 5' @ background	
260	Grab BH 9"				collect 260' archive	
265	Grab BH 9"				collect 265' archive	
270	Grab BH 9"				collect 270' archive	
275	Grab BH 9"			275 - 285' gravelly SAND (gs) 20% gravel, 75% sand, 5% silt. Gravel poorly sorted, pea-size - 1/4 pebbles, msG basaltic, SR-A, Sand, poorly sorted, vfn-vsse grained, SR-A, 55% basalt, 45% qtz/other	collect 275' archive collect sample from cyclone (275'-280') for sieve analysis	

Reported By: Charles Martinez

Title: Geologist

Signature: Charles Martinez

Reviewed By: L.D. Walker

Title: Geologist

Signature: L.D. Walker

Date: 07/21/03

Date: 9/30/03

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>8</u> of <u>8</u>
						Date: <u>07/21/03</u>
Well ID: <u>C 4127</u>		Well Name: <u>299-227-21</u>		Location: <u>S. of CR-vault</u>		
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample Type No.	Blows Recovery	Graphic Log	Sample Description <small>Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl</small>	Comments <small>Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level</small>	
280	BH 911	N/A		285' - 318' Sandy GRAVEL (s.g.) 45% gravel, 30% sand, 5% silt. Gravel, gravel, med-sorted, 80% basalt, 20% quartzite, SR-R, pea-size-med pebbles. Sand, poorly sorted, SR-SA, 60% basalt, 40% quartzite. Unconsolidated	Becker Hammer using 9" dual-wall casing. Collect 280' archive	
285	BH 911				Collect 285' archive	
290	BH 911				Collect 290' archive	
295	BH 911				Collect 295' archive	
300	BH 911				Collect 300' archive	
305	BH 911				v. hard drilling @ 303' bgs.	
310	BH 911				Collect 305' archive. @ 305' gravel & poorly sorted, sm pebbles - lg cobbles mps ~ 5"-6". No visible cementation. Basalt content down to 40%, 60% quartzite.	
312	BH 911				Collect 310' archive	
315	BH 911	Sieve Analysis			P.m. IH tech reported oxygen in casing is decreasing. Unknown substance is eating oxygen (~ 310' bgs) Collect sample from cyclone (312-315') for sieve analysis	
318	BH 911				Collect 315' archive	
TD => 318' bgs (07/21/03)				lg. cobble @ 318' bgs Collect TD @ 318' bgs		

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>07/21/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/30/03</u>

A-6003-642 (03/03)

WELL DEVELOPMENT AND TESTING DATA																		
Well Name: <u>299-627-21</u>		Well ID: <u>C4127</u>	Well Location: <u>South of CR Vault</u>															
		Date: <u>08/28/03</u>	Report 1 Page 1 of 3															
Reference Measuring Point (unless otherwise noted): TOP OF OUTER CASING (TOC)																		
Has the well been surveyed? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		Does the well have a cement pad? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No																
<b>PART 1</b>		<b>PART 4</b>																
<b>STATIC WATER LEVEL:</b> Start of Job <u>274.56' TOC</u> End of Job <u>274.47' TOC</u> <b>DEPTH TO BOTTOM:</b> Start of Job <u>312.0' TOC</u> End of Job <u>311.9' TOC</u>		<div style="display: flex; justify-content: space-between;"> <div style="border: 1px solid black; padding: 5px; width: 45%;">             Last Recorded Measurements              Date: <u>08/28/03</u> </div> <div style="border: 1px solid black; padding: 5px; width: 45%;">             Current Measurements              Date: _____           </div> </div> <div style="text-align: center; margin-top: 20px;"> </div> <div style="display: flex; justify-content: space-between; margin-top: 10px;"> <div style="width: 45%;">             A = <u>2.35' TOC</u>              B = <u>1.24</u>              C = <u>1.11</u> </div> <div style="width: 45%;">             A' = _____              B' = _____              C' = _____           </div> </div>																
<b>PART 2</b>		Are there any reference marks on the casing strings? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No																
<b>WELL DEVELOPMENT DATA</b> Pump Model <u>Franklin 5 HP submersible</u> Intake Depth <u>306.7' TOC</u> Starting Turbidity <u>11.8</u> <table border="1" style="width: 100%; border-collapse: collapse; margin-top: 5px;"> <thead> <tr> <th>Pump Start</th> <th>Stop</th> <th>Flow Rate</th> </tr> </thead> <tbody> <tr> <td>0940</td> <td>1043</td> <td>23.9 gpm</td> </tr> <tr> <td>1055</td> <td>1143</td> <td>23.5 gpm</td> </tr> <tr> <td>1243</td> <td>1345</td> <td>21.0 gpm</td> </tr> <tr> <td colspan="2">1449 + 1128 + 1300 =</td> <td>3879 gals</td> </tr> </tbody> </table>		Pump Start	Stop	Flow Rate	0940	1043	23.9 gpm	1055	1143	23.5 gpm	1243	1345	21.0 gpm	1449 + 1128 + 1300 =		3879 gals	<b>PART 5</b> <b>COMMENTS:</b> <u>0600 P.O.D. / Safety meeting.</u> <u>0615 Back to office</u> <u>0705 At site.</u> <u>0730 Tagged g.w. =&gt; 274.56' TOC</u> <u>0730 Setting up rig.</u> <u>0735 Tagged TD =&gt; 312' TOC. No fill in well.</u> <u>0753 Tripping in Franklin 5 HP submersible pump.</u> <u>0755 Calibrating instruments.</u> <u>0900 Running 20.0 psi to depth. Initial XD =&gt; 47.78'</u> <u>Begin test 1 on Hermit 3000. (No Test)</u> <u>Initial Readings: TURB CONO TEMP XD</u> <u>0915 Transducer NOT working. Will develop old-fashioned</u>	
Pump Start	Stop	Flow Rate																
0940	1043	23.9 gpm																
1055	1143	23.5 gpm																
1243	1345	21.0 gpm																
1449 + 1128 + 1300 =		3879 gals																
<b>PART 3</b> <b>INSTANTANEOUS SLUG TEST</b> Static Water Level (TOC) _____ Transducer Depth _____ Baseline Start _____ Injection Start _____ Baseline Start _____ Withdrawal Start _____ Slug Volume _____ XD SN/Range (PSI) _____		Prepared by (print name): <u>Charles Martinez</u> Signature: <u>Charles Martinez</u> Date: <u>08/28/03</u> Reviewed by (print name): <u>L.D. Walker</u> Signature: <u>L.D. Walker</u> Date: <u>9/30/03</u>																

A-6003-644 (03/03)

FIELD ACTIVITY REPORT - DAILY DRILLING						Page <u>2</u> of 3	
						Date: <u>08/28/03</u>	
Well ID: <u>C4127</u>				Well Name: <u>299-G27-21</u>			
Location: <u>South of CR-Vault</u>				Report No.: <u>1 (well development)</u>			
Start		Finish		Total			
Time <u>0600</u>		Time _____		Time _____			
Hole Depth/Csg _____ / _____		Hole Depth/Csg _____ / _____		Hole Depth/Csg _____ / _____			
Reference Measuring Point: <b>GROUND SURFACE</b>				Casing String No. 1 2 3 4 _____ Rod Size: <u>N/A</u> See Report No. 1 <u>well development</u>			
Time/Depth		Description of Activities/Operations with Depth (Attach applicable drawings and document straightness test results)					
From	To						
0935		Running F-tape into well					
0935		Driller hooking up pump & flow meter.					
0940		Initial XD = 274.62' (TOS) Test #1					
0940:00		Begin test: XD = 274.65' (23 gpm. Flow open all the way).					
Time	XD	Readings: Test #1				Time	XD (ft)
		Column 2	Column 3			Turb	Cond
0940:15	274.64	0945:00	274.64	1013:15	274.64	0948	274.64
0940:30	274.64	0945:20	274.64	1016:01	274.64	1000	274.64
0940:45	274.64	0945:30	274.64	1018:45	274.65	1020	274.65
0941:00	274.64	0946:00	274.64	1020:15	274.65	1032	274.65
0941:20	274.64	0946:25	274.64	1025:30	274.65	1041	274.65
0941:30	274.64	0947:00	274.64	1027:12	274.65	1050	Test #1 complete. Final XD
0942:00	274.64	0950:30	274.65	1031:40	274.64	274.62' 100% recovery	
0942:30	274.64	0953:00	274.65	1032:15	274.65	1050. Remove 9' tremmie pipe.	
0942:45	274.64	0957:30	274.65	1035:01	274.64	Intake set @ 297.7' TOS. Test #2	
0943:00	274.64	1000:02	274.64	1037:19	274.65	Initial XD => 274.62' TOS	
0943:20	274.64	1003:09	274.64	1039:28	274.65		
0943:43	274.64	1007:11	274.64	1041:01	274.65		
0944:07	274.64	1010:30	274.64	1055 Test #2 Start. Readings test #2			
1043		shut pump off Recovery test #1				Time	XD (ft)
1043:15	274.60	1044:30	274.61	1046:00	274.62	1100	274.68
1043:30	274.60	1044:47	274.62	1046:30	274.62	1110	274.67
1043:45	274.60	1045:00	274.62	1046:45	274.62	1120	274.66
1043:55	274.61	1045:15	274.62	1047:00	274.62	1128	274.66
1044:10	274.61	1045:45	274.62	1048:00	274.62	1143	274.66
Reported By: <u>Charlene Martinez</u>				Reviewed By: <u>L.D. Walker</u>			
Title: <u>Geologist</u>				Date: <u>08/28/03</u>		Date: <u>9/30/03</u>	
Signature: <u>Charlene Martinez</u>				Signature: <u>L.D. Walker</u>			

A-6003-651 (04/03)


FIELD ACTIVITY REPORT - DAILY DRILLING						Page <u>3</u> of 3	
Continuation Page						Date: 08/28/03	
Well Name: 299-E27-21				Well ID: C4127			
Location: South of CR-vault				Continuation of Report No.: 1 (well development)			
Time/Depth		Description of Activities/Operations with Depth					
From	To	well development					
Time	XD	Test #	Start	End	Flow meter	Open	Flow rate
1055:15	274.64	Test #2	1055:00	1109:00	274.67	1128:15	274.66
1055:30	274.65	1055:40	274.68	1110:00	274.67	1130:03	274.67
1055:45	274.67	1059:00	274.68	1112:05	274.67	1131:00	274.67
1056:00	274.67	1059:15	274.68	1114:15	274.68	1132:15	274.66
1056:10	274.67	1059:30	274.68	1116:00	274.66	1133:30	274.68
1056:25	274.67	1059:45	274.68	1117:00	274.66	1134:00	274.67
1056:45	274.67	1100:00	274.68	1120:00	274.66	1135:17	274.67
1057:00	274.67	1102:25	274.68	1122:00	274.66	1136:30	274.68
1057:15	274.67	1104:15	274.68	1123:00	274.66	1138:15	274.68
1057:30	274.68	1106:00	274.68	1125:01	274.67	1140:00	274.68
1057:45	274.68	1107:12	274.68	1126:00	274.66	1142:00	274.68
1058:00	274.68	1108:00	274.67	1127:04	274.66	1143:00	274.68
1143		STOP test #2. Recovery 100%. Final XD = 274.62'					
1145	1230	Purge water truck full. off site.					
1143	1159	B. Edgington on site to ck transducer & Hermit. Something wrong. Off-site w/ transducer.					
1148	1157	move pump up to next interval. (285.6' TOC)					
		Test #3 Readings:					
Time	XD	Test #3	Start	End	Flow rate	Time	XD
1243:17	274.62	1243:17	274.62	1306:01	274.62	1245	274.62
1243:45	274.62	1246:00	274.63	1310:00	274.62	1255	274.63
1244:02	274.62	1250:05	274.63	1312:31	274.62	1324	274.62
1244:20	274.63	1253:01	274.63	1318:07	274.62	1343	274.62
1244:31	274.62	1255:15	274.63	1324:00	274.62		
1244:45	274.62	1300:01	274.62	1333:08	274.62	STOP TEST #3 @ 1345	
1244:58	274.62	1303:00	274.62	1343:00	274.62	Recovery 100% 274.58'	
1348	1421	Tripping out tremmie pipe & development pump					
1425		Tagged g.w. 274.47' TOC. Tagged bottom => 311.9' TOC.					
1433		Pumping off site. Site secure. End of shift.					
Reported By: Charlene Martinez				Reviewed By: L.D. Walker			
Title: Geologist		Date: 08/28/03		Title: Geologist		Date: 9/30/03	
Signature: Charlene Martinez				Signature: L.D. Walker			

A-6003-652 (04/03)

FIELD ACTIVITY REPORT - WELL SERVICES					Page <u>1</u> of <u>1</u>	
Date <u>09/19/03</u>	Well No. <u>C 4127</u>	Rig Type/Model <u>Pump setting rig</u>	Rig No.	Contract/Work Order No.	Report No.	
Purpose <u>Install pumps in C403 RCRA wells.</u>				Reference	Location <u>South of the CR-Vault</u>	
HISTORICAL DATA			PUMP SYSTEM CONFIGURATION			
Construction Depth <u>308.83' bgs</u>					Pre-Maintenance	Post-Maintenance
Casing Size <u>4" ID</u>	Type <u>SS 304, sch. 10</u>	Set At <u>+2.0' - 271.37' bgs</u>	Pump Type <u>0.7 HP</u>		Grundfos Rediflo3	
Casing Perforations Schedule <u>Interval</u>			Pump Model <u>model A, 960309</u>		Prod # <u>139</u>	
Well Screen(s) Type <u>0.020" slot</u>			Tubing Size/Type <u>0.75" OD SS 304</u>			
Interval <u>4" ID SS 304 sch 10 306.43' bgs</u>			Length-Bottom of Tubing to Pump Intake <u>1.10'</u>			
Last Recorded Depth-to-Water <u>274.56' TOC</u>			Tubing Length <u>280.0'</u>			
Last Recorded Depth-to-Bottom <u>312.0' TOC</u>			Length-Top of Tubing to Reference Point			
Current Depth-to-Water <u>274.46' TOC</u>			Pump Intake Set at (Depth) <u>281.10'</u>			
Current Depth-to-Bottom <u>311.95' TOC</u>			Reference/Measuring Point <u>TOC (TOP OF CASING)</u>			
Start Time <u>1215</u>		Personnel <u>Layne Christensen</u>		Materials Used <u>28 X 10" sections</u>		
End Time <u>1400</u>		• Dave DeWitt		<u>SS 304 schedule 40, 0.75" OD</u>		
Time		• Ken Johnson Jones		<u>tremmie pipe, &amp; couplers</u>		
Contract Time		Pilot Hanford		<u>Grundfos Rediflo3 (0.7 HP)</u>		
Total Time <u>1.75 hrs</u>		• Ed Rafuse (BTR)		<u>electric submersible pump.</u>		
		Chaz Hill (CHG)				
		• Charlene Martinez (geologist)				
Description of Operations/Remarks						
<u>1215 P.O.D. / Safety meeting</u>						
<u>1235 on site. Pump setting rig set up.</u>						
<u>1245 Tagged g.w. @ 274.56' TOC.</u>						
<u>Tagged TD @ 311.95' TOC.</u>						
<u>1250 Preparing to install Grundfos Rediflo3 (0.7 HP) pump using SS 304,</u>						
<u>schedule 40, 0.75" OD tremmie pipe.</u>						
<u>1255 Begin installing pump.</u>						
<u>By the way -&gt; happy birthday to me. Happy birthday to me.</u>						
<u>1400 Done. Mast on rig down.</u>						
<u>1405 Pump setting rig off-site to C4190</u>						
<u>09/19/03 Tested pump -&gt; works.</u>						
<u>09/19/03</u>						
<del>Charlene Martinez 09/18/03</del>						
Report By <u>Charlene Martinez</u>			Reviewed By <u>L.D. Walker</u>			
Title <u>Geologist</u>			Title <u>Geologist</u>		Date <u>9/30/03</u>	
Signature <u>Charlene Martinez</u>			Signature <u>L.D. Walker</u>			

DISTRIBUTION: White-Field File Custodian Yellow-Group Files Pink-Project Coordinator Goldenrod-Team Leader BC-6000-278 (04/91)



<b>WELL SURVEY DATA REPORT</b>					
<b>Project:</b>			<b>Prepared By:</b> Neil P. Fastabend <b>Company:</b> Fluor Federal Services		
<b>Date Requested:</b> 9/29/03			<b>Requestor:</b> Chris S. Wright (FH)		
<b>Date of Survey:</b> 10/31/03			<b>Surveyor:</b> Fluor Federal Services Survey Dept.		
<b>ERC Point of Contact:</b>			<b>Survey Co. Point of Contact:</b> Grant F. Brazil, P.L.S.		
<b>Description of Work:</b>  Civil Survey of Groundwater Monitoring Well C4127 (299-E27-21).			<b>Horizontal Datum:</b> NAD83(91)		
			<b>Vertical Datum:</b> NAVD88		
			<b>Units:</b> Meters		
			<b>Hanford Area Designation:</b> 200E		
<b>Coordinate System:</b> Washington State Plane Coordinates (South Zone)					
<b>Horizontal Control Monuments:</b> 2E-127 (FFS) and 2E-134 (FFS)					
<b>Vertical Control Monuments:</b> 2E-33 (FFS) and 2E-38 (FFS)					
<b>Well ID</b>	<b>Well Name</b>	<b>Easting</b>	<b>Northing</b>	<b>Elevation</b>	
C4127	299-E27-21	575145.03	136407.21		Center of Casing
				205.728	Top Casing, N. Edge
				204.995	Brass Survey Marker
				205.734	Top Pump Base- plate, N. Edge
<b>Notes:</b>					
<b>Surveyor Statement:</b> I, Grant F. Brazil, a Professional Land Surveyor registered in the State of Washington (Registration No. 22326), hereby certify that this report is based on a field survey performed in October, 2003 under my direct supervision, and that the data contained here is true and correct.					

Original to:  
Distribution by DIS:

**Well 299-E27-23**





WELL CONSTRUCTION SUMMARY REPORT				Start Date: 09/05/03			
				Finish Date: 09/02/03			
				Page 1 of 1			
Well ID: C 4190		Well Name: 299-E27-23		Approximate Location: west of C-Tank Farm			
Project: C403 RCR drilling		Other Companies: CHG, FH		Geologist(s): C. Martinez, M.J. Hocking			
Drilling Company: Layne Christensen		Driller: Paul ("Derry") Loder		License #: 1628			
TEMPORARY CASING AND DRILL DEPTH			DRILLING METHOD	HOLE DIAMETER (in.) / INTERVAL (ft)			
*Size/Grade/Lbs. Per Ft.	Interval	Shoe O.D./I.D.	Auger:	Diameter _____ From _____ to _____			
Carbon Steel dual-wall	0' - 318'	9"	Cable Tool:	Diameter _____ From _____ to _____			
casing, FS. 9"OD(outer)	_____ - _____		Air Rotary:	Diameter _____ From _____ to _____			
7"16" inner	_____ - _____		A.R. w/Sonic:	Diameter _____ From _____ to _____			
	_____ - _____		Reverse Air (Becker Hammer)	Diameter 9" From 0' to 318'			
	_____ - _____			Diameter _____ From _____ to _____			
*Indicate Welded (W) - Flush Joint (FJ) Coupled (C) & Thread Design				Diameter _____ From _____ to _____			
			Drilling Fluid: n/a				
Total Drilled Depth: 318'		Hole Dia @ TD: 9"		Total Amt. Of Water Added During Drilling: none			
Well Straightness Test Results: Passed using 4" ID, 20.4' long			Static Water Level: 273.1'		Date: 08/12/03		
GEOPHYSICAL LOGGING							
Sondes (type)	Interval	Date	Sondes (type)	Interval	Date		
Spectral Gamma	0' - 318'	08/07/03 & 08/08/03		_____ - _____			
	_____ - _____			_____ - _____			
	_____ - _____			_____ - _____			
COMPLETED WELL							
Size/Wt./Material	Depth	Thread	Slot Size	Type	Interval Annular Seal/Filter Pack	Volume	Mesh Size
4" x 5.3204 sch. 10 casing	41.8' - 273.51'	4480	n/a	Portland Cement (94#)	0' - 9.9'	5 bags	n/a
4" x 5.3204 sch. 10 well screen	273.51' - 308.54'	"	0.030"	Granular Bentonite (50#)	9.9' - 263.0'	107.5 bags	n/a
4" x 5.3204 sch. 10 pump	308.54' - 310.97'	"	n/a	Bentonite Pellets (50#)	263.0' - 267.8'	2 buckets	1/4"
	_____ - _____			Colorado Silica Sand (50#)	267.8' - 318.0'	29.5 bags	10-20
	_____ - _____						
OTHER ACTIVITIES							
Aquifer Test: well development		Date: 09/02/03		Well Decommission:		Yes:	No: Date:
Description: SHF Franklin Submersible pump. Developed 3				Description:			
Stages Intake 311.3' / 301.3' / 291.3'. Pump rate 24.5 gpm, 24 gpm, 16 gpm. Final turb (NTU) 3.93 / 0.72 / 3.0							
WELL SURVEY DATA (If applicable)							
				Protective Casing Elevation:			
Washington State Plane Coordinates:				Brass Survey Marker Elevation:			
COMMENTS / REMARKS							
Vol. calcs: P.C., 5 bags * 1.285 <sup>ft</sup> ³/bag = 6.43 <sup>ft</sup> ³; Granules, 107.5 bags * 0.71 <sup>ft</sup> ³/bag = 76.33 <sup>ft</sup> ³; pellets, 2 buckets * 0.62 <sup>ft</sup> ³/bucket = 1.24 <sup>ft</sup> ³; 10-20 sand, 29.5 bags * 0.535 = 15.78 <sup>ft</sup> ³							
Reported By: Charlene Martinez		Title: Geologist		Signature: Charlene Martinez		Date: 09/04/03	

A-6003-658 (04/03)

## WELL ATTRIBUTES REPORT

FIELD ORDER NO

ELL ID

C 4190

WELL NAME

299-E 27-23

HOST WELL ID

DRILL DATE

08/05/03

CONST DATE

08/11/03

CONST DEPTH

310.97'

LAST INSPECTION

NORTHING

EASTING

ELEVATION

MEASUREMENT INFORMATION		
	LAST	CURRENT
A DEPTH TO WATER(ft)	<u>276.46' TOC</u>	<u>276.52' (TOC)</u>
DEPTH TO WATER DATE	<u>09/18/03</u>	<u>09/29/03</u>
B DEPTH TO BOTTOM(ft)	<u>314.45' TOC</u>	<u>N/A</u>
DEPTH TO BOTTOM DATE	<u>09/18/03</u>	<u>N/A</u>
C STICK UP(ft)	<u>3.42'</u>	<u>2.93'</u>
D REFERENCE MARK(ft)		
REFERENCE MARK IS TOC	<input checked="" type="checkbox"/> YES <input type="checkbox"/> NO <input checked="" type="checkbox"/> ND*	<input checked="" type="checkbox"/> YES <input type="checkbox"/> NO

### PERFORATION INFORMATION

CASING SIZE	TOP	BOTTOM	CUTS/FT/ROUND

CHANGES 3.42' measured from ground surface  
+ not from top of cement pad.  
g.w. => 276.54' - 0.02' (landing plate) = 276.52' TOC

### CASING INFORMATION

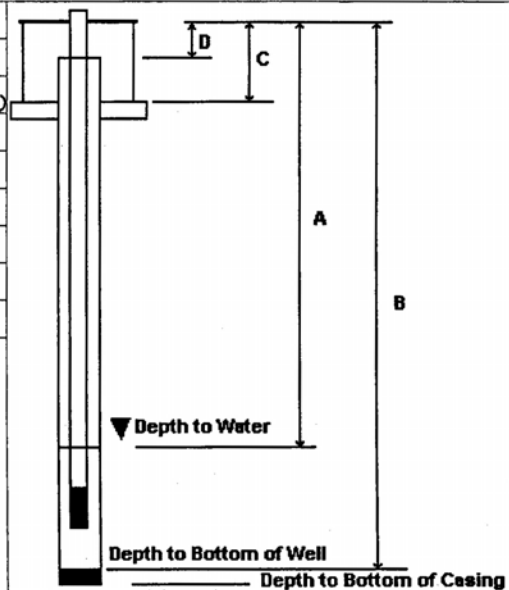
SIZE	TOP	BOTTOM	MATERIAL	TYPE	CONNECTION	THICKNESS
<u>4" ID</u>	<u>41.8'</u>	<u>273.51'</u>	<u>stainless steel</u>	<u>304, sch. 10</u>		

CHANGES

### SCREEN INFORMATION

SIZE	TOP	BOTTOM	MATERIAL	TYPE	SLOT SIZE
<u>4" ID</u>	<u>273.51'</u>	<u>309.54'</u>	<u>stainless steel</u>	<u>304, schedule 10</u>	<u>0.020 inch</u>

CHANGES



- A DEPTH TO WATER FROM TOP OF CASING
- B DEPTH TO BOTTOM OF WELL FROM TOP OF CASING
- C TOP OF CASING TO GROUND SURFACE/PAD
- D TOP OF CASING TO SURVEY REFERENCE MARKER

BOREHOLE LOG						Page <u>1</u> of <u>2</u>
						Date: <u>08/05/03</u>
Well ID: <u>C4190</u>			Well Name: <u>299-E27-23</u>		Location: <u>West of C-Tank Farm</u>	
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample Type No.	Blows Recovery	Graphic Log	Sample Description	Comments	
				Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level	
0	BH 9"	N/A	△△△△	0' - 1.5' Back-fill material. Crushed gravel.	Becker Hammer using 9" OD dual wall casing	
			△△△△	1.5' - 10' SAND(S) 100% v. well sorted, vfn-med grained, R. 10YR 4/3 brown (moist). Strong rxn HCl.	Redrill of C4126. No archive samples collected until 280' bgs.	
5			△△△△	10' - 12' gravelly sand (GS) 20% gravel, 80% sand. Gravel, poorly sorted sm pebbles - med cobbles, mps ~ 3.5, SR-SA sand, vfn-med, v. well sorted. 10YR 4/3 brown (moist) strong rxn HCl.	Continuous TH support from 0' ~ 170' bgs due to NH <sub>3</sub> detected @ C4126. NH <sub>3</sub> ranged from 0 ppm - 5 ppm (~110' bgs) in borehole.	
10			△△△△	12' - 15' sandy GRAVEL(SG) 40% gravel, 55% sand, 5% silt. Gravel, v. poorly sorted, SR-SA, sm pebbles - med cobbles, mps ~ 4". Sand, SR-SA, poorly sorted, vfn-v. coarse, 75% basalt, 25% gsz/other. 10YR 3/2 v. dark grayish brown (moist) no rxn HCl.		
15			△△△△	15' - 20' gravelly SAND(S) 15% gravel, med-sorted, lg. pebbles - sm cobbles. Sand, fn-v. coarse, poorly sorted, SR-SA 2.5Y 4/2 dark grayish brown (moist) 60% basalt, 40% gsz/other. No rxn HCl.		
20			△△△△	20' - 103' SAND(S) 92% sand, 8% gravel. Gravel, basaltic, well-sorted, pea-sized. Sand, SR-SA, poorly sorted vfn-v. coarse, 60% basalt, 40% gsz/other 2.5Y 4/2 dark grayish brown (moist) No rxn HCl.		
25			△△△△			
30			△△△△			
35			△△△△			

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>09/05/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/23/03</u>

A-6003-642 (03/03)


BOREHOLE LOG					Page <u>2</u> of <u>8</u>	
					Date: <u>08/05/03</u>	
Well ID: <u>C4190</u>		Well Name: <u>299-E27-23</u>		Location: <u>West of C-Tank Farm</u>		
Project: <u>CY03 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments	
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level	
40	3H9"	11A		@ 40' no trace of gravel. 95% sand, 5% silt. Sand, vfm vese	Becker Hammer using 9"OD dual-wall casing	
45						
50						
55					@ 55' trace gravel, basaltic, mps ~ 3" sand, v. poorly sorted.	
60						
65					@ 65' trace gravel, basaltic, mps ~ 1.5" sand, v. poorly sorted.	
70						
75					@ 75' increase in pea-size basaltic gravel (~ 9%), sand, v. poorly sorted.	

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>08/05/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/24/03</u>


A-6003-642 (03/03)





BOREHOLE LOG					Page <u>4</u> of <u>8</u>
					Date: <u>08/05/03</u>
Well ID: <u>C4190</u>		Well Name: <u>299-E27-23</u>		Location: <u>west of C-Tank Farm</u>	
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>	
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level
120	B49"	N/A		@ 120' sand grading to med-sorted, SR-R, fn-cse grained, 45% basalt, 55% gtz/other, 2.5 Y 4/3 olive brown (moist) no rxn HCl.	Becker Hammer using 9" OD dual-wall casing
125				@ 125' trace silt.	
130				@ 130' 8% basaltic, med-size gravel, sand grading to 60% basalt, 40% gtz/ other, poorly sorted, vfn-vsse grain, SR-SH 2.5 Y 4/3 dk grayish brown (moist), no rxn HCl.	
135					
140				@ 140' trace gravel, mps ~ 1"	
145				@ 145' trace mica. Increase in silt (~5%) trace gravel, mps ~ 1". Sand, poorly sorted, vfn-vsse, 60% basalt, 40% gtz/other	
150					
155					
160					
165					
Reported By: <u>Charlene Martinez</u>			Reviewed By: <u>L.D. Walker</u>		
Title: <u>Geologist</u>			Title: <u>Geologist</u>		
Signature: <u>Charlene Martinez</u>		Date: <u>08/05/03</u>	Signature: <u>L.D. Walker</u>		Date: <u>9/24/03</u>


A-6003-642 (03/03)

BOREHOLE LOG					Page <u>5</u> of <u>8</u>
					Date: <u>08/05/03</u>
Well ID: <u>C4190</u>		Well Name: <u>299-E27-23</u>		Location: <u>west of C-Tank Farm</u>	
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground surface</u>	
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level
160	849	N/A		160' - 200' silty SAND(ms) 5% gravel, 82% sand, 13% silt. Gravel, well-sorted, basaltic, pea-size, SR-R. Sand, poorly-sorted, fn-vcse, SR-SA, 50% basalt, 50% qtz/other. 2.5 Y 5/1 gray (dry) 2.5 Y 5/3 grayish brown (dry) No rxn HCl.	Becker Hammer using 9" OD dual-wall casing
165					
170					
175					
180				@180' basalt content down to 40%. qtz/other 60% sand, fn-vcse, poorly sorted.	
186				@183' sand grading to well-sorted, fn-med grained, trace mica. 2.5 Y 4/4 olive brown (dry)	
190					
195				@195' sand grading to v. poorly sorted, SR-SA, fn-vcse grained. Basalt 40%, qtz/other 40%. 10YR 4/1 dk. grayish brown (moist) No rxn HCl	

Reported By: <u>Charlene Martner</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martner</u>	Date: <u>08/05/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/23/03</u>

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>6</u> of <u>8</u>
						Date: <u>08/05/03</u>
Well ID: <u>C4190</u>		Well Name: <u>299-E27-23</u>		Location: <u>West of C-Tank Farm</u>		
Project: <u>C403 RCB drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments	
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level	
200	BH 9"	N/A		200' - 210.0' silty sandy GRAVEL (mG) 30% gravel, 60% sand, 10% silt. Gravel, well-sorted, SR-R, pea-size to 5m pebbles, mps ~ 0.5", basaltic. Sand, poorly sorted, SR-SA, vfn-vcsz, micaceous, 50% qtz/other, 50% basalt. 2.5 Y 4/2 dk. grayish brown (moist), no rxn HCl.	Becker Hammer using 9" dual-wall casing	
210				210' - 226' SAND(S) 95% sand, 5% silt. Sand, well sorted, med-coe grained SR-SA, micaceous. 10 Y 5/2 grayish brown (dry) 40% basalt, 40% qtz/other no rxn HCl.		
215				226' - 230' gravelly SAND(S) 20% gravel, 75% sand, 5% silt. Gravel, well-sorted, SR-SA, basaltic, pea-size to 5m pebbles. Sand, poorly sorted, SR-SA vfn-vcsz, 40% basalt, 40% qtz/other 10 Y 4/2, dk. grayish brown (moist) no rxn HCl.	A.m. RCT on site. CK'd spoils pile from 0' - 220' bgs. of A.R. @ background.	
220				230' - 245' SAND(S) 95% sand, 5% silt, trace gravel. Sand, med- sorted SR-SA, fn-vcsz, 50% basalt, 50% qtz/other		
225				@ 235' trace basaltic gravel, mps ~ 2". sand, v. well sorted, vfn-med, SR-R micaceous, 35% basalt, 1.5% qtz/ other. 2.5 Y 5/2 grayish brown (dry) no rxn HCl.		
230						
235						


Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>08/05/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/24/03</u>

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>7</u> of <u>8</u>
						Date: <u>08/05/03</u>
Well ID: <u>C4190</u>		Well Name: <u>299-E27-23</u>		Location: <u>West of C-Tank Farm</u>		
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground Surface</u>		
Depth (Ft.)	Sample		Graphic Log	Sample Description	Comments	
	Type No.	Blows Recovery		Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level	
240	BH 9"	N/A		<u>245' - 255' Silty Sand, GRAVEL (msg)</u> <u>40% gravel, 50% sand, 10% silt.</u> <u>Gravel, well sorted, SR-SA, pea-size</u> <u>~sm pebbles, 70% basalt, 20% quartzite</u> <u>Sand, poorly sorted, SR-SA, vfn-veg.</u> <u>40% basalt, 60% quartzite, micaceous.</u> <u>Silt nodules, 10YR 5/3 brown (moist)</u> <u>No rxn HCl.</u>	<u>Dual-wall casing 9" OD</u> <u>Becker Hammer</u>	
245				<u>@ 250' gravel increase to 70% sand,</u> <u>20% silt 10%. Gravel, v. poorly</u> <u>sorted, pea-size - med. cobbles.</u> <u>mps ~ 5"</u>		
250				<u>255' - 260' GRAVEL (g) 80% gravel,</u> <u>15% sand, 5% silt. Gravel, poorly</u> <u>sorted, sm. pebbles ~ med cobbles, 65% basalt,</u> <u>35% quartzite, SR-SA.</u> <u>Sand, poorly sorted, SR-SA, 50% basalt,</u> <u>50% quartzite, no rxn HCl, vfn-veg.</u> <u>grained.</u>		
255				<u>260' - 318' sandy GRAVEL (SG) 55% gravel,</u> <u>38% sand, 7% silt. Gravel,</u> <u>poorly sorted, SR-SA, mps ~ 3.5", sm-</u> <u>pebble to med. cobbles, 65% basalt,</u> <u>35% quartzite 10YR 4/2 dk. grayish</u> <u>brown (moist) No rxn HCl.</u>		
260						
265						
270						
275						
					<u>@ 275' bgs =&gt; increase in basalt content</u> <u>70% basalt, 30% quartzite</u>	

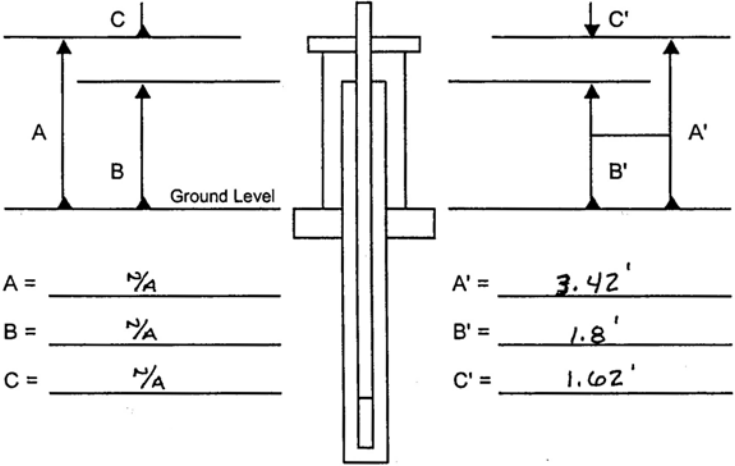
Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>08/05/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/24/03</u>

A-6003-642 (03/03)

BOREHOLE LOG						Page <u>8</u> of <u>8</u>
						Date: <u>08/05/03</u>
Well ID: <u>C4190</u>		Well Name: <u>29A-E27-23</u>		Location: <u>west of C-Tank Farm</u>		
Project: <u>C403 RCRA drilling</u>				Reference Measuring Point: <u>Ground surface</u>		
Depth (Ft.)	Sample Type No.	Blows Recovery	Graphic Log	Sample Description Group Name, Grain Size Distribution, Soil Classification, Color, Moisture Content, Sorting, Angularity, Mineralogy, Max Particle Size, Reaction to HCl	Comments Depth of Casing, Drilling Method Method of Driving Sampling Tool Sampler Size, Water Level	
280	BH 9" Grab	N/A		@ 280' gravel v. poorly sorted, med. lg pebbles - lg cobbles. SE-A, very fragmented, basaltic. Sand, v. poorly sorted, vfn-vcs, 80-85% basalt, 15-20% quartz other	Becker Hammer using 9" OD dual-wall casing collect 280' archive	
285	BH 9" Grab				collect 285' archive	
290	BH 9" Grab				@ 290' increase in gravel content ~ 70% gravel, 25% sand, < 5% silt.	collect 290' archive
295	BH 9" Grab					collect 295' archive
300	BH 9" Grab					collect 300' archive
305	BH 9" Grab					collect 305' archive
310	BH 9" Grab	Sieve analysis sample			collect 310' archive collect sieve analysis sample (310' - 312' bgs)	
315	BH 9" Grab	N/A			large basalt boulder @ 311' bgs. collect 315' archive	
319	Grab	TD @ 318' bgs			collect 319' archive TD @ 319' bgs	

Reported By: <u>Charlene Martinez</u>		Reviewed By: <u>L.D. Walker</u>	
Title: <u>Geologist</u>		Title: <u>Geologist</u>	
Signature: <u>Charlene Martinez</u>	Date: <u>08/05/03</u>	Signature: <u>L.D. Walker</u>	Date: <u>9/24/03</u>

A-6003-642 (03/03)

WELL DEVELOPMENT AND TESTING DATA				1 of 5
Well Name: <u>299-E27-23</u>	Well ID: <u>C4190</u>	Well Location: <u>West of 241-C Tank Farm</u>	Date: <u>9-2-03</u>	
Reference Measuring Point (unless otherwise noted): TOP OF OUTER CASING (TOC)				
Has the well been surveyed? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		Does the well have a cement pad? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No		
<b>PART 1</b>		<b>PART 4</b>		
<b>STATIC WATER LEVEL:</b>		<div style="display: flex; justify-content: space-between;"> <div style="width: 45%;"> <p>Last Recorded Measurements Date: <u>N/A</u></p> </div> <div style="width: 45%;"> <p>Current Measurements Date: <u>9-2-03</u></p> </div> </div>		
Start of Job <u>276.52' TOC</u>				
End of Job <u>276.40' TOC</u>		<p>A = <u>N/A</u>      A' = <u>3.42'</u></p> <p>B = <u>N/A</u>      B' = <u>1.8'</u></p> <p>C = <u>N/A</u>      C' = <u>1.62'</u></p>		
<b>DEPTH TO BOTTOM:</b>		Are there any reference marks on the casing strings? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		
Start of Job <u>314.4' TOC</u>		<b>PART 5</b>		
End of Job <u>314.4' TOC</u>		<b>COMMENTS:</b>		
<b>PART 2</b>		0600 - POD / Safety Mtg.		
<b>WELL DEVELOPMENT DATA</b>		0610 - Geologist on site.		
Pump Model <u>SHP Franklin Electric</u>		0615 - Geologist waits on Layne to set up pump rig.		
Intake Depth <u>311.3' TOC</u> <u>301.3' TOC</u> <u>291.3' TOC</u>		0700 - Layne to go get generator & forklift; Geologist takes measurements.		
Starting Turbidity <u>35 NTU</u> <u>1.8 NTU</u> <u>2.6 NTU</u>		0715 - DTW = 276.52' TOC (273.10' bgs); DTB = 314.4' TOC (310.98' bgs); Stkup = 3.42'; fill = 311.0' - 310.98' = 0.02'		
Pump Start	Stop	Flow Rate	0730 - Layne set up and ready to start.	
<u>0940</u>	<u>1037</u>	<u>24.5 GPM</u>	0745 - Layne wants to pull bailer loads (even though there is only 0.02'); waiting for barrel from FWS	
<u>1105</u>	<u>1135</u>	<u>2.6 GPM</u>	Tim Hottell.	
<u>1347</u>	<u>1505</u>	<u>6 GPM</u>	0750 - Begin bailing.	
				0817 - End bailing; begin dropping pump.
Total Pumped <u>3,624.5 Gal.</u>				
Final Turbidity <u>3.93 NTU</u> <u>0.74 NTU</u> <u>3.00 NTU</u>				
XD SN/Range (PSI) <u>20.0 PSI</u>				
<b>PART 3</b>				
<b>INSTANTANEOUS SLUG TEST</b>				
Static Water Level (TOC)				
Transducer Depth				
Baseline Start				
Injection Start				
Baseline Start				
Withdrawal Start				
Slug Volume				
XD SN/Range (PSI)				
Prepared by (print name): <u>Jess Hocking</u>		Signature: <u>Jess Hocking</u>		Date: <u>9/2/03</u>
Reviewed by (print name): <u>L.D. Walker</u>		Signature: <u>L.D. Walker</u>		Date: <u>9/24/03</u>

A-6003-644 (03/03)

FIELD ACTIVITY REPORT - DAILY DRILLING		Page <u>2</u> of 5
Continuation Page		Date: 9-2-03
Well Name: <u>Z99-E27-23</u>		Well ID: <u>C4190</u>
Location: <u>West of 241-C Tank Farm</u>		Continuation of Report No.: <u>Well Development</u>
Time/Depth	Description of Activities/Operations with Depth	
From	To	
	0830	Geologist calibrates field equipment: Z100 P HACH TURBIDIMETER, YSI SS D.O. METER, Orion model 124 conductivity & Orion model 290 A pH METER are all running within standard specs; details on last page of Development <sup>report.</sup> <del>page.</del>
	0930	Pump at depth; Layne hooks up flow meters; Geologist drops transducer
	0936	Initial XD = 27.390' H <sub>2</sub> O
	0940	Start test; Development begins.
	0942	XD = 27.260' H <sub>2</sub> O (0.13' draw) @ ~26 GPM [MAX]
	0945	Initial attributes sample taken; Turb. = 35 NTU; Details on back page.
	0951	XD = 27.232' H <sub>2</sub> O (0.158' draw) @ ~26 GPM
	1001	XD = 27.235' H <sub>2</sub> O (0.155' draw) @ ~26 GPM.
	1014	XD = 27.225' H <sub>2</sub> O (0.165' draw) @ ~26 GPM.
	1021	XD = 27.255' H <sub>2</sub> O (0.135' draw) @ ~26 GPM.
	1028	XD = 27.225' H <sub>2</sub> O (0.165' draw) @ ~26 GPM
	1034	XD = 27.252' H <sub>2</sub> O (0.138' draw) @ ~26 GPM.
	1037	Pump shut off; Recovery test started
	1038	XD = 27.248' H <sub>2</sub> O (99.5% Rec.); possible mistake made by Layne w/ pump shut-off.
	1041	XD = 27.278' H <sub>2</sub> O (99.6% Rec.)
	1043	Layne does not shut off pump for first several minutes of recovery test - which will explain jump in hydrograph later.
	1052	XD = 27.277' H <sub>2</sub> O (99.6% Rec.); Recovery test ended, ready to move pump up ~10'.
	1056	Layne begins to move pump up 10'.
	1104	Pump intake @ 301.3' w.c.; Initial XD = 18.287' H <sub>2</sub> O.
	1105	Start pump and draw test.
	1106	XD = 18.308' H <sub>2</sub> O (draw = -0.021') @ ~26 GPM.
	1114	XD = 18.268' H <sub>2</sub> O (draw = 0.019') @ ~26 GPM.
	1121	XD = 18.274' H <sub>2</sub> O (draw = 0.013') @ ~26 GPM.
	1127	XD = 18.277' H <sub>2</sub> O (draw = 0.010') @ ~26 GPM.
Reported By: <u>Jess Hocking</u>		Reviewed By: <u>L.D. Walker</u>
Title: <u>Geologist / Hydrogeologist</u>	Date: <u>9/2/03</u>	Title: <u>Geologist</u> Date: <u>9/24/03</u>
Signature: <u>Jess Hocking</u>		Signature: <u>L.D. Walker</u>

A-6003-652 (04/03)



FIELD ACTIVITY REPORT - DAILY DRILLING		Page <u>3</u> of <u>5</u>
Continuation Page		Date: <u>9-2-03</u>
Well Name: <u>299-E27-Z3</u>		Well ID: <u>C4190</u>
Location: <u>West of 241-C Tank Farm.</u>		Continuation of Report No.: <u>Well Development</u>
Time/Depth	Description of Activities/Operations with Depth	
From	To	
	1131	XD = 18.259' H <sub>2</sub> O (draw = 0.028')
	1134	XD = 18.256' H <sub>2</sub> O (draw = 0.031')
	1135	Draw test ended; recovery test started.
	1137	XD = 18.298' H <sub>2</sub> O ( <del>0</del> 100% Rec.)
	1140	XD = 18.298' H <sub>2</sub> O (100% Rec.); Purge truck full - will be emptied before final pump test (top of three sections).
	1143	XD = 18.307' H <sub>2</sub> O (100% Rec.); Recovery test shut off; Layne begins to move pump to third and final stage (10 ft. higher than last stage).
	1304	Purge truck back.
	1310	Problem w/ transducer; pull pipe to find source.
	1340	Problem found and solved
	1345	Initial XD = 0.066' H <sub>2</sub> O
	1347	Begin third draw test; Flow @ 3 GPM
	1350	Kicked flow up to <del>7 GPM</del> 5 GPM
	1351	XD = 0.055' H <sub>2</sub> O (draw = 0.011') @ <del>7 GPM</del> 5 GPM
	1358	XD = 0.040' H <sub>2</sub> O (draw = 0.026') @ <del>6</del> 6 GPM
	1408	XD = 0.016' H <sub>2</sub> O (draw = 0.05') @ 6 GPM
	1424	XD = -0.004' H <sub>2</sub> O ("sucking air") @ 6 GPM
	1425	XD = 0.011' H <sub>2</sub> O (draw = 0.055') @ 6 GPM; Geologist suspects Hermit or transducer of malfunction and non-sense readings to correlate.
	1428	XD = 0.015' H <sub>2</sub> O (draw = 0.051') @ 6 GPM.
	1435	XD = 0.003' H <sub>2</sub> O (draw = 0.063') @ 6 GPM.
	1500	XD = -0.020' H <sub>2</sub> O ("sucking air") @ 6 GPM - transducer out of water, pump intake still in water.
	1505	Stop draw test and begin recovery test.
	1506	XD = -0.010' H <sub>2</sub> O (transducer still out of water)
	1511	XD = 0.008' H <sub>2</sub> O (12% Rec)
	1512	XD = 0.011' H <sub>2</sub> O (16% Rec.)
Reported By: <u>Jess Hocking</u>		Reviewed By: <u>L.D. Walker</u>
Title: <u>Geologist / Hydrogeologist</u>		Title: <u>Geologist</u>
Date: <u>9/2/03</u>		Date: <u>9/24/03</u>
Signature: <u>Jess Hocking</u>		Signature: <u>L.D. Walker</u>


A-6003-652 (04/03)



A-6003-652 (04/03)

FIELD ACTIVITY REPORT - WELL SERVICES					Page <u>1</u> of <u>1</u>	
Date <u>09/18/03</u>	Well No. <u>C4190</u>	Rig Type/Model <u>Pump setting rig</u>	Rig No.	Contract/Work Order No.	Report No.	
Purpose <u>Install pump in C403 RCAF wells.</u>				Reference	Location <u>west of</u> <u>C-Tank Farm</u>	
HISTORICAL DATA			PUMP SYSTEM CONFIGURATION			
Construction Depth <u>310.97' bgs</u>					Pre-Maintenance	Post-Maintenance
Casing Size <u>4" 20 SS 304 sch 10</u>	Type <u>118' - 273.51'</u>	Set At	Pump Type <u>0.7 HP</u>		Grundfos Rediflo 3	
Casing Perforations Schedule			Pump Model <u>Prod. II 94030-139</u>		Model <u>A</u>	
Well Screen(s) Type <u>0.020" slot</u>			Tubing Size/Type <u>0.75" OD SS 304, sch 40</u>			
Interval <u>273.51' - 309.54'</u>			Length-Bottom of Tubing to Pump Intake <u>1.11'</u>			
Last Recorded Depth-to-Water <u>276.52' TOC</u>			Tubing Length <u>280.0'</u>			
Last Recorded Depth-to-Bottom <u>314.4' TOC</u>			Length-Top of Tubing to Reference Point			
Current Depth-to-Water <u>276.46' TOC</u>			Pump Intake Set at (Depth) <u>281.11'</u>			
Current Depth-to-Bottom <u>314.45' TOC</u>			Reference/Measuring Point <u>TOC (TOP OF CASING)</u>			
Start Time <u>1400</u>		Personnel <u>Layne Christensen</u> <u>Dave Dewitt</u> <u>Ken Jones</u> <u>Almer Hanford</u> <u>Ed Rafuse</u> <u>Chazm Hill (CMH)</u> <u>Charlene Martinez</u>		Materials Used <u>28 x 10' long SS 304, schedule 40, 0.75" OD tremmie pipe + couplers</u> <u>0.7 HP Grundfos Rediflo 3 electric submersible pump.</u>		
End Time <u>1630</u>						
Time						
Contract Time						
Total Time <u>2.5 hrs</u>						
Description of Operations/Remarks						
<u>1405 on site from C4127</u>						
<u>1410 Drill crew off site to pick up tremmie pipe + pump for installation.</u>						
<u>1415 Tagged g.w. =&gt; 276.46' TOC</u>						
<u>Tagged TD =&gt; 314.45' TOC</u>						
<u>Still my birthday. Happy birthday to me. Happy birthday to me.</u>						
<u>1440 Drill crew on site. Setting up rig to install Grundfos Rediflo 3 (0.7 Hp) pump.</u>						
<u>1445 Installing pump + tremmie pipe.</u>						
<u>1449 Done</u> <span style="float: right;"><u>09/19/03 tested pump =&gt; works</u></span>						
<u>1458 Lowering mast on pump setting rig.</u> <span style="float: right;"><u>(cm) 09/19/03</u></span>						
<u>1459 Site secure. End of shift.</u>						
<del><u>Charlene Martinez</u> <u>not used</u> <u>09/18/03</u></del>						
Report By <u>Charlene Martinez</u>			Reviewed By <u>L.D. Walker</u>			
Title <u>Geologist</u>			Title <u>Geologist</u>		Date <u>9/30/03</u>	
Signature <u>Charlene Martinez</u>			Signature <u>L.D. Walker</u>			

DISTRIBUTION: White-Field File Custodian Yellow-Group Files Pink-Project Coordinator Goldenrod-Team Leader BC-6000-278 (04/91)

<b>WELL SURVEY DATA REPORT</b>					
<b>Project:</b>			<b>Prepared By:</b> Neil P. Fastabend <b>Company:</b> Fluor Federal Services		
<b>Date Requested:</b> 9/29/03			<b>Requestor:</b> Chris S. Wright (FH)		
<b>Date of Survey:</b> 10/31/03			<b>Surveyor:</b> Fluor Federal Services Survey Dept.		
<b>ERC Point of Contact:</b>			<b>Survey Co. Point of Contact:</b> Grant F. Brazil, P.L.S.		
<b>Description of Work:</b>  Civil Survey of Groundwater Monitoring Well C4190 (299-E27-23).			<b>Horizontal Datum:</b> NAD83(91)		
			<b>Vertical Datum:</b> NAVD88		
			<b>Units:</b> Meters		
			<b>Hanford Area Designation:</b> 200E		
<b>Coordinate System:</b> Washington State Plane Coordinates (South Zone)					
<b>Horizontal Control Monuments:</b> 2E-127 (FFS) and 2E-134 (FFS)					
<b>Vertical Control Monuments:</b> 2E-33 (FFS) and 2E-38 (FFS)					
<b>Well ID</b>	<b>Well Name</b>	<b>Easting</b>	<b>Northing</b>	<b>Elevation</b>	
C4190	299-E27-23	575069.46	136452.23		Center of Casing
				206.563	Top Casing, N. Edge
				205.661	Brass Survey Marker
				206.569	Top Pump Base- plate, N. Edge
<b>Notes:</b>					
<b>Surveyor Statement:</b> I, Grant F. Brazil, a Professional Land Surveyor registered in the State of Washington (Registration No. 22326), hereby certify that this report is based on a field survey performed in October, 2003 under my direct supervision, and that the data contained here is true and correct.					

Original to:  
Distribution by DIS:

## **Appendix B**

### **Sediment Samples Physical Properties Data, Chain of Custody Forms, Core Photographs and Core Log**

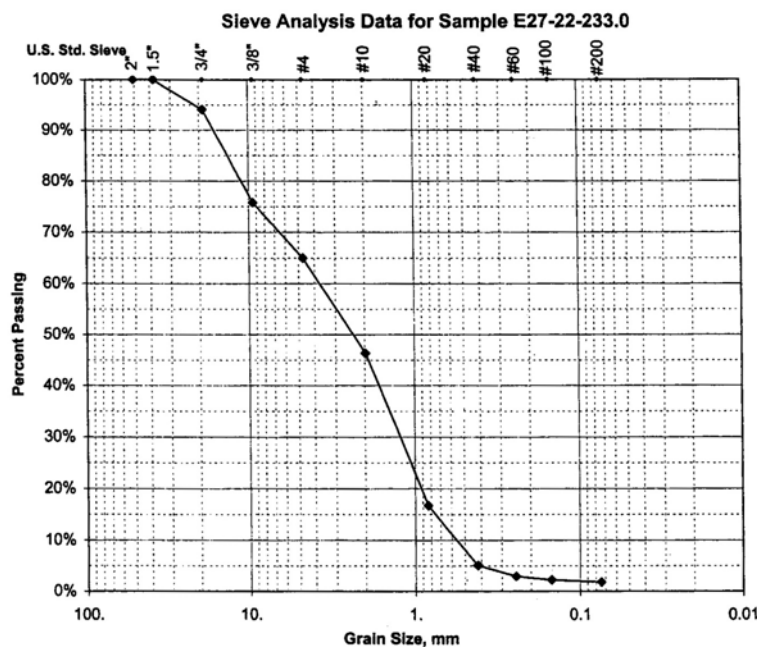
## Appendix B

### Sediment Samples Physical Properties Data, Chain of Custody Forms, Core Photographs and Core Log

CH2M Hill Hanford, Inc.	
<b>SIEVE ANALYSIS</b>	

WELL NAME 299-E27-22	DEPTH 233	SAMPLE# E27-22-233.0	WELL ID# C4124
TESTED BY CRM	CONTACT Dave Weekes	PHONE 372-9350	DATE 09/05/2003

SAMPLE WT (g)	SIEVE SIZE IN.	CUMULATIVE WEIGHT(g)	% WEIGHT RETAINED	% PASSING	Grain Size (mm)	COMMENTS
1495.50	2"	0.0	0.0	100.0	50.80	
	1.5"	0.0	0.0	100.0	38.10	
	3/4"	88.8	5.9	94.1	19.05	
	3/8"	362.9	24.3	75.7	9.42	
	#4	523.8	35.0	65.0	4.70	
	#10	802.3	53.6	46.4	1.98	
	#20	1245.5	83.3	16.7	0.83	
	#40	1419.8	94.9	5.1	0.42	
	#60	1451.8	97.1	2.9	0.25	
	#100	1462.3	97.8	2.2	0.150	
	#200	1468.9	98.2	1.8	0.074	



Comments: Sandy gravel. Sample collected from cyclone.

Sample representative of formation.

All data are accurately and completely recorded.

Checked By: L.D. U&Ket Date: 9/30/03

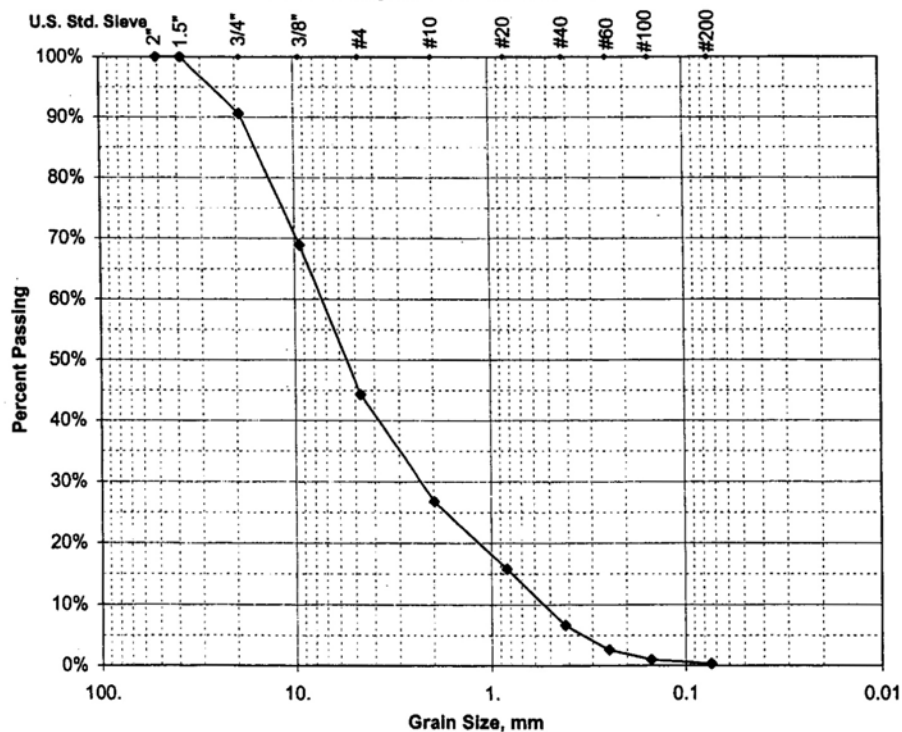
CH2M Hill Hanford, Inc.

SIEVE ANALYSIS

WELL NAME	299-E27-22	DEPTH	268	SAMPLE#	E27-22-268.0	WELL ID#	C4124
TESTED BY	CRM	CONTACT	Dave Weekes	PHONE	372-9350	DATE	09/05/2003

SAMPLE WT (g)	SIEVE SIZE IN.	CUMULATIVE WEIGHT(g)	% WEIGHT RETAINED	% PASSING	Grain Size (mm)	COMMENTS
1417.80	2"	0.0	0.0	100.0	50.80	
	1.5"	0.0	0.0	100.0	38.10	
	3/4"	133.8	9.4	90.6	19.05	
	3/8"	441.1	31.1	68.9	9.42	
	#4	790.1	55.7	44.3	4.70	
	#10	1038.0	73.2	26.8	1.98	
	#20	1193.9	84.2	15.8	0.83	
	#40	1324.0	93.4	6.6	0.42	
	#60	1381.0	97.4	2.6	0.25	
	#100	1403.7	99.0	1.0	0.150	
	#200	1413.5	99.7	0.3	0.074	

Sieve Analysis Data for Sample E27-22-268.0



Comments: Sandy gravel. Sample collected from cyclone.

Sample representative of formation.

All data are accurately and completely recorded.

Checked By: L.D. Walker Date: 9/30/03



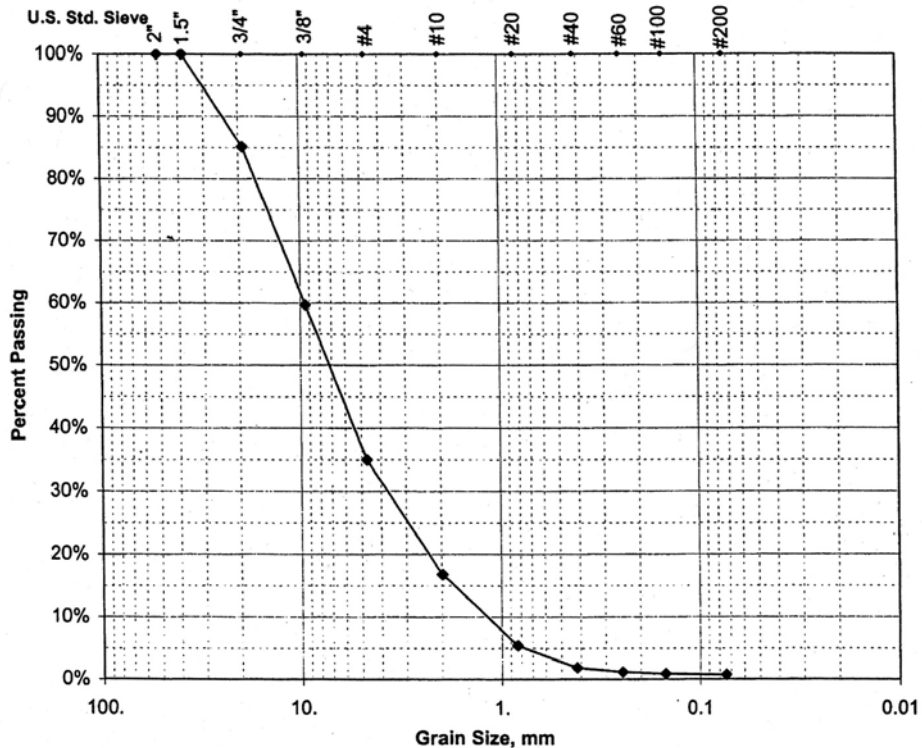
CH2M Hill Hanford, Inc.

SIEVE ANALYSIS

WELL NAME	299-E27-4	DEPTH	270-271	SAMPLE#	E27-4-270.0	WELL ID#	C4125
TESTED BY	CRM	CONTACT	Dave Weekes	PHONE	372-9350	DATE	08/14/2003

SAMPLE WT (g)	SIEVE SIZE IN.	CUMULATIVE WEIGHT(g)	% WEIGHT RETAINED	% PASSING	Grain Size (mm)	COMMENTS
1674.50	2"	0.0	0.0	100.0	50.80	
	1.5"	0.0	0.0	100.0	38.10	
	3/4"	249.2	14.9	85.1	19.05	
	3/8"	675.2	40.3	59.7	9.42	
	#4	1089.0	65.0	35.0	4.70	
	#10	1393.3	83.2	16.8	1.98	
	#20	1583.7	94.6	5.4	0.83	
	#40	1643.4	98.1	1.9	0.42	
	#60	1655.3	98.9	1.1	0.25	
	#100	1659.5	99.1	0.9	0.150	
	#200	1662.3	99.3	0.7	0.074	

Sieve Analysis Data for Sample E27-4-270.0



Comments: Gravel. Sample collected from cyclone.

Sample representative of formation.

All data are accurately and completely recorded.

Checked By: L.D. Walker Date: 9/30/03

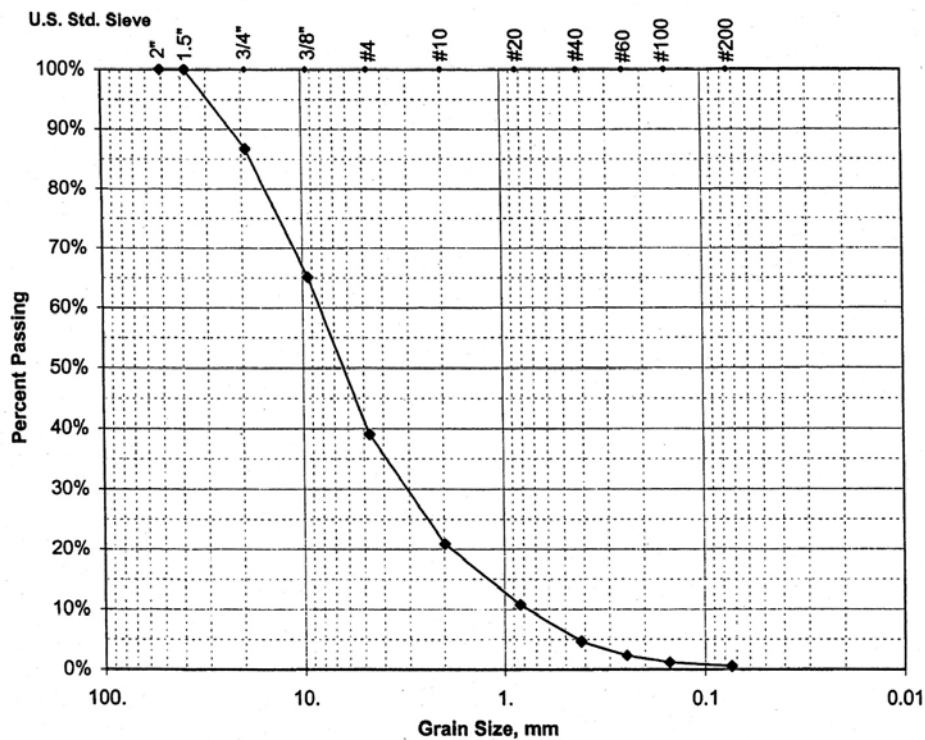
CH2M Hill Hanford, Inc.

SIEVE ANALYSIS

WELL NAME	299-E27-4	DEPTH	301-303	SAMPLE#	E27-4-301.0	WELL ID#	C4125
TESTED BY	CRM	CONTACT	Dave Weekes	PHONE	372-9350	DATE	08/14/2003

SAMPLE WT (g)	SIEVE SIZE IN.	CUMULATIVE WEIGHT(g)	% WEIGHT RETAINED	% PASSING	Grain Size (mm)	COMMENTS
1502.20	2"	0.0	0.0	100.0	50.80	
	1.5"	0.0	0.0	100.0	38.10	
	3/4"	200.4	13.3	86.7	19.05	
	3/8"	524.6	34.9	65.1	9.42	
	#4	916.4	61.0	39.0	4.70	
	#10	1188.8	79.1	20.9	1.98	
	#20	1341.0	89.3	10.7	0.83	
	#40	1431.8	95.3	4.7	0.42	
	#60	1467.0	97.7	2.3	0.25	
	#100	1484.5	98.8	1.2	0.150	
	#200	1494.2	99.5	0.5	0.074	

Sieve Analysis Data for Sample E27-4-301.0



Comments: Sandy gravel. Sample collected from cyclone.

Sample representative of formation.

All data are accurately and completely recorded.

Checked By: *L.D. Walker* Date: *9/30/03*

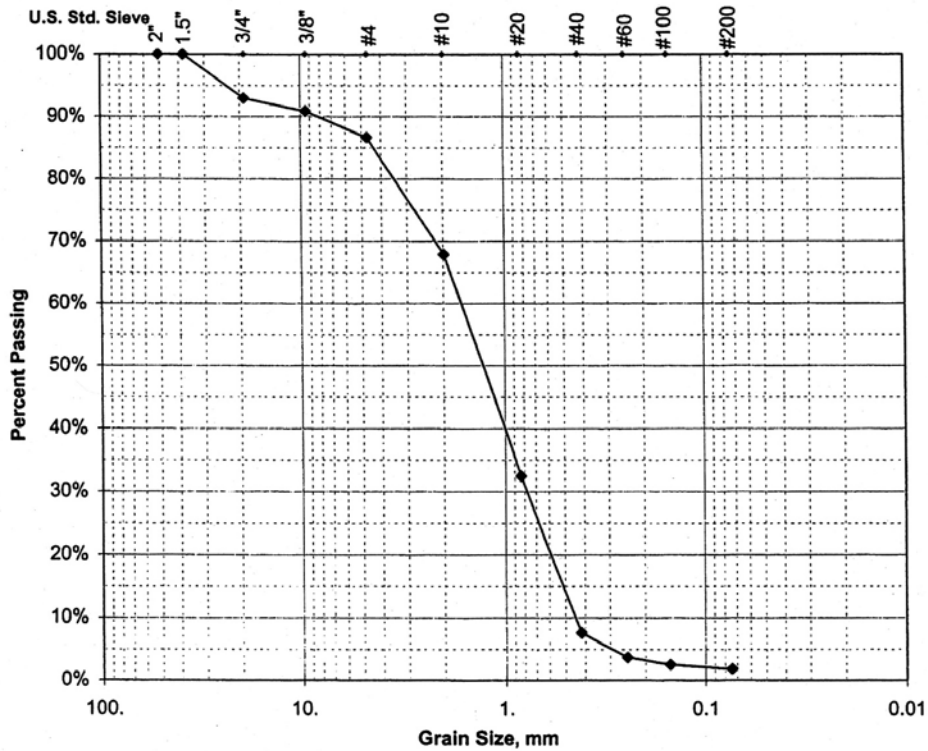
CH2M Hill Hanford, Inc.

SIEVE ANALYSIS

WELL NAME	299-E27-21	DEPTH	277.0-280.0	SAMPLE#	E27-21-277.0	WELL ID#	C4127
TESTED BY	CRM	CONTACT	Dave Weekes	PHONE	372-9350	DATE	07/22/2003

SAMPLE WT (g)	SIEVE SIZE IN.	CUMULATIVE WEIGHT(g)	% WEIGHT RETAINED	% PASSING	Grain Size (mm)	COMMENTS
1625.60	2"	0.0	0.0	100.0	50.80	
	1.5"	0.0	0.0	100.0	38.10	
	3/4"	114.8	7.1	92.9	19.05	
	3/8"	148.8	9.2	90.8	9.42	
	#4	217.2	13.4	86.6	4.70	
	#10	522.5	32.1	67.9	1.98	
	#20	1098.4	67.6	32.4	0.83	
	#40	1502.1	92.4	7.6	0.42	
	#60	1565.5	96.3	3.7	0.25	
	#100	1584.6	97.5	2.5	0.150	
	#200	1596.2	98.2	1.8	0.074	

Sieve Analysis Data for Sample E27-21-277.0



Comments: Gravelly sand. Sample collected from cyclone.

Sample is representative of formation.

All data are accurately and completely recorded.

Checked By: L.D. Walker

Date: 9/30/03

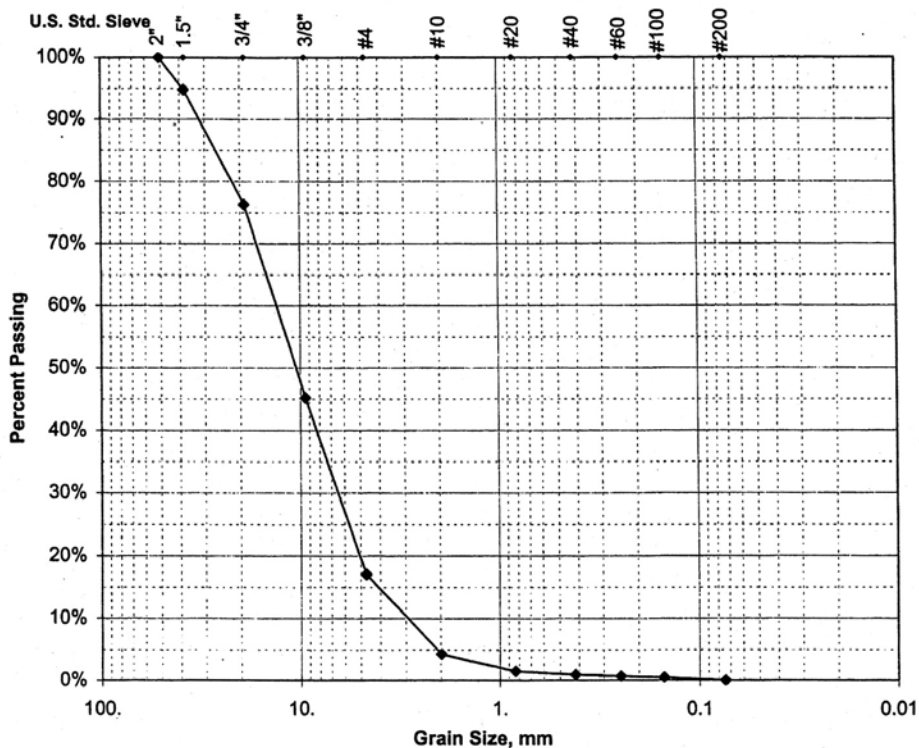
CH2M Hill Hanford, Inc.

SIEVE ANALYSIS

WELL NAME	299-E27-21	DEPTH	312-315	SAMPLE#	E27-21-312.0	WELL ID#	C4127
TESTED BY	CRM	CONTACT	Dave Weekes	PHONE	372-9350	DATE	07/22/2003

SAMPLE WT (g)	SIEVE SIZE IN.	CUMULATIVE WEIGHT(g)	% WEIGHT RETAINED	% PASSING	Grain Size (mm)	COMMENTS
1743.50	2"	0.0	0.0	100.0	50.80	
	1.5"	91.1	5.2	94.8	38.10	
	3/4"	413.1	23.7	76.3	19.05	
	3/8"	956.1	54.8	45.2	9.42	
	#4	1446.6	83.0	17.0	4.70	
	#10	1668.9	95.7	4.3	1.98	
	#20	1717.2	98.5	1.5	0.83	
	#40	1726.5	99.0	1.0	0.42	
	#60	1731.1	99.3	0.7	0.25	
	#100	1735.0	99.5	0.5	0.150	
	#200	1743.5	100.0	0.0	0.074	

Sieve Analysis Data for Sample E27-21-312.0



Comments: Gravel. Sample collected from cyclone. Fines washed away.

Sample not representative of formation.

All data are accurately and completely recorded.

Checked By: L.D. Walker Date: 9/30/03

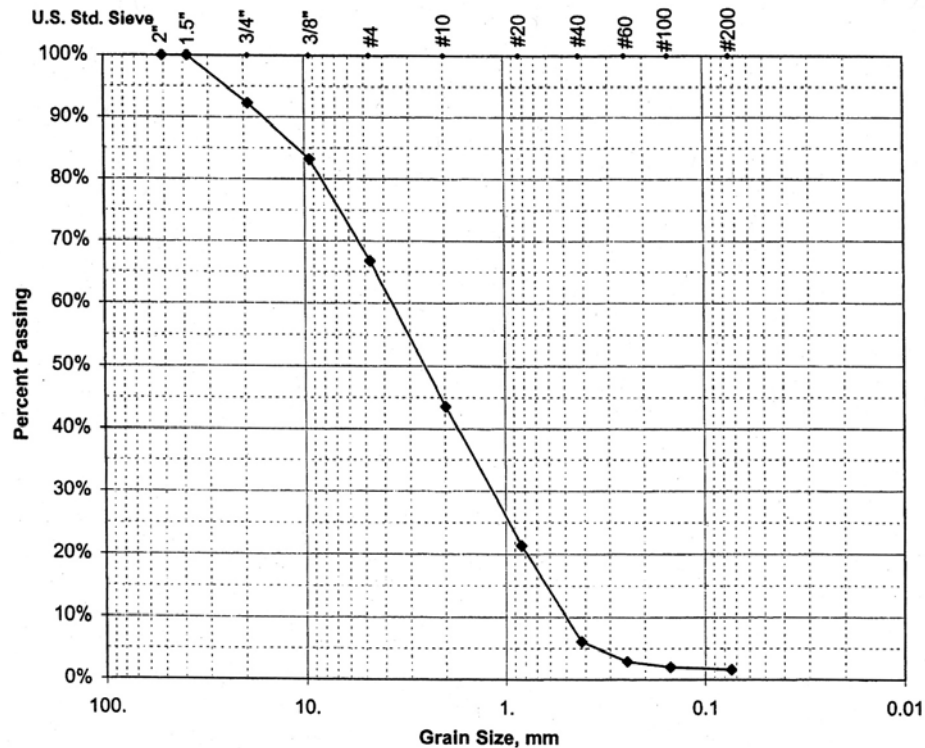
CH2M Hill Hanford, Inc.

SIEVE ANALYSIS

WELL NAME	299-E27-20	DEPTH	275.0-277.0	SAMPLE#	E27-20-275.0	WELL ID#	C4126
TESTED BY	CRM	CONTACT	Dave Weekes	PHONE	372-9350	DATE	07/30/2003

SAMPLE WT (g)	SIEVE SIZE IN.	CUMULATIVE WEIGHT(g)	% WEIGHT RETAINED	% PASSING	Grain Size (mm)	COMMENTS
1669.70	2"	0.0	0.0	100.0	50.80	
	1.5"	0.0	0.0	100.0	38.10	
	3/4"	128.8	7.7	92.3	19.05	
	3/8"	281.1	16.8	83.2	9.42	
	#4	555.7	33.3	66.7	4.70	
	#10	943.2	56.5	43.5	1.98	
	#20	1313.1	78.6	21.4	0.83	
	#40	1568.2	93.9	6.1	0.42	
	#60	1620.7	97.1	2.9	0.25	
	#100	1635.7	98.0	2.0	0.150	
	#200	1642.7	98.4	1.6	0.074	

Sieve Analysis Data for Sample E27-20-275.0



Comments: Sandy gravel. Sample collected from cyclone.

Sample is representative of formation.

All data are accurately and completely recorded.

Checked By: *L.D. Walker*

Date: *9/30/03*

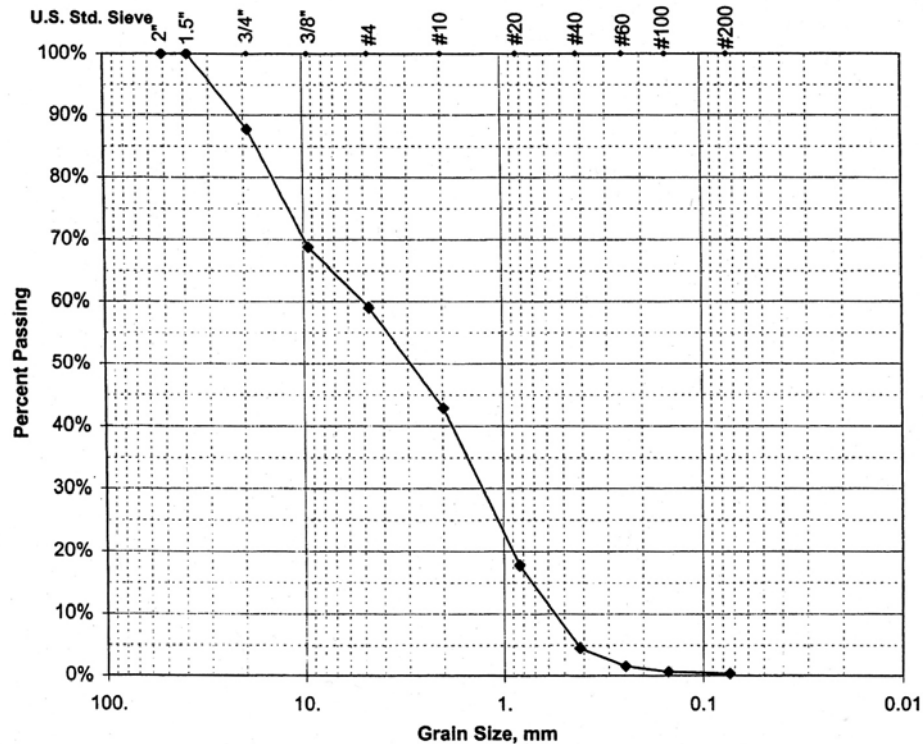
CH2M Hill Hanford, Inc.

SIEVE ANALYSIS

WELL NAME	299-E27-23	DEPTH	310-312	SAMPLE#	E27-23-310.0	WELL ID#	C4190
TESTED BY	CRM	CONTACT	Dave Weekes	PHONE	372-9350	DATE	08/06/2003

SAMPLE WT (g)	SIEVE SIZE IN.	CUMULATIVE WEIGHT(g)	% WEIGHT RETAINED	% PASSING	Grain Size (mm)	COMMENTS
1575.60	2"	0.0	0.0	100.0	50.80	
	1.5"	0.0	0.0	100.0	38.10	
	3/4"	193.2	12.3	87.7	19.05	
	3/8"	492.2	31.2	68.8	9.42	
	#4	645.9	41.0	59.0	4.70	
	#10	901.4	57.2	42.8	1.98	
	#20	1296.2	82.3	17.7	0.83	
	#40	1504.6	95.5	4.5	0.42	
	#60	1551.2	98.5	1.5	0.25	
	#100	1565.1	99.3	0.7	0.150	
	#200	1570.4	99.7	0.3	0.074	

Sieve Analysis Data for Sample E27-23-310.0



Comments: Sandy Gravel. Sample collected from cyclone.

Sample representative of formation.

All data are accurately and completely recorded.

Checked By: L.D. Walker

Date: 9/24/03

C.O.C. No.
------------

Page 1 of 1

Collector Fluor Hanford	Contact/Requestor Chris Wright	Telephone No. 273-3994	MSIN E4-35	FAX
SAF No.	Sample Origin 299-E27-22 (C4124)	Purchase Order/Charge Code		
Project Title C403 RCRA drilling.	Logbook No.	Ice Chest No.	Temp.	
Shipped To (Lab)	Method of Shipment	Bill of Lading/Air Bill No.		
Protocol	Data Turnaround	Offsite Property No.		

[illegible]

POSSIBLE SAMPLE HAZARDS/REMARKS (List all known wastes)		MSDS	<input type="checkbox"/> Yes	<input type="checkbox"/> No
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SPECIAL INSTRUCTIONS

Hold Time

Charlene Martinez Charlene Martinez 08/21/03

Relinquished By	Print	Sign	Date/Time
-----------------	-------	------	-----------

Relinquished By \_\_\_\_\_ Date/Time \_\_\_\_\_

Relinquished By \_\_\_\_\_ Date/Time \_\_\_\_\_

Relinquished By	Date/Time
-----------------	-----------

Received By	Print	Sign
-------------	-------	------

Received By \_\_\_\_\_

Received By \_\_\_\_\_

Received By \_\_\_\_\_

Date/Time

Date/Time

Date/Time

Date/Time

Matrix\*

S = Soil	DS = Drum Solids
SE = Sediment	DL = Drum Liquids
SO = Solid	T = Tissue
SL = Sludge	WI = Wipe
W = Water	L = Liquid
O = Oil	V = Vegetation
A = Air	X = Other

**FINAL SAMPLE  
DISPOSITION**

Disposal Method (e.g., Return to customer, per lab procedure, used in process)	
--	--

Disposed By

Date/Time

All samples containing hazardous materials shall be picked up by requestor and returned to parent container or site of origin.

A-6003-432 (05/02)

B.9

CHAIN OF CUSTODY/SAMPLE ANALYSIS REQUEST										C.O.C. No.	
										Page <u>1</u> of <u>2</u>	
Collector <u>Fluor Hanford</u>				Contact/Requestor <u>Chris Wright</u>				Telephone No. <u>373-3994</u>		MSIN FAX	
SAF No.				Sample Origin <u>299-E 27-22 (C4124)</u>				Purchase Order/Charge Code			
Project Title <u>C403 RCRP drilling</u>				Logbook No.				Ice Chest No.		Temp.	
Shipped To (Lab)				Method of Shipment				Bill of Lading/Air Bill No.			
Protocol				Data Turnaround				Offsite Property No.			
Sample No.	Lab ID	*	Date	Time	No./Type Container	Sample Analysis				Preservative	
C4124-26.5-29.0		S	08/22/03	0655	2 Lexan Liners						
C4124-29.0-31.5		S	08/22/03	0733	2 Lexan Liners						
C4124-31.5-34.0		S	08/22/03	0747	2 Lexan Liners						
C4124-34.0-36.5		S	08/22/03	0814	2 Lexan Liners						
C4124-36.5-39.0		S	08/22/03	0845	2 Lexan Liners						
C4124-39.0-41.5		S	08/22/03	0902	2 Lexan Liners						
C4124-41.5-44.0		S	08/22/03	0926	2 Lexan Liners						
C4124-44.0-46.5		S	08/22/03	0945	2 Lexan Liners						
C4124-46.5-49.0		S	08/22/03	1014	2 Lexan Liners						
C4124-49.0-51.5		S	08/22/03	1035	2 Lexan Liners						
POSSIBLE SAMPLE HAZARDS/REMARKS (List all known wastes) MSDS <input type="checkbox"/> Yes <input type="checkbox"/> No						SPECIAL INSTRUCTIONS					
						Hold Time					
Relinquished By		Print	Sign	Date/Time	Received By		Print	Sign	Date/Time	Matrix*	
Charlene Martinez			Charlene Martinez	08/22/03	RENEA WILLIAMS				8/25/03	S = Soil DS = Drum Solids	
Relinquished By				Date/Time	Received By				Date/Time	SE = Sediment DL = Drum Liquids	
RENEA WILLIAMS				8/25/03	Ginni LECOR				8/25/03	SO = Solid T = Tissue	
Relinquished By				Date/Time	Received By				Date/Time	SL = Sludge WI = Wipe	
Relinquished By				Date/Time	Received By				Date/Time	W = Water L = Liquid	
Relinquished By				Date/Time	Received By				Date/Time	O = Oil V = Vegetation	
Relinquished By				Date/Time	Received By				Date/Time	A = Air X = Other	
FINAL SAMPLE DISPOSITION		Disposal Method (e.g., Return to customer, per lab procedure, used in process)				Disposed By		Date/Time			

All samples containing hazardous materials shall be picked up by requestor and returned to parent container or site of origin.

A-6003-432 (05/02)



CHAIN OF CUSTODY/SAMPLE ANALYSIS REQUEST							C.O.C. No.	
							Page <u>2</u> of <u>2</u>	
Collector <u>Fluor Hanford</u>			Contact/Requestor <u>Chris Wright</u>			Telephone No. <u>373-3994</u> MSIN FAX		
SAF No.			Sample Origin <u>299-E27-22 (C4124)</u>			Purchase Order/Charge Code		
Project Title <u>C403 RCRA Drilling</u>			Logbook No.			Ice Chest No. Temp.		
Shipped To (Lab)			Method of Shipment			Bill of Lading/Air Bill No.		
Protocol			Data Turnaround			Offsite Property No.		
Sample No.	Lab ID	*	Date	Time	No./Type Container	Sample Analysis		Preservative
<u>C4124-51.5-54.0</u>		<u>S</u>	<u>08/22/03</u>	<u>1100</u>	<u>2 Lexan Liners</u>			
<u>C4124-54.0-56.5</u>		<u>S</u>	<u>08/22/03</u>	<u>1121</u>	<u>2 Lexan Liners</u>			
<u>C4124-56.5-59.0</u>		<u>S</u>	<u>08/22/03</u>	<u>1253</u>	<u>2 Lexan Liners</u>			
<u>C4124-61.5-64.0</u>		<u>S</u>	<u>08/22/03</u>	<u>1341</u>	<u>2 Lexan Liners</u>			
<u>C4124-64.0-66.5</u>		<u>S</u>	<u>08/22/03</u>	<u>1404</u>	<u>1 Lexan Liner</u>	<u>64 - 65 - EMPTY - NO RECOVERY</u>		
<u>C4124-66.5-69.0</u>		<u>S</u>	<u>08/22/03</u>	<u>1435</u>	<u>2 Lexan Liners</u>			
POSSIBLE SAMPLE HAZARDS/REMARKS (List all known wastes)					MSDS <input type="checkbox"/> Yes <input type="checkbox"/> No		SPECIAL INSTRUCTIONS	
							Hold Time	
Relinquished By		Print	Sign	Date/Time	Received By		Print	Sign
<u>Charlene Martinez</u>		<u>Charlene Martinez</u>		<u>08/22/03</u>	<u>BRUCE WILLIAMS</u>		<u>Bruce Williams</u>	
Relinquished By				Date/Time	Received By			Date/Time
<u>Bruce A. Williams</u>				<u>8/25/03 10:00</u>	<u>Ginny Leggett</u>		<u>Ginny Leggett</u>	<u>8/25/03 10:00</u>
Relinquished By				Date/Time	Received By			Date/Time
Relinquished By				Date/Time	Received By			Date/Time
Relinquished By				Date/Time	Received By			Date/Time
Relinquished By				Date/Time	Received By			Date/Time
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Relinquished By				Date/Time	Received By			Date/Time
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Relinquished By				Date/Time	Received By			Date/Time
Relinquished By			</					

CHAIN OF CUSTODY/SAMPLE ANALYSIS REQUEST							C.O.C. No.	
							Page <u>1</u> of <u>1</u>	
Collector <u>Fluor Hanford</u>			Contact/Requestor <u>Chris Wright</u>			Telephone No. <u>373-3994</u> MSIN FAX		
SAF No.			Sample Origin <u>299-E27-22 (C4124)</u>			Purchase Order/Charge Code		
Project Title <u>C403 RCRA drilling</u>			Logbook No.			Ice Chest No. Temp.		
Shipped To (Lab)			Method of Shipment			Bill of Lading/Air Bill No.		
Protocol			Data Turnaround			Offsite Property No.		
Sample No.	Lab ID	*	Date	Time	No./Type Container	Sample Analysis		Preservative
<u>C4124-71.5-74.0</u>	<u>S</u>	<u>08/25/03</u>	<u>0735</u>	<u>2 Lexan Liners</u>				
<u>C4124-74.0-76.5</u>	<u>S</u>	<u>08/25/03</u>	<u>0803</u>	<u>2 Lexan Liners</u>				
<u>C4124-76.5-79.0</u>	<u>S</u>	<u>08/25/03</u>	<u>0842</u>	<u>2 Lexan Liners</u>				
<u>C4124-79.0-81.5</u>	<u>S</u>	<u>08/25/03</u>	<u>0918</u>	<u>2 Lexan Liners</u>				
<u>C4124-81.5-84.0</u>	<u>S</u>	<u>08/25/03</u>	<u>0950</u>	<u>2 Lexan Liners</u>				
<u>C4124-84.0-86.5</u>	<u>S</u>	<u>08/25/03</u>	<u>1017</u>	<u>2 Lexan Liners</u>				
<u>C4124-86.5-89.0</u>	<u>S</u>	<u>08/25/03</u>	<u>1100</u>	<u>2 Lexan Liners</u>				
<u>C4124-89.0-91.5</u>	<u>S</u>	<u>08/25/03</u>	<u>1123</u>	<u>2 Lexan Liners</u>				
<u>C4124-91.5-94.0</u>	<u>S</u>	<u>08/25/03</u>	<u>1236</u>	<u>2 Lexan Liners</u>				
<u>C4124-94.0-96.5</u>	<u>S</u>	<u>08/25/03</u>	<u>1308</u>	<u>2 Lexan Liners</u>				
POSSIBLE SAMPLE HAZARDS/REMARKS (List all known wastes) MSDS <input type="checkbox"/> Yes <input type="checkbox"/> No					SPECIAL INSTRUCTIONS			
					Hold Time			
Relinquished By		Print	Sign	Date/Time	Received By		Print	Sign
<u>Charlene Martinez</u>		<u>Charlene Martinez</u>	<u>08/25/03</u>	<u>08/23/03</u>	<u>BOB WILLIAMS</u>		<u>Bob Williams</u>	<u>08/23/03</u>
Relinquished By		Date/Time	Received By		Date/Time	Matrix*		
<u>BOB WILLIAMS</u>		<u>8/27/03</u>	<u>Ray Clayton</u>		<u>8/27/03</u>	S = Soil DS = Drum Solids		
Relinquished By		Date/Time	Received By		Date/Time	SE = Sediment DL = Drum Liquids		
						SO = Solid T = Tissue		
						SL = Sludge WI = Wipe		
						W = Water L = Liquid		
						O = Oil V = Vegetation		
						A = Air X = Other		
Relinquished By		Date/Time	Received By		Date/Time			
FINAL SAMPLE DISPOSITION		Disposal Method (e.g., Return to customer, per lab procedure, used in process)				Disposed By		
						Date/Time		

All samples containing hazardous materials shall be picked up by requestor and returned to parent container or site of origin.

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CHAIN OF CUSTODY/SAMPLE ANALYSIS REQUEST							C.O.C. No.	
							Page <u>1</u> of <u>2</u>	
Collector <u>Fluor Hanford</u>			Contact/Requestor <u>Chris Wright</u>			Telephone No. <u>373-3994</u> MSIN FAX		
SAF No.			Sample Origin <u>299-BA7-22 (C4124)</u>			Purchase Order/Charge Code		
Project Title <u>C403 REEA drilling</u>			Logbook No.			Ice Chest No. Temp.		
Shipped To (Lab)			Method of Shipment			Bill of Lading/Air Bill No.		
Protocol			Data Turnaround			Offsite Property No.		
Sample No.	Lab ID	*	Date	Time	No./Type Container	Sample Analysis		Preservative
✓ C4124-96.5-99.0		S	08/26/03	0645	2 Lexan Liners			
✓ C4124-99-101.5		S	"	0714	"			
✓ C4124-101.5-104.0		S	"	0747	"			
✓ C4124-104.0-106.5		S	"	0817	"			
✓ C4124-106.5-109.0		S	08/26/03	0859	2 Lexan Liners			
✓ C4124-109.0-111.5		S	"	0928	"			
✓ C4124-111.5-114.0		S	"	1026	"			
✓ C4124-114.0-121.5		S	"	1104	"			
✓ C4124-121.5-126.5		S	"	1143	"			
✓ C4124-126.5-129.0		S	08/26/03	1310	2 Lexan Liners			
POSSIBLE SAMPLE HAZARDS/REMARKS (List all known wastes) MSDS <input type="checkbox"/> Yes <input type="checkbox"/> No						SPECIAL INSTRUCTIONS Hold Time		
Relinquished By Print Sign		Date/Time		Received By Print Sign		Date/Time		Matrix*
Charlene Martinez / Charlene Martinez		08/26/03		Bruce Williams / Bruce Williams		8/27/03 1100		S = Soil DS = Drum Solids
Relinquished By		Date/Time		Received By		Date/Time		SE = Sediment DL = Drum Liquids
Bruce Williams / Bruce Williams		8/27/03 1100		Ray Clayton / Ray Clayton		8/27/03 1100		SO = Solid T = Tissue
Relinquished By		Date/Time		Received By		Date/Time		SL = Sludge WI = Wipe
								W = Water L = Liquid
Relinquished By		Date/Time		Received By		Date/Time		O = Oil V = Vegetation
								A = Air X = Other
FINAL SAMPLE DISPOSITION	Disposal Method (e.g., Return to customer, per lab procedure, used in process)			Disposed By			Date/Time	

All samples containing hazardous materials shall be picked up by requestor and returned to parent container or site of origin.

A-6003-432 (05/02)

CHAIN OF CUSTODY/SAMPLE ANALYSIS REQUEST							C.O.C. No.	
							Page <u>2</u> of <u>2</u>	
Collector <u>Fluor Hanford</u>			Contact/Requestor <u>CHRIS WRIGHT</u>			Telephone No. <u>373-3994</u> MSIN FAX		
SAF No.			Sample Origin <u>299-627-23</u>			Purchase Order/Charge Code		
Project Title <u>C403 RCEA drilling</u>			Logbook No.			Ice Chest No. Temp.		
Shipped To (Lab)			Method of Shipment			Bill of Lading/Air Bill No.		
Protocol			Data Turnaround			Offsite Property No.		
Sample No.	Lab ID	*	Date	Time	No./Type Container	Sample Analysis		Preservative
<u>C4124-134.0-136.5</u>	<u>S</u>	<u>08/24/03</u>	<u>1401</u>	<u>2 Lexan Liners</u>				
<u>C4124-139.0-141.5</u>	<u>S</u>	<u>11</u>	<u>1446</u>	<u>11</u>				
<u>C4124-144.0-146.5</u>	<u>S</u>	<u>08/26/03</u>	<u>1545</u>	<u>2 Lexan Liners</u>				
POSSIBLE SAMPLE HAZARDS/REMARKS (List all known wastes)					MSDS <input type="checkbox"/> Yes <input type="checkbox"/> No		SPECIAL INSTRUCTIONS	
							Hold Time	
Relinquished By		Print	Sign	Date/Time	Received By		Print	Sign
<u>Charlene Martinez</u>		<u>Charlene Martinez</u>	<u>08/26/03</u>	<u>11:00</u>	<u>Ray Clayton</u>		<u>Ray Clayton</u>	<u>8/27/03</u>
Relinquished By		Date/Time	Received By		Date/Time	Matrix*		
<u>RA WILLIAMS</u>		<u>8/27/03</u>	<u>Ray Clayton</u>		<u>11:00</u>	S = Soil DS = Drum Solids		
Relinquished By		Date/Time	Received By		Date/Time	SE = Sediment DL = Drum Liquids		
						SO = Solid T = Tissue		
						SL = Sludge WI = Wipe		
						W = Water L = Liquid		
						O = Oil V = Vegetation		
						A = Air X = Other		
Relinquished By		Date/Time	Received By		Date/Time			
Relinquished By		Date/Time	Received By		Date/Time			
Relinquished By		Date/Time	Received By		Date/Time			
FINAL SAMPLE DISPOSITION		Disposal Method (e.g., Return to customer, per lab procedure, used in process)				Disposed By		Date/Time

CHAIN OF CUSTODY/SAMPLE ANALYSIS REQUEST										C.O.C. No.	
										Page <u>1</u> of <u>1</u>	
Collector <u>Fiber Hamford</u>				Contact/Requestor <u>Chris Wright</u>				Telephone No. <u>373-3994</u> MSIN FAX			
SAF No.				Sample Origin <u>299-627-22 (C4124)</u>				Purchase Order/Charge Code			
Project Title <u>C403 RCRA drilling</u>				Logbook No.				Ice Chest No. Temp.			
Shipped To (Lab)				Method of Shipment				Bill of Lading/Air Bill No.			
Protocol				Data Turnaround				Offsite Property No.			
Sample No.	Lab ID	*	Date	Time	No./Type Container	Sample Analysis				Preservative	
C4124-149.0-151.5	S		08/27/03	0707	2 Lexan Liners						
C4124-154.0-156.5	S		"	0821	1 Lexan Liner						
C4124-159.0-161.5	S		08/27/03	0915	2 Lexan Liners						
C4124-164.0-166.5	S		"	1018	"						
C4124-169.0-171.5	S		08/27/03	1115	2 Lexan Liners						
C4124-174.0-176.5	S		"	1307	"						
C4124-179.0-181.5	S		08/27/03	1354	2 Lexan Liners						
C4124-184.0-186.5	S		"	1454	"						
C4124-189.0-191.5	S		08/27/03	1549	2 Lexan Liners						
POSSIBLE SAMPLE HAZARDS/REMARKS (List all known wastes) MSDS <input type="checkbox"/> Yes <input type="checkbox"/> No						SPECIAL INSTRUCTIONS					
						Hold Time					
Relinquished By <u>Print</u> <u>Sign</u>			Date/Time			Received By <u>Print</u> <u>Sign</u>			Date/Time		
<u>Charles Martinez</u>			<u>08/27/03</u>			<u>RECEA WILLIAMS</u>			<u>9/3/03</u>		
Relinquished By <u>Print</u> <u>Sign</u>			Date/Time			Received By <u>Print</u> <u>Sign</u>			Date/Time		
<u>RECEA WILLIAMS</u>			<u>9/3/03</u>			<u>Tanya V. Green</u>			<u>9/3/03 1340</u>		
Relinquished By			Date/Time			Received By			Date/Time		
Relinquished By			Date/Time			Received By			Date/Time		
Matrix*											
S = Soil					DS = Drum Solids						
SE = Sediment					DL = Drum Liquids						
SO = Solid					T = Tissue						
SL = Sludge					WI = Wipe						
W = Water					L = Liquid						
O = Oil					V = Vegetation						
A = Air					X = Other						
FINAL SAMPLE DISPOSITION		Disposal Method (e.g., Return to customer, per lab procedure, used in process)				Disposed By				Date/Time	

All samples containing hazardous materials shall be picked up by requestor and returned to parent container or site of origin.

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CHAIN OF CUSTODY/SAMPLE ANALYSIS REQUEST										C.O.C. No. _____	
										Page <u>1</u> of <u>1</u>	
Collector <u>Fluor Hanford</u>				Contact/Requestor <u>Chris Wright</u>				Telephone No. <u>373-3994</u> MSIN FAX			
SAF No.				Sample Origin <u>299-E27-22 (C4124)</u>				Purchase Order/Charge Code			
Project Title <u>C403 RCRA drilling</u>				Logbook No.				Ice Chest No. Temp.			
Shipped To (Lab)				Method of Shipment				Bill of Lading/Air Bill No.			
Protocol				Data Turnaround				Offsite Property No.			

Sample No.	Lab ID	*	Date	Time	No./Type Container	Sample Analysis	Preservative
C4124-194.0-196.5		S	09/02/03	0749	2 Lexan Liners		
C4124-199.0-201.5		S	09/02/03	0925	2 Lexan Liners		
C4124-204.0-206.5		S	09/02/03	1029	2 Lexan Liners		
C4124-209.0-211.5		S	09/02/03	1125	2 Lexan Liners		
C4124-214.0-216.5		S	09/02/03	1324	2 Lexan Liners	MISS LABELED (?) 2 SETS OF 209-211.5	
C4124-219.0-221.5		S	09/02/03	1448	1 Lexan Liner		
C4124-224.0-226.5		S	09/02/03	1548	2 Lexan Liners		

POSSIBLE SAMPLE HAZARDS/REMARKS (List all known wastes) MSDS <input type="checkbox"/> Yes <input type="checkbox"/> No		SPECIAL INSTRUCTIONS		Hold Time

Relinquished By <u>Print</u> <u>Sign</u> <u>Date/Time</u>		Received By <u>Print</u> <u>Sign</u> <u>Date/Time</u>		<b>Matrix*</b> S = Soil      DS = Drum Solids SE = Sediment    DL = Drum Liquids SO = Solid      T = Tissue SL = Sludge      WI = Wipe W = Water      L = Liquid O = Oil          V = Vegetation A = Air          X = Other
<u>Charlene Martinez</u> <u>Charlene Martinez</u> <u>09/02/03</u> <u>TRACY WILLIAMS</u> <u>TRACY WILLIAMS</u> <u>9/3/03 13:40</u>		<u>RENEA WILLIAMS</u> <u>RENEA WILLIAMS</u> <u>9/3/03 08:00</u> <u>Tanya Vickerman</u> <u>Tanya Vickerman</u> <u>9/3/03 1340</u>		
Relinquished By <u>Date/Time</u>		Received By <u>Date/Time</u>		
Relinquished By <u>Date/Time</u>		Received By <u>Date/Time</u>		
Relinquished By <u>Date/Time</u>		Received By <u>Date/Time</u>		

FINAL SAMPLE DISPOSITION	Disposal Method (e.g., Return to customer, per lab procedure, used in process)	Disposed By	Date/Time

All samples containing hazardous materials shall be picked up by requestor and returned to parent container or site of origin.

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C.O.C. No. \_\_\_\_\_

Page 1 of 1

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POSSIBLE SAMPLE HAZARDS/REMARKS (List all known wastes)	MSDS	<input type="checkbox"/> Yes	<input type="checkbox"/> No	SPECIAL INSTRUCTIONS	Hold Time
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Relinquished By	Print	Sign	Date/Time	Received By	Print	Sign	Date/Time	Matrix*	
Charlene Martinez	Charlene Martinez		09/03/03	RENEA WILLIAMS	RENEA WILLIAMS		9/3/03 0857	S = Soil	DS = Drum Solids
Relinquished By			Date/Time	Received By			Date/Time	SE = Sediment	DL = Drum Liquids
RENEA WILLIAMS			09/03/03	Tanya Vickerman	Tanya Vickerman		1340 9/3/03	SO = Solid	T = Tissue
Relinquished By			Date/Time	Received By			Date/Time	SL = Sludge	WI = Wipe
								W = Water	L = Liquid
Relinquished By			Date/Time	Received By			Date/Time	O = Oil	V = Vegetation
								A = Air	X = Other

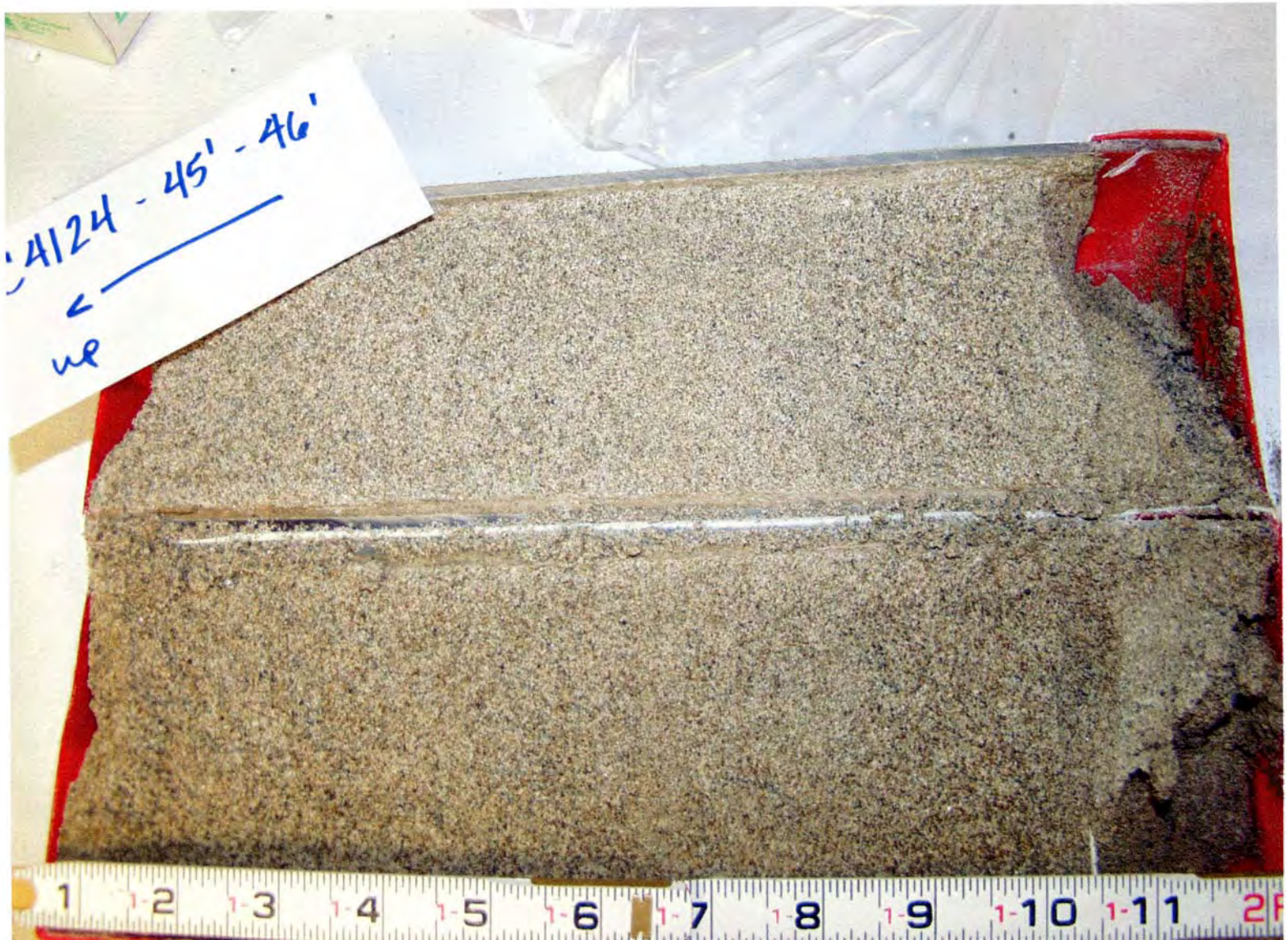
FINAL SAMPLE DISPOSITION	Disposal Method (e.g., Return to customer, per lab procedure, used in process)	Disposed By	Date/Time

All samples containing hazardous materials shall be picked up by requestor and returned to parent container or site of origin.

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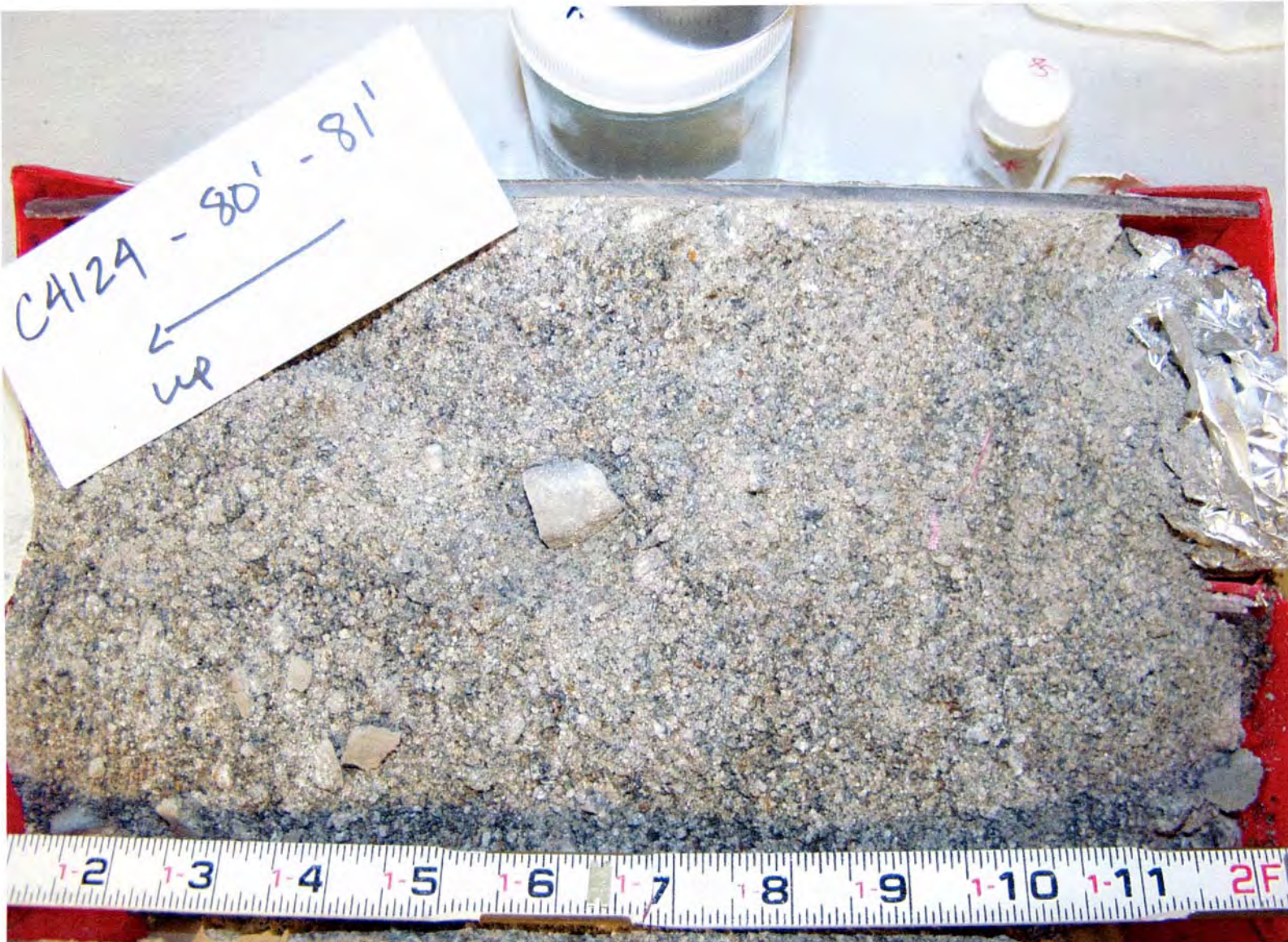




















Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124 (299-E21-22)</u>		Depth <u>19-25'</u>	Date <u>10-28-03</u>	Sheet <u>1</u> of <u>23</u>	
Location <u>C Tank Farm</u>				Project <u>Vadose Zone</u>					
Logged by <u>RNBjornstad</u>						Drilling Contractor _____			
Reviewed by _____						Date _____			
Lithologic Class. Scheme _____						Procedure _____ Rev _____			
Steel Tape/E-Tape <u>1</u>						Field Indicator Equip. 1) _____ 2) _____			
						Driller _____			
						Rig/Method _____			
						Depth Control Point _____			

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
19		SS				SM	0	0	0	0				Cores collected in late August - stored at room temp. for about two months.
							0	0	0	0				
20		SS					0	0	0	0				SI = slough
							0	0	0	0				
21							0	0	0	0				mostly cgs sand to fin pebbles, 60-70% bas
							0	0	0	0				
21.5						SM	0	0	0	0				sand, mid-crs, wkly stratified, oxidized blebs, 30-40% bas, 1st clast = 1cm, loose, wk rxn w/ HCl, 2.5x 5/2, poorly sorted
							0	0	0	0				
22.5							0	0	0	0				1st clast = 2cm
							0	0	0	0				
23.5							0	0	0	0				pebbly sand, v loose, 2.5x 5/2 1st clast = 2cm 40-50% basalt, subangular no rxn w/ HCl, massive
							0	0	0	0				
24						D	0	0	0	0				
25							0	0	0	0				

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DCL001

B.25

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>25-31'</u>	Date <u>10-28-03</u>	Sheet <u>2</u> of <u>23</u>
				Location <u>C Tank Farm</u>		Project <u>Vadose Zone</u>		
Logged by <u>BN Bjornstad</u>						Drilling Contractor _____		
Reviewed by _____						Driller _____		
Lithologic Class. Scheme _____						Rig/Method _____		
Steel Tape/E-Tape <u>1</u>						Depth Control Point _____		
Field Indicator Equip. 1) _____ 2) _____								

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG	LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING						
25		S.S.				D		pebbly sand, loose, msv, S = 30-40% bas. max part size = 1.5 cm, poorly sorted, 2.5 x 5/2 (dry), no rxn w/ HCl			
26						↓		20% fin pebbles, 50% crs sand, 30% fin-mid sand			
26.5		S.S.				D		empty			
27.5		S.S.				↓		poorly sorted, loose, msv sand			
28.5						↓		pebbly sand, mod. strong rxn w/ HCl, 20% pebbles 80% sand, S = 40-50% bas. loose, msv, max part size = 1cm, poorly sorted			
29		S.S.				D		empty			
30		S.S.				SM		pebbly sand, max part = 3cm, poorly sorted, msv, wk rxn w/ HCl, S = 40-50% bas larger clasts @ top, no rxn w/ HCl 5% fin pebbles, 60% crs sand, 30% fin-mid sand			fine sample
31						↓					

W = Wet, M = Moist, D = Dry

1998/DCU/PROC/DBL/001



Pacific Northwest National Laboratory		DAILY BOREHOLE LOG		Boring/Well No <u>C4124</u>		Depth <u>31.5-37.5'</u>		Date <u>10/28/03</u>		Sheet <u>3</u> of <u>23</u>	
Location <u>C Tank Farm</u>				Project <u>Vadose Zone</u>							
Logged by <u>BN Bjornstad</u>						Drilling Contractor _____					
Reviewed by _____						Driller _____					
Lithologic Class. Scheme _____						Procedure _____ Rev _____					
Steel Tape/E-Tape <u>1</u>						Field Indicator Equip. 1) _____ 2) _____					
Depth Control Point _____											

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
31.5		S.S.				D								
32.5		S.S.												
33.5														
34		S.S.				SM								
35		S.S.												
36														
36.5						SN								
37.5														

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DBL/001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>37.5-43.5'</u>		Date <u>10-28-03</u>		Sheet <u>4</u> of <u>23</u>	
				Location <u>C Tank Farm</u>		Project <u>Vadose Zone</u>					
Logged by <u>B. L. Bjornstad</u>						Drilling Contractor _____					
Reviewed by _____						Driller _____					
Lithologic Class. Scheme _____						Procedure _____					
Rev _____						Rig/Method _____					
Steel Tape/E-Tape <u>1</u>						Field Indicator Equip. 1) _____ 2) _____					
Depth Control Point _____											

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)	
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G					
37.5		S.S.				SM									
38.5															
39		S.S.				SM									
40		S.S.													
41															
41.5		S.S.				SM									
42.5		S.S.													
43.5															

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DBL/001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>44-50'</u>	Date <u>10-28-03</u>	Sheet <u>5</u> of <u>23</u>
Location <u>C Tank Farm</u>				Project <u>Vadoso Zone</u>				
Logged by <u>B. N. Bjornstad</u>						Drilling Contractor _____		
Reviewed by _____						Driller _____		
Lithologic Class. Scheme _____						Rig/Method _____		
Steel Tape/E-Tape _____						Depth Control Point _____		
Field Indicator Equip. 1) _____ 2) _____								

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
44		S.S.				SM				SI?	msv fin. sand, loose			
											silty fin. sand, mottled (paleosol?)			? paleosol - thin?
											sand, fin. med, well sorted, compact			
											massive, 15-20% mafic			
45		J.S.									2.5 Y 5/3, wk rxn w/ HCl, max			
											part. size: med sand, mottled			
											toward base?			
46						V								
46.5		S.S.				SM				SI	loose, fine sand, 2.5 Y 6/2			
											sand, fin. med, well sorted, wkly lam.			
											compact, 2.5 Y 5/3, max part. size = crs sand			
47.5		S.S.									15-20% mafic			
						V								sharp contact
						M				PM	silty fin. sand, well lam. 10 YR 5/3 (fine) brown			paleosol synth @ 48.2'
48.5											v. well sorted, crscons downward, compact			mod rxn w/ HCl
49		S.S.				SM				SI	pebbly sand, loose, poorly sorted			
						D					pebbly sand, mostly crs to v. crs sand, poorly sorted, loose, msv			
											max part. size = 5mm, S = 50-60% basalt			5% fin pebbles, 70% crs-v. crs S,
50						V					25% fin. med sand, mod rxn w/ HCl			

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DBL/001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>50-56'</u>		Date <u>10/28/03</u>		Sheet <u>6</u> of <u>23</u>	
				Location <u>C Tank Farm</u>		Project <u>Vadoso Zone</u>					
Logged by <u>B N Bjornstad</u>						Drilling Contractor _____					
Reviewed by _____ Date _____						Driller _____					
Lithologic Class. Scheme _____ Procedure _____ Rev _____						Rig/Method _____					
Steel Tape/E-Tape <u>1</u>						Field Indicator Equip. 1) _____ 2) _____					
						Depth Control Point _____					

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
50		S.S.				D								
51						↓								
51.5		S.S.				M								
						↓								
52.5		S.S.				D								
53.5						↓								
54		S.S.				D								
55		S.S.												
56						↓								

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DBL/001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>				Boring/Well No. <u>C4124</u>		Depth <u>56.5-66.0'</u> Date <u>10/28/03</u>		Sheet <u>7</u> of <u>23</u>	
Location <u>C Tank Farm</u>						Project <u>Vadose Zone</u>					
Logged by <u>BN Bjornstad</u>								Drilling Contractor _____			
Reviewed by _____ Date _____								Driller _____			
Lithologic Class. Scheme _____ Procedure _____ Rev _____								Rig/Method _____			
Steel Tape/E-Tape _____ / _____ Field Indicator Equip. 1) _____ 2) _____								Depth Control Point _____			

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
56.5		S.S.				D	o o sl				pebbly sand, loose, poorly sorted			
							o o				Sand, 80% crs. vcrs, 20% fm.			
											md. mod. sorted, 2.5-5/2,			
											Max part size - 3cm			
57.5		S.S.					o o				clasts up to 3cm			
											S = 70-80% basalt, salt and pepper			
58.5							o o							
61.5		S.S.				D	o o o o				Sandy gravel, lgst clast = 5cm, loose, msV			
											Pebbly sand, poorly sorted, loose, msV,			
											2.5-5/3. Fe oxide kldis and rootings,			
62.5							o o				lgst clast = 5mm S = 60-70% basalt			
		S.S.									Salt and pepper, wk rxn w/ HCl			
63.5							o o							
65.0		S.S.				D	o o o o				All slaty? Angular gravel w/ little			
											matrix			
											loose, v. poorly sorted silty fcrs			
66.0							o o				sand 2.5-6/2			

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DBL/001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>66.5-75.0'</u>	Date <u>10/29/03</u>	Sheet <u>8</u> of <u>23</u>	
				Location <u>C Tank Farm</u>		Project <u>Vadose Zone</u>			
Logged by <u>BN Bjornstad</u>				Drilling Contractor _____					
Reviewed by _____				Date _____				Driller _____	
Lithologic Class. Scheme _____				Procedure _____				Rev _____	
Steel Tape/E-Tape _____				Field Indicator Equip. 1) _____				2) _____	
				Rig/Method _____				Depth Control Point _____	

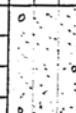


DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
66.5		S.S.				▷								
67.5		S.S.												
68.5						↓								
71.5		S.S.				▷								
72.5		S.S.												
73.5						↓								
74		S.S.				▷								
75						↓								

W = Wet, M = Moist, D = Dry

1998/DCU/PROC/DBL/001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u> Location <u>C Tank Farm</u>		Depth <u>75-81'</u> Project <u>Vadose Zone</u>		Date <u>10-29-03</u> Sheet <u>9</u> of <u>23</u>	
Logged by <u>B N Bjornstad</u>						Drilling Contractor _____			
Reviewed by _____ Date _____						Driller _____			
Lithologic Class. Scheme _____ Procedure _____ Rev _____						Rig/Method _____			
Steel Tape/E-Tape _____ / _____ Field Indicator Equip. 1) _____ 2) _____						Depth Control Point _____			

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION <small>(particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)</small>	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS <small>(drilling rate, down time, blow counts, water level, drill fluid, etc.)</small>
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
75		s.s.				D							slightly pebbly sand, 5% sm. pebbles, 50% crs-v. crs sand, 2.5 Y 5/2 40% fn-mud. sand, mod. sorted, msy, loose, S = 40-50% basalt, wk rxn w/ HCl	
						I								
76						Y								
76.5		s.s.				SM							slightly pebbly sand, ≤ 5% sm. pebbles 50-60% crs-v. crs sand, 30-40% fn-mud sand msv, loose, 1st clast = 1cm, S = 50-60% basalt mod. sorted, wk rxn w/ HCl	
77.5		s.s.												
78.5						Y								
79		s.s.				D							silty pebbly sand, loose, v. poorly sorted msv, 1st clast = 2cm, 2.5 Y 6/2 slightly pebbly sand, ≤ 5% sm. pebbles, 40-50% crs-v. crs sand 50-60% fn-mud sand, msv, loose, mod sorted, S = 50-60% basalt wk rxn w/ HCl, 1st clast = 2cm	
						↓								
						SM								
80		s.s.												
81						Y								

W = Wet, M = Moist, D = Dry



Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>				Boring/Well No <u>C4124</u>		Depth <u>81.5-87.5'</u>		Date <u>10-29-03</u>		Sheet <u>10</u> of <u>23</u>	
Location <u>C Tank Farm</u>						Project <u>Vadose Zone</u>							
Logged by <u>B.N. Bjornstad</u>										Drilling Contractor _____			
Reviewed by _____										Date _____			
Lithologic Class. Scheme _____										Procedure _____			
Rev _____										Rig/Method _____			
Steel Tape/E-Tape <u>1</u>										Field Indicator Equip. 1) _____ 2) _____			
Depth Control Point _____													

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
81.5		SS					X				Empty			
						M	PM				Sand, fn-crs, well sorted, sl. compact			
											WK laminated, lgst particles = crs sand			
82.5		SS									2.5Y4/4 (olive brn - moist),			Paleomag smpl @ 82.6
										micaceous, S = 15-20% mafic				
										mod rxn w/ HCl, crsers toward bottom				
83.5							X				Well laminated, drag folding, Fe oxide blebs			
							SM							
											Sand, few sm pebbles, 50%			
											crs-4 crs. sand, 50% fn-vnd sand,			
										mod. sorted, MSV, loose				
85		SS								40-50% mafic, lgst clast = 1cm,				
										WK rxn w/ HCl				
							SM							
											Sand, mostly crs at top, md-crs			
											and bottom, WK lam, mod			
										sorted 2.5Y5/2, WK rxn w/ HCl				
87.5										lgst particle = v. crs sand, loose to				
										sl. compact				

W = Wet, M = Moist, D = Dry

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Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>87.5-93.5'</u>		Date <u>10-29-03</u>		Sheet <u>11</u> of <u>23</u>	
				Location <u>C Tank Farm</u>		Project <u>Vadose Zone</u>					
Logged by <u>B.N. Bjornstad</u>						Drilling Contractor _____					
Reviewed by _____						Driller _____					
Lithologic Class. Scheme _____						Procedure _____					
Steel Tape/E-Tape _____						Rev _____					
Field Indicator Equip. 1) _____						2) _____					
Depth Control Point _____											

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
87.5		SS				SM								
88.5														PM @ 88.2
89		SS				SM								
90		SS												
91														
91.5		SS				D								
						SM								
92.5		SS												
93.5														

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DBL/001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>94-100'</u>		Date <u>10-29-03</u>		Sheet <u>12 of 23</u>	
				Location <u>C Tank Farm</u>		Project <u>Vadose Project</u>					
Logged by <u>B N Bjornstad</u>						Drilling Contractor _____					
Reviewed by _____						Driller _____					
Lithologic Class. Scheme _____						Rig/Method _____					
Steel Tape/E-Tape <u>1</u>						Field Indicator Equip. 1) _____ 2) _____					
						Depth Control Point _____					

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
94		S.S.				D								
						↓								
						SM								
95		S.S.												
96														
96.5		S.S.				SM								
						↓								
						SM								
97.5		S.S.	Mages core #1										except endcaps Core unopened & crs sand at top fn sand at bottom	
98.5						SM							filter paper removed and 4200 g for chem from bottom of core	
99		S.S.				SM								
						↓								
						D								
100														

W = Wet, M = Moist, D = Dry

1998/DCU/PROC/DBU/001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>100-106'</u>	Date <u>10-29-03</u>	Sheet <u>13</u> of <u>23</u>
				Location <u>C Tank Farm</u>		Project <u>Vadose Zone</u>		
Logged by <u>B N Bjornstad</u>						Drilling Contractor _____		
Reviewed by _____						Driller _____		
Lithologic Class. Scheme _____						Rig/Method _____		
Steel Tape/E-Tape _____						Depth Control Point _____		
		Procedure _____		Rev _____				
		Field Indicator Equip. 1) _____		2) _____				

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
100		S.S.				D	o				Sand, 70% crs.-v.crs. 30% fn-md, one v. sm.-pebble, sl. compact, msv, 2.5Y5/2, 1st clast = 1cm			
101						Y	o				poorly sorted, wk rxn w/ HCl			
101.5		S.S.				D	o				msv, loose, v. poorly sorted, matrix-supported pebbles			
102.5		S.S.					o				sand, 40% crs.-v.crs, 50% fn-md, mod. sorted, msv., sl. compact 2.5Y5/2, wk rxn w/ HCl, 1st clast = v. sm. pebble			
103.5						Y	o							
104						D	o				silty sand w/ angular pebbles, v. poorly sorted, loose, msv Sand, 40% crs.-v.crs, 50% fn.-md, wk 1 am., 2.5Y5/2, wk rxn w/ HCl			
105						Y	o				2" silty sand @ 105.4', 2.5Y5/3, 1 am. 1st clast = 2m. pebble			
106						Y	o							

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DBU/001

Pacific Northwest National Laboratory		DAILY BOREHOLE LOG		Boring/Well No <u>C4124</u>		Depth <u>106.5-115'</u>		Date <u>10-29-03</u>		Sheet <u>14</u> of <u>23</u>	
Location <u>C Tank Farm</u>				Project <u>Vadose Zone</u>							
Logged by <u>B N Bjornstad</u>						Drilling Contractor _____					
Reviewed by _____						Date _____					
Lithologic Class. Scheme _____						Procedure _____ Rev _____					
Steel Tape/E-Tape <u>1</u>						Field Indicator Equip. 1) _____ 2) _____					
Depth Control Point _____											

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
106.5		S.S.				D								
107.5		S.S.					2 ft. mid sand, 2.5Y 5/3 Sand, 50% CRS - v. CRS sand, 50% fin. mid sand, WK lam., 2.5Y 5/2, Fe oxide blebs and coatings, 1st part = 1cm, mod. sorted, S = 40-50% basalt							
108.5														
109		S.S.				D							sl = slough	
							pebbly sand, loose, MSV pebbly sand, 10% sm pebbles, 70% CRS - v. CRS sand, poorly sorted, loose							
110		S.S.					sl. pebbly sand, loose, S = 50-60% bas, ≤ 5% pebbles 2.5Y 5/2, no rxn w/ HCl, 1st part = sm. pebbles, Fe oxide blebs and coatings							
111														
114		S.S.				SM								
							loose CRS sand, MSV Sand, 50% CRS, 30% mid 10% fin., mod sorted, 2.5Y 5/3, 1st part = v. CRS sand WK lam, S = 30-40% basalt WK rxn. w/ HCl							
115														

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DBU001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u> Location <u>C Tank Farm</u>		Depth <u>115-126</u> Date <u>10-29-03</u> Project <u>Vadose Zone</u>		Sheet <u>15</u> of <u>23</u>						
Logged by <u>B N Bjornstad</u> _____ Reviewed by _____ Lithologic Class. Scheme _____ Procedure _____ Rev _____ Steel Tape/E-Tape <u>1</u> Field Indicator Equip. 1) _____ 2) _____						Drilling Contractor _____ Driller _____ Rig/Method _____ Depth Control Point _____								
DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR	READING		C	Z	S	G				
115		S.S.				D								
119		S.S.				D								
120		S.S.												
121														
124		S.S.				D								
125		S.S.				SM								
126														

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/OBL/001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>129 - 140</u>		Date <u>10-29-03</u>		Sheet <u>16</u> of <u>23</u>	
				Location <u>C Tank Farm</u>		Project <u>Vadose Zone</u>					
Logged by <u>B N Bjornstad</u>						Drilling Contractor _____					
Reviewed by _____ Date _____						Driller _____					
Lithologic Class. Scheme _____ Procedure _____ Rev _____						Rig/Method _____					
Steel Tape/E-Tape _____ / _____						Field Indicator Equip. 1) _____ 2) _____					
						Depth Control Point _____					

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)	
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G					
129		S.S.				D					SI?				
130		S.S.				↓									
						SM					*				
131						↓									
134		S.S.				D									
135		S.S.													
136		S.S.				↓									
139		S.S.				SM									
140															

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DBL/001



Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>140-151</u>	Date <u>10-29-03</u>	Sheet <u>17</u> of <u>23</u>
				Location <u>C Tank Farm</u>		Project <u>Vadose Zone</u>		
Logged by <u>B N Bjornstad</u>						Drilling Contractor _____		
Reviewed by _____						Driller _____		
Lithologic Class. Scheme _____						Rig/Method _____		
Steel Tape/E-Tape <u>1</u>						Depth Control Point _____		
Field Indicator Equip. 1) _____ 2) _____								

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
140		S.S.				D								
141						↓								
144						D								
145						↓								
146						↓								
149						D								
150						↓								
151						↓								

W = Wet, M = Moist, D = Dry

1998/DCU/PROC/DBL/001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>154-166</u>	Date <u>10-30-03</u>	Sheet <u>18</u> of <u>23</u>
				Location <u>C Tank Farm</u>		Project <u>Vadose Zone</u>		
Logged by <u>BN Bjornstad</u>						Drilling Contractor _____		
Reviewed by _____						Driller _____		
Lithologic Class. Scheme _____						Rig/Method _____		
Steel Tape/E-Tape <u>1</u>						Depth Control Point _____		
Field Indicator Equip. 1) _____ 2) _____								

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
154							X						No recovery from 153-154	
155						D							pebble gravel, v. loose, mod sorted 2.5Y5/2, max part = 4cm	All slough? - looks like it
156													silty pebbly sand, v. poorly sorted loose, 2.5Y5/2, msv, wk rxn w/ HCl, max part = 2cm	
160						D							Pebbly sand, 10% pebbles, 50% crs - vers. sand, 40% fn-und sand, poorly sorted, 2.5Y5/2, wk rxn w/ HCl, msv	
161													loose	
164						SM							Sand, 50% crs, 30% und 20% fn, mod sorted, msv, S = 30-40% bas, 2.5Y5/3, wk rxn w/ HCl, sl. compact max part = v. crs. sand	
165			Magos Gre #2											Core unopened (except end caps)
166						D							crs sand, 2.5Y5/2, mod sorted, wk rxn	Filter paper + 200g removed from bot

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DBL/001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>169-180</u>		Date <u>10-30-03</u>		Sheet <u>19</u> of <u>23</u>	
				Location <u>CTank Farm</u>		Project <u>Vadose Zone</u>					
Logged by <u>BN Bjornstad</u>				Reviewed by _____ Date _____				Drilling Contractor _____			
Lithologic Class. Scheme _____ Procedure _____ Rev _____				Steel Tape/E-Tape <u>1</u> Field Indicator Equip. 1) _____ 2) _____				Driller _____			
Rig/Method _____				Depth Control Point _____							

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
169		ss				D								fine-grained clasts fell in from above?
170		ss												
171														
174		ss				SM								fine-grained mud clasts like @ 169'
175		ss												
176														
179						SM								
180														

W = Wet, M = Moist, D = Dry

1998/DCU/PROC/DBL001

B.43

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>180-191</u>		Date <u>10-30-03</u>		Sheet <u>20</u> of <u>23</u>	
				Location <u>C Tank Farm</u>		Project <u>Vadose Zone</u>					
Logged by <u>BN Bjornstad</u>						Drilling Contractor _____					
Reviewed by _____						Driller _____					
Lithologic Class. Scheme _____						Procedure _____ Rev _____					
Steel Tape/E-Tape <u>1</u>						Field Indicator Equip. 1) _____ 2) _____					
						Depth Control Point _____					

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
180						SM	↓				Sand, same as 179-180			
181						↓	↓							
184						SM	X							
185						SM	↓				fine pebbly gravel, v. loose, mod sorted 80-90% basalt			
186						↓	↓				Sand, 60% crs-v.crs. 20% md, 20% fn, poorly sorted, msv, max part = fn. rubble, 2.5 x 5/2, sl. compact, mod rxn w/ HCl, 50-60% basalt			
189						SM	↓				v. loose crs-v.crs. sand Sand, 50% crs-v.crs., 50% fn-md 40-50% basalt, few pebbles toward top, mod sorted, msv, max part = 1.5cm wk rxn w/ HCl, sl. compact			
190						↓	↓							
191						↓	↓							

W = Wet, M = Moist, D = Dry

1998/DCU/PROC/DBL/001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>194-205</u>		Date <u>10-30-03</u>		Sheet <u>21</u> of <u>23</u>	
				Location <u>C Tank Farm</u>		Project <u>Vadose Zone</u>					
Logged by <u>BN Bjorstad</u>				Drilling Contractor _____							
Reviewed by _____				Driller _____							
Lithologic Class. Scheme _____				Procedure _____				Rev _____			
Steel Tape/E-Tape _____				Field Indicator Equip. 1) _____				2) _____			
				Depth Control Point _____							

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)	
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G					
194		S.G.				D							Gravel, no matrix, broken clasts, max clast = 60cm pebbly sand, 10% pebbles, 50% crs-vcrs sand, 20% med 20% fn, poorly sorted, msv, 2.5Y5/3, sl. compact, S = 40-50% bas. fewer pebbles below		Sl = slough
195		S.G.													
196															
199						D							sandy pebbly gravel, v. loose, mod sorted, 80-90% basalt		
200													Silty pebbly sand, 10% silt, 10% pebbles 40% crs-vcrs sand, 40% fine sand, msv, poorly sorted, max part = 3cm S = 25-35% basalt, wk rxn w/ HCl 2.5Y6/2, sl. compact		
201															
204						D							sandy pebbly gravel, v. loose, 80-90% bas		
205													Pebbly sand, 5-10% pebbles, 40% crs-vcrs sand 40% fine sand, 10% silt, poorly sorted, msv, sl. compact, Max part = 3cm 2.5Y6/2, wk rxn w/ HCl		

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DBU/001

B.45

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>205-211</u>	Date <u>10-30-03</u>	Sheet <u>22 of 23</u>						
				Location <u>C Tank Farm</u>		Project <u>Vadose Zone</u>								
Logged by <u>B N Bjornstad</u>				Drilling Contractor _____										
Reviewed by _____ Date _____				Driller _____										
Lithologic Class. Scheme _____ Procedure _____ Rev _____				Rig/Method _____										
Steel Tape/E-Tape _____ / _____				Depth Control Point _____										
DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG				LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING		C	Z	S	G				
205						D					Same as above (204-205)			
206						V								
209	A					D					Angular gravel (looks like broken cobble) not basalt			
210						V					Sand, 30% crs. v.ers sand, 30% med sand, 30% silty, 10% silt, v. poorly sorted sl. compact, max part = 3mm pebbles, w/ HCl/msv, S=30-40% basalt	2.5Y 6/2 med rxn		Repeated core intervals
209	B					D					1 large broken-up cobble			
210						V								
210	A					D					Pebbly, silty sand, v. poorly sorted, mottled, dv. compact, med rxn w/ HCl max part = 0.5cm, 2.5Y 7/2			
211						V					like imm. above but more sand and better sorted			Repeated core intervals
210	B					D					pebbly, silty sand, v. loose, v. poorly sorted silty pebbly sand, 10% pebbles, 50% crs. v.ers sand 40% fin-med sand, v. poorly sorted, sl. compact, msv, 2.5Y 6/2, max part = 1.5cm			
211						V								

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DBU/001

Pacific Northwest National Laboratory		<b>DAILY BOREHOLE LOG</b>		Boring/Well No <u>C4124</u>		Depth <u>219-230</u>	Date <u>10-30-03</u>	Sheet <u>23</u> of <u>23</u>
				Location <u>C Tank Farm</u>		Project <u>Vadose Zone</u>		
Logged by <u>BN Bjornstad</u>				Drilling Contractor _____				
Reviewed by _____				Date _____		Driller _____		
Lithologic Class. Scheme _____				Procedure _____		Rev _____		
Steel Tape/E-Tape _____				Field Indicator Equip. 1) _____ 2) _____		Depth Control Point _____		

DEPTH ( )	TIME	SAMPLES		CONTAMINATION		MOIS- TURE	GRAPHIC LOG C Z S G	LITHOLOGIC DESCRIPTION (particle size distribution, sorting, mineralogy, roundness, color, reaction to HCl, etc.)	H <sub>2</sub> O ADDED	CASING	DRILLING COMMENTS (drilling rate, down time, blow counts, water level, drill fluid, etc.)
		TYPE	ID NUMBER	INSTR.	READING						
219		SS -					X				
220							○○○○	Gravel, rounded to angular (broken), fr. cgs rubble size, no matrix, 25% basalt, others include gtzite and volcanic porphyry			
224						SM	X	1 lg gtzite clast, rounded except where broken, 80 mm dia			
225							●●●●	silty pebbly sand, 5-10% pebbles, 30% cgs-vcrs sand, 30% md sand, 20% fn sand 10% silt, poorly sorted, msv, 1 gtz clast = 1 cm 25% 4/2, wk rxn w/ HCl, sl. compact, S = 50-60% basalt			
226							●●●●				
229							X				
230						D	○○○○	Gravel, rounded to angular, unbroken clasts, subrounded, ~25% basalt, lgst clast = 5 cm (broken), no matrix other l. ths = gtzite, volcanic porphyry totally loose			

W = Wet, M = Moist, D = Dry

1998/DCL/PROC/DBL/001



## **Appendix C**

### **Spectral Gamma Ray Logs and Gyroscope Survey Data Results**

## Appendix C

### Spectral Gamma Ray Logs and Gyroscope Survey Data Results



#### C-4124 Log Data Report

##### Borehole Information:

Borehole: C-4124		Site: North of C Tank Farm			
Coordinates (WA St Plane)		GWL <sup>1</sup> (ft): 230		GWL Date: 09/08/03	
North (Estimated)	East (Estimated)	Drill Date	Ground Level Elevation	Total Depth (ft)	Type
136650 m	575200 m	09/03	Not available	268.0	Becker

##### Casing Information:

Casing Type	Stickup (ft)	Outer Diameter (in.)	Inside Diameter (in.)	Thickness (in.)	Top (ft)	Bottom (ft)
Threaded Steel	3.55	9.0	8.0	0.50	+3.55	268.0
Steel Tubing	3.1	6.24	6.0	0.120	+3.1	268.0

##### Borehole Notes:

The casing dimensions are derived from published values for Becker drill casing. Casing thicknesses at the joints are 0.875- and 0.240-in. for the 8- and 6-in. casings, respectively. The total depth of the borehole was provided by the driller. The well site geologist provided the depth to water. Borehole coordinates were provided by Fluor Hanford's person in charge and are estimates. Ground level elevation was not available. Logging data acquisition is referenced to the ground surface.

##### Logging Equipment Information:

Logging System: Gamma 1E		Type: SGLS (70%) SN: 34TP11019B
Calibration Date: 07/03	Calibration Reference: GJO-2003-468-TAC	
	Logging Procedure: MAC-HGLP 1.6.5, Rev. 0	

##### Spectral Gamma Logging System (SGLS) Log Run Information:

Log Run	1	2 Repeat			
Date	09/08/03	09/08/03			
Logging Engineer	Kos	Kos			
Start Depth (ft)	266.45	31.45			
Finish Depth (ft)	0.45	4.45			
Count Time (sec)	100	100			
Live/Real	R	R			
Shield (Y/N)	N	N			
MSA Interval (ft)	1.0	1.0			
ft/min	N/A <sup>2</sup>	N/A			
Pre-Verification	AE031CAB	AE031CAB			
Start File	AE031000	AE031267			
Finish File	AE031266	AE031294			

Log Run	1	2 Repeat			
Post-Verification	AE031CAA	AE031CAA			
Depth Return Error (in.)	-1.25	0			
Comments	No fine-gain adjustment.	No fine-gain adjustment.			

### **Logging Operation Notes:**

Spectral gamma logging was performed in this borehole on September 8, 2003. Logging was conducted with a centralizer on the sonde. Logging was inadvertently initialized at the top of casing. Because the casing was not permanent, during analysis all measurements were corrected by the amount of stickup (3.55 ft) so that the ground surface is the reference point. A repeat section was collected in this borehole to evaluate system performance.

### **Analysis Notes:**

<b>Analyst:</b>	Henwood	<b>Date:</b>	09/10/03	<b>Reference:</b>	GJO-HGLP 1.6.3, Rev. C
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Pre-run and post-run verifications for the logging system were performed before and after data acquisition. Acceptance criteria were met.

A combined casing correction for 0.620-in.-thick casing was applied throughout the borehole for both casings. The combined thickness at casing joints is 1.115 in. This thickness results in a significant reduction in gamma activity detection as the detector passes by a casing joint. However, it is not practical to correct individual data points for the effect of casing joints. The influence of the thick joints is apparent on the total gamma and <sup>40</sup>K logs where reduced count rates and concentrations are exhibited at approximately 10-ft depth intervals.

SGLS spectra were processed in batch mode using APTEC SUPERVISOR to identify individual energy peaks and determine count rates. Concentrations were calculated with an EXCEL worksheet template identified as G1EJul03.xls using efficiency functions and corrections for casing, water, and dead time as determined from annual calibrations. Dead time corrections are applied where dead times exceed 10.5 percent; no dead times in excess of 10.5 percent were encountered. Correction for water was applied to the data below 230 ft.

### **Log Plot Notes:**

Separate log plots are provided for the man-made radionuclide (<sup>137</sup>Cs) detected in the borehole, naturally occurring radionuclides (<sup>40</sup>K, <sup>238</sup>U, <sup>232</sup>Th [KUT]), a combination of man-made, KUT, and dead time, and total gamma plotted with dead time. For each radionuclide, the energy value of the spectral peak used for quantification is indicated. Unless otherwise noted, all radionuclides are plotted in picocuries per gram (pCi/g). The open circles indicate the minimum detectable level (MDL) for each radionuclide. Error bars on each plot represent error associated with counting statistics only and do not include errors associated with the inverse efficiency function, dead time correction, casing corrections, or water corrections. A repeat log section is also included.

### **Results and Interpretations:**

<sup>137</sup>Cs was the only man-made radionuclide detected in this borehole. <sup>137</sup>Cs was detected at a few sporadic locations throughout the borehole near its MDL of approximately 0.2 pCi/g.

The repeat section indicated good agreement of the naturally occurring KUT.

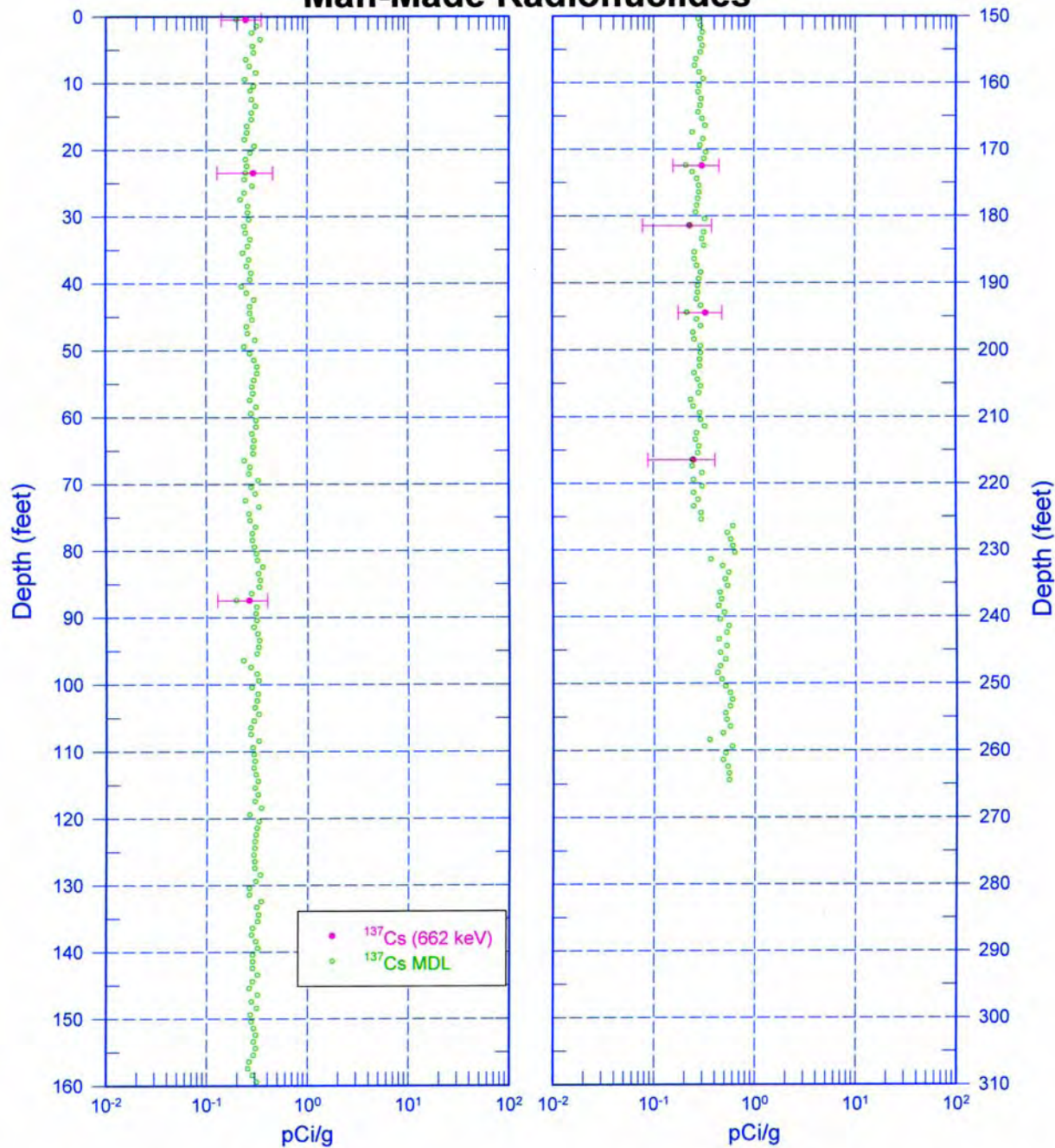
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<sup>1</sup> GWL – groundwater level

<sup>2</sup> N/A – not applicable

# C-4124

## Man-Made Radionuclides



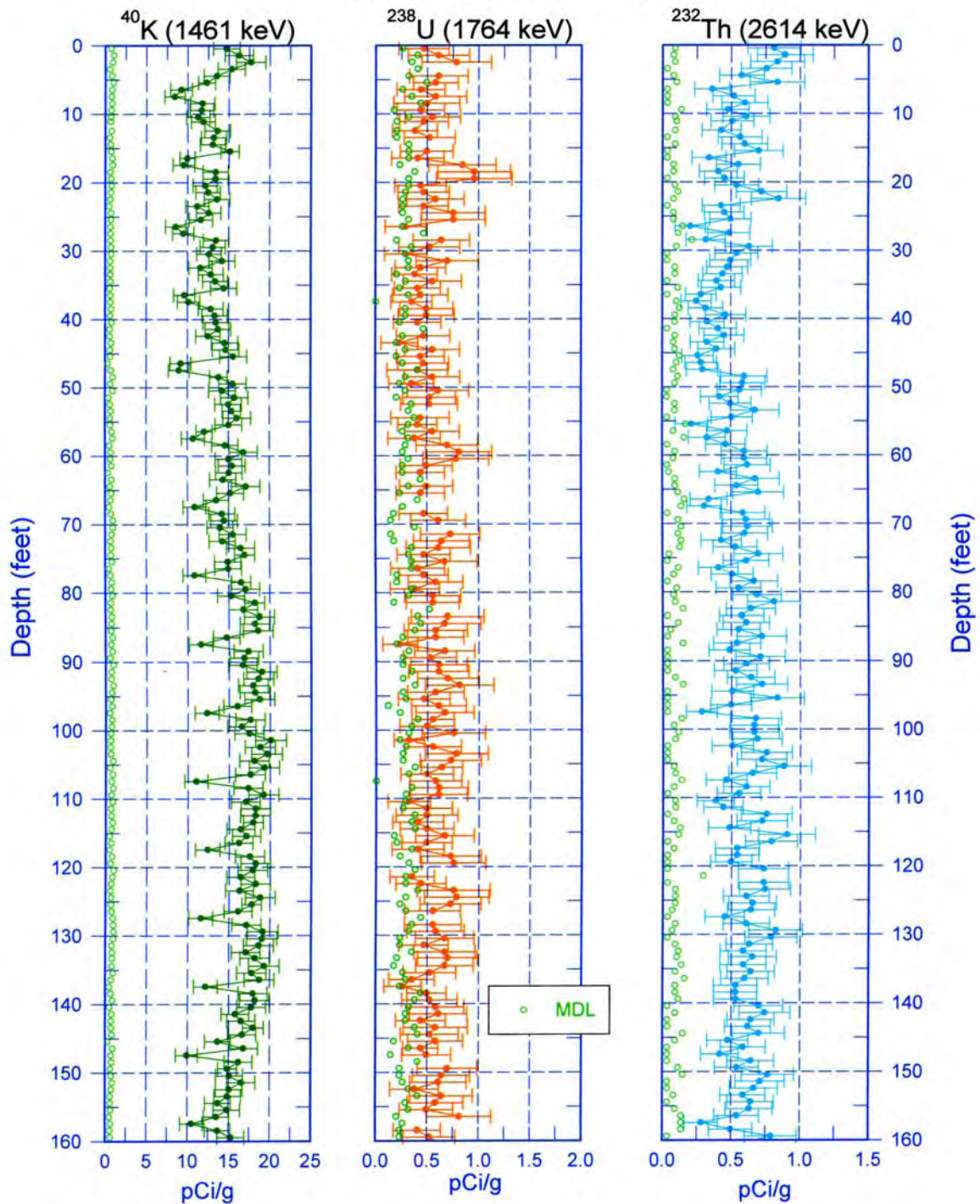
Zero Reference = Ground Surface

Depth scale: 1" = 20 ft

Last Log Date - 09/08/03

# C-4124

## Natural Gamma Logs



Zero Reference = Ground Surface

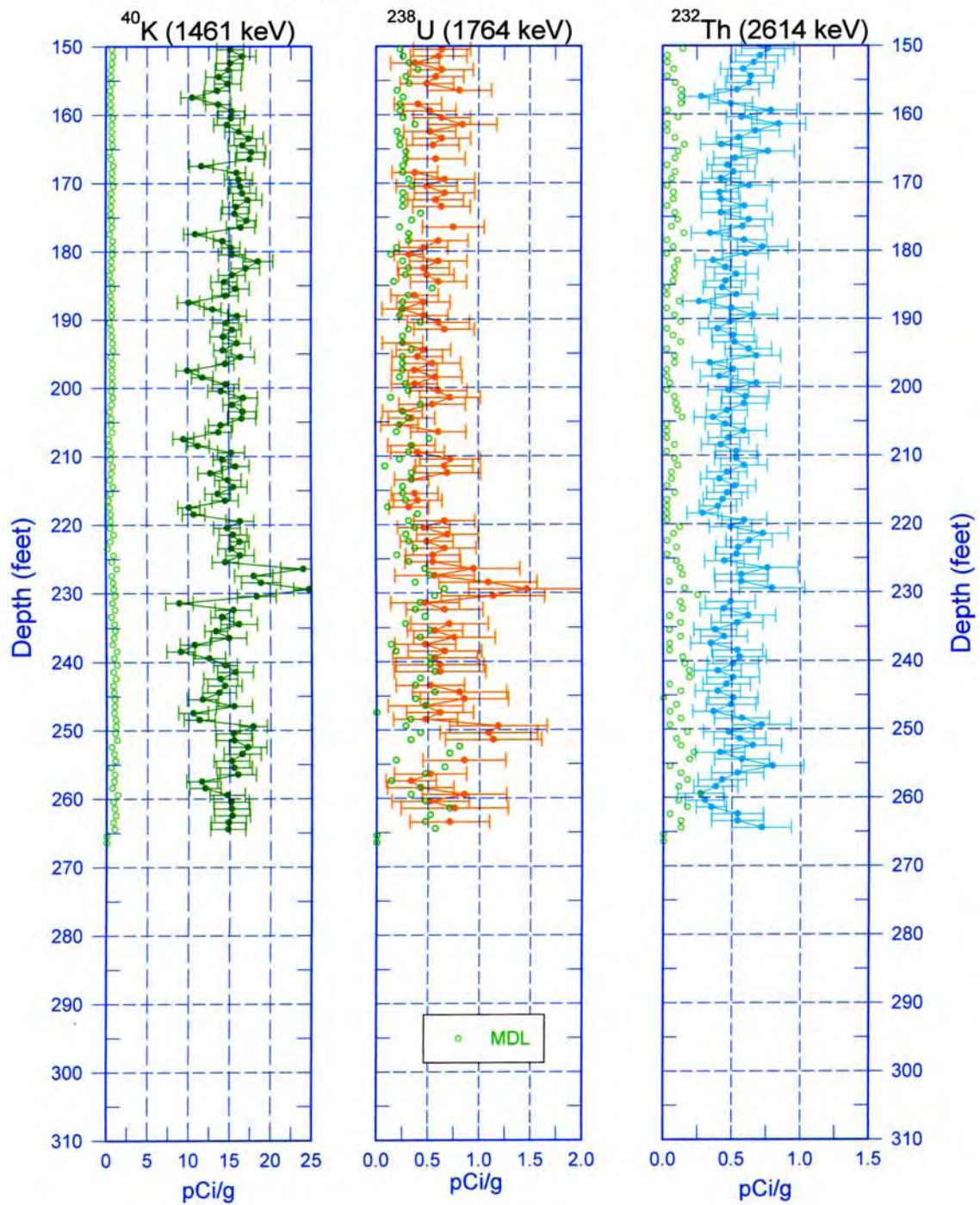
Depth scale: 1" = 20 ft

Last Log Date - 09/08/03



# C-4124

## Natural Gamma Logs



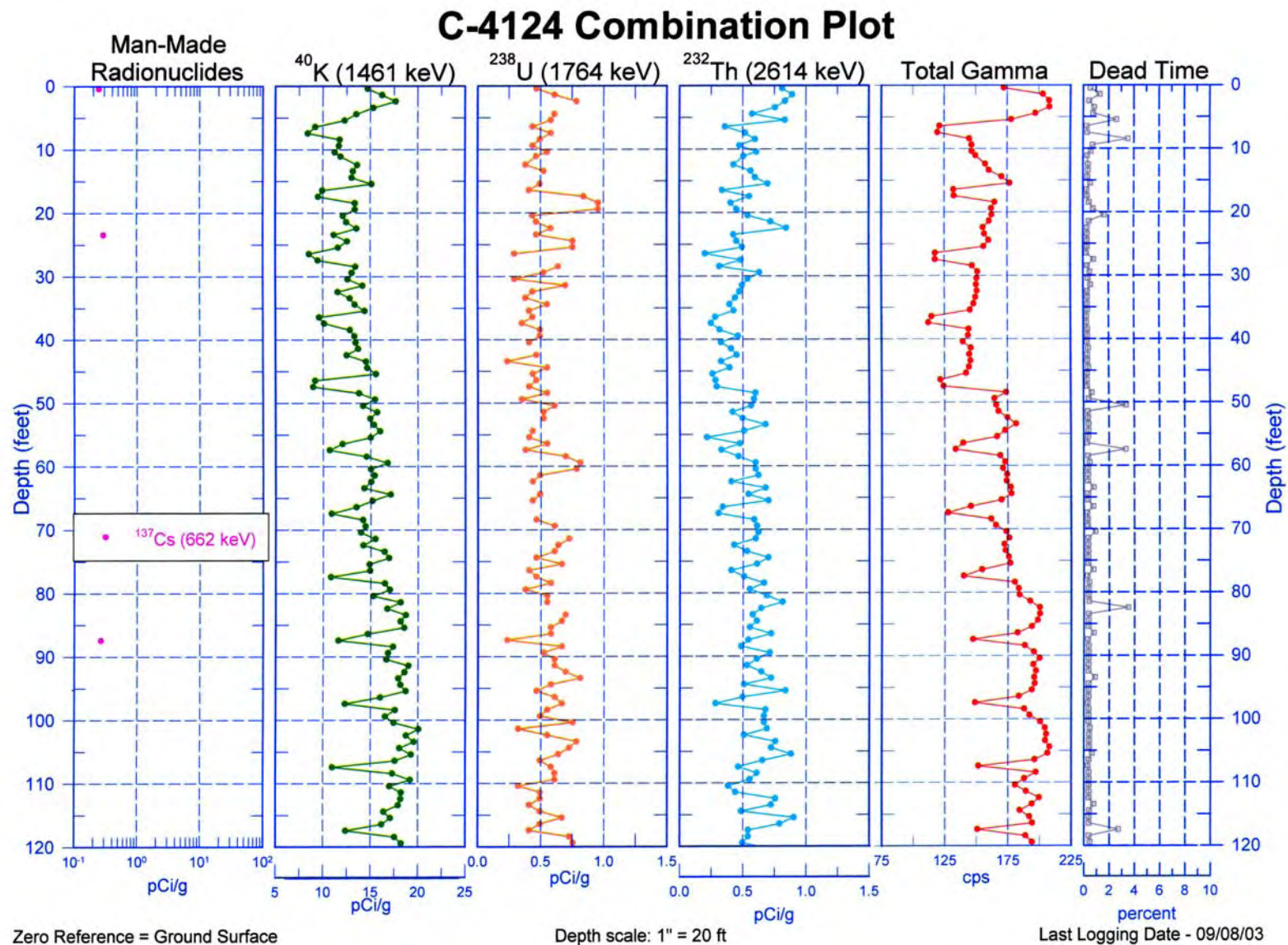
Zero Reference = Ground Surface

Depth scale: 1" = 20 ft

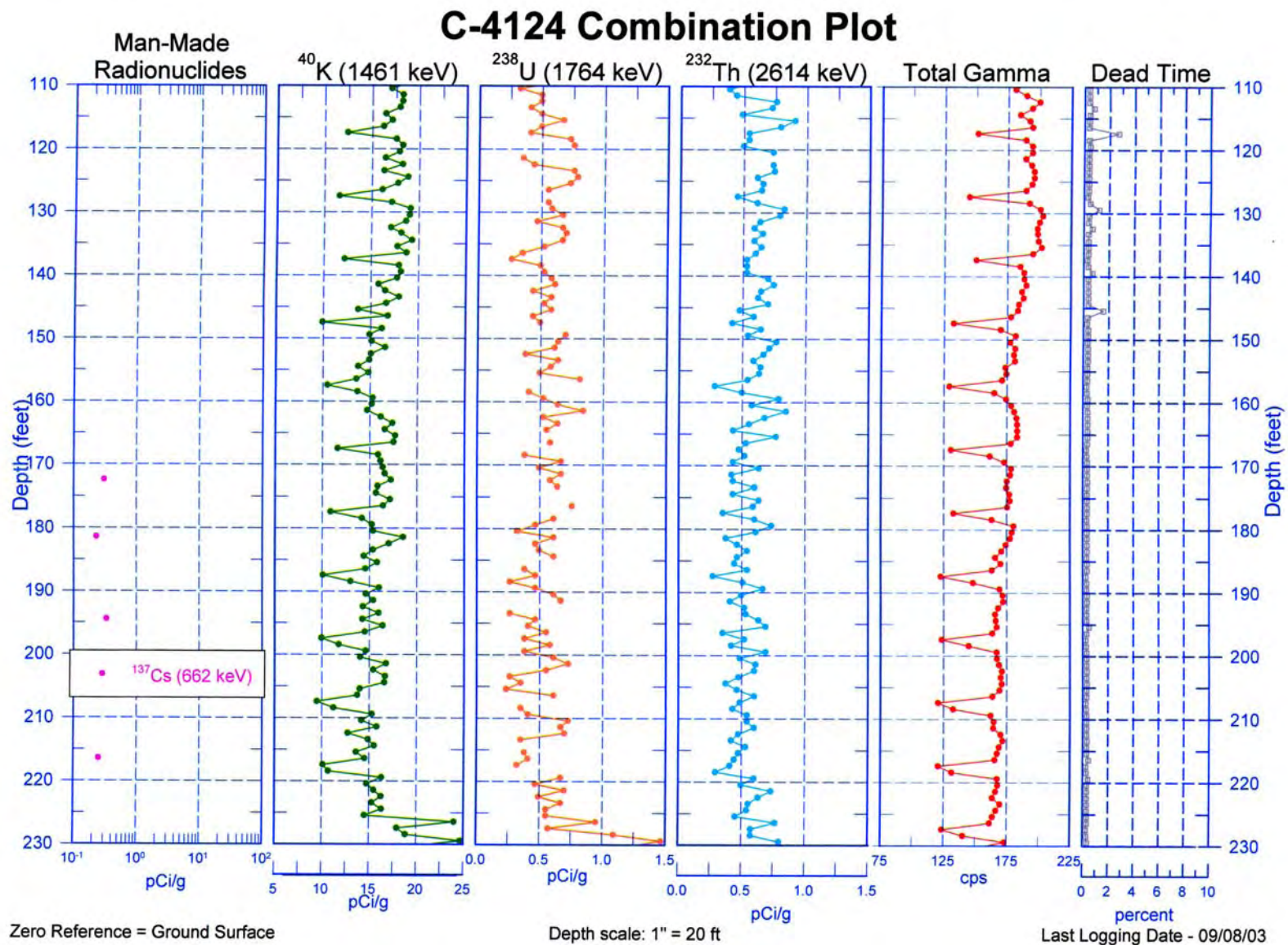
Last Log Date - 09/08/03



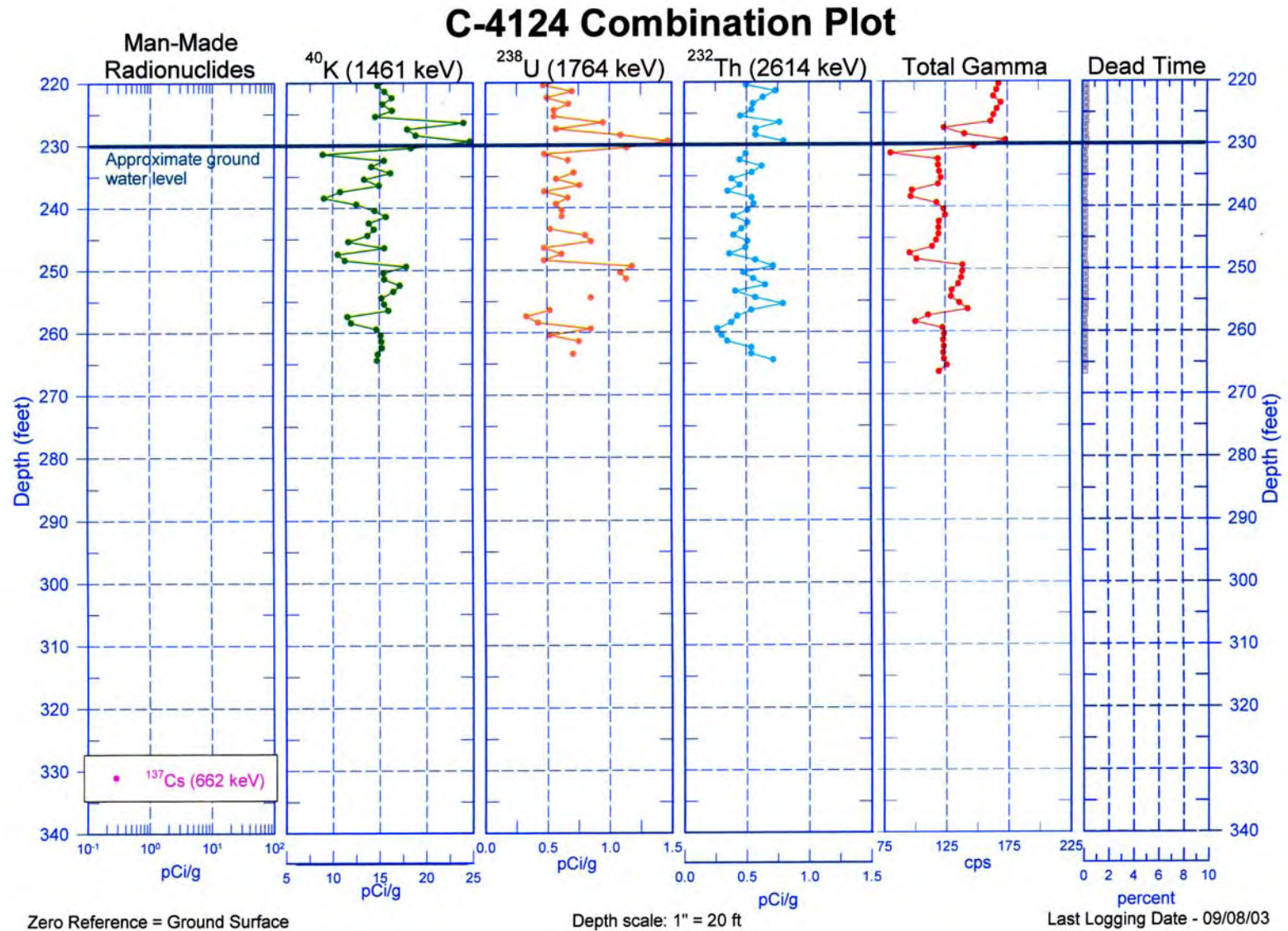
C.7



C.8

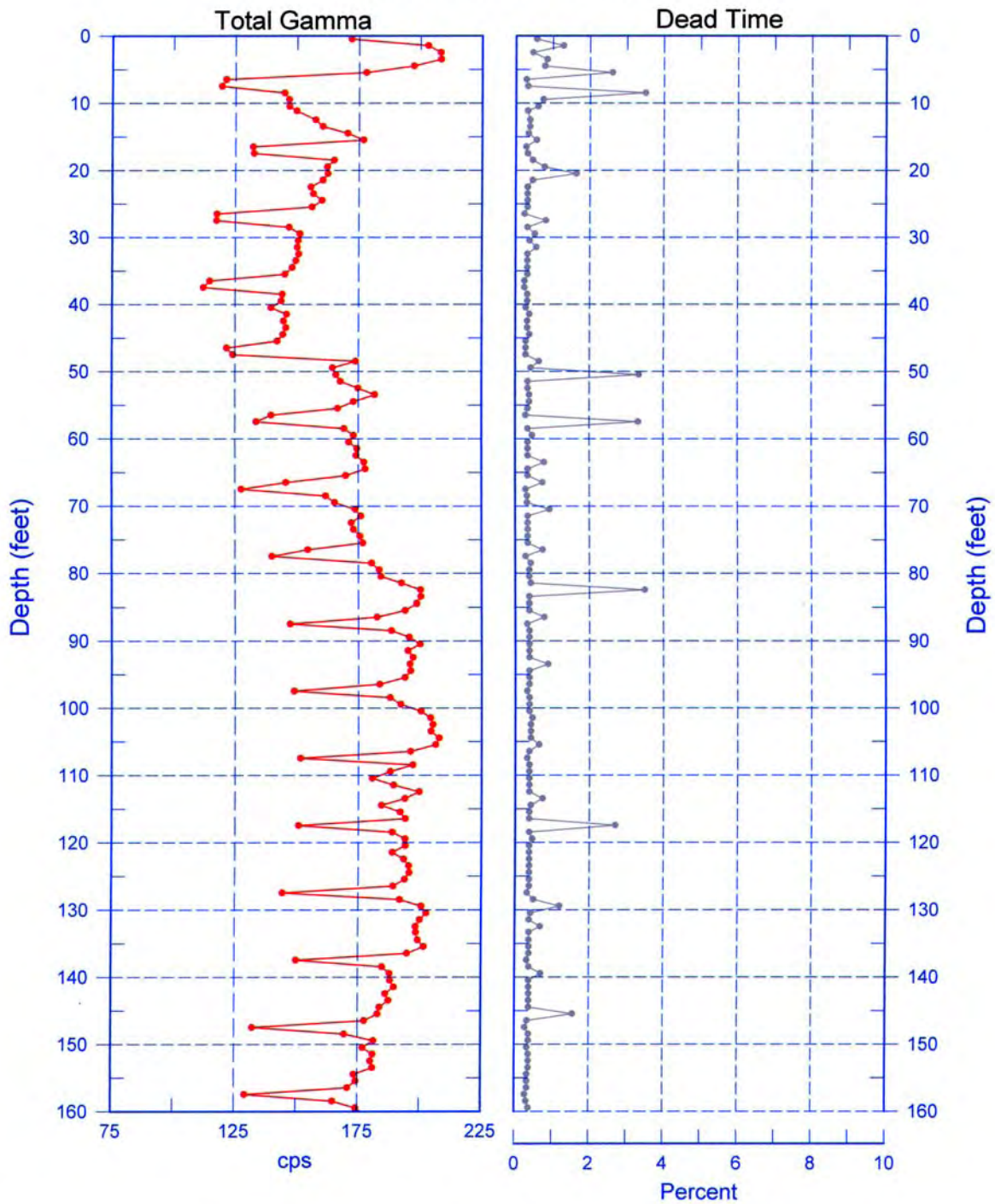






# C-4124

## Total Gamma & Dead Time



Reference - Ground Surface

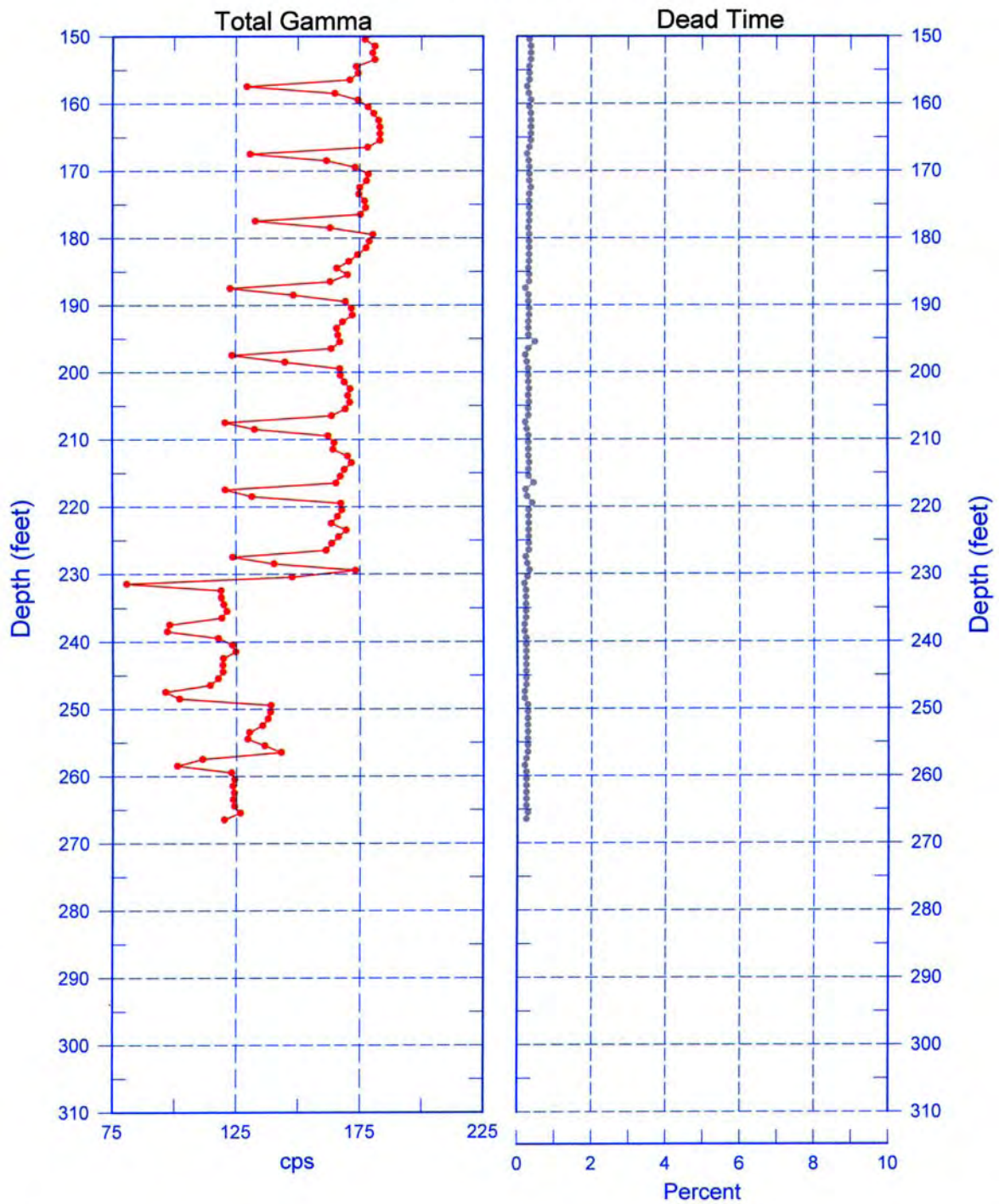
Depth scale: 1" = 20 ft

Last Log Date - 09/08/03



# C-4124

## Total Gamma & Dead Time



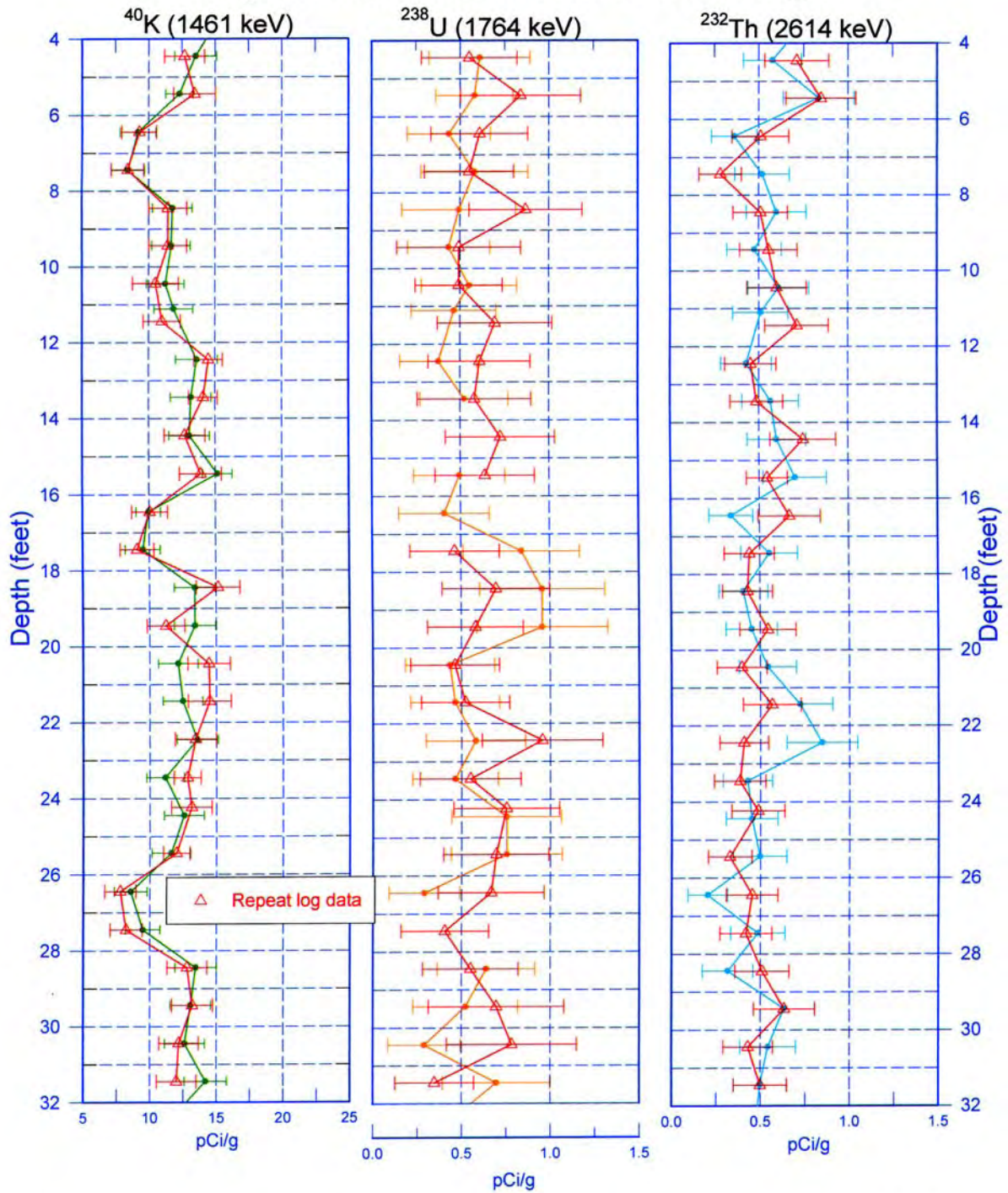
Reference - Ground Surface

Depth scale: 1" = 20 ft

Last Log Date - 09/08/03

# C-4124

## Repeat Section of Natural Gamma Logs



Zero Reference = Ground Surface

Last Log Date - 09/08/03

## C-4125 Log Data Report

### Borehole Information:

Borehole: C-4125		Site: West of C Tank Farm			
Coordinates (WA St Plane)		GWL <sup>1</sup> (ft): 268		GWL Date: 08/15/03	
North (Estimated) 136500	East (Estimated) 575025	Drill Date 08/03	Ground Level Elevation Not available	Total Depth (ft) 309.0	Type Becker

### Casing Information:

Casing Type	Stickup (ft)	Outer Diameter (in.)	Inside Diameter (in.)	Thickness (in.)	Top (ft)	Bottom (ft)
Threaded steel	1.7	11.0	10.0	0.50	+1.7	30
Becker	3.1	6.24	6.0	0.12	+3.1	309.0
Becker	2.7	9.0	8.0	0.5	+2.7	309.0

### Borehole Notes:

The casing dimensions are derived from published values for Becker drill casing. Casing thicknesses at the joints are 0.875- and 0.240-in. for the 8- and 6-in. casings, respectively. The Fluor Hanford drilling supervisor provided the total drilling depth, depth to water, and borehole coordinates. Ground level elevation was not available. Logging data acquisition is referenced to the ground surface.

### Logging Equipment Information:

Logging System: Gamma 1E		Type: SGLS (70%) SN: 34TP40587A
Calibration Date: 07/03	Calibration Reference: GJO-2003-468-TAC	
Logging Procedure: MAC-HGLP 1.6.5, Rev. 0		

### Spectral Gamma Logging System (SGLS) Log Run Information:

Log Run	1	2 Repeat	3		
Date	08/15/03	08/16/03	08/16/03		
Logging Engineer	Spatz	Spatz	Spatz		
Start Depth (ft)	301.0	121.0	89.0		
Finish Depth (ft)	90.0	90.0	25.0		
Count Time (sec)	100	100	100		
Live/Real	R	R	R		
Shield (Y/N)	N	N	N		
MSA Interval (ft)	1.0	1.0	1.0		
ft/min	N/A <sup>2</sup>	N/A	N/A		
Pre-Verification	AE018CAB	AE019CAB	AE019CAB		
Start File	AE018000	AE019000	AE019032		
Finish File	AE018211	AE019031	AE019096		



Log Run	1	2 Repeat	3		
Post-Verification	AE018CAA	AE019CAA	AE019CAA		
Depth Return Error (in.)	-1	N/A	N/A		
Comments	Fine-gain adjustment made after files -102, -144, -177, -182.	No fine-gain adjustment.	No fine-gain adjustment.		

### **Logging Operation Notes:**

Spectral gamma logging was performed in this borehole on August 15 and 16, 2003. Logging was conducted with a centralizer on the sonde. Measurements are referenced to ground surface. A repeat section was collected in this borehole to evaluate system performance. No logging was performed between the ground surface and 25 ft because a 10-in. casing was present in addition to the 6- and 8-in. casings. Logging depth achieved was 301 ft, 8.0 ft less than the reported drilling depth.

### **Analysis Notes:**

<b>Analyst:</b>	Henwood	<b>Date:</b>	08/28/03	<b>Reference:</b>	GJO-HGLP 1.6.3, Rev. 0
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Pre-run and post-run verifications for the logging system were performed before and after data acquisition. Acceptance criteria were met.

A combined casing correction for 0.620-in.-thick casing (0.5 +.12 in.) was applied below 25 ft for the 8- and 6-in. casings. The combined thickness at casing joints is 1.115 in. This thickness results in a significant reduction in gamma activity detection as the detector passes by a casing joint. However, it is not practical to correct individual data points for the effect of casing joints. The influence of the thick joints is apparent in the total gamma and <sup>40</sup>K logs where reduced count rates and concentrations are exhibited at approximately 10-ft depth intervals. For the depth interval between 25 and 30 ft a correction for 1.12-in. casing was applied where 10, 6, and 8-in. casings were present.

SGLS spectra were processed in batch mode using APTEC SUPERVISOR to identify individual energy peaks and determine count rates. Concentrations were calculated with an EXCEL worksheet template identified as G1EJul03.xls using efficiency functions and corrections for casing, water, and dead time as determined from annual calibrations. Dead time corrections are applied where dead times exceed 10.5 percent; no dead times in excess of 10.5 percent were encountered. Correction for water was applied to the data below 268 ft.

### **Log Plot Notes:**

Separate log plots are provided for the man-made radionuclide (<sup>137</sup>Cs) detected in the borehole, naturally occurring radionuclides (<sup>40</sup>K, <sup>238</sup>U, <sup>232</sup>Th [KUT]), a combination of man-made, KUT, and dead time, and total gamma plotted with dead time. For each radionuclide, the energy value of the spectral peak used for quantification is indicated. Unless otherwise noted, all radionuclides are plotted in picocuries per gram (pCi/g). The open circles indicate the minimum detectable level (MDL) for each radionuclide. Error bars on each plot represent error associated with counting statistics only and do not include errors associated with the inverse efficiency function, dead time correction, casing corrections, or water corrections. A repeat log section is also included.

### **Results and Interpretations:**

<sup>137</sup>Cs was the only man-made radionuclide detected in this borehole. <sup>137</sup>Cs was detected at a few sporadic locations in the borehole near its MDL of approximately 0.2 pCi/g.

The repeat sections indicated good agreement of the naturally occurring KUT.

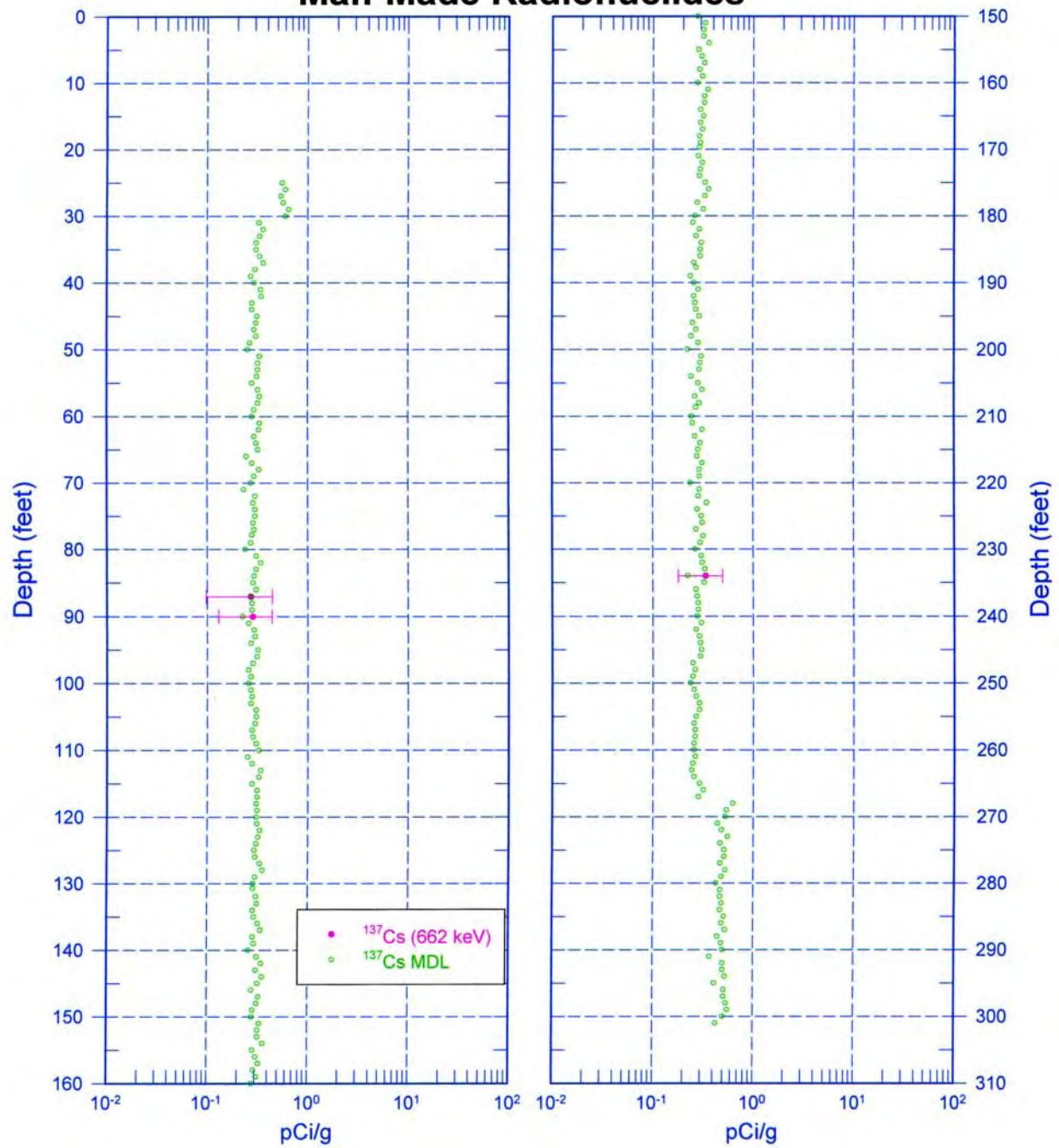
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<sup>1</sup> GWL – groundwater level

<sup>2</sup> N/A – not applicable

# C-4125

## Man-Made Radionuclides

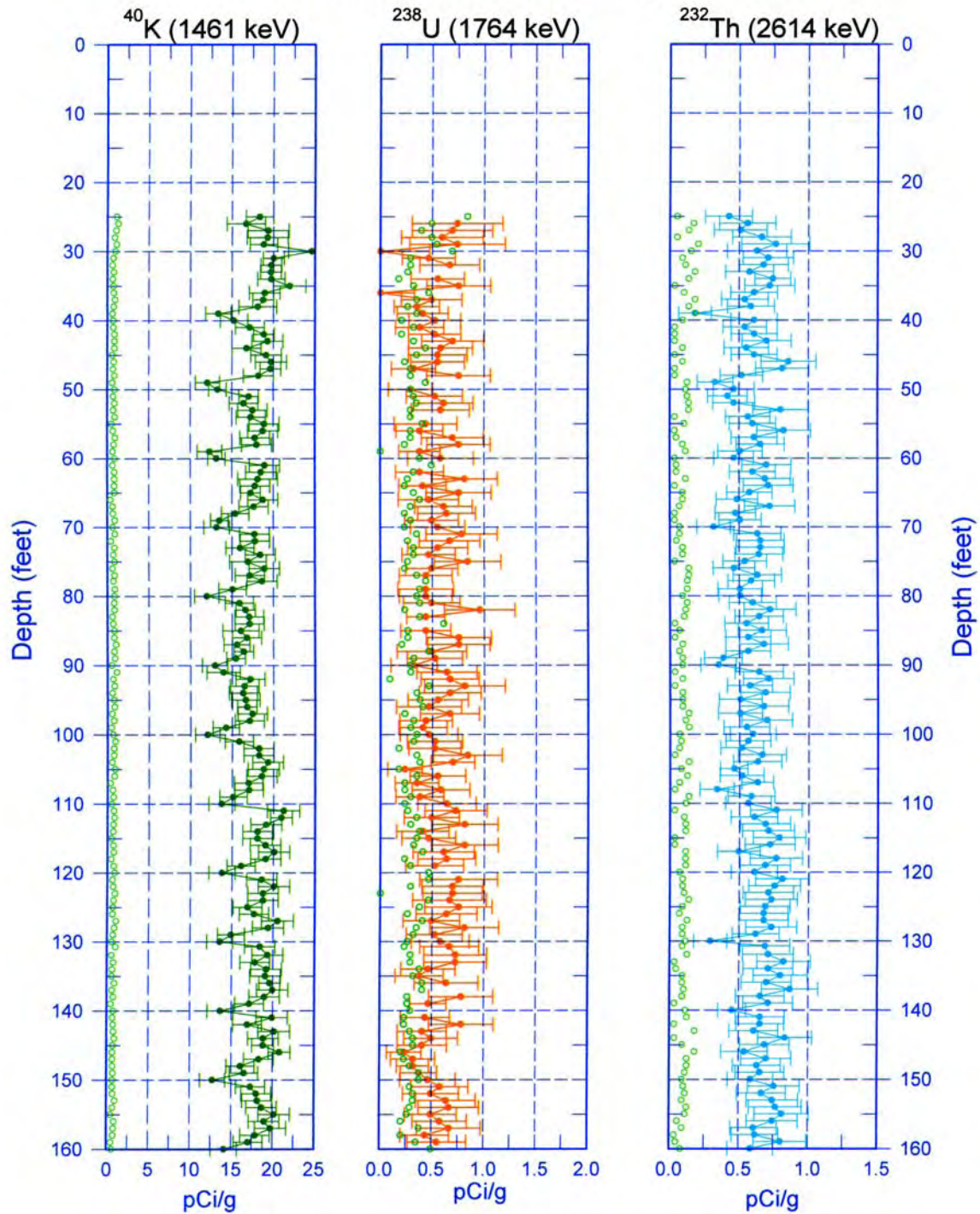


Zero Reference = Ground Surface

Last Log Date - 08/16/03

# C-4125

## Natural Gamma Logs



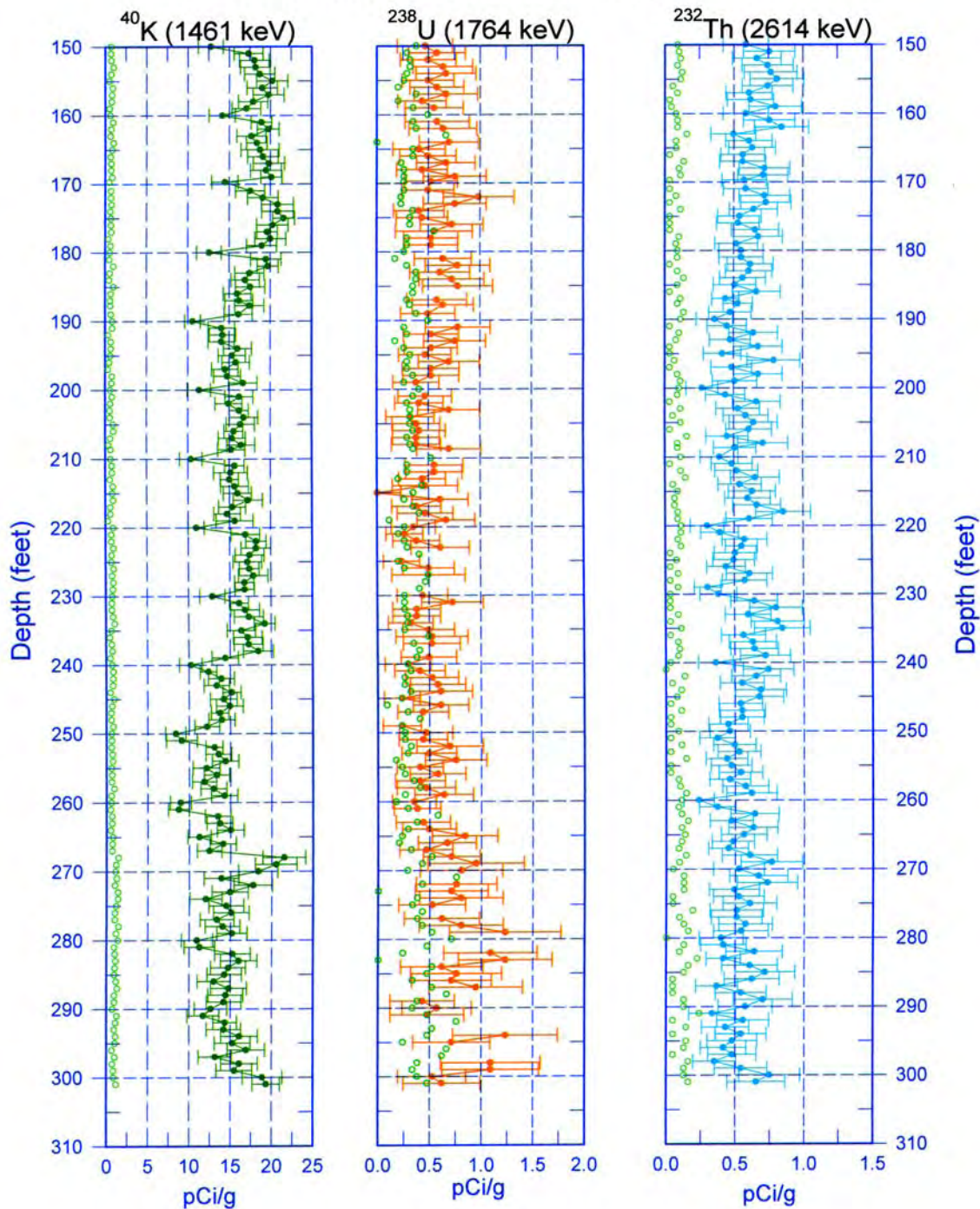
Zero Reference = Ground Surface

MDL

Last Log Date - 08/16/03



# C-4125 Natural Gamma Logs

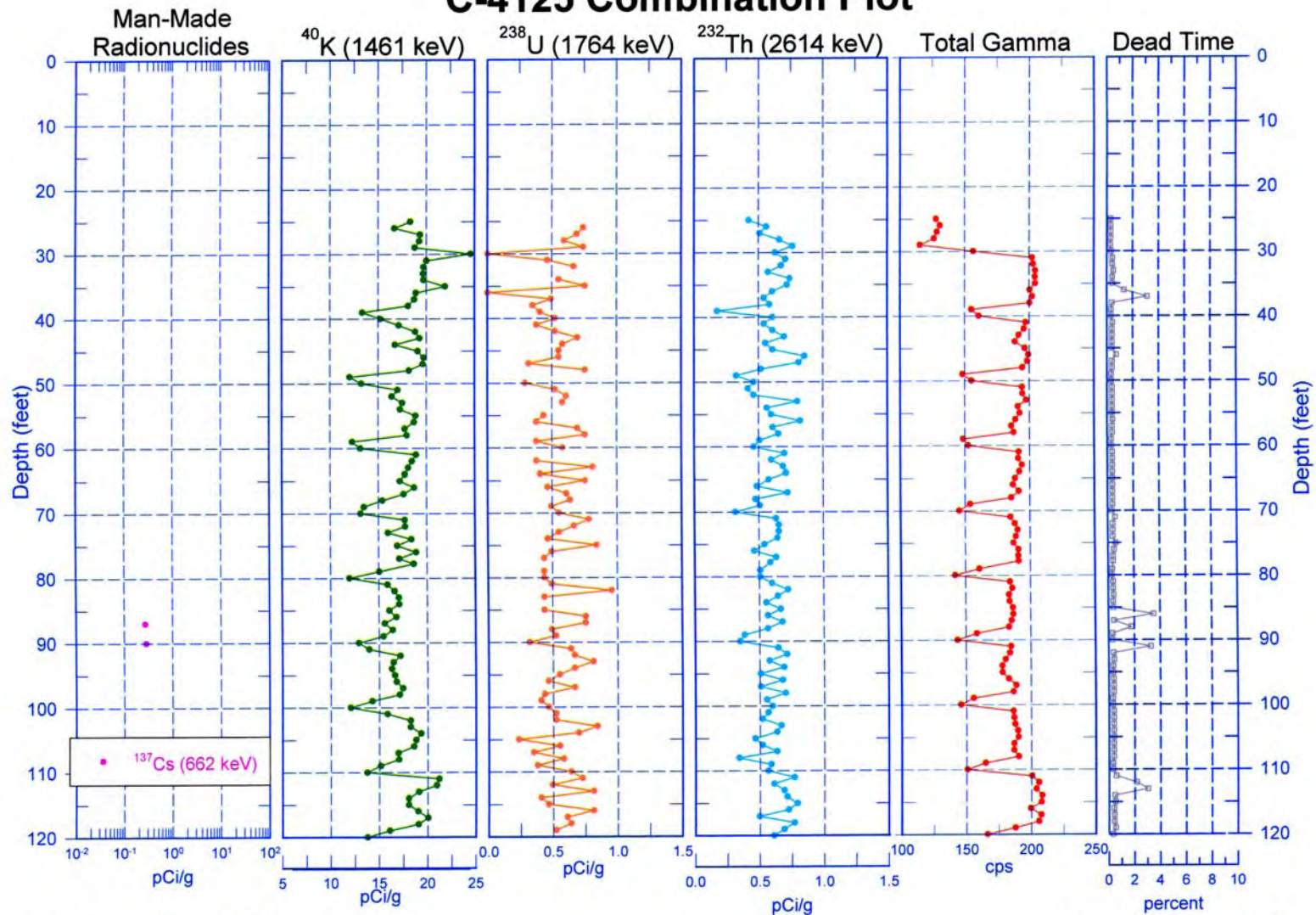


Zero Reference = Ground Surface

○ MDL

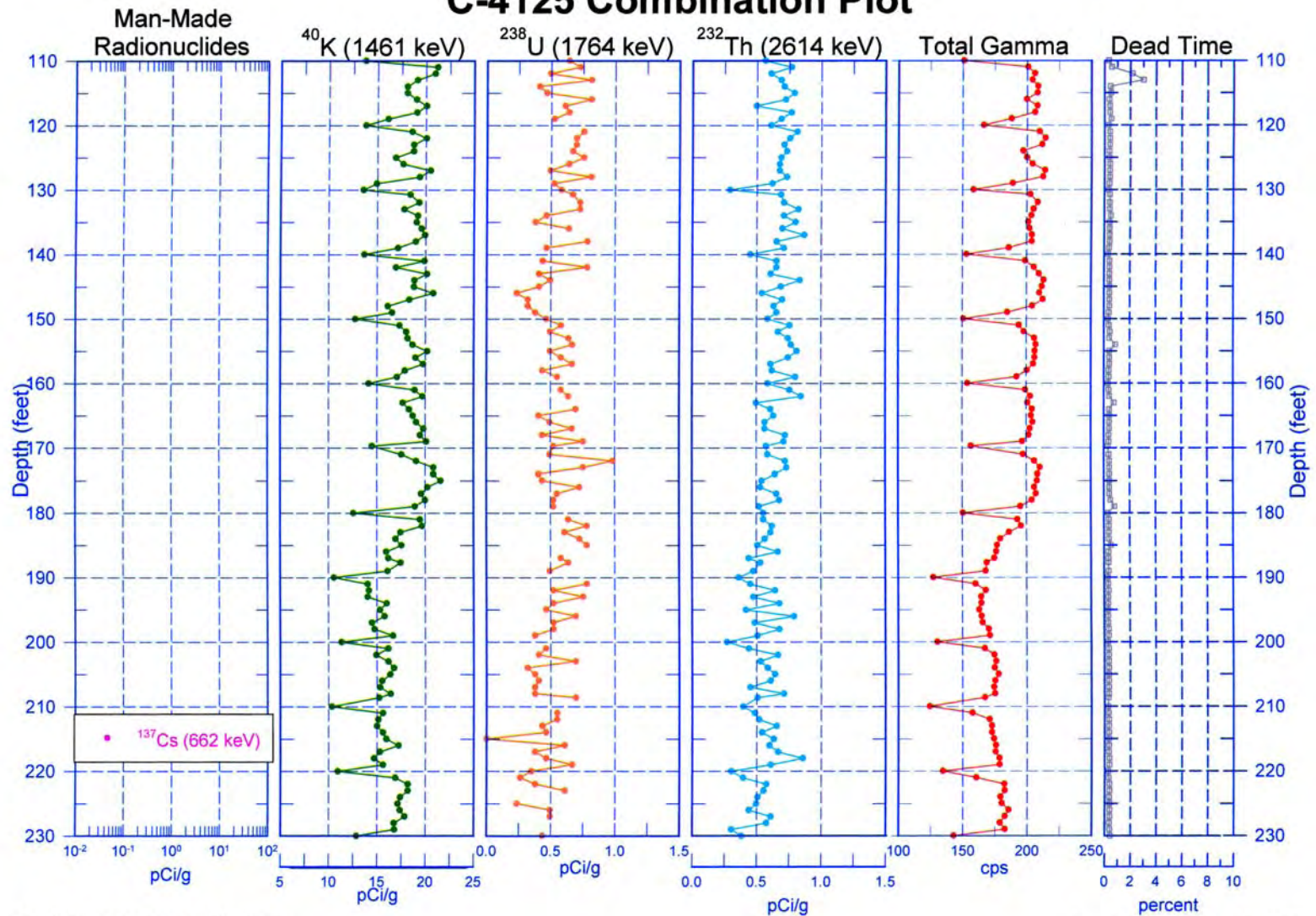
Last Log Date - 08/16/03

# C-4125 Combination Plot





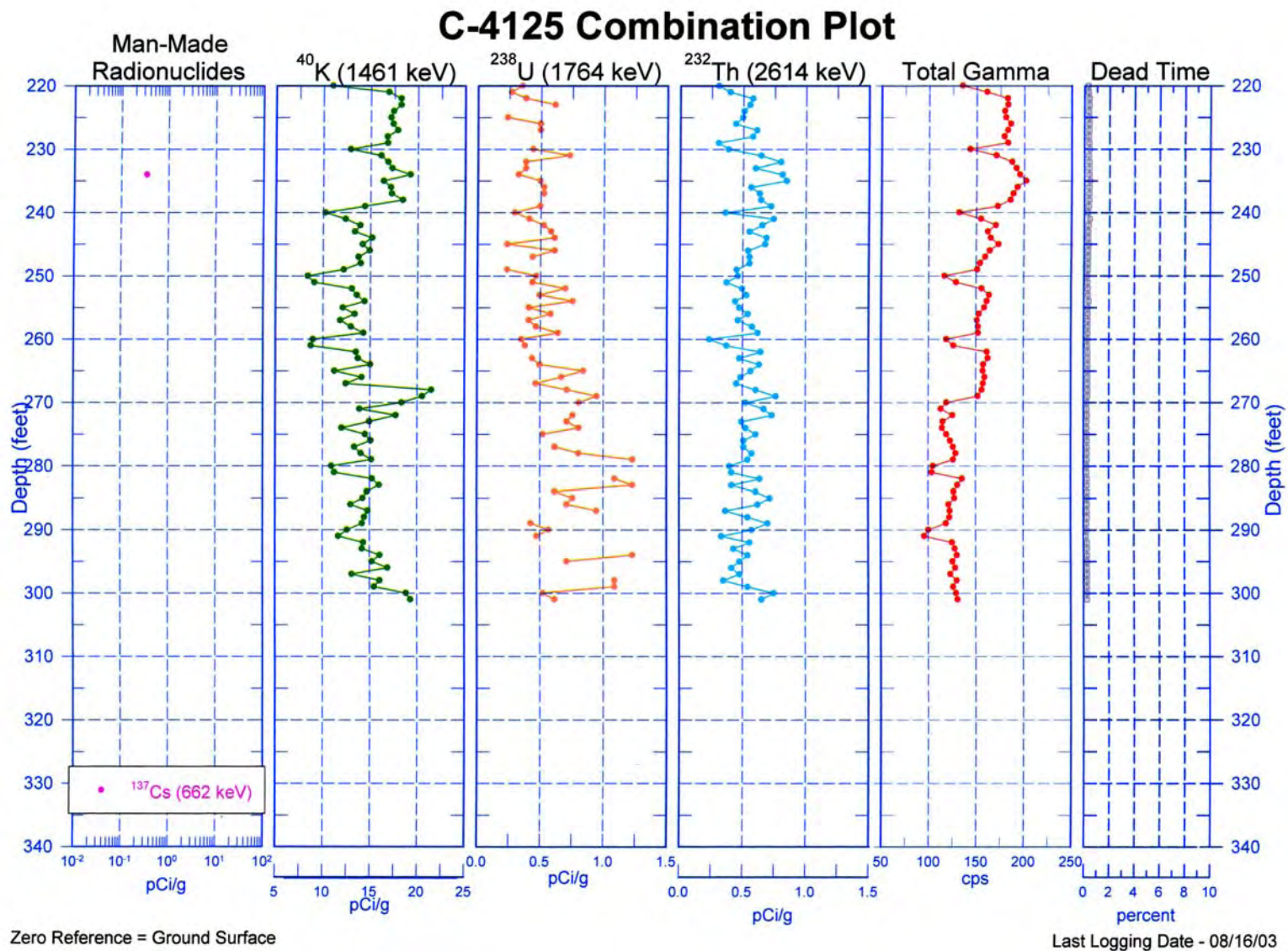
# C-4125 Combination Plot



Zero Reference = Ground Surface

Last Logging Date - 08/16/03

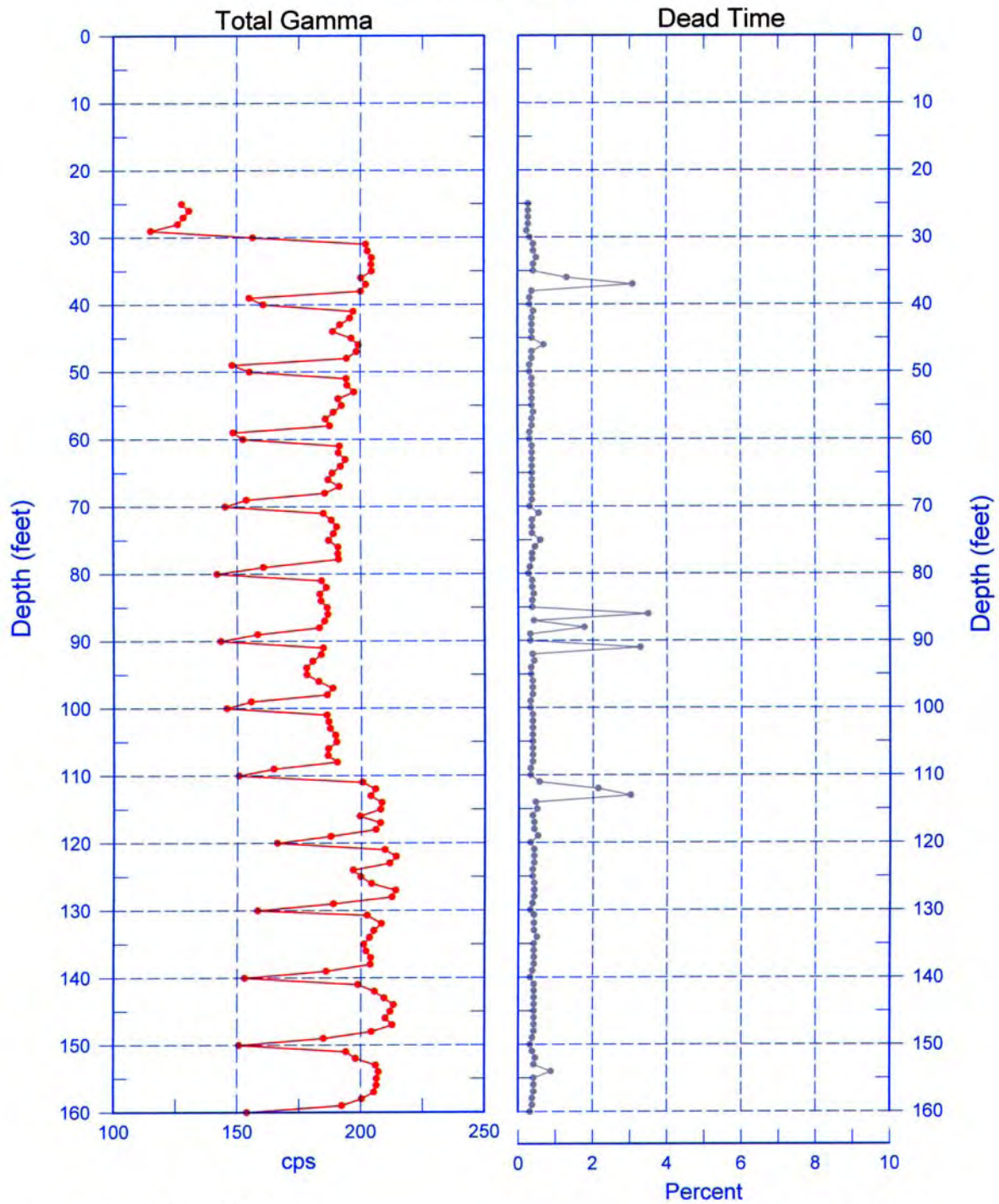
C.21





# C-4125

## Total Gamma & Dead Time

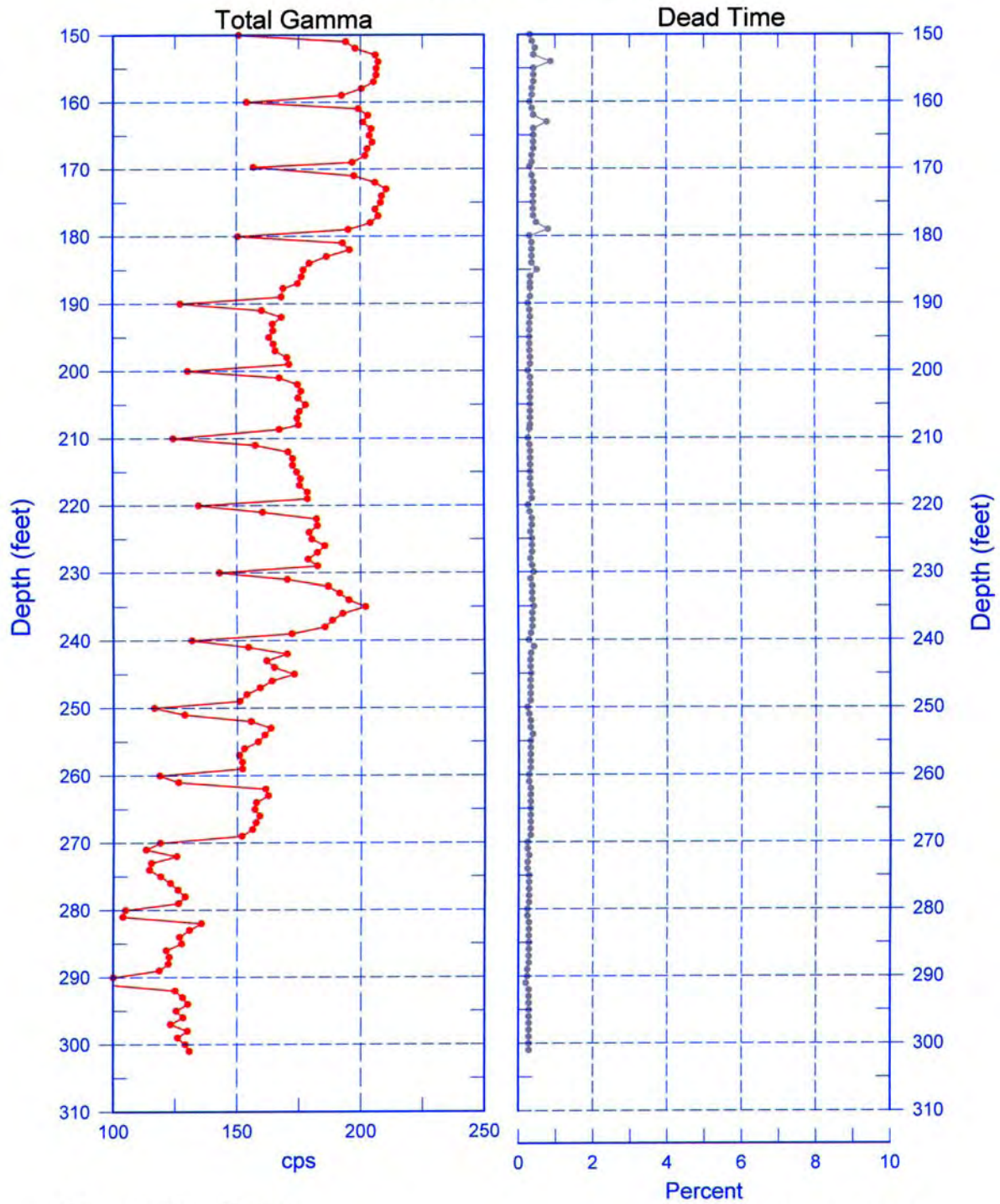


Reference - Ground Surface

Last Log Date - 08/16/03

# C-4125

## Total Gamma & Dead Time



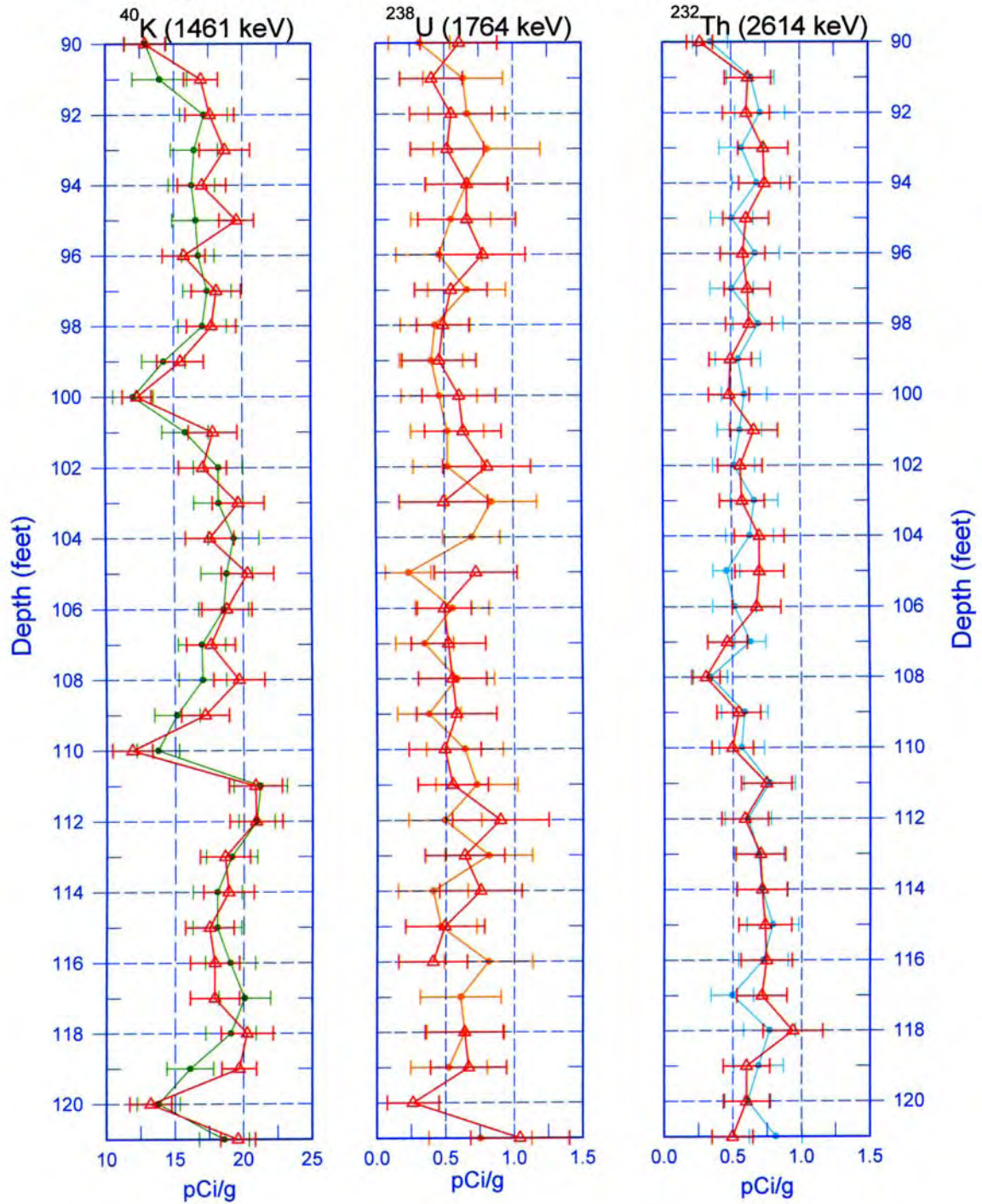
Reference - Ground Surface

Last Log Date - 08/16/03



# C-4125

## Repeat Section of Natural Gamma Logs



Zero Reference = Ground Surface

Last Log Date - 08/16/03

## C-4127 Log Data Report

### Borehole Information:

<b>Borehole:</b> C-4127		<b>Site:</b> South of C Tank Farm			
<b>Coordinates (WA St Plane)</b>		<b>GWL' (ft):</b> 272	<b>GWL Date:</b> 07/21/03		
<b>North</b> Not available	<b>East</b> Not available	<b>Drill Date</b> 07/03	<b>Ground Level Elevation</b> Not available	<b>Total Depth (ft)</b> 318.0	<b>Type</b> Becker

### Casing Information:

Casing Type	Stickup (ft)	Outer Diameter (in.)	Inside Diameter (in.)	Thickness (in.)	Top (ft)	Bottom (ft)
Steel tubing	2.7	6.24	6.0	0.125	0	318.0
Threaded Steel	2.1	9.0	8.0	0.50	0	318.0

### Borehole Notes:

The casing dimensions are derived from published values for Becker drill casing. Casing thicknesses at the joints are 0.875 in. and 0.240 in. for the 8-in. and 6-in. casings, respectively. The total depth of the borehole was provided by the driller. The well site geologist provided the depth to water. Logging data acquisition is referenced to the ground surface.

### Logging Equipment Information:

<b>Logging System:</b> Gamma 1E	<b>Type:</b> SGLS (70%) SN: 34TP40587A
<b>Calibration Date:</b> 07/03	<b>Calibration Reference:</b> GJO-2003-468-TAR
<b>Logging Procedure:</b> MAC-HGLP 1.6.5, Rev. 0	

### Spectral Gamma Logging System (SGLS) Log Run Information:

Log Run	1	2	3 Repeat	4	
Date	07/21/03	07/22/03	07/22/03	07/22/03	
Logging Engineer	Kos	Kos	Kos	Kos	
Start Depth (ft)	30.0	318.0	142.0	109.0	
Finish Depth (ft)	0.0	110.0	110.0	29.0	
Count Time (sec)	100	100	100	100	
Live/Real	R	R	R	R	
Shield (Y/N)	N	N	N	N	
MSA Interval (ft)	1.0	1.0	1.0	1.0	
ft/min	N/A <sup>2</sup>	N/A	N/A	N/A	
Pre-Verification	AE002CAB	AE003CAB	AE003CAB	AE003CAB	
Start File	AE002000	AE003000	AE003207	AE003240	
Finish File	AE002030	AE003206	AE003239	AE003320	
Post-Verification	AE002CAA	AE003CAA	AE003CAA	AE003CAA	



Log Run	1	2	3 Repeat	4	
Depth Return Error (in.)	0	N/A	N/A	-1.75	
Comments	No fine-gain adjustment.	No fine-gain adjustment.	No fine-gain adjustment.	Gain adjustment files -3250, -3271, and -3297	

### **Logging Operation Notes:**

Spectral gamma logging was performed in this borehole on July 21 and 22, 2003. Logging was conducted with a centralizer on the sonde and measurements are referenced to ground surface. A repeat section was collected in this borehole to evaluate system performance.

### **Analysis Notes:**

<b>Analyst:</b>	Henwood	<b>Date:</b>	07/28/03	<b>Reference:</b>	GJO-HGLP 1.6.3, Rev. 0
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Pre-run and post-run verifications for the logging system were performed before and after data acquisition. Acceptance criteria were met.

A combined casing correction for 0.675-in.-thick casing was applied throughout the borehole for both casings. The combined thickness at casing joints is 1.115 in. This thickness results in a significant reduction in gamma activity detection as the detector passes by a casing joint. However, it is not practical to correct individual data points for the effect of casing joints. The influence of the thick joints is apparent on the total gamma and  $^{40}\text{K}$  logs where reduced count rates and concentrations are exhibited at approximately 10-ft depth intervals.

SGLS spectra were processed in batch mode using APTEC SUPERVISOR to identify individual energy peaks and determine count rates. Concentrations were calculated with an EXCEL worksheet template identified as G1EJul03.xls using efficiency functions and corrections for casing, water, and dead time as determined from annual calibrations. Dead time corrections are applied where dead times exceed 10.5 percent; no dead times in excess of 10.5 percent were encountered. Correction for water was applied to the data below 272 ft.

### **Log Plot Notes:**

Separate log plots are provided for the man-made radionuclide ( $^{137}\text{Cs}$ ) detected in the borehole, naturally occurring radionuclides ( $^{40}\text{K}$ ,  $^{238}\text{U}$ ,  $^{232}\text{Th}$  [KUT]), a combination of man-made, KUT, and dead time, and total gamma plotted with dead time. For each radionuclide, the energy value of the spectral peak used for quantification is indicated. Unless otherwise noted, all radionuclides are plotted in picocuries per gram (pCi/g). The open circles indicate the minimum detectable level (MDL) for each radionuclide. Error bars on each plot represent error associated with counting statistics only and do not include errors associated with the inverse efficiency function, dead time correction, casing corrections, or water corrections. A repeat log section is also included.

### **Results and Interpretations:**

<sup>137</sup>Cs was the only man-made radionuclide detected in this borehole. <sup>137</sup>Cs was detected at a few sporadic locations throughout the borehole near its MDL of approximately 0.2 pCi/g.

The repeat sections indicated good agreement of the naturally occurring KUT.

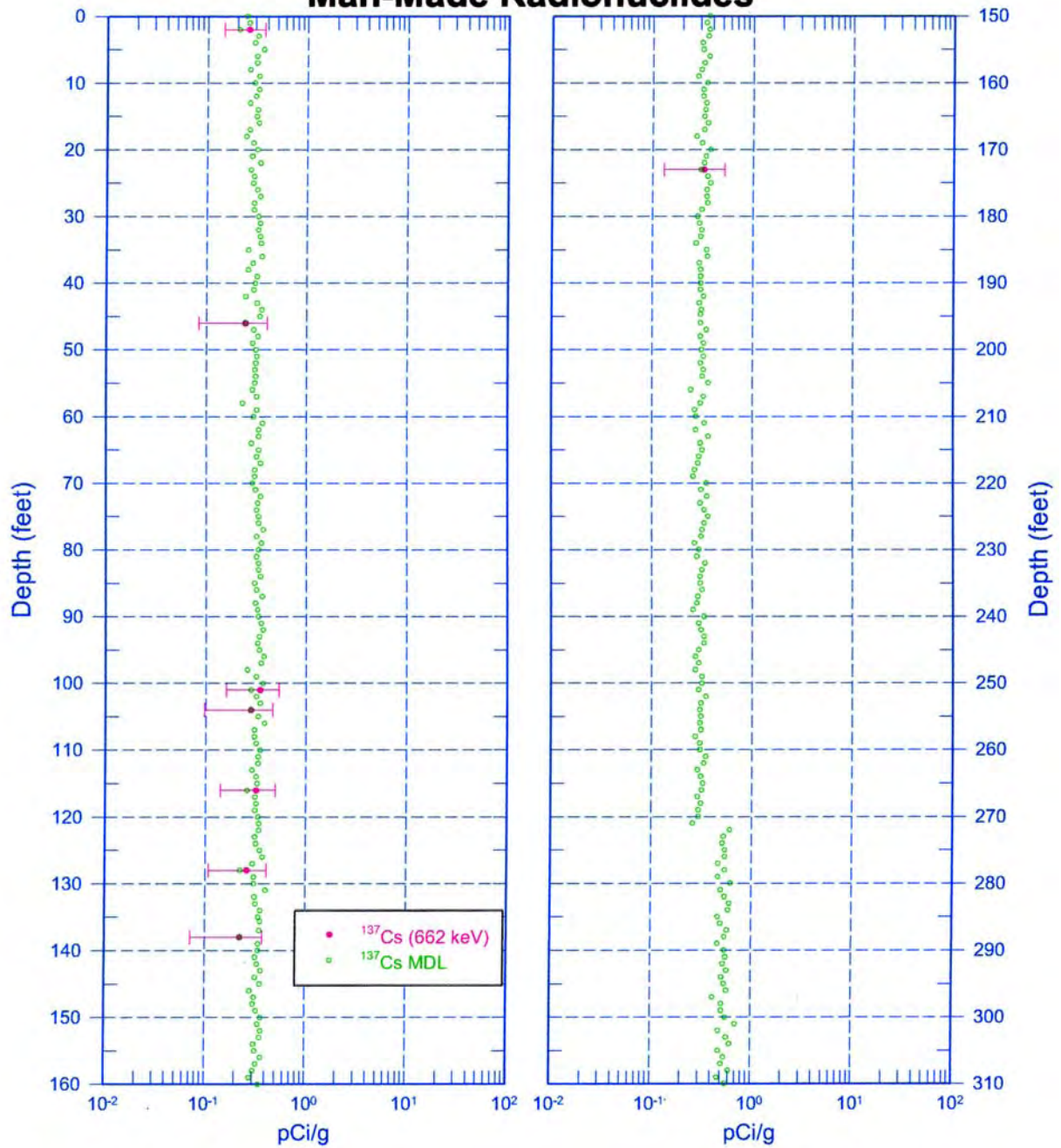
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<sup>1</sup> GWL – groundwater level

<sup>2</sup> N/A – not applicable

# C-4127

## Man-Made Radionuclides

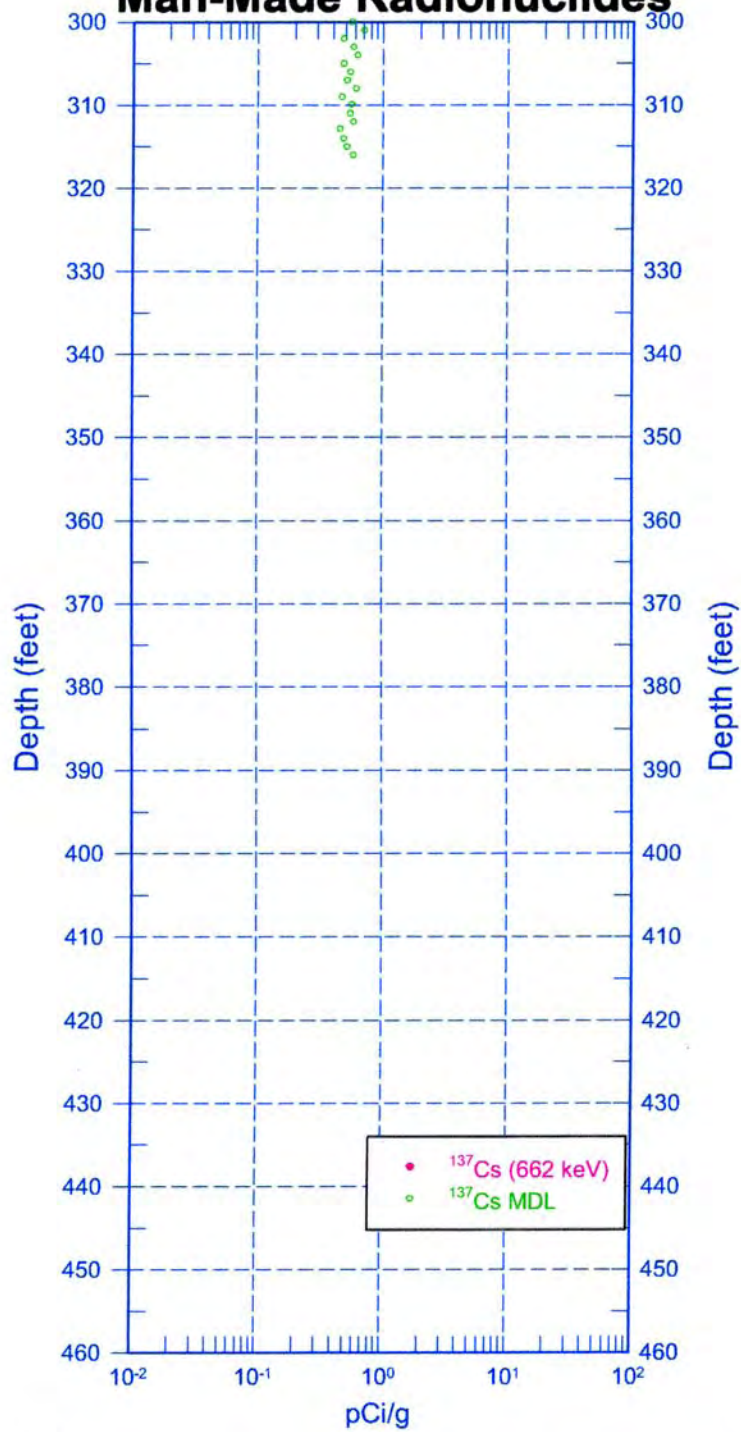


Zero Reference = Ground Surface

Last Log Date - 07/22/03

# C-4127

## Man-Made Radionuclides



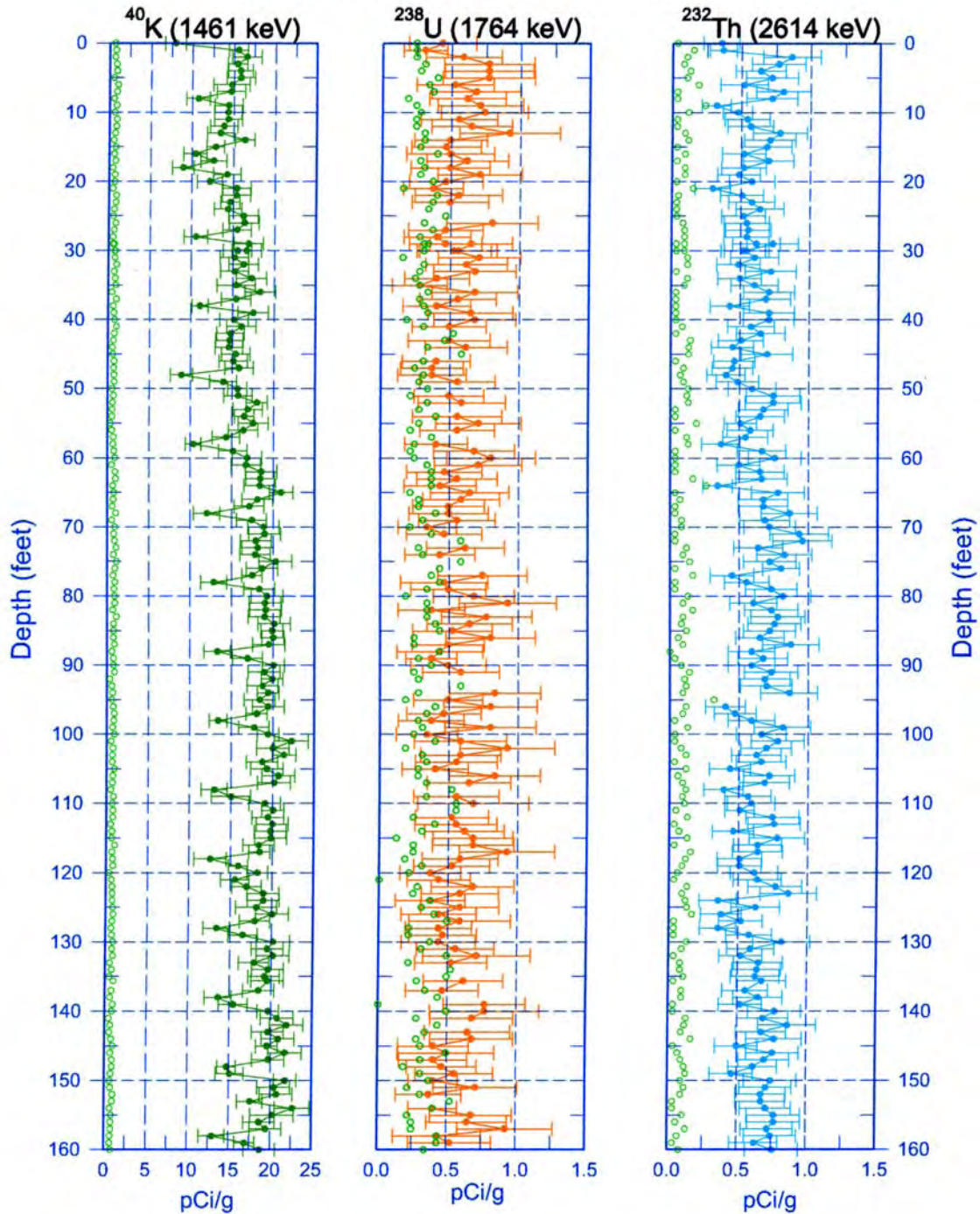
Zero Reference = Ground Surface

Last Log Date - 07/22/03



# C-4127

## Natural Gamma Logs



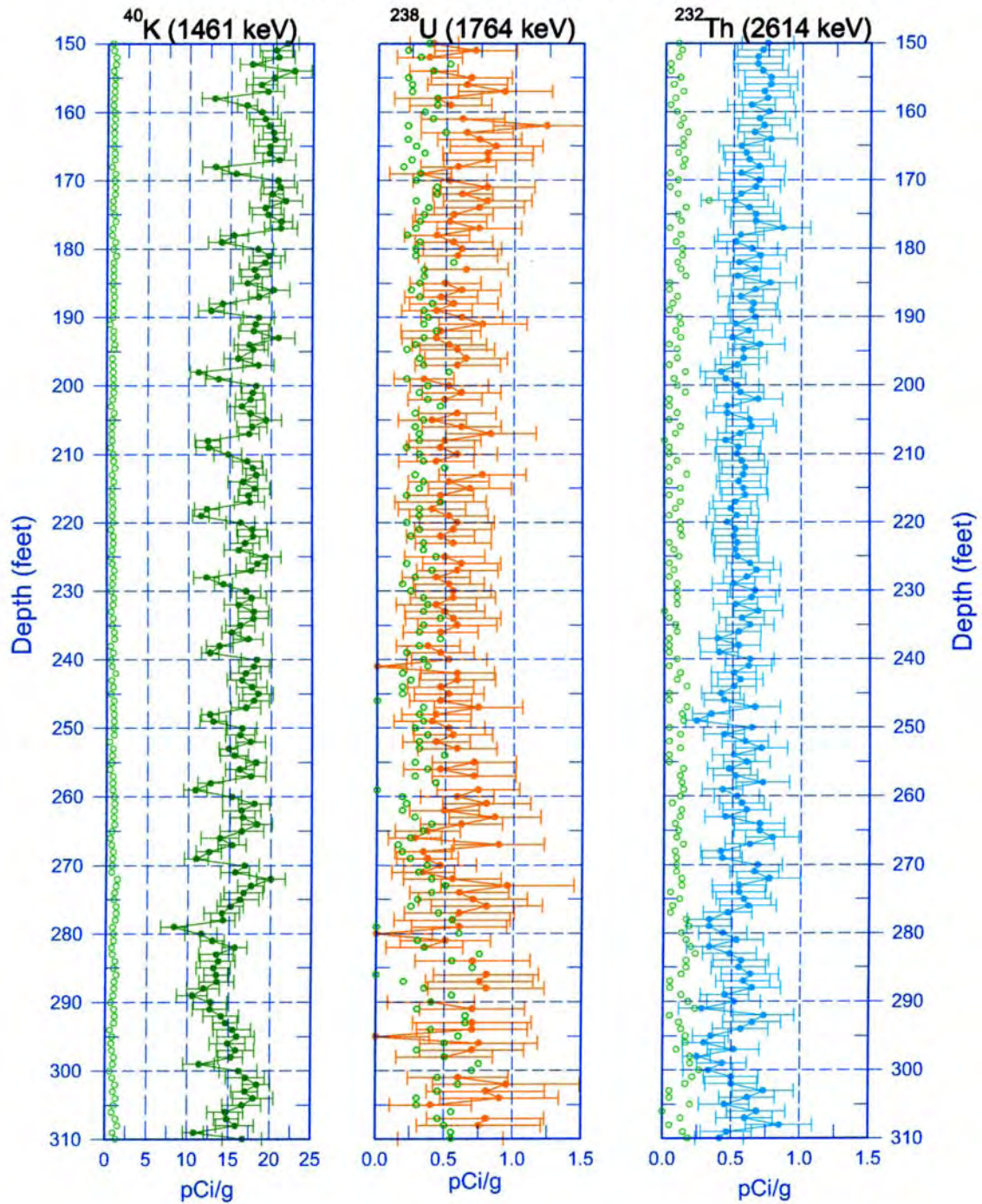
Zero Reference = Ground Surface

○ MDL

Last Log Date - 07/22/03

# C-4127

## Natural Gamma Logs



Zero Reference = Ground Surface

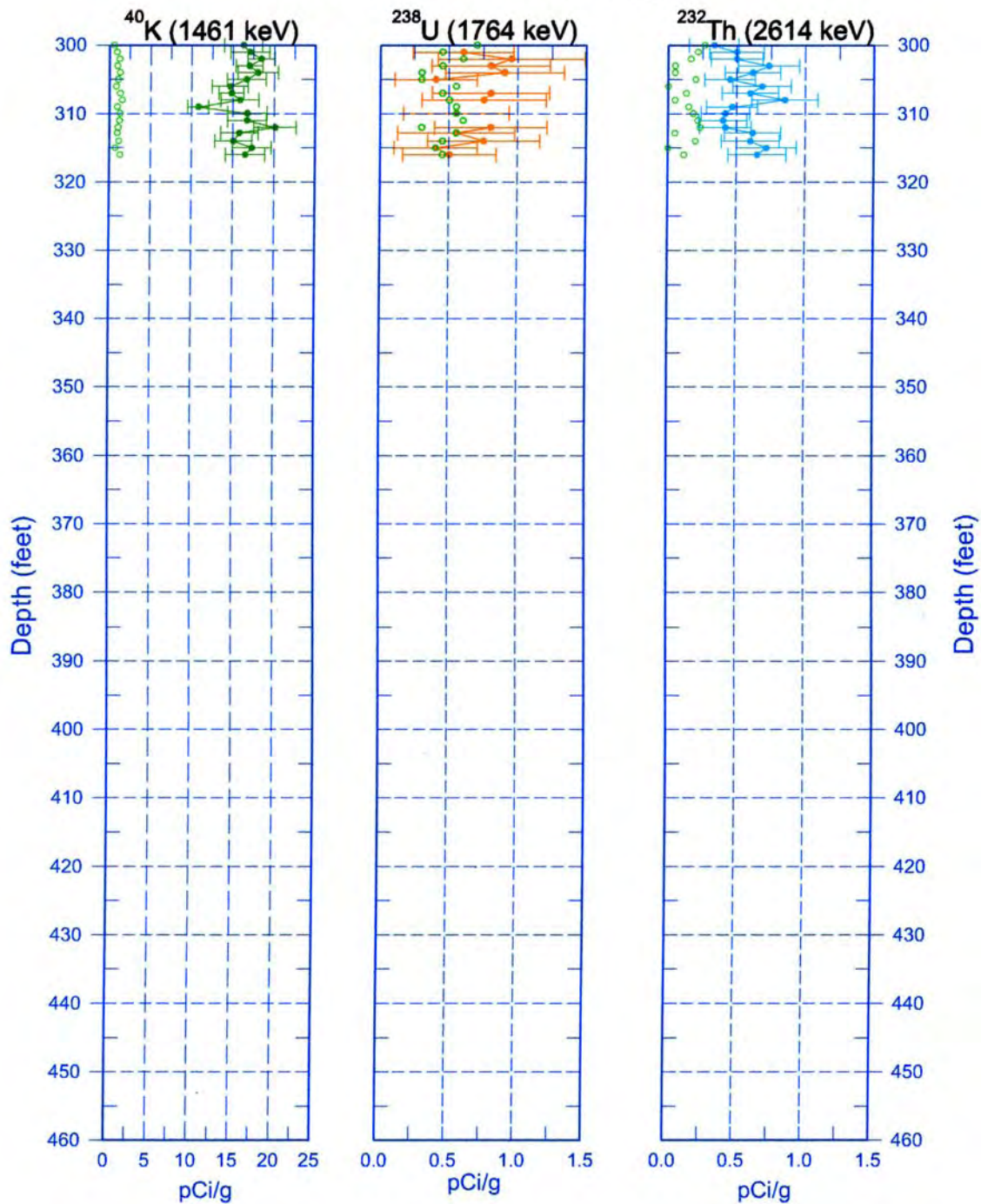
○ MDL

Last Log Date - 07/22/03



# C-4127

## Natural Gamma Logs

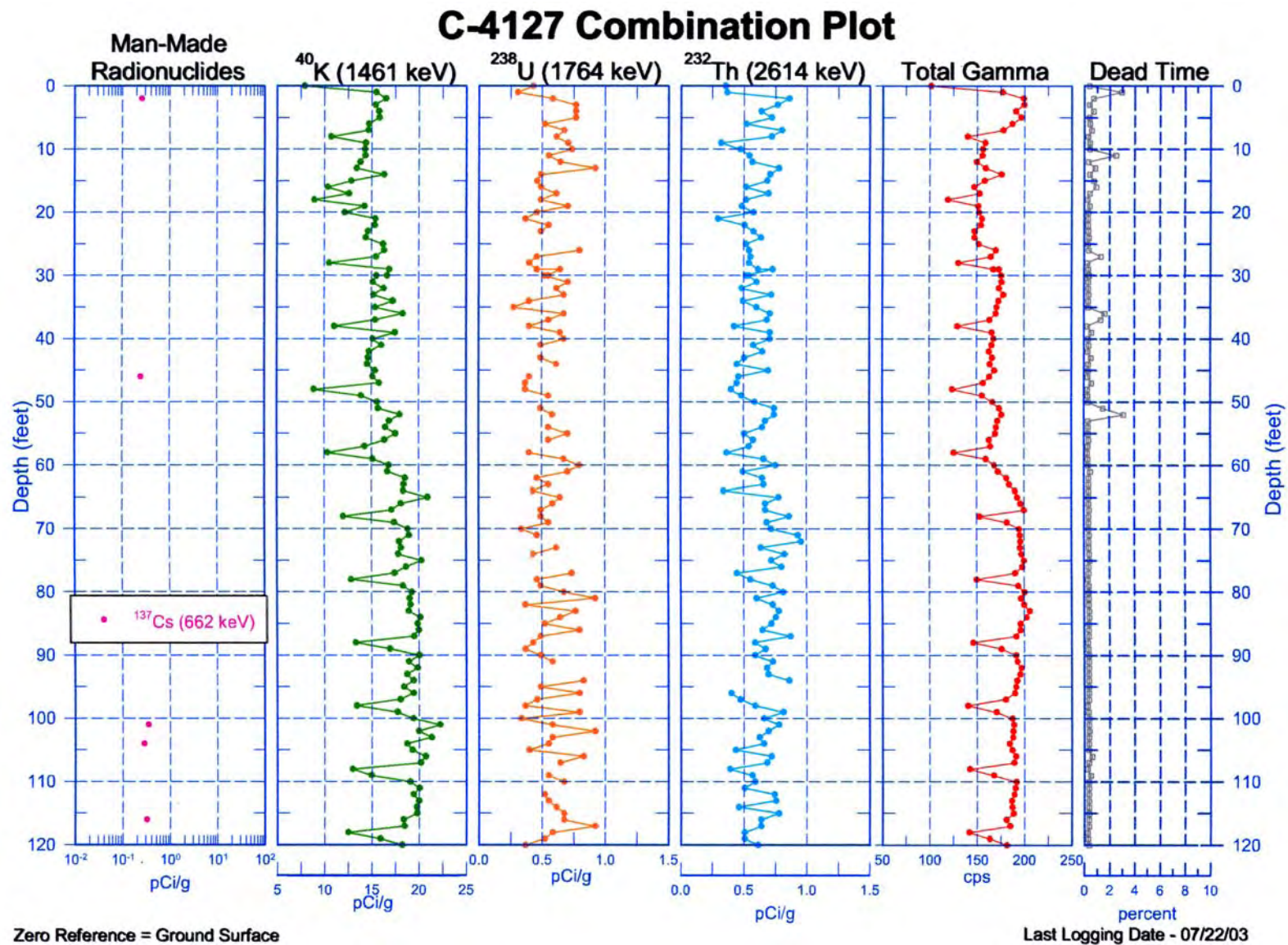


Zero Reference = Ground Surface

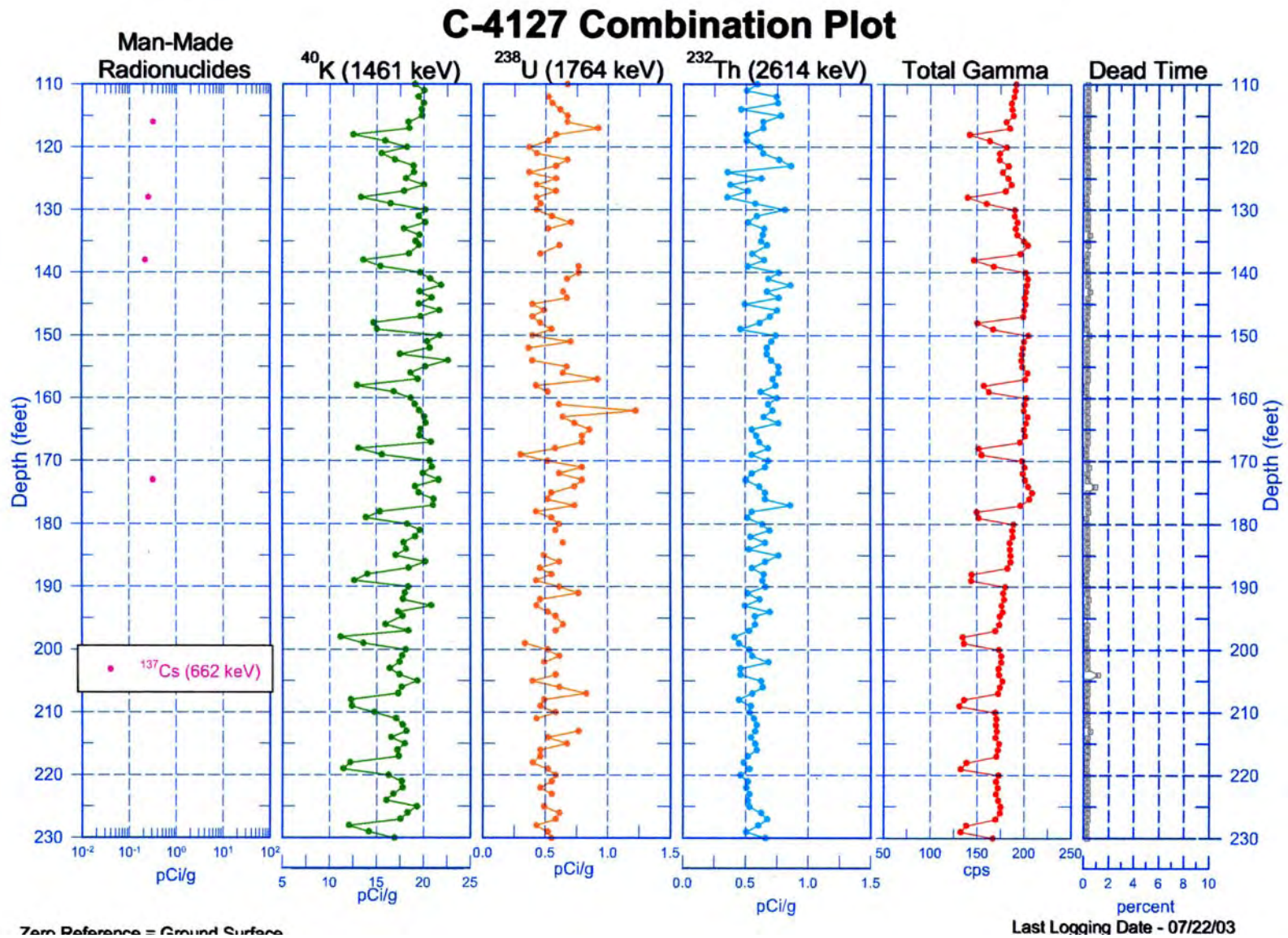
○ MDL

Last Log Date - 07/22/03

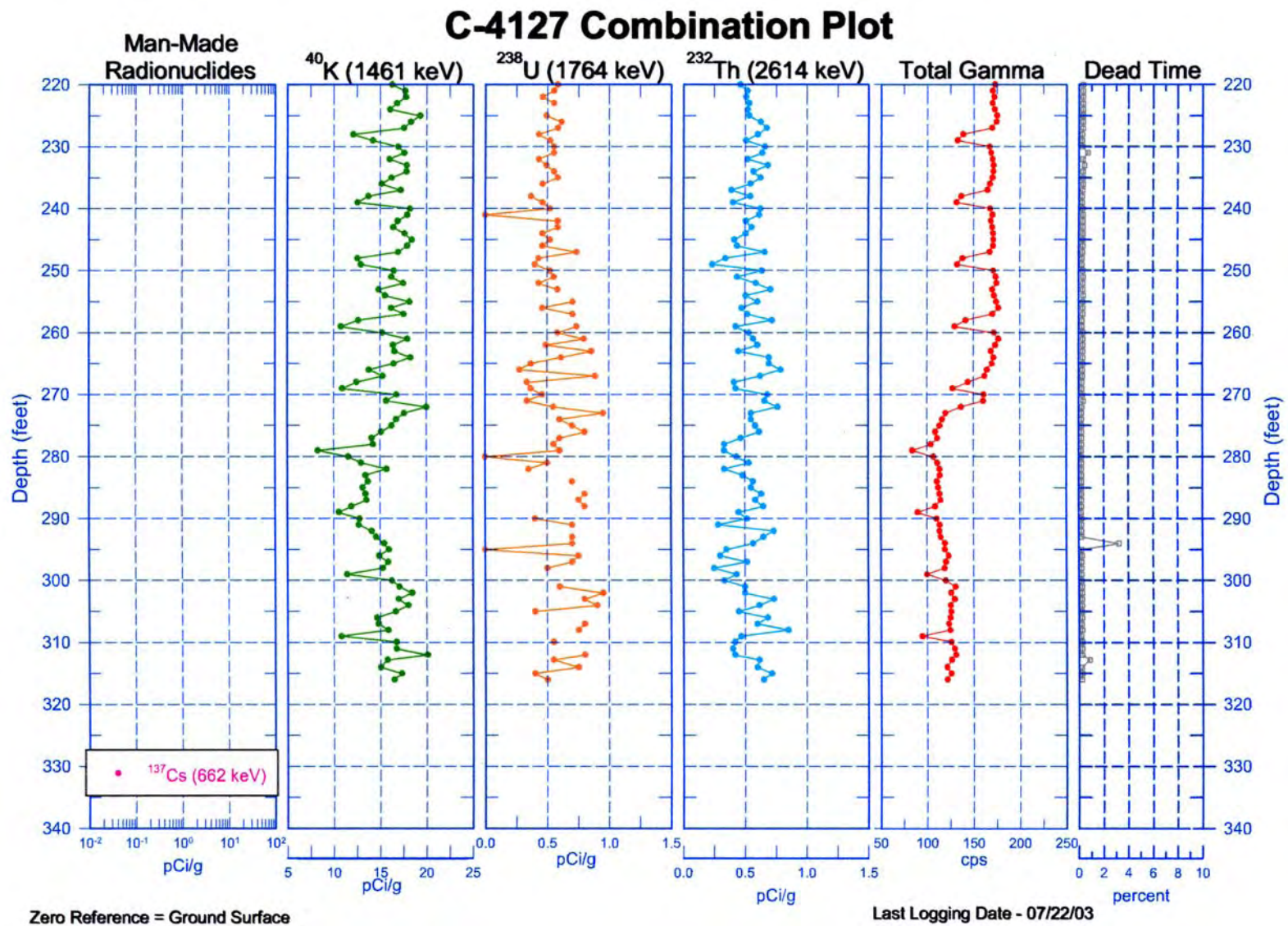
C.33







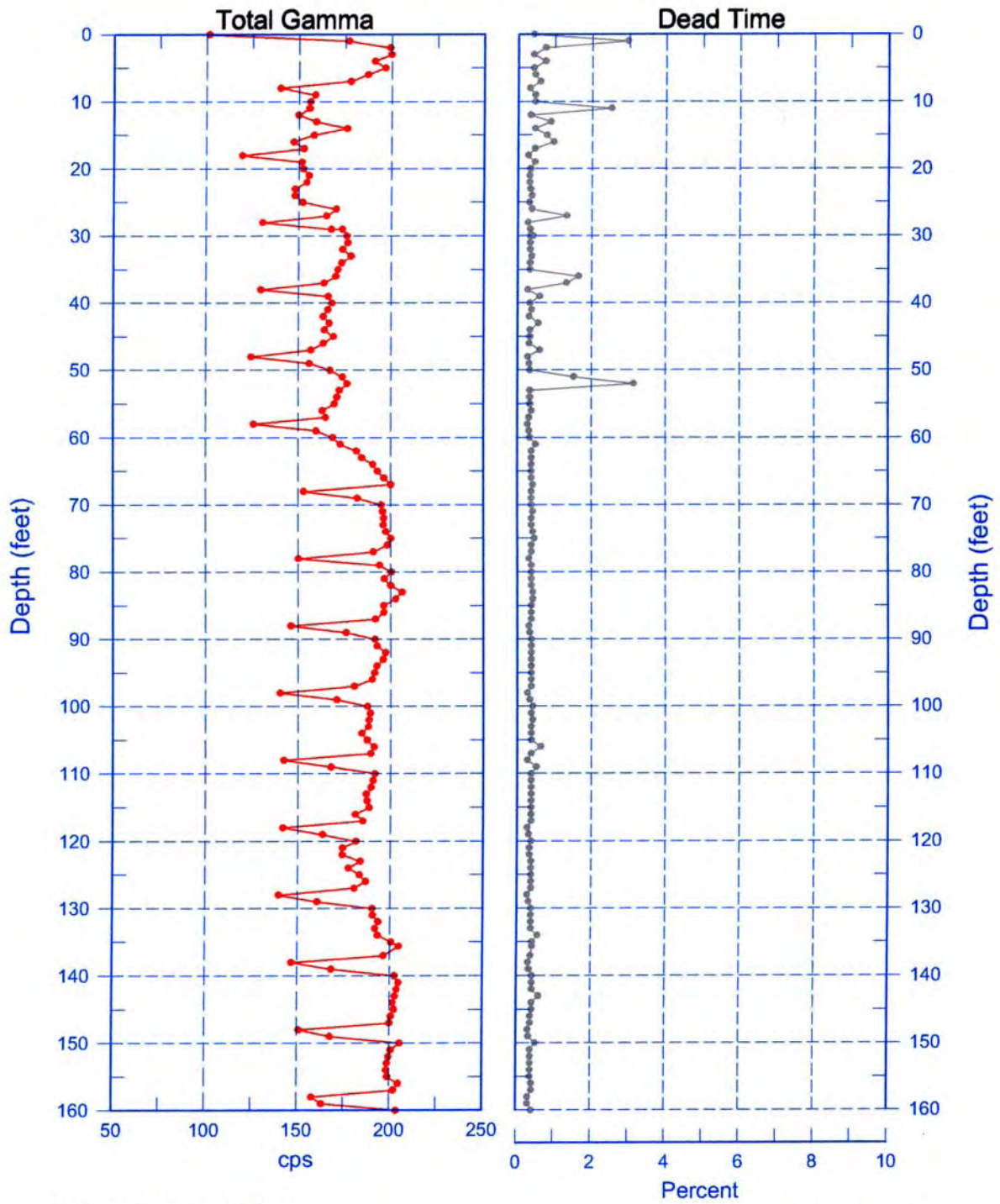
C.35





# C-4127

## Total Gamma & Dead Time

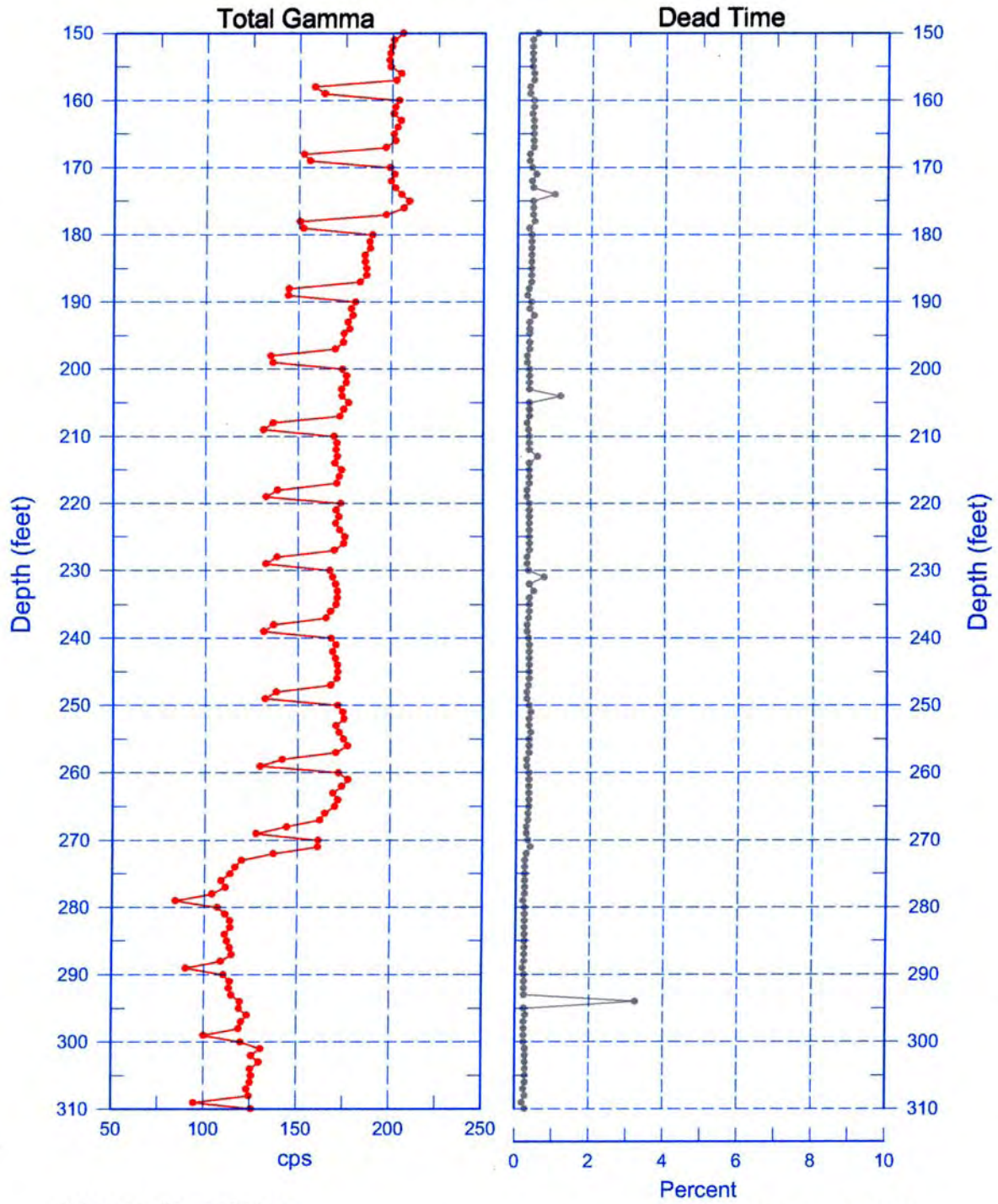


Reference - Ground Surface

Last Log Date - 07/22/03

# C-4127

## Total Gamma & Dead Time



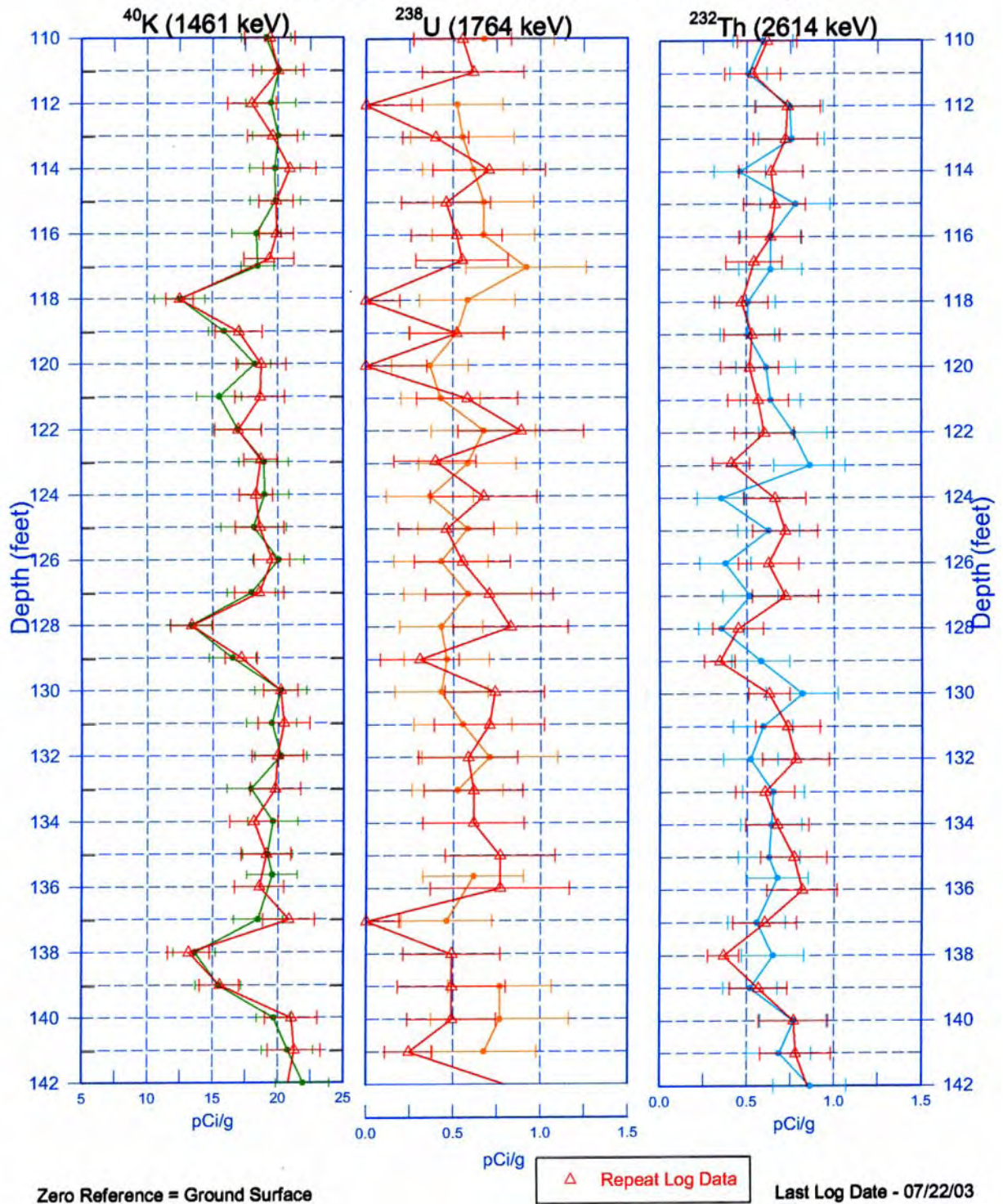
Reference - Ground Surface

Last Log Date - 07/22/03



# C-4127

## Repeat Section of Natural Gamma Logs



## C4190 Log Data Report

### Borehole Information:

<b>Borehole:</b> C4190		<b>Site:</b> Southwest of C Tank Farm			
<b>Coordinates (WA State Plane)</b>		<b>GWL (ft)<sup>1</sup>:</b> 273	<b>GWL Date:</b> 8/6/2003		
<b>North</b>	<b>East</b>	<b>Drill Date</b>	<b>TOC<sup>2</sup> Elevation</b>	<b>Total Depth (ft)</b>	<b>Type</b>
N/A <sup>3</sup>	N/A	August 2003	N/A	318	Becker

### Casing Information:

Casing Type	Stickup (ft)	Outer Diameter (in.)	Inside Diameter (in.)	Thickness (in.)	Top (ft)	Bottom (ft)
Threaded steel	2.85	6 1/4	6	1/8	+2.85	318
Threaded steel	2.25	9	8	1/2	2.25	318

Casing stickup was measured using a steel tape. The logging engineer measured the outside diameters for both the 6- and 8-in. casings using a caliper. The caliper and 6-in. inside casing diameter were measured using a steel tape; measurements were rounded to the nearest 1/16 in.

### Borehole Notes:

Zero reference is the ground surface. This borehole was logged through the drill pipe. The borehole is located approximately 30 ft east of UPR 200-E-86 and 20 ft north of the MO 822 change trailer. A 6-in. layer of crushed gravel is present on the ground surface surrounding the drill site.

The Becker drilling system utilizes a special dual-wall casing string. Air passes through the annular space between the inner and outer casing, and drill cuttings are brought up inside the inner casing. For this well, the casing consisted of a 6-in. ID inner casing with 0.125-in. wall thickness inside an 8-in. ID outer casing with 0.5-in. wall thickness. The inner casing is thicker at casing joints, where wall thickness is 0.406 in. Casing joints are approximately 1 ft long overall and occur at 10-ft intervals.

### Logging Equipment Information:

<b>Logging System:</b>	Gamma 1E	<b>Type:</b>	70% HPG <sub>e</sub> (34-TP40587A)
<b>Calibration Date:</b>	07/2003	<b>Calibration Reference:</b>	GJO-2003-488-TAR
		<b>Logging Procedure:</b>	MAC-HGLP 1.6.5, Rev. 0

### Spectral Gamma Logging System (SGLS) Log Run Information:

Log Run	1	2/Repeat	3		
Date	8/07/03	8/08/03	8/08/03		
Logging Engineer	Spatz	Spatz	Spatz		
Start Depth (ft)	319.0	147.0	114.0		
Finish Depth (ft)	115.0	115.0	0		
Count Time (sec)	100	100	100		

Log Run	1	2/Repeat	3		
Live/Real	R	R	R		
Shield (Y/N)	N	N	N		
MSA Interval (ft)	1.0	1.0	1.0		
ft/min	n/a <sup>4</sup>	n/a	n/a		
Pre-Verification	AE013CAB	AE014CAB	AE014CAB		
Start File	AE013000	AE014000	AE014033		
Finish File	AE013204	AE014032	AE014147		
Post-Verification	AE013CAA	AE014CAA	AE014CAA		
Depth Return Error (in.)	-2.5	n/a	-1		
Comments	No fine-gain adjustment.	No fine-gain adjustment.	Fine-gain adjustment after files -101 and -116.		

### **Logging Operation Notes:**

Zero reference was the ground surface, and the borehole was logged through drill pipe.

SGLS data were collected using Gamma 1E. Pre- and post-survey verification measurements employed the Amersham KUT (<sup>40</sup>K, <sup>238</sup>U, and <sup>232</sup>Th) verifier with serial number 118. Logging was performed with a centralizer installed on the sonde.

### **Analysis Notes:**

<b>Analyst:</b>	Sobczyk	<b>Date:</b>	8/14/03	<b>Reference:</b>	GJO-HGLP 1.6.3, Rev. 0
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SGLS pre-run and post-run verification spectra were collected at the beginning and end of the day and compared to the control limits. All of the verification spectra were within the control limits, except for spectrum AE013CAB. This spectrum was slightly above the upper control limit for the 609-keV peak counts per second (cps) value. The peak counts per second at the 609-keV, 1461-keV, and 2615-keV photopeaks on the post-run verification spectra as compared to the pre-run verification spectra for each day were between 0.5 percent higher and 7.0 percent lower at the end of the day. Examinations of spectra indicate that the detector functioned normally during all of the logging runs, and the spectra are accepted.

Log spectra were processed in batch mode using APTEC SUPERVISOR to identify individual energy peaks and determine count rates. The pre-run verification spectrum was used to determine the energy and resolution calibration for processing the data using APTEC SUPERVISOR. Concentrations were calculated in EXCEL (source file: G1EJul03.xls). Zero reference was the ground surface. Based on measurements supplied by the logging engineer, the casing configuration was assumed to be a string of 6-in. and 8-in. casings to 319 ft. The casing correction factor was calculated using a combined casing thickness of 5/8 in. This casing thickness is based upon the field measurements. The combined thickness at casing joints is 1.115 in. This thickness results in a significant reduction in gamma activity detection as the detector passes by a casing joint. However, it is not practical to correct individual data points for the effect of casing joints every 10.0 ft. The influence of the thick joints is apparent on the total gamma and <sup>40</sup>K logs where reduced count rates and concentrations are exhibited at approximately 10-ft depth intervals. Water corrections were applied to the data below 273 ft. SGLS dead time corrections were not applied because dead time did not exceed 10 percent.

### **Log Plot Notes:**

Separate log plots are provided for gross gamma and dead time, naturally occurring radionuclides (<sup>40</sup>K, <sup>238</sup>U, and <sup>232</sup>Th), and man-made radionuclides. Plots of the repeat logs versus the original logs are

included. For each radionuclide, the energy value of the spectral peak used for quantification is indicated. Unless otherwise noted, all radionuclides are plotted in picocuries per gram (pCi/g). The open circles indicate the minimum detectable level (MDL) for each radionuclide. Error bars on each plot represent error associated with counting statistics only and do not include errors associated with the inverse efficiency function, dead time correction, or casing correction. These errors are discussed in the calibration report. A combination plot is also included to facilitate correlation. The  $^{214}\text{Bi}$  peak at 1764 keV was used to determine the naturally occurring  $^{238}\text{U}$  concentrations on the combination plot rather than the  $^{214}\text{Bi}$  peak at 609 keV because it exhibited higher net counts per second.

### **Results and Interpretations:**

$^{137}\text{Cs}$  was the only man-made radionuclide detected in this borehole.  $^{137}\text{Cs}$  was detected near the ground surface at 2 ft and in the interval from 11 through 13 ft at concentrations ranging from the MDL (0.3 pCi/g) to 0.6 pCi/g. The maximum concentration of  $^{137}\text{Cs}$  was measured at 12 ft.  $^{137}\text{Cs}$  was also detected at log depths of 65, 130, and 218 ft with concentrations near the MDL.

Logging through the drill pipe used in the construction of this borehole precludes the acquisition of SGLS spectra that consistently have statistically valid photopeaks. The relatively thick casing joints effectively shield the detector from the formation over a 3.0-ft zone at 10.0-ft intervals. Energy levels below 1461 keV are severely attenuated by the drill pipe.

The plots of the repeat logs demonstrate reasonable repeatability of the SGLS. The natural radionuclides at energy levels of 609, 1461, 1764, and 2614 keV are comparable between the repeat and original SGLS log runs.  $^{137}\text{Cs}$  encountered at 130 ft on the original log run did not repeat.

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<sup>1</sup> GWL – groundwater level

<sup>2</sup> TOC – top of casing

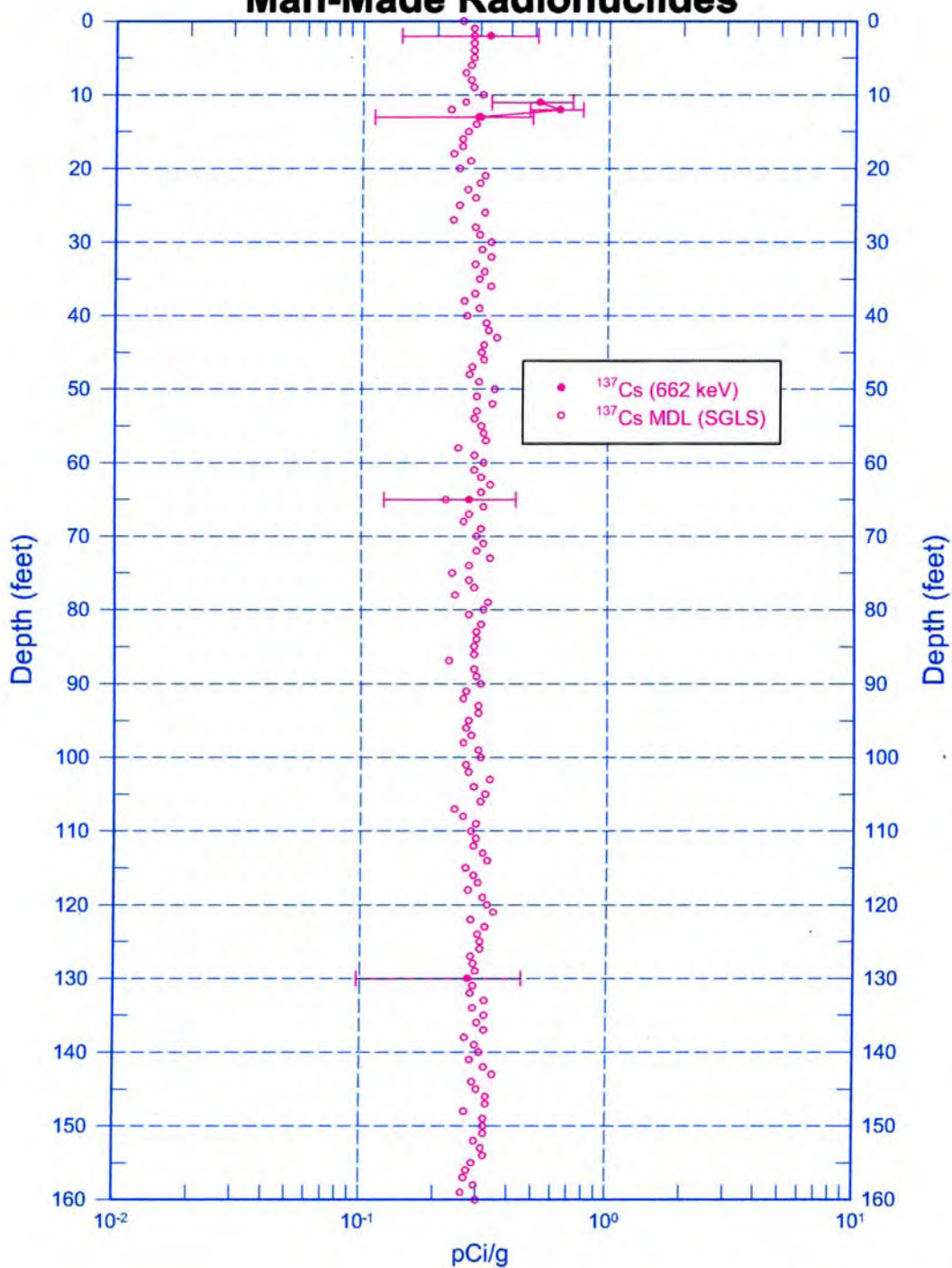
<sup>3</sup> N/A – not available

<sup>4</sup> n/a – not applicable



# C4190

## Man-Made Radionuclides

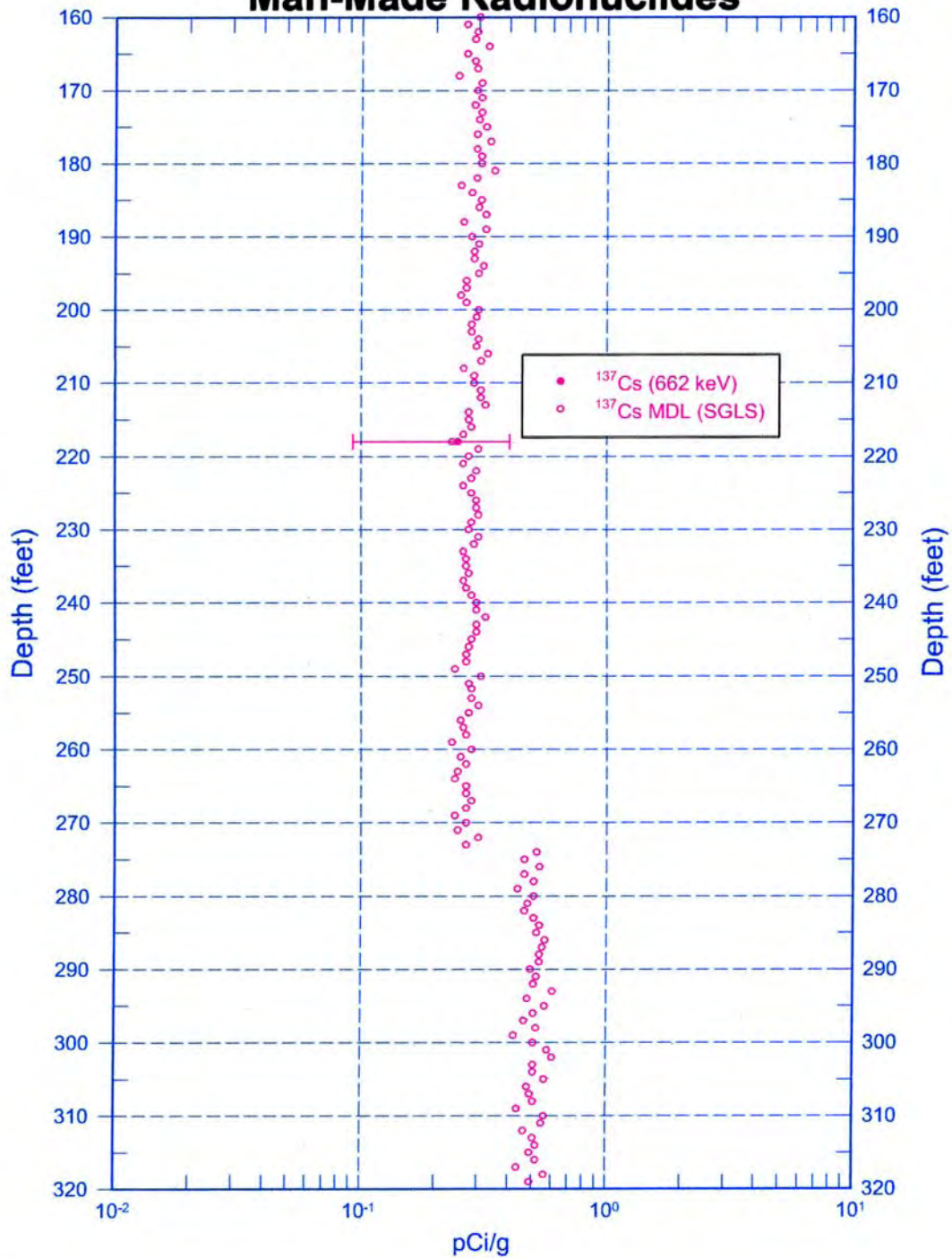


Zero Reference = Ground Surface

Date of Last Logging Run  
8/08/2003

# C4190

## Man-Made Radionuclides



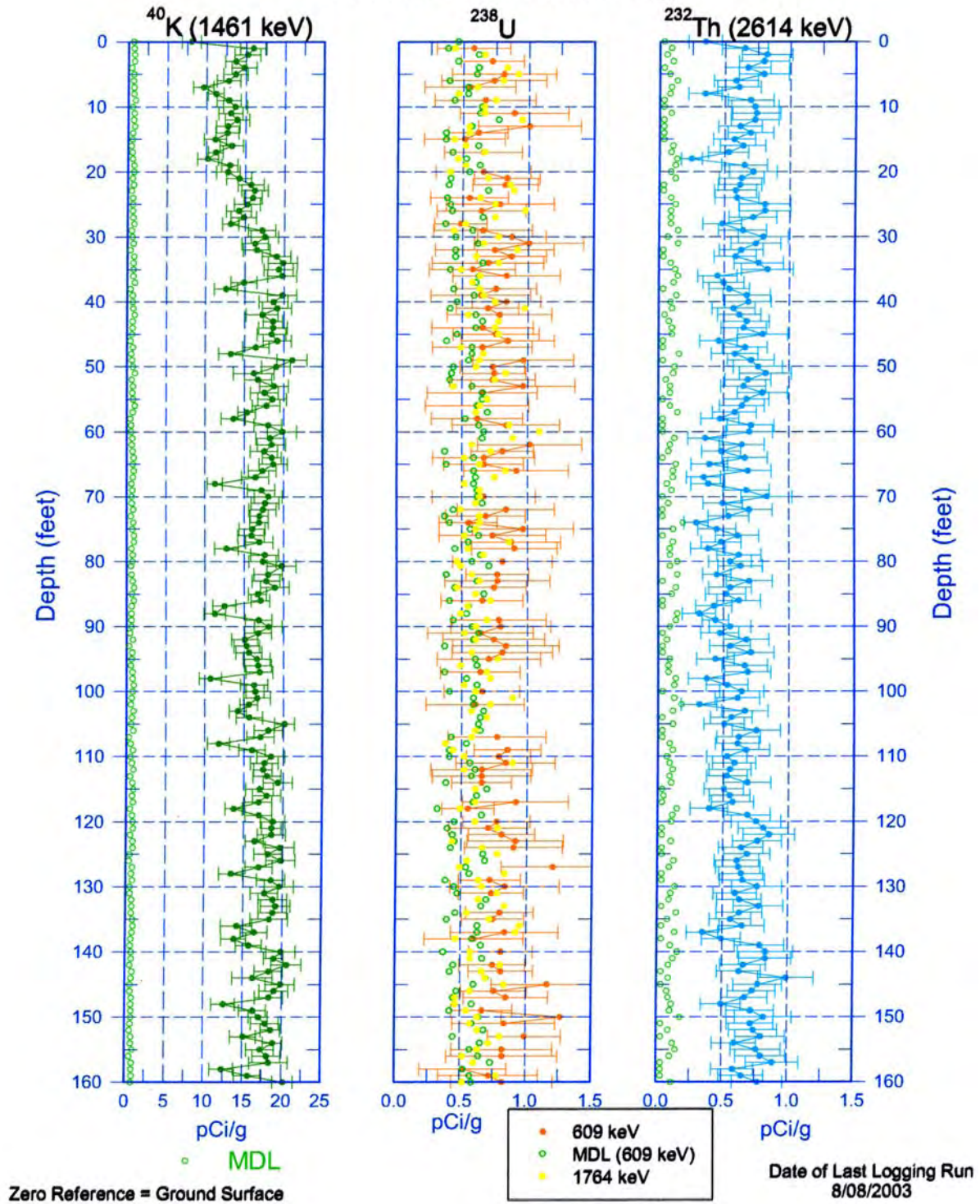
Zero Reference = Ground Surface

Date of Last Logging Run  
8/08/2003

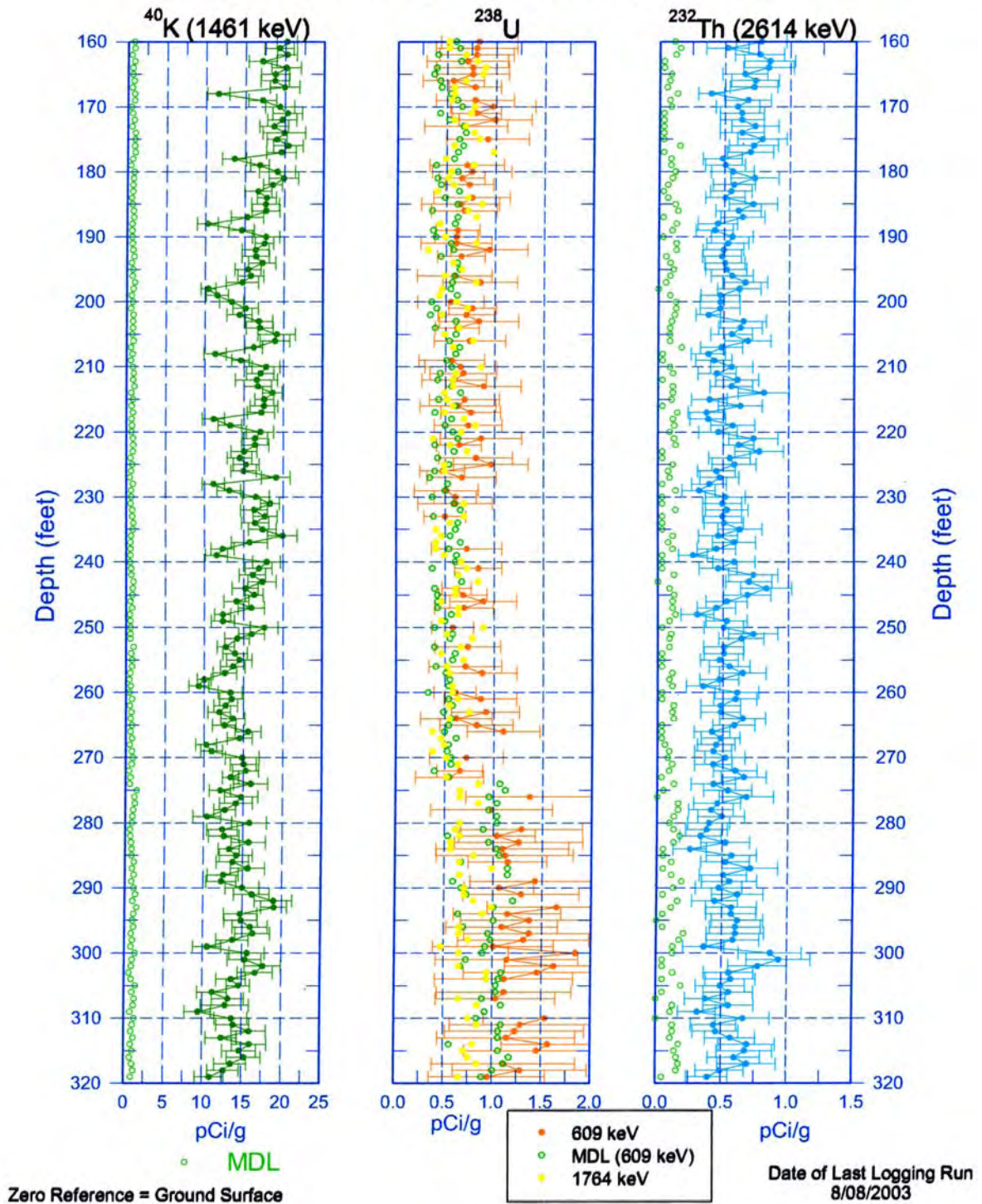


# C4190

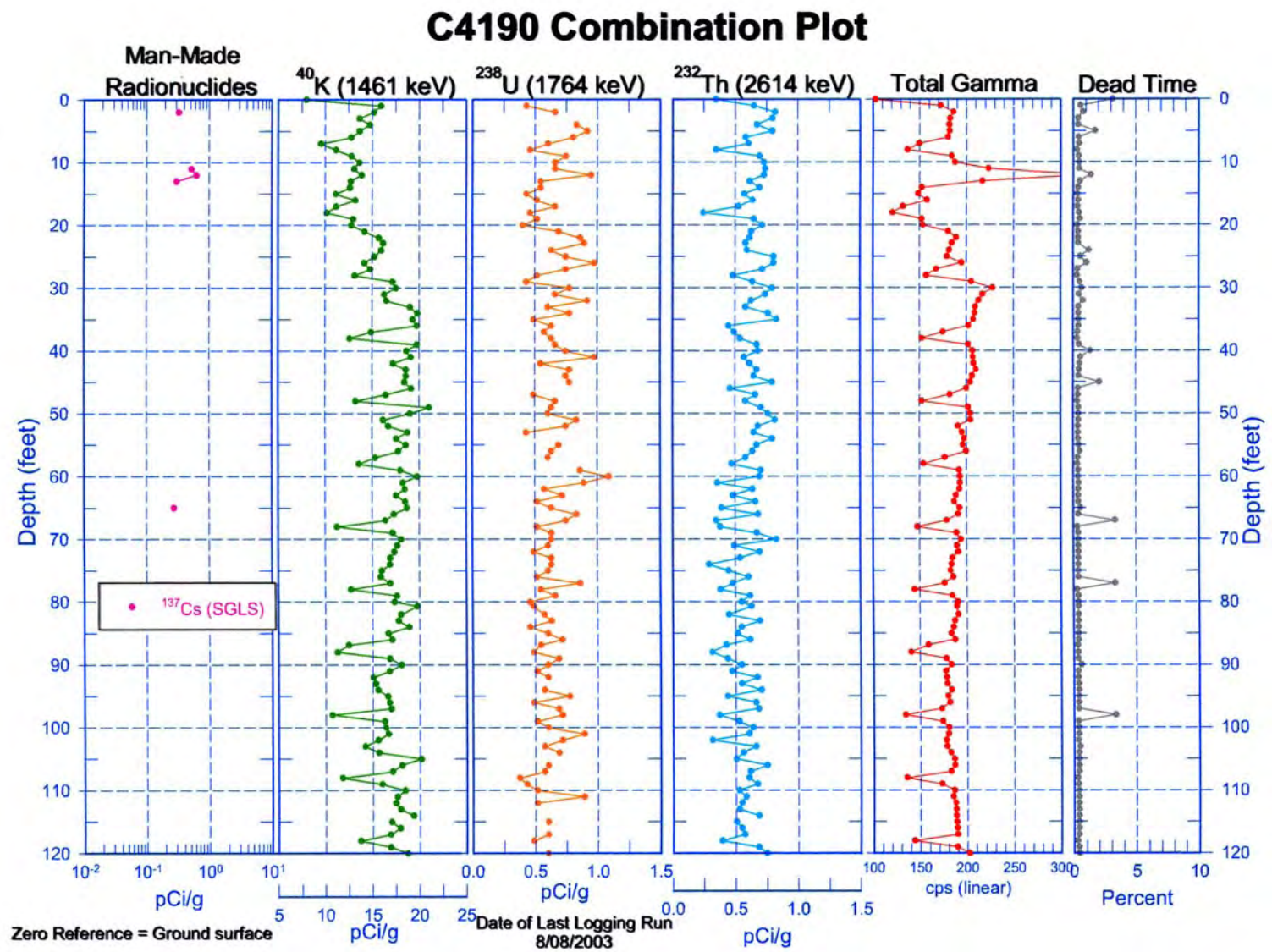
## Natural Gamma Logs



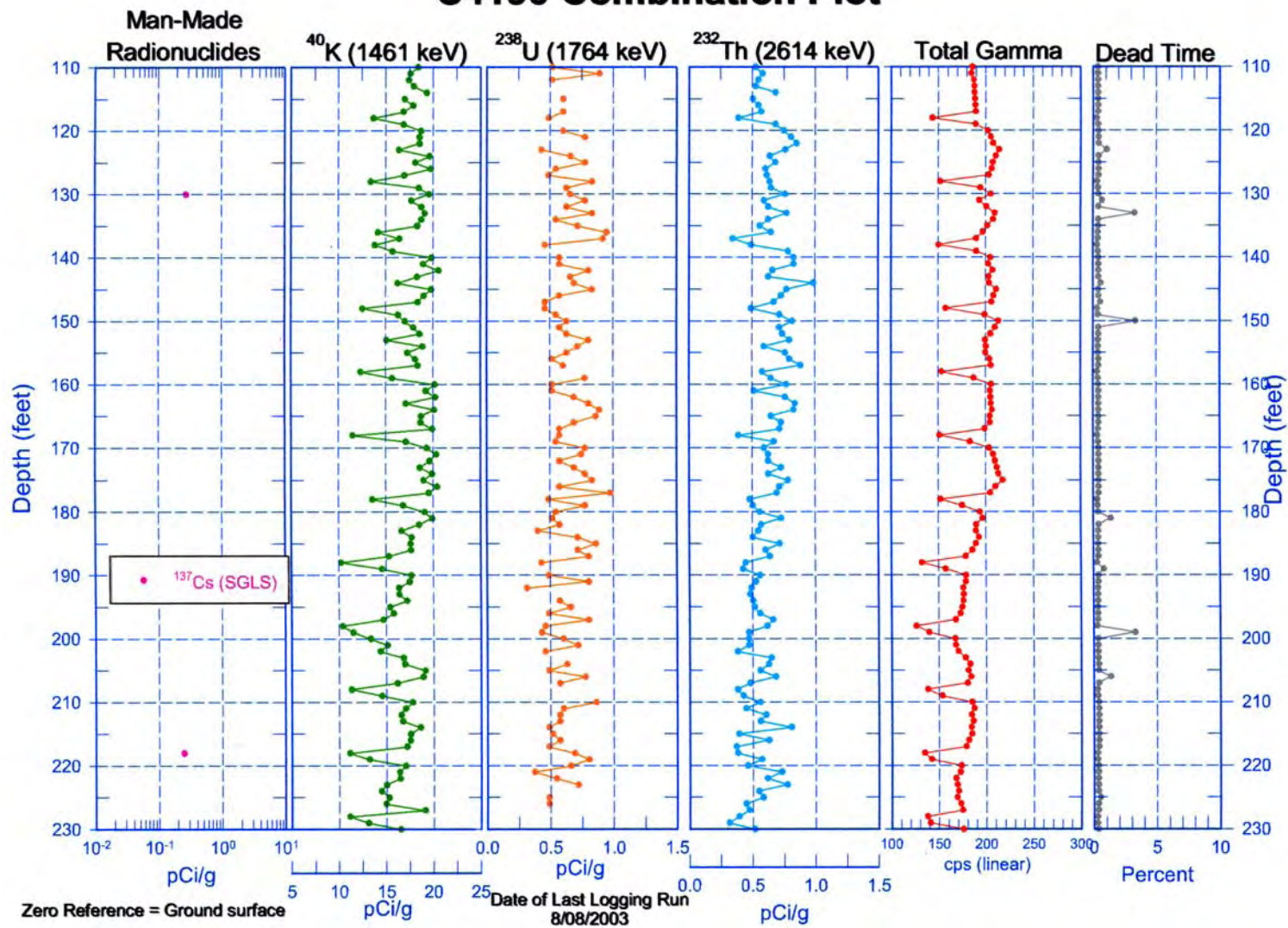
# C4190 Natural Gamma Logs





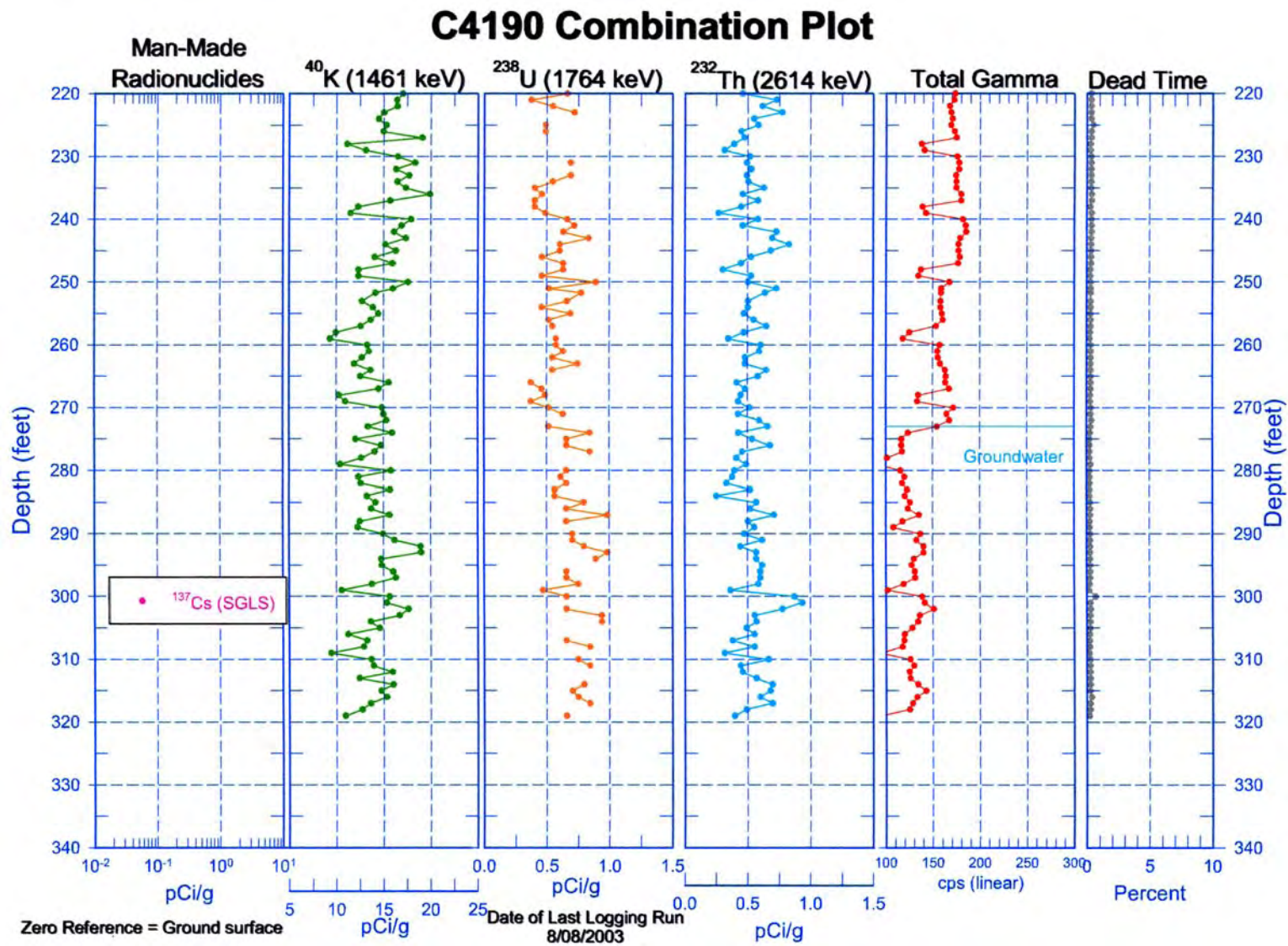


# C4190 Combination Plot



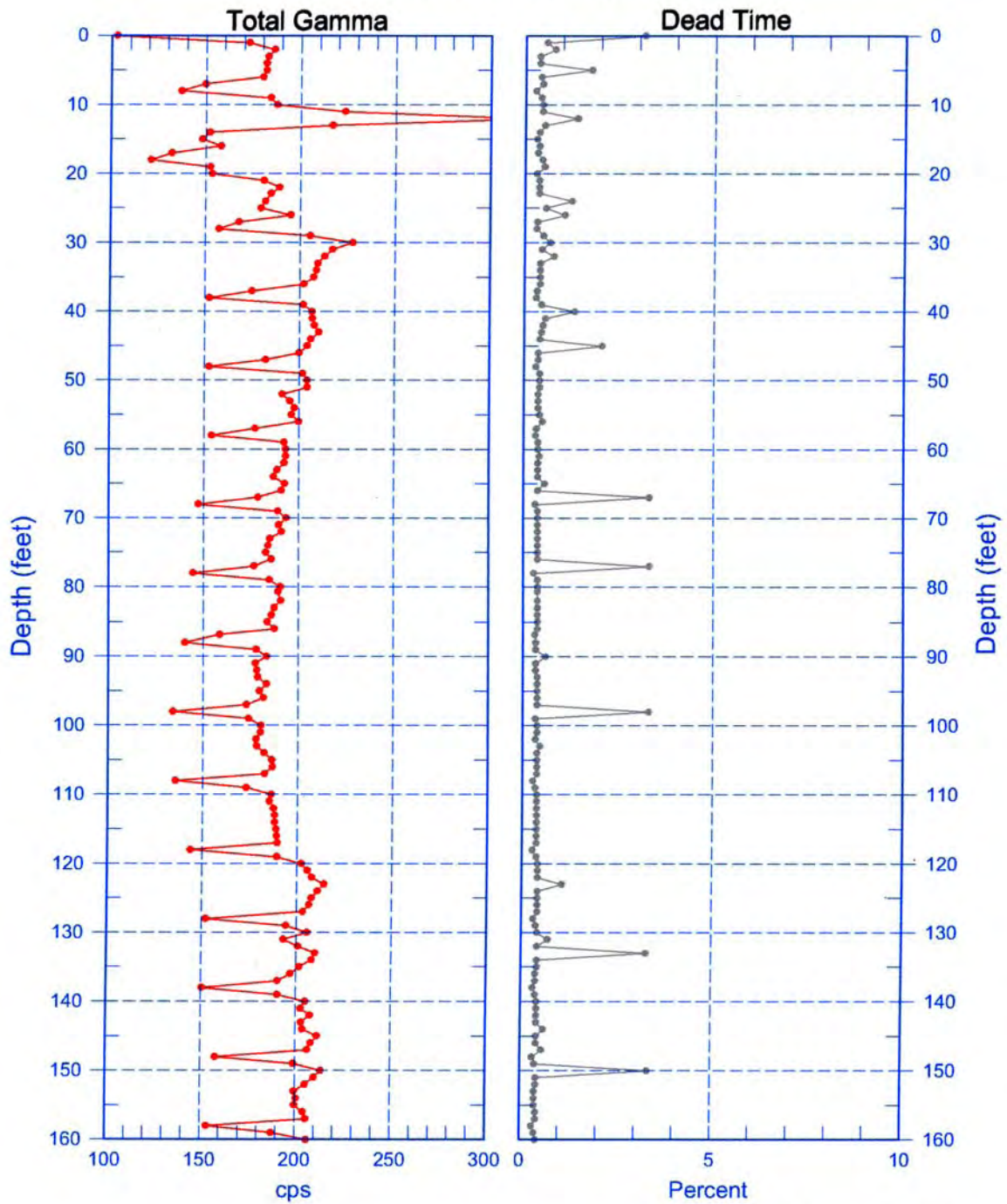


C.48



# C4190

## Total Gamma & Dead Time



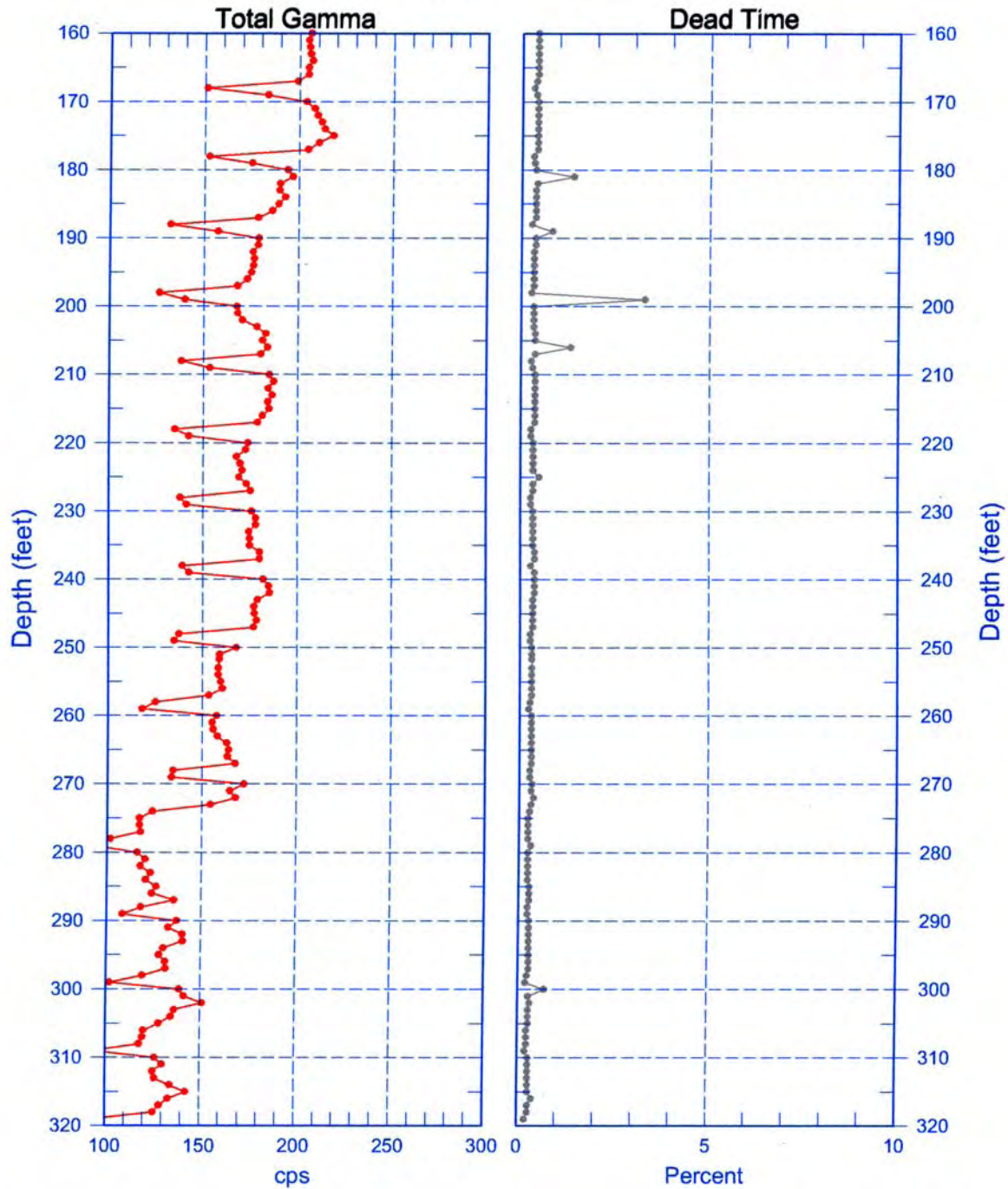
Zero Reference = Ground Surface

Date of Last Logging Run  
8/08/2003



# C4190

## Total Gamma & Dead Time

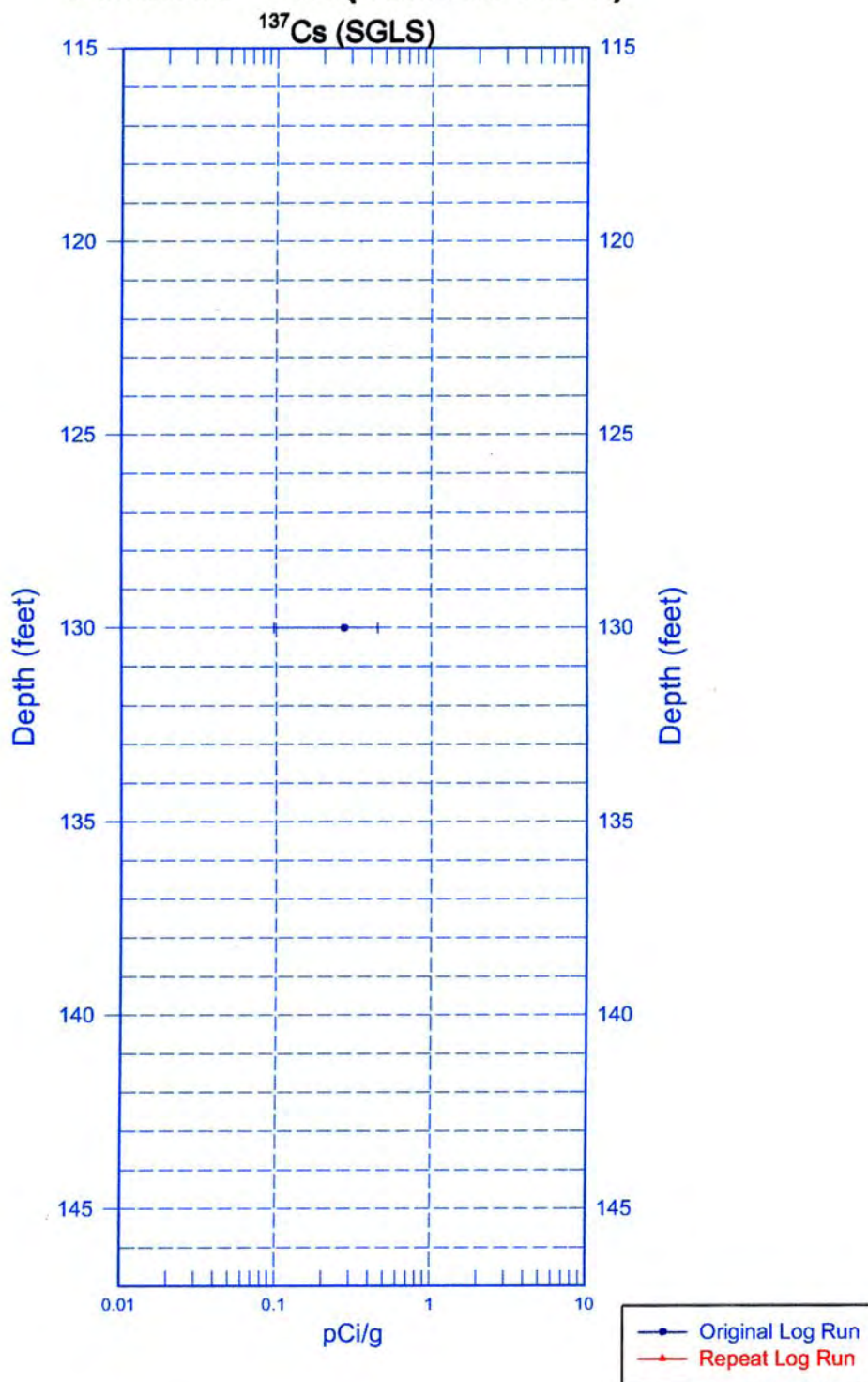


Zero Reference = Ground Surface

Date of Last Logging Run  
8/08/2003

# C4190

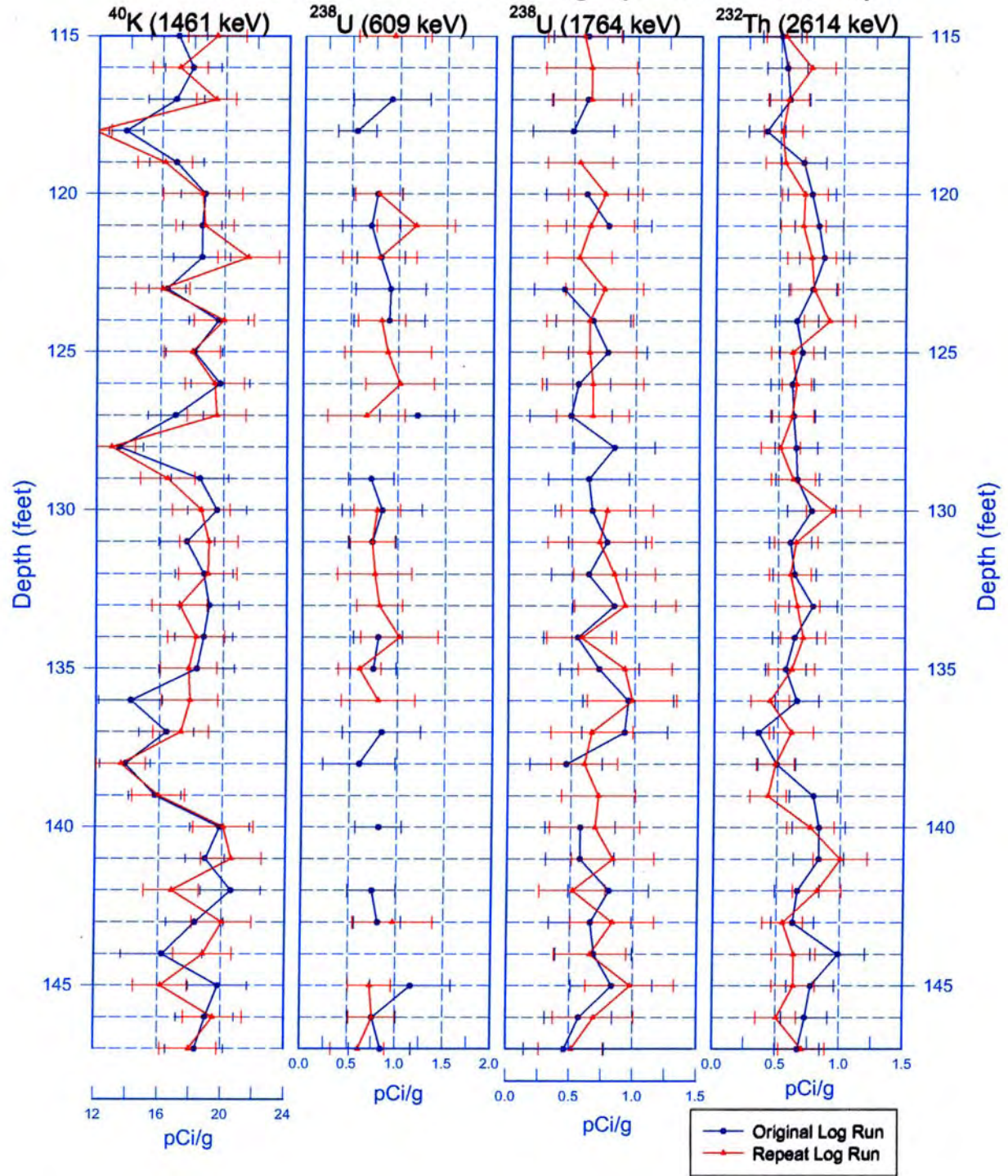
## Rerun of $^{137}\text{Cs}$ (147.0 to 115 ft)





# C4190

## Rerun of Natural Gamma Logs (147.0 to 115.0 ft)



**Gyroscope Data Table for Well 299-E27-22**

Hole: C4124	Time	CablLength (feet)	Inclination (from Vert.)	TF Gyro	TFHighSide	CourseDir (0°..360°)	Rec.ID (17)	ClosureDir (0°..360°)	ClosureDist (feet)	TVD (+feet)	+N/-S (feet)	+E/-W (feet)	Dogleg °/ 100f
2 S	2.85	0	0.15	157	293	306	2 S	0	0	0	0	0	0
3 S	3.42	20	0.06	310	90	302	3 S	305	0.04	20	0.02	-0.03	0.5
4 S	4.06	40	0.64	13.3	232	223	4 S	244	0.13	40	-0.1	-0.11	3.2
5 S	4.6	60	1.07	36.6	258	221	5 S	229	0.42	60	-0.3	-0.31	2.1
6 S	5.16	80	1.44	18.7	244	216	6 S	223	0.85	79.99	-0.6	-0.58	1.9
7 S	5.75	100	2.12	63	291	214	7 S	220	1.47	99.98	-1.1	-0.94	3.4
8 S	6.26	120	2.8	96.3	330	208	8 S	216	2.32	119.96	-1.9	-1.37	3.6
9 S	6.93	140	3.51	113	0.9	194	9 S	211	3.38	139.93	-2.9	-1.75	5.2
10 S	7.83	160	4.49	144	38.1	188	10 S	205	4.71	159.89	-4.3	-2	5.4
11 S	8.32	180	5.42	225	123	184	11 S	200	6.37	179.81	-6	-2.16	4.9
12 S	8.86	200	6.19	309	211	179	12 S	196	8.31	199.71	-8	-2.22	4.5
13 S	9.37	220	7.31	352	256	177	13 S	192	10.6	219.57	-10	-2.14	5.8
14 S	9.89	240	7.37	10.4	276	177	14 S	189	13.1	239.4	-13	-2	0.5
15 S	11.2	257	8.4	57.3	316	183	15 S	188	15.4	256.24	-15	-1.99	7.8

**Gyroscope Data Table for Well 299-E27-4**

Hole: C4125	Time	CablLength (feet)	Inclination (from Vert.)	TF Gyro	TFHighSide	CourseDir (0°..360°)	Rec.ID (17)	ClosureDir (0°..360°)	ClosureDist (feet)	TVD (+feet)	+N/-S (feet)	+E/-W (feet)	Dogleg ° / 100f
2 S	2.46	0	0.15	357	338	270	2 S	0	0	0	0	0	0
3 S	3.25	20	0.16	335	331	255	3 S	263	0.06	20	-0	-0.05	0.2
4 S	4.02	40	0.5	359	52	199	4 S	229	0.15	40	-0.1	-0.11	2.2
5 S	4.72	60	1	342	52	182	5 S	202	0.38	60	-0.4	-0.14	2.7
6 S	5.31	80	1.48	349	64	177	6 S	190	0.8	79.99	-0.8	-0.13	2.4
7 S	5.8	100	2.38	21.7	105	168	7 S	181	1.45	99.98	-1.5	-0.04	4.7
8 S	6.39	120	2.74	64	154	162	8 S	175	2.32	119.96	-2.3	0.19	2.3
9 S	6.98	140	4.47	127	215	165	9 S	171	3.56	139.92	-3.5	0.54	8.7
10 S	7.57	160	4.56	167	257	162	10 S	169	5.13	159.86	-5	0.99	1.3
11 S	8.11	180	6.37	219	310	161	11 S	167	7.02	179.77	-6.8	1.6	9.1
12 S	8.67	200	6.87	238	331	160	12 S	165	9.31	199.63	-9	2.38	2.7
13 S	9.13	220	7.8	247	345	154	13 S	163	11.8	219.47	-11	3.39	5.7
14 S	9.72	240	8.53	271	10	154	14 S	162	14.7	239.27	-14	4.64	3.7
15 S	10.3	260	9.17	284	26.9	150	15 S	160	17.7	259.03	-17	6.11	4.4
16 S	10.9	280	9.83	280	25.3	148	16 S	158	20.9	278.76	-19	7.82	3.6
17 S	12.7	297	10.1	274	18.3	149	17 S	157	23.9	295.5	-22	9.37	1.9

**Gyroscope Data Table for Well 299-E27-21**

Hole: C4127	Time	CabLength (feet)	Inclination (fromVert.)	TF Gyro	TFHighSide	CourseDir (0°.360°)	Rec.ID (17)	ClosureDir (0°.360°)	ClosureDist (feet)	TVD (+feet)	+N/-S (feet)	+E/-W (feet)	Dogleg °/ 100f
2 S	2.43	0	0.93	297	199	241	2 S	0	0	0	0	0	0
3 S	3.51	20	0.96	262	156	249	3 S	245	0.33	20	-0.1	-0.3	0.7
4 S	4.49	40	1.57	290	174	259	4 S	251	0.77	39.99	-0.3	-0.72	3.2
5 S	5.1	60	2.04	242	112	273	5 S	258	1.38	59.98	-0.3	-1.35	3.2
6 S	5.77	80	3.13	242	109	276	6 S	265	2.26	79.96	-0.2	-2.25	5.5
7 S	6.39	100	3.34	292	165	270	7 S	268	3.38	99.93	-0.2	-3.38	1.9
8 S	7.05	120	4.12	303	175	271	8 S	268	4.68	119.89	-0.1	-4.68	3.9
9 S	7.8	140	4.9	304	178	269	9 S	269	6.25	139.83	-0.1	-6.25	4
10 S	8.41	160	5.01	312	190	264	10 S	268	7.98	159.75	-0.3	-7.97	2.2
11 S	9.13	180	5.41	56.4	295	263	11 S	267	9.79	179.67	-0.5	-9.78	2
12 S	10.5	200	6.02	150	36	256	12 S	266	11.8	199.57	-0.8	-11.73	4.8
13 S	11.2	220	6.39	184	78.2	248	13 S	264	13.9	219.45	-1.5	-13.79	4.6
14 S	11.9	240	6.25	209	108	244	14 S	261	16	239.33	-2.4	-15.8	2.6
15 S	12.6	260	6.48	267	173	237	15 S	259	18.1	259.21	-3.5	-17.72	4.1
16 S	13.6	280	5.88	39.8	306	236	16 S	257	20.1	279.09	-4.7	-19.51	3
17 S	16.2	298	5.82	93.8	6.5	230	17 S	255	21.7	296.5	-5.8	-20.93	3.8



**Gyroscope Data Table for Well 299-E27-23**

Hole: C4190	Time	CabLength (feet)	Inclination (from Vert.)	TF Gyro	TFHighSide	CourseDir (0°..360°)	Rec.ID (17)	ClosureDir (0°..360°)	ClosureDist (feet)	TVD (+feet)	+N/-S (feet)	+E/-W (feet)	Dogleg °/ 100f
2 S	2.48	0	0.09	328	342	315	2 S	0	0	0	0	0	0
3 S	3.07	20	0.18	279	141	106	3 S	82.9	0.02	20	0	0.02	1.3
4 S	3.79	40	0.56	342	197	113	4 S	107	0.15	40	-0	0.14	1.9
5 S	4.49	60	1.85	18	248	97.5	5 S	103	0.57	59.99	-0.1	0.55	6.6
6 S	5.05	80	2.02	330	216	82.4	6 S	95.6	1.23	79.98	-0.1	1.22	2.7
7 S	5.69	100	2.36	25.1	285	68.4	7 S	87.7	1.96	99.97	0.08	1.96	3.2
8 S	6.21	120	2.28	62.8	338	52.6	8 S	79.9	2.7	119.95	0.47	2.66	3.2
9 S	6.69	140	1.11	115	52.4	30.8	9 S	74	3.19	139.94	0.88	3.07	6.6
10 S	7.23	160	0.06	190	90	68.2	10 S	71.7	3.35	159.94	1.05	3.18	5.3
11 S	7.77	180	0.68	251	90	129	11 S	73.4	3.42	179.94	0.98	3.28	3.3
12 S	8.34	200	1.75	338	171	135	12 S	79.1	3.65	199.94	0.69	3.59	5.4
13 S	8.82	220	2.64	136	345	120	13 S	86.7	4.21	219.92	0.24	4.2	5.3
14 S	9.36	240	2.87	189	62.4	94.8	14 S	90.3	5.1	239.9	-0	5.1	6.1
15 S	10.1	260	2.86	338	225	80.5	15 S	89.9	6.09	259.88	0.01	6.09	3.6
16 S	10.8	280	3.1	35.5	287	76.7	16 S	88.3	7.11	279.85	0.22	7.11	1.6
17 S	11.7	300	3.64	337	226	79.6	17 S	86.8	8.27	299.81	0.46	8.26	2.8
18 S	13.4	301	3.49	199	85.9	81.2	18 S	86.8	8.3	300.31	0.46	8.29	35.2

## **Appendix D**

### **Slug Test Characterization Results for Well 299-E27-22 (C4124)**

## Appendix D

### Slug Test Characterization Results for Well 299-E27-22 (C4124)



Project No. E43944

Date September 30, 2003  
To J.V. Borghese  
From F.A. Spane  
Subject Slug Test Characterization Results for Multi-  
Test/Depth Intervals Conducted During the  
Drilling of WMA-C Well 299-E27-22

Internal Distribution

F.J. Anderson  
M. Connelly  
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The following letter report presents test descriptions and analysis results for multi-stress slug tests that were performed at four specific test/depth intervals within well 299-E27-22. The well is located within Waste Management Area SST C (WMA-C). The tests were performed at four, selected test/depth intervals, as the borehole was advanced to its final depth to the top of basalt at 81.7 m below ground surface (bgs). The primary objective of the hydrologic tests was to provide information pertaining to the variability and vertical distribution of hydraulic conductivity with depth within this region of the WMA-C facility. This type of characterization information is important for predicting/simulating contaminant migration (i.e., numerical flow/transport modeling) and designing proper monitor well strategies for WMA locations. A secondary objective of the program was to evaluate whether acceptable test results could be obtained via the "drill-and-test" method, using the Becker, dual-wall casing, air-percussion, hammer drilling method within anticipated highly permeable test formation conditions. With this respect, a number of slug testing methods and equipment deployments were evaluated for maximizing the quality of the test results obtained. Based on the results of this initial test evaluation, recommendations are also provided in this letter report for improving future, vertical characterization efforts employing the "drill-and-test" technique.

Discrete depth/interval groundwater samples were also obtained periodically during drilling (from cutting slurry returns) for the purpose of qualitatively determining the hydrochemical characteristics and vertical distribution of contaminants at this site. Results from the hydrochemical sampling are not presented in this letter report.

#### 1. Executive Summary

Overall, the test results indicate that slug testing can be utilized rapidly and efficiently with a dual-wall, drill casing system to provide high-quality, vertically distributed hydraulic property characterization information. Slug test characterization of four test/depth intervals (Table 1) within the Hanford formation were attempted during the drilling of well 299-E27-22, to final depth to the top of basalt (81.7 m bgs). Three of the four test/depth intervals ranging in thickness from 0.3 to 1.1 m, were successfully characterized using the slug test method, providing hydraulic conductivity

estimates for these discrete Hanford formation test zones ranging from 0.04 to  $6.9E3$  m/day. The estimated hydraulic conductivity values obtained for the higher permeability test zones are well within the permeability range of  $1.0E3$  to  $5.0E5$  m/day assigned to the Hanford formation in this general area, based on site-wide groundwater flow, inverse calibration modeling (e.g., Wurstner et al. 1995)). Generally such highly permeable formations cannot be characterized using short-duration constant-rate pumping tests. The use of designed slug test characterization programs, where the test interval length ( $L$ ) and well casing radius ( $r_c$ ) can be manipulated offers significant promise for the characterization of highly permeable test formations. When combined with drill-and-test borehole programs, the opportunity of determining the vertical distribution of hydraulic conductivity can also be realized.

## **2. General Hydrologic Test Plan Description**

The original hydrologic test plan, as presented in Spane (2003), identified six test/depth intervals that would be characterized at approximate depths below the water table of: 3, 4.5, 6, 12, 18, and 24 m. Testing would commence when the approximate target depth intervals were reached during drilling, and the drilling casing string was retracted exposing an approximate 1.5-m open borehole section. Minor test interval development was identified in the plan to be performed prior to testing for the purpose of removing drilling produced suspended materials from the borehole fluid-column to minimize the effects of borehole/test interval plugging during testing. The interval development was to be completed using either bailing, air-lifting or portable submersible pump methods.

After the borehole development activities were completed, the drilling casing string would be retracted  $\sim 1.5$  m, and the borehole depth measured. The purpose of the borehole depth measurement was to assess the amount of borehole collapse and to determine the open borehole test interval. A series of multi-stress slug tests would then be performed on the open test interval section. The reason for utilizing a multi-stress slug test approach is to determine whether the slug test response exhibits either variable or stress-level dependence. As noted in Butler (1998) and Spane et al. (2003a), tests exhibiting either variable or stress-level dependence can provide valuable information pertaining to presence of dynamic well skin or non-linear (i.e., turbulence) test response conditions occurring within the test section. Anticipated slug test stress levels applied during testing were expected to be within the range of  $\sim 0.3$  to  $0.5$  m for low-stress tests and  $\sim 1$  m for high-stress tests. The slug tests were to be initiated pneumatically using compressed gas to depress the fluid-column levels to the designed test stress levels. Actual stress levels applied for each test were to be determined by comparing pressure transducer readings below and above the borehole fluid column surface. After the monitored fluid column had stabilized for several minutes at the prescribed stress level, the slug test (slug withdrawal test) would be initiated by suddenly releasing the compressed gas used to depress the borehole fluid-column level. The compressed gas would be released from the borehole column by opening valves (e.g., ball valves) mounted on the surface wellhead used to seal the casing system. As noted in Spane et al. (1996), the gas release valves should have a cross-sectional area that is greater (e.g.  $>1.5$  times) than the cross-sectional area of the test system where fluid level surface is recovering during testing.

As a minimum, two low- and two high-stress tests were recommended to be conducted for each

test/depth interval. Individual slug tests should be fully recovered prior to depressing the fluid column for preparation of the next slug test within the characterization sequence. A wide-range in recovery times were expected based on anticipated range in permeability conditions. For example Spane (2003) predicted recovery times as rapid as <10 secs for high permeability test intervals to >5 min for lower permeability test sections. After slug testing activities were completed, the borehole depth would be re-measured for the purpose of determining any changes to the open borehole interval that may have occurred during testing.

A number of changes to the original test plan had to be made due to unforeseen test/site conditions. These included:

- a shallower depth to the top of basalt
- high instability of the open borehole test intervals
- changes to the general test system utilized

The top of basalt was encountered at a shallower depth than originally anticipated, which reduced the total number of intervals tested from the planned six to an actual four. The high instability of the test formation (i.e., Hanford formation) also caused several changes in the planned testing design. The exposed open borehole test interval produced by retracting the dual-wall casing system was reduced from 1.5 m to ~0.6 m and planned borehole development activities prior to testing were eliminated. The most significant departure from the planned testing design, however, pertains to changes in the downhole test system employed. These changes are discussed in the following report section.

### **3. Hydrologic Test System Description**

Figure 1 shows the general test system configuration that was originally designed to be employed during slug testing. Salient features of the test system configuration are the: dual-wall drilling casing string, a central packer within the inner-casing string, and a surface-seal well-head installation.

The dual-wall, drilling casing string is the system used for borehole advancement during the drilling process. The dimensions of the casing string are reported as:

- Inner Casing: 0.1524-m I.D.; 0.1588-m. O.D.
- Outer Casing: 0.2032-m I.D.; 0.2286-m O.D.

As shown in the figure, an inflatable packer was to be used to isolate/seal the inner casing string from the annular zone between the two casings, where slug test response was originally planned to be initiated and to take place. A 1.5 m well-screen section (not shown in the figure) was also designed to be attached below the packer to maintain an open section for testing after retracting the dual-wall casing. A strain-gauge, 0 to 345 kPa (0 to 35 m) pressure transducer was to be mounted above the packer, with a pressure sensor by-pass tube that connected to the pressure transducer to the test zone below the packer.



These casing dimensions indicate a composite cross-sectional area for the annular space between the two casing strings (which is the location where the slug test responses was design originally to occur) of  $0.013 \text{ m}^2$ . This calculated cross-sectional area is equivalent to a 0.127-m representative test well casing diameter.

As noted in Section 2, the slug tests were originally designed to be conducted pneumatically, using compressed air to depress fluid levels within the borehole as part of initiating the test. The performance of pneumatic slug tests requires that a surface wellhead (not identified in Figure 1) be utilized to isolate/seal the annular cross-sectional area between the two casing strings. This wellhead isolation of the two casing strings allows containment of the administered compressed gas that will be used to pneumatically depress the annular fluid column to the designed slug test stress levels discussed in Section 2. Salient features of the well-head assembly include:

- an annular surface seal between the dual casing string
- a sealed through-pass connection allowing for passage of pressure transducer and cable to be used to measure pressure response below the inner-casing packer
- an outside pressure probe connection that allows direct measurement of the gas pressure within the annular area below the surface seal
- a gas line connection to allow compressed air to be introduced directly to the annular zone
- surface valves for the rapid/immediate release of the compressed air within the annular zone, which allows for the *immediate* initiation of slug test application.

The preceding discussion describes the test system as originally designed for use during drilling of the well. At a field-site meeting to examine assembled equipment to be utilized during testing approximately 1-week prior to the commencement of well drilling activities at the site, however, it was discovered that a significant flow restriction existed within the percussion bit assembly (i.e.,  $\sim 1/10$  the calculated cross-sectional annular zone area;  $0.0013 \text{ m}^2$  vs.  $0.013 \text{ m}^2$ ). It was decided that the test system as originally designed would be utilized on the first test/depth interval (Zone 1; Table 1), and if the system proved to be not completely successful, modifications to the test system would be made for subsequent test/depth intervals. In addition (as noted in Section 2), a number of unforeseen test/site conditions (e.g., borehole instability) were encountered during slug test characterization activities that were attempted for the first test/depth interval. Results obtained during the testing of Zone 1 and initial testing phases of Zone 2 indicated that the flow-restriction area within the bit was being clogged by infilling/collapsing borehole material, which significantly reduced the hydraulic communication between the casing annular zone and the underlying, effected test depth interval (produced by the retracted dual-wall drill casing). As a result, a number of test equipment and test performance modifications were examined during slug testing of the second

test/depth interval (Zone 2; Section 5.2). Based on these test results, the test equipment and test procedures for slug testing were modified for characterizing subsequent test/depth intervals. The modifications included:

- removal of the surface wellhead seal that isolated the inner casing area from the annular zone between the dual-wall casing string
- removal of the packer/screen assembly from the inner casing during testing
- slug tests were conducted both pneumatically and with slugging rods

The removal of the surface wellhead seal was needed to change the primary test response location from the dual-wall casing outer annular zone, to the area monitored by the inside casing string (i.e., I.D. = 0.1524 m). This modification required test stresses to be applied directly to the inner casing string. This change in test response area was necessitated due to results obtained during testing of Zones 1 and 2 that indicated that the annular zone (the zone of active testing) was not in communication with the underlying test/depth interval that was created by retracting the dual-wall casing string. As previously discussed, the lack of communication between the casing outer annular zone and the underlying test/depth interval appears to have been the result of borehole instability and the clogging of the small entry port openings in the percussion bit assembly that provide fluid access at the base of the dual-wall casing, annular zone.

To produce analyzable slug test response data within the inner casing string area, the smaller I.D. working string used to deploy the packer/well screen assembly (Figure 1) could not be used. This allowed test responses to be monitored within the larger inner casing string, which is important for characterizing high-permeability test formations. Not using a packer/well-screen system, however, increases the uncertainty of the actual depth interval tested, due to borehole collapse/instability.

Slug testing for Zones 2 through 4 were conducted both pneumatically and using a slugging rod (0.0762 m O.D.), which theoretically produces a maximum initial displacement stress of 0.51 m within the 0.1524 m I.D. inner casing. Using both test methods provides a means of comparing results obtained for tests, where the initial test stress was applied solely within the inner casing (i.e., using the slugging rod) and when the inner casing and outer annular zone were stressed concurrently (i.e., during pneumatic tests).

#### **4. Slug Test Response Predictions/Analysis**

As shown in Figure 2 and discussed in Butler (1998) and Spane et al. (2003b), water levels within a stress well can respond in one of three ways to the instantaneously applied stress of a slug test. These response model patterns are: 1) an over-damped response, where the water levels recovers in an exponentially decreasing recovery pattern; 2) an underdamped response, where the slug test response oscillates above and below the initial static, with decreasing peak amplitudes with time; and 3) critically damped, where the slug test behavior exhibits characteristics that are transitional to the

over- and under-damped response patterns. Factors that control the type of slug test response model that will be expressed within a well include a number of aquifer properties (hydraulic conductivity) and well dimension characteristics (well-screen length, well-casing radius, well-radius, aquifer thickness, fluid-column length) and can be expressed by the response damping parameter,  $C_D$ , which Butler (1998) reports for unconfined aquifer tests as:

$$C_D = (g/L_e)^{1/2} r_c^2 \ln(R_e/r_w)/(2 K L) \quad (1)$$

where  $g$  = acceleration due to gravity

$L_e$  = effective well water-column length

$r_c$  = well casing radius; i.e., radius of well water-column that is active during testing

$R_e$  = effective test radius parameter; as defined by Bouwer and Rice (1976)

$r_w$  = well radius

$K$  = hydraulic conductivity of test interval

$L$  = well-screen length.

Given the multitude of possible combinations of aquifer properties, well casing dimensions, and test interval lengths, no universal  $C_D$  value ranges can be provided that describe slug test response conditions. However, for various combinations anticipated for testing at well 299-E27-22 during drilling the following general guidelines on slug test response prediction are provided:

- $C_D > 2$  = over-damped response
- $C_D 1 - 2$  = critically-damped response
- $C_D < 1$  = under-damped response

Over-damped test response generally occurs within stress wells monitoring test formations of low to moderately high hydraulic conductivity (e.g., Ringold Formation), and are indicative of test conditions where frictional forces (i.e., resistance of groundwater flow from the test interval to the well) are predominant over test system inertial forces.

Under-damped test response patterns are exhibited within stress wells where inertial forces are predominant over formation frictional forces. This commonly occurs in wells with extremely long well fluid columns (i.e., large water mass within the well column) and/or that penetrate highly permeable aquifers (e.g., Hanford formation). Tests exhibiting under-damped behavior should be conducted with very small stress level applications. If too high of a stress is applied, the slug test response will commonly exhibit oscillatory behavior superimposed on an over- or critically damped recovery response. Methods are currently not available for the analysis of slug tests exhibiting this type of composite slug test response. For test sites exhibiting composite oscillatory behavior, the

tests should be re-run at lower stress levels to allow analysis and quantitative hydraulic property determination using the appropriate, individual, analysis model method (under-, over-, or critically damped).

As mentioned previously, critically damped test responses are indicated by stress well water-level responses that are transitional to the over- and under-damped test conditions, as shown in Figure 2. They typically occur in wells that monitor test formations exhibiting high hydraulic conductivity. As noted in Butler (1998), distinguishing between over- and critically damped slug test response may be difficult in some cases (i.e., due to test signal noise) when examined on arithmetic plots. Proper model identification may be enhanced when semi-log plots are utilized, i.e., log head versus time. Critically damped slug tests exhibit a diagnostic concave-downward pattern when plotted in semi-log plot format. This is in contrast to over-damped response behavior, which displays either a linear or concave upward pattern.

High permeability test sites exhibiting over-damped or composite model response behavior are particularly limiting in the ability to define formations exhibiting higher hydraulic property values. Figure 3 shows predicted slug test responses for hydraulic conductivities ranging between 1 and 100 m/d, for a 1.5 m test interval. It should be noted that the test predictions shown in this section are based on responses occurring within the dual-wall annular zone (i.e., cross-sectional area =  $0.013 \text{ m}^2$ ). These results would be similar, however, for test responses occurring within the inner casing (I.D. = 0.1524 m), due to its similar cross-sectional area of  $0.018 \text{ m}^2$ . As shown in Figure 3, test intervals having hydraulic conductivity values of approximately 100 m/d or less, should be readily resolved for tests exhibiting over-damped slug test behavior. Under ideal test conditions (i.e., for test not exhibiting complicating early-time transient effects), this permeability characterization limit may be extended up to ~150 m/d.

Because the annular zone cross-sectional area between the dual casing string (i.e., where the test response will occur) is relatively large ( $0.013 \text{ m}^2$ ), under-damped (oscillatory) test responses will not occur except under high hydraulic conductivity conditions. Since this type of test response is dependent on the fluid-column length (i.e., the inertial/mass effect), it is not possible to develop test prediction plots that are universally applicable for all test interval depths. Based on preliminary scoping calculations (not shown), however, under-damped slug test responses are likely to be exhibited during testing only when test interval permeabilities exceed 500 to 1,000 m/d (based on the test interval depth).

Methods that can be employed for analyzing unconfined aquifer tests exhibiting high permeability under-, over- or critically damped characteristics include techniques described in Springer and Gelhar (1991), Butler (1998), McElwee and Zenner (1998), Butler and Garnett (2000), Zurbuchen et al. (2002), and Butler et al. (2003). Because of the ease provided by a spreadsheet-based approach, the test analysis method presented in Butler and Garnett (2000) was used for the analysis of all tests, which exhibited high permeability/oscillatory response characteristics. For tests exhibiting intermediate to low permeability response characteristics, the unconfined aquifer analysis methods discussed in Butler (1998) can be employed. A summary and examples of their use under Hanford Site conditions is provided in Spane et al. (2003a).

## **5. Slug Test Results**

The following discussion presents pertinent information describing slug testing activities and analysis results for the four test/depth intervals that were hydrologically characterized, as the borehole was advanced to its final depth to the top of basalt (i.e., 81.7 m bgs). Table 1 summarizes selected test information for the four test/depth intervals.

### **5.1 Zone 1**

At ~0900 hours Pacific Daylight Time (PDT) on September 3, 2003, after reaching a depth of 73.9 m bgs, the dual-wall drill casing was pulled-back (retracted) 0.9 m, producing a theoretical test/depth interval for Zone 1 of 73.0 to 73.9 m bgs. The packer was set at a depth of 72.2 m bgs inside the inner casing string, with the bottom of the attached well-screen assembly set at a depth of 73.8 m bgs. Four pneumatic slug tests (Tests #1 - #4) were conducted between 1200 and 1255 hours, by pressurizing the dual-wall drill casing annular zone using applied stress pressures ranging between 0.50 and 1.0 m for individual tests. No downhole test responses were observed during the application or upon release of the applied compressed gas used to initiate the pneumatic slug tests. Infilling of sand within the packer/well screen assembly and clogging of the restricted entry ports within the percussion air-hammer bit (located at the base of the dual-wall drill casing annular zone) were suspected to have contributed to the unsuccessful hydraulic characterization of this test/depth interval. Although the test characterization results obtained for Zone 1 proved to be unsuccessful, it was decided that the same test system setup and procedure would be used initially for characterizing the next test/depth interval (Zone 2).

### **5.2 Zone 2**

After reaching a depth of 76.2 m bgs at 0800 hours PDT on September 4, 2003, the dual-wall casing was retracted 0.6 m, producing a theoretical test/depth interval for Zone 2 of 75.6 to 76.2 m bgs. The packer was set at a depth of approximately 76.2 m bgs inside the inner casing string, with the bottom of the attached well-screen assembly set at a depth of 73.8 m bgs. Five pneumatic slug tests (Tests #5 - #9) were conducted between 0819 and 0942 hours, by pressurizing the dual-wall drill casing annular zone using applied stress pressures ranging between 0.27 and 1.7 m for individual tests. This was the same test procedure as utilized during testing Zone 1. As was exhibited during testing of Zone 1, no downhole test responses were observed during the application or upon release of the applied compressed gas used to initiate the pneumatic slug tests. This lack of annular zone test response was again attributed to infilling of sand within the packer/well screen assembly and clogging of the restricted entry ports within the percussion air-hammer bit (located at the base of the dual-wall drill casing annular zone). These combined factors were suspected to have contributed to the unsuccessful hydraulic characterization using this test system design.

Based on the unsuccessful test characterization results obtained previously for Zone 1 (tests #1 - #4) and the initial characterization results for Zone 2 (tests #5 - #9), the test equipment and testing procedure were modified for subsequent hydraulic characterization efforts (Note: these



modifications are discussed in Section 3). To initiate characterization of Zone 2 using the modified test system/procedures, the packer/well-screen assembly was removed from the inner casing at 0950 hours PDT, and the borehole re-advanced to a depth of 75.9 m bgs and the dual-wall casing retracted 0.8 m, producing a theoretical test/depth interval of 75.1 to 75.9 m bgs for subsequent characterization testing of Zone 2. Two standard slug withdrawal tests (Tests #10 - #11) were conducted between 1053 and 1059 hours, PDT by rapidly removing a previously submerged slugging rod (0.0762 m O.D.), which theoretically produced a maximum initial displacement stress of 0.51 m within the 0.1524 m I.D. inner casing. Well responses within the inner casing were monitored with a pressure transducer system, which was suspended (in the inner casing) approximately 3.3 m below the static water level. Both slug withdrawal tests produced identical oscillatory test responses, with oscillation periods of approximately 5 secs. Oscillatory test response recovered to static conditions after approximately 40 secs after slug withdrawal initiation.

Figure 4 shows the oscillatory response for test #10 and associated analysis solution match using the high permeability underdamped method as described in Butler and Garnett (2000) and Butler et al. (2003). As shown, a good solution match was obtained using a response dampening parameter,  $C_D$ , value of 0.2. Test analysis results for tests #10 and #11 produced nearly identical analysis parameter results, with hydraulic conductivity estimate values ranging between 1.9E3 and 2.1E3 m/day, for the two tests. It should be noted that the test interval length utilized in the analysis was based on a test interval of 1.1 m, which is reflective of the total depth *disturbed* by drilling and the open interval exposed by the retracted dual-wall casing.

After slug withdrawal test #11 was conducted using a slugging rod, modified pneumatic tests (tests #12 and #13) were attempted by resetting the packer/well-screen assembly (bottom set at 75.9 m bgs) back within the inner casing. The pneumatic slug tests were conducted for these tests by pressurizing the small-diameter (I.D. = 0.0254 m) working string used to set the packer, with pressure response monitored immediately below the packer within the test interval section. Tests #12 and #13 were conducted between 1223 and 1233 hours, using applied stress pressures ranging between 1.4 and 2.3 m for individual tests, and then rapidly releasing the introduced compressed air within the small-diameter working string. These pneumatic slug tests were not successful for several technical reasons. First, oscillatory test response characteristics are directly related to the square of the casing radius,  $r_c$ , where the oscillatory response takes place as noted in Butler and Garnett (2000). Reducing the casing diameter from 0.1524 m where oscillatory response characteristics were displayed during tests #10 and #11, to 0.0254 m during tests #12 and #13 causes the oscillatory behavior to be theoretically compressed (by a factor of 36!) producing turbulent, non-analyzable responses. Secondly, as noted in Butler et al., (2003) for high-permeability, under-damped tests, the test response should be monitored in proximity to the oscillating surface. For these tests, the pressure response should have been monitored within the 0.0254 tubing, which was not possible due to the O.D. size constraints of the pressure transducers available for this test borehole characterization.

Following completion of test #13, another slug test method was evaluated for possible further characterization use. For test #14, ~19 liters of water were added to the annular zone between the inner casing (0.1524 m) and the 0.0254 m packer working string. To initiate the test, the packer was deflated with the objective of rapidly producing a slug injection oscillatory test response within this inner annular zone, which would be produced by the column of added water above the packer. This

test proved to be unsuccessful, due to the slow and gradual deflation characteristics exhibited by the packer (i.e., > 30 seconds). Because of the response information observed for these tests, pneumatic slug tests using the small-diameter packer working string (e.g., tests #12 and #13) and slug injection tests using packer deflation were not utilized further in characterizing subsequent test/depth intervals.

### 5.3 Zone 3

After reaching a depth of 77.4 m bgs at 1440 hours PDT on September 4, 2003, the dual-wall casing was retracted 0.6 m, producing a theoretical test/depth interval for Zone 3 of 76.8 to 77.4 m bgs. No inner casing packer/well-screen assembly was utilized for test characterization of Zone 3. A series of four slug tests (Tests #15 - #18) were conducted between 1530 and 1620 hours, PDT by either rapidly removing a previously submerged slugging rod (i.e., slug withdrawal test), or rapidly submerging the slugging rod (i.e., slug injection test). The test responses within the inner casing were monitored with a pressure transducer system, which was suspended (in the inner casing) approximately 3.3 m below the static water level. In all cases, the slug tests exhibited slow over-damped recovery response behavior. Since the recovery times for these tests were extremely slow, consecutive slug injection/withdrawal tests were combined and analyzed compositely using a test history match approach. This approach is particularly useful when analysis of individual tests may be uncertain (i.e., due to only small recovery %), and relies on superimposing the predicted test responses of subsequent tests responses, which can be used to match the entire composite test sequence (test history match).

Figure 5 shows the observed well response for the two slug injection tests and two slug withdrawal tests using the 0.0762 m O.D. slugging rod. Also shown in the figure, is the predicted test history match for the four tests, which was produced by superimposing the four individual slug tests at their appropriate time of test initiation. An increasing water-level trend of +0.0008 m/min was observed over the test period and included in the test history match. As indicated, a hydraulic conductivity,  $K$ , of 0.04 m/day provides a good match to the observed test response sequence. To demonstrate the sensitivity of the analytical solution, Figure 6 shows the predicted history match using  $K$  values of 0.04, 0.4 and 4 m/day. As indicated, significant departures in the test history matches of the observed test responses are produced with higher  $K$  values. This suggests that the interval tested exhibits a  $K$  value of  $\leq 0.04$  m/day. It is not completely certain whether the relatively low hydraulic conductivity indicated for Zone 3 is actually representative of in-situ formation conditions or an artifact of the drilling process or borehole instability. Depth measurements made prior to and after completion of the slug testing sequence, however, indicated that the 0.6 m test/depth interval remained opened during characterization testing.

A series of three pneumatic slug withdrawal tests (tests #19 - #21) were also conducted between 0722 and 0750 hours, PDT on September 5, 2003. The pneumatic slug tests were conducted by pressurizing the inner-casing (I.D. = 0.1524 m) and the outside annular zone (at the same time) between the dual-wall casing. Both casing areas were pressurized to minimize any non-formational test system effects caused by the outer annular zone being hydraulically connected to the underlying test/depth interval. All pneumatic tests used applied stress (compressed gas) pressures ranging between 0.9 and 1.0 m for individual tests, which was then rapidly released using the wellhead

surface release valves. The pneumatic slug test responses were examined compositely like the slugging rod tests #15 - #18. These tests produced very similar results (i.e., in comparison to the composite slugging rod tests), but are not included in the final test analysis results for this test zone, due to pressure variability exhibited during the pressurization phase.

#### 5.4 Zone 4

After reaching the top of basalt at a depth of 81.7 m bgs at 0915 hours PDT on September 5, 2003, the dual-wall casing was retracted 0.3 m, producing a theoretical test/depth interval for Zone 4 of 81.4 to 81.7 m bgs. As for the proceeding testing for Zone 3, no inner casing packer/well-screen assembly was utilized for test characterization of Zone 4. Two slug tests were conducted between 1007 and 1015 hours, PDT by rapidly submerging (slug injection test #22) and removing the previously submerged slugging rod (slug withdrawal test #23), which theoretically produces a maximum initial displacement stress of 0.51 m within the 0.1524 m I.D. inner casing. Well responses within the inner casing were monitored with a pressure transducer system, which was suspended (in the inner casing) approximately 3.3 m below the static water level. Both slug withdrawal tests produced identical oscillatory test responses, with oscillation periods of approximately 7 secs. Oscillatory test response recovered to static conditions after approximately 70 secs after slug test initiation.

Figure 7 shows the oscillatory response for slug withdrawal test #23 and pertinent analysis solution match using the high permeability underdamped method as described in Butler and Garnett (2000) and Butler et al. (2003). As shown, a good solution match was obtained using a response dampening parameter,  $C_D$ , value of 0.175. Similar test analysis results were obtained for slug injection test #22 (not shown), with hydraulic conductivity estimate values ranging between 6.0E3 and 6.9E3 m/day, for the two tests. It should be noted that the test interval length utilized in the analysis was based on a test interval of 0.3 m, which is reflective of the open interval exposed by the retracted dual-wall casing.

After completion of slug withdrawal test #23, two pneumatic slug withdrawal tests (tests #24 and #25) were conducted between 1033 and 1107 hours, PDT on September 5, 2003. The pneumatic slug tests were conducted by pressurizing the inner-casing diameter (I.D. = 0.1524 m) and the outside annular zone (at the same time) between the dual-wall casing. Both casing areas were pressurized to minimize any non-formational test system effects caused by the annular zone being hydraulically connected to the underlying test/depth interval. The pneumatic tests used applied stress (compressed gas) pressures ranging between 0.4 and 0.8 m for the individual tests, which was then rapidly released using the wellhead surface release valves. The pneumatic slug tests (#24 and #25) exhibited similar test results, as were obtained for the slugging-rod slug tests (#22 and #23). Figure 8 shows the oscillatory response for slug withdrawal test #24, and the associated analysis solution match using the high permeability underdamped method as described in Butler and Garnett (2000) and Butler et al. (2003). As shown, a good solution match was obtained using a response dampening parameter,  $C_D$ , value of 0.175. Identical test analysis results were obtained for slug withdrawal test #25 (not shown), with a hydraulic conductivity estimate value of 6.0E3 m/day, derived from the two tests.

## 6. Conclusions

Overall, general test results indicated that slug testing can be utilized rapidly and efficiently with a dual-wall, drill casing system to provide high-quality, vertically distributed hydraulic property characterization information. Results from discrete test/depth interval slug test characterization of the Hanford formation during construction of well 299-E27-22 indicate a wide range in hydraulic conductivity (Table 1), with estimates ranging from 0.04 to 6.9E3 m/day. These hydraulic conductivity estimates were derived for open borehole, test/depth thickness sections ranging from 0.3 to 0.9 m in length, which were calculated based primarily on the length to test formation exposed by retracting the dual-wall drilling casing upon reaching pre-designated drilling depths. Borehole instability and the test interval deformation, however, may significantly decrease or increase the test zone thickness characterized by the slug test methods employed. Because of the dependence of hydraulic conductivity on *actual* test interval length, a  $\pm 50\%$  uncertainty is arbitrarily assigned to the hydraulic conductivity estimates derived from the slug test characterizations. This relatively high uncertainty is a function not only of the unstable, open borehole conditions, but also the relatively small test interval lengths utilized during characterization (i.e., test intervals  $\leq 1$  m).

The high hydraulic conductivity values determined for test zones exhibiting oscillatory, under-damped slug test behavior (i.e., Zone 2 and Zone 4), demonstrate the ability of the slug testing method to characterize highly permeable test formations, such as the Hanford formation. The estimated hydraulic conductivity values (i.e., 1.9E3 to 6.9E3 m/day) obtained for these high permeability test zones are well within the permeability range of 1.0E3 to 5.0E5 m/day assigned to the Hanford formation in this general area, based on site-wide groundwater flow, inverse calibration modeling (e.g., Figure 9). Generally such highly permeable formations cannot be characterized using short-duration ( $< 8$  hours) constant-rate pumping tests within standard monitoring well facilities. This is primarily due to the extremely small drawdown produced ( $< 0.1$  m), which can be attributed to limitations in pumping capacity (i.e., within 0.1016 m I.D. casing  $\sim 100$  L/min) and long saturated well-screen lengths (e.g., 10 m). As discussed in Spane et al. (2003b), the use of designed slug test characterization programs, however, where the test interval length ( $L$ ) and well casing radius ( $r_c$ ) can be manipulated offers significant promise for the characterization of highly permeable test formations. When combined with drill-and-test borehole programs, the opportunity of determining the vertical distribution of hydraulic conductivity can also be realized.

Because of the developmental nature of using slug test characterization methods with the Becker, dual-wall casing, air-percussion, hammer drilling method during the construction of well 299-E27-22, a number of conclusions were derived that relate to the performance evaluation of various slug test strategies and equipment systems. These conclusions are included in the following recommendations section that focuses on improving the drill-and-test slug test characterization method, when coupled with a dual-wall, drill casing percussion system.

## **7. Recommendations**

Based on experience derived from evaluating the slug test characterization results obtained during the construction of well 299-E2-22, a number of slug testing strategy and equipment system design recommendations are provided for the improving the performance of drill-and-test characterization programs.

1. Slug test responses should be initiated and monitored within the inner casing string and not the outer annular zone within the dual-wall drill casing system. This is attributed primarily to the flow entry restriction that occurs within the drill bit that is connected directly to the base of annular zone. To eliminate any complicating effects during testing, the annular zone should be isolated from the inner casing area using a wellhead seal (i.e., when using pneumatic slug tests).
2. Slug tests initiated pneumatically using compressed air and physically using slugging rods, both produced high quality characterization information in high-permeability formations. Pneumatic slug tests provide greater flexibility in controlling slug test response over fixed-volume/stress tests produced by slugging rods.
3. To exercise more control on the test/depth interval section during testing (i.e., open borehole instability concerns), a retrievable packer/well screen should be utilized within the inner casing string, as was utilized during the testing of Zones 1 and 2. Pressure transducers used in monitoring of the imposed slug stress applications should be located a short distance below (i.e., within 3 meters) the fluid-column surface within the casing that the slug test response takes place, and not in the test zone below the inflatable packer setting.
4. A variety of working string casing diameters (that are used to set the packer/well-screen assembly) should be available to control/manipulate slug test response for characterizing the full range of expected permeability conditions (e.g., small diameter casing for low permeability test zones; large diameters for high permeability intervals).
5. While acceptable test results were obtained for most test/depth intervals using the drilling rig compressor to initiate pneumatic slug tests, greater stability and control can be realized for these tests using compressed air cylinders and a high precision laboratory regulator system.
6. A real-time test software program should be utilized in the field in concert with the data acquisition system so that test responses can be more rapidly evaluated. This will improve the efficiency of running the test characterization program in the field.



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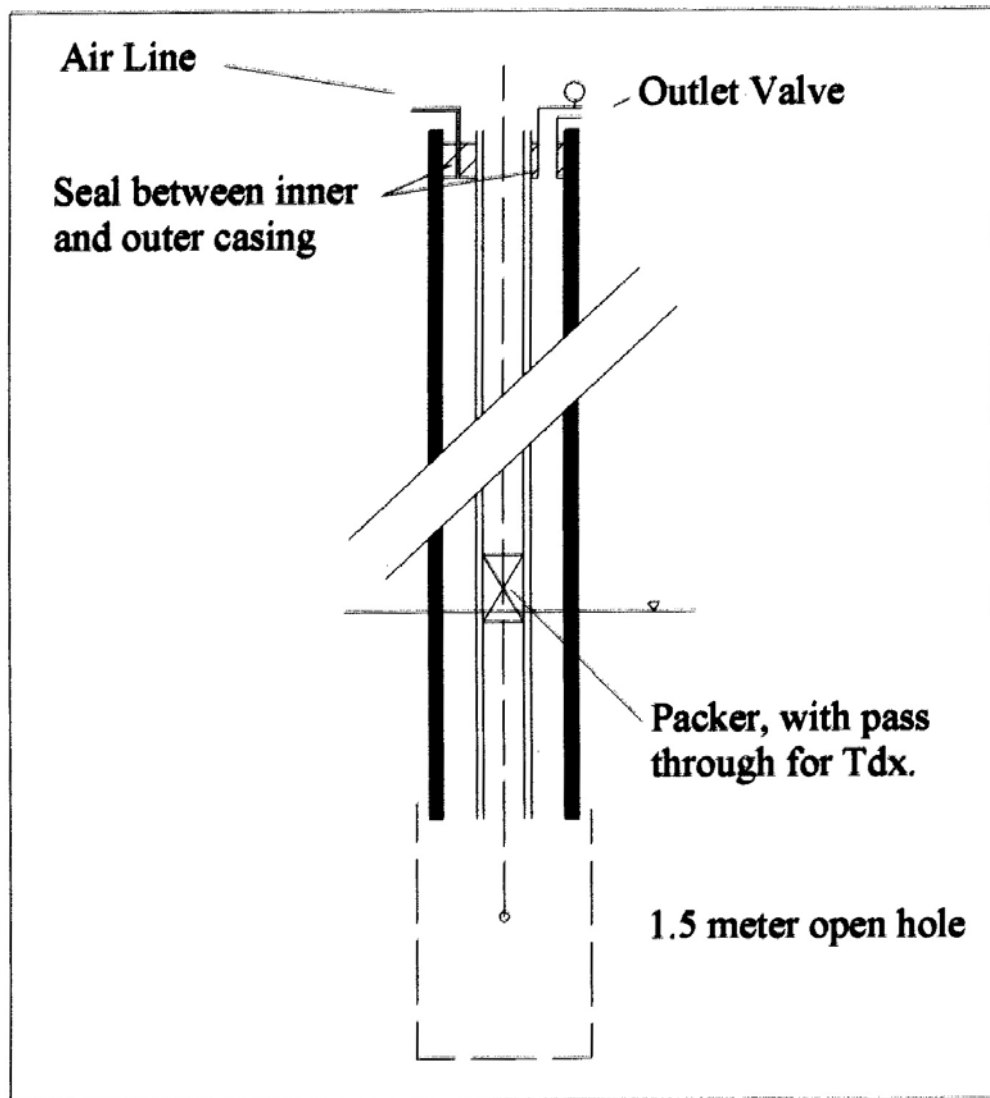
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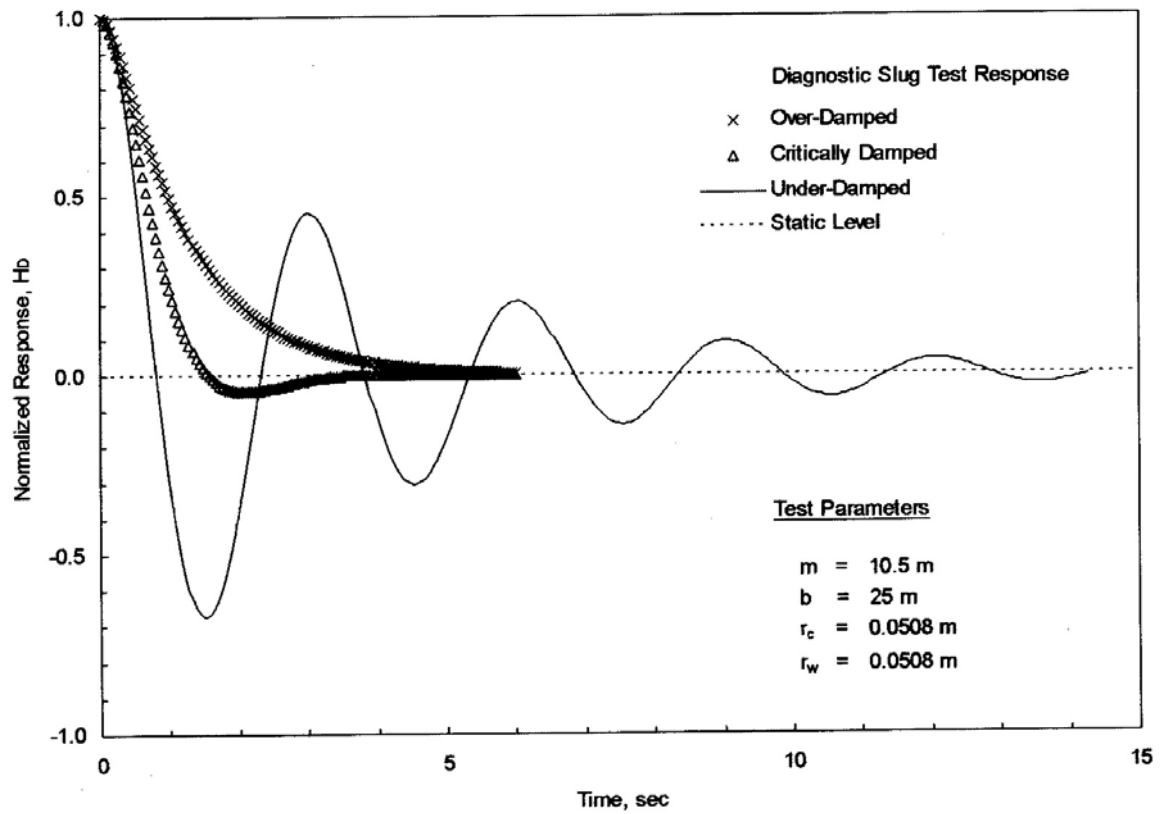
**Table 1.** Slug-Test Results for Selected Test/Depth Intervals at Well 299-E27-22.

Test Zone	Test Parameters				Slug Test Response Model	Horizontal Hydraulic Conductivity, $K_h^{(b)}$ m/d	
	Test Date	Slug Test #	Depth to Water, m bgs	Depth/Test Interval, m bgs		High-K (Oscillatory) Analysis Method <sup>(c)</sup>	Test History Matching/ Type-Curve Analysis Method <sup>(d)</sup>
Zone 1	9/3/03	1 - 4	~70.4	73.0 - 73.9 (0.9)	(a)	(a)	(a)
Zone 2	9/4/03	5 - 9	70.2	75.6 - 76.2 (0.6)	(a)	(a)	(a)
		10 - 11		75.1 - 75.9 (0.8)	Oscillatory (under-damped)	1.9E3 - 2.1E3	NA
		12 - 14			(a)	(a)	(a)
Zone 3	9/4 - 5/03	15 - 21	70.7 (70.3)*	76.8 - 77.4 (0.6)	Exponential decay (over-damped)	NA	0.04
Zone 4	9/5/03	22 - 25	70.1	81.4 - 81.7 (0.3)	Oscillatory (under-damped)	6.0E3 - 6.9E3	NA
NA: Not applicable * Depth to water measurement made on September 5, 2003 prior to initiating of pneumatic slug tests (#19 - #21). (a) No successful tests were completed (b) Assumed to be uniform within the well-screen test section. (c) Oscillatory, High-K analysis method as presented in Butler and Garnett (2000) and Butler et al. (2003). (d) Test history matching, utilizing superposition of sequential test responses. Individual test response predicted using the type-curve analysis method, as presented in Butler (1998).							

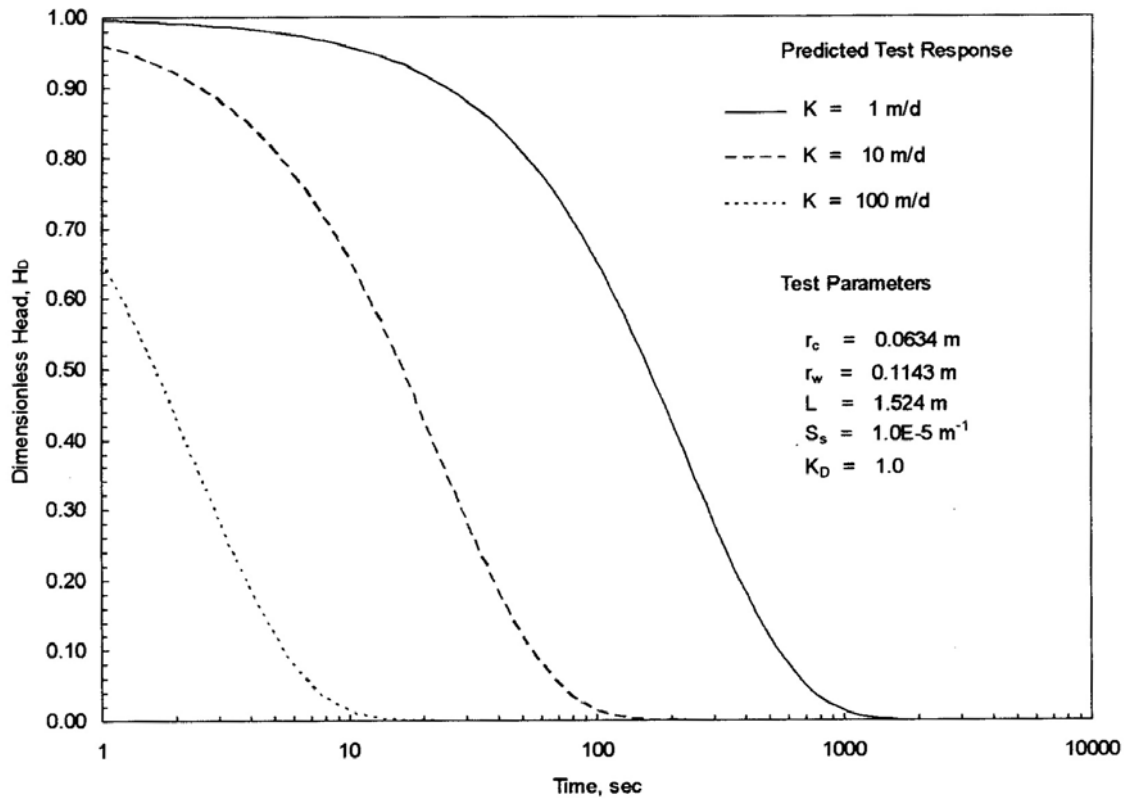
**Figure 1.** General Slug Test System Configuration (modified from Wright, 2003).



**Figure 2.** Diagnostic Slug Test Response (taken from Spane et al. (2003b))

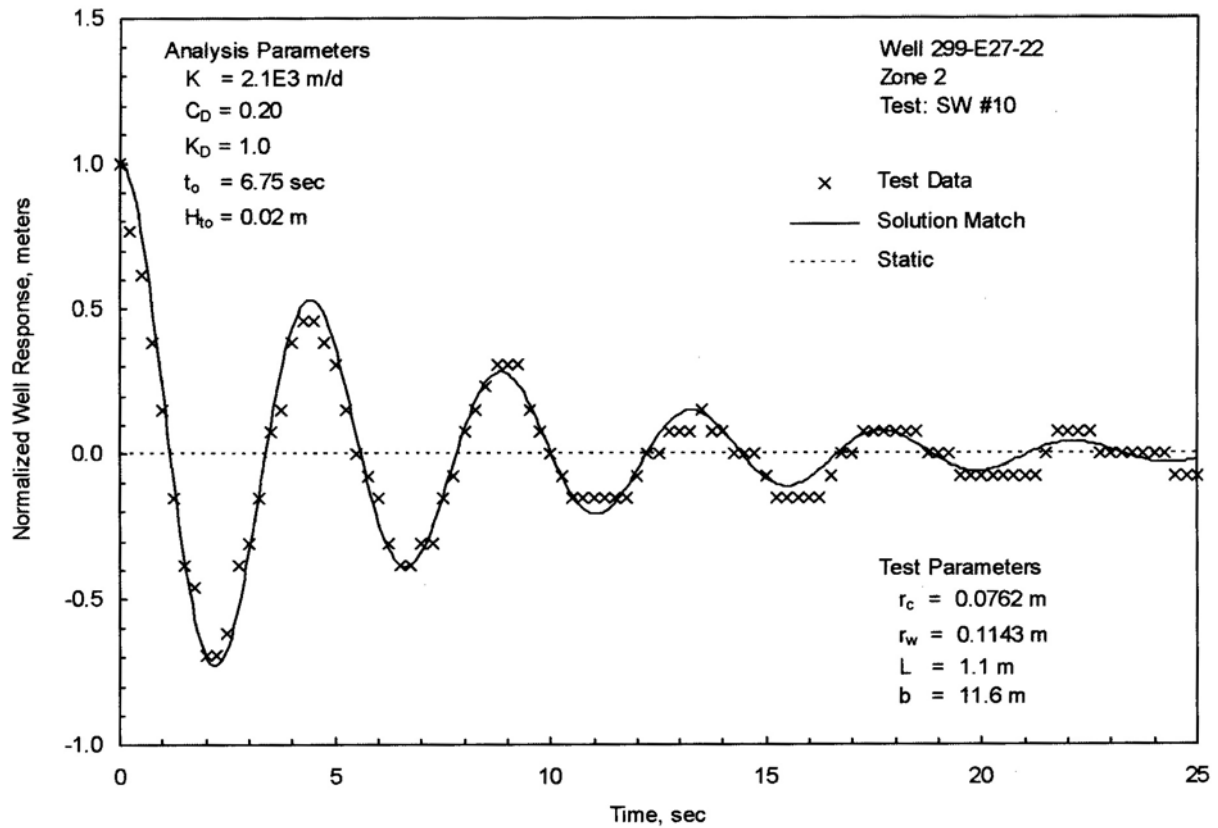


**Figure 3.** Predicted Over-Damped Slug Test Response as a Function of Test Interval Hydraulic Conductivity

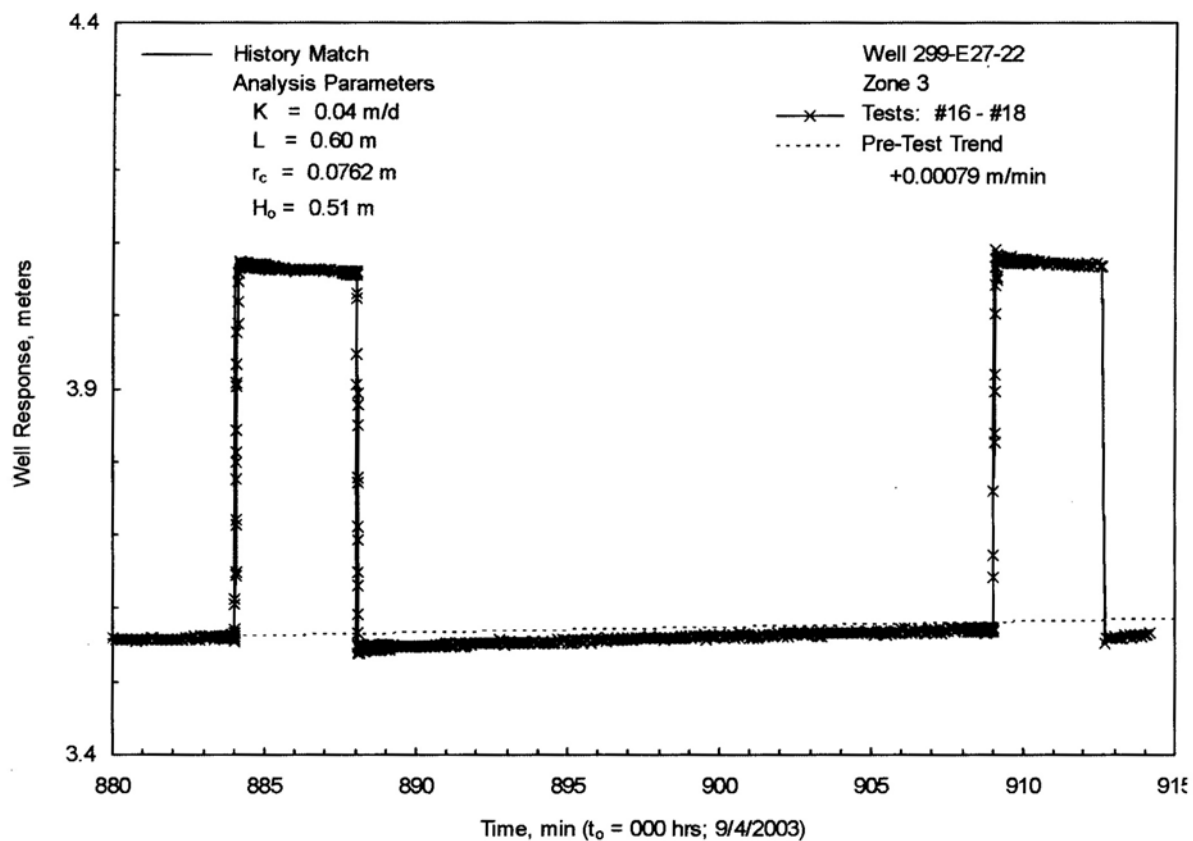




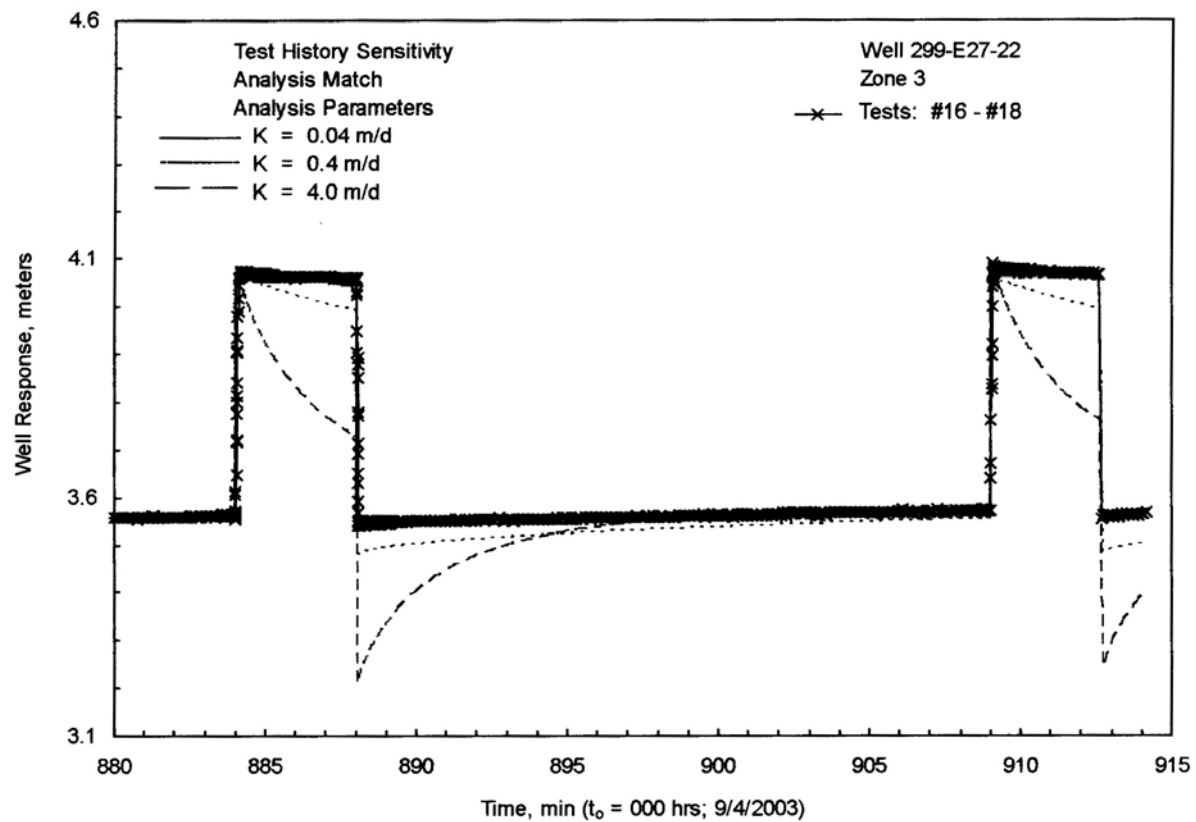
**Figure 4.** Test Zone 2 Observed Oscillatory Under-Damped Slug Withdrawal Test #10:  
Response and Analysis



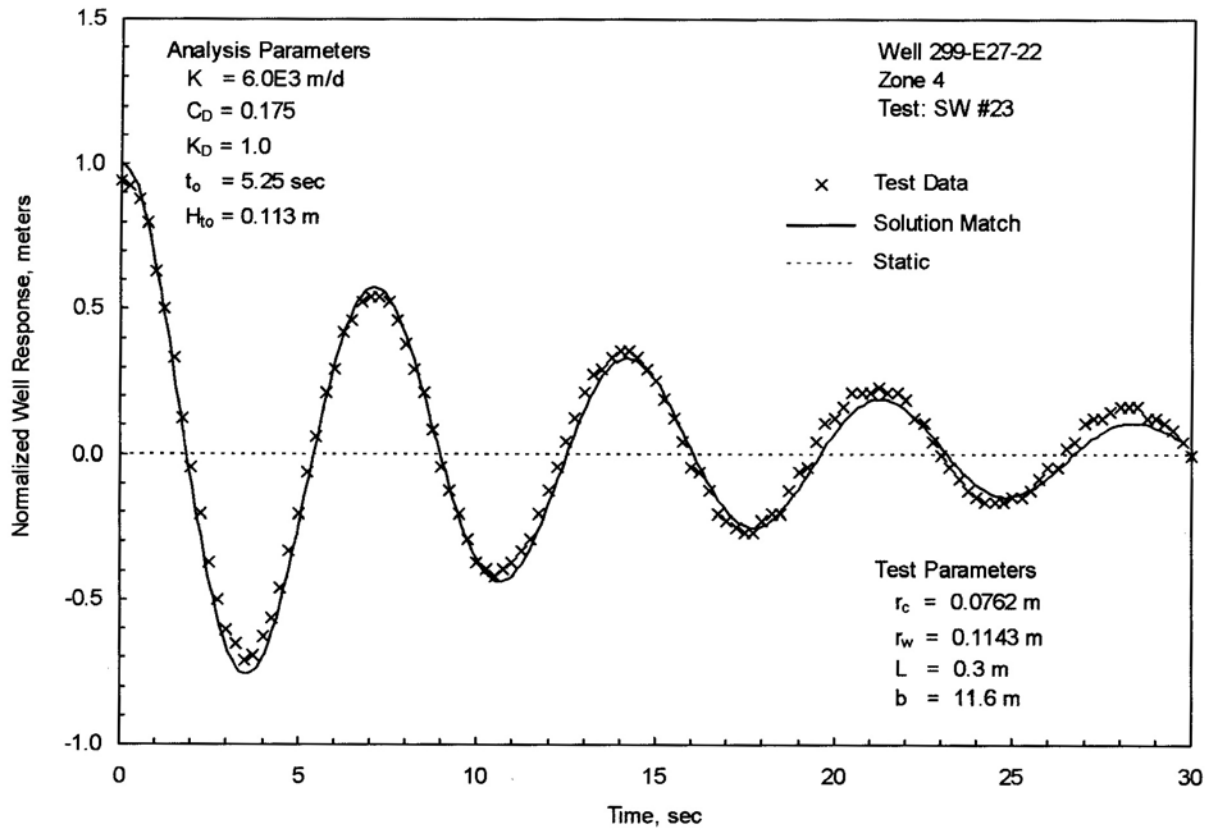
**Figure 5.** Test Zone 3 Observed Slug Testing Response Sequence, and Test History Match



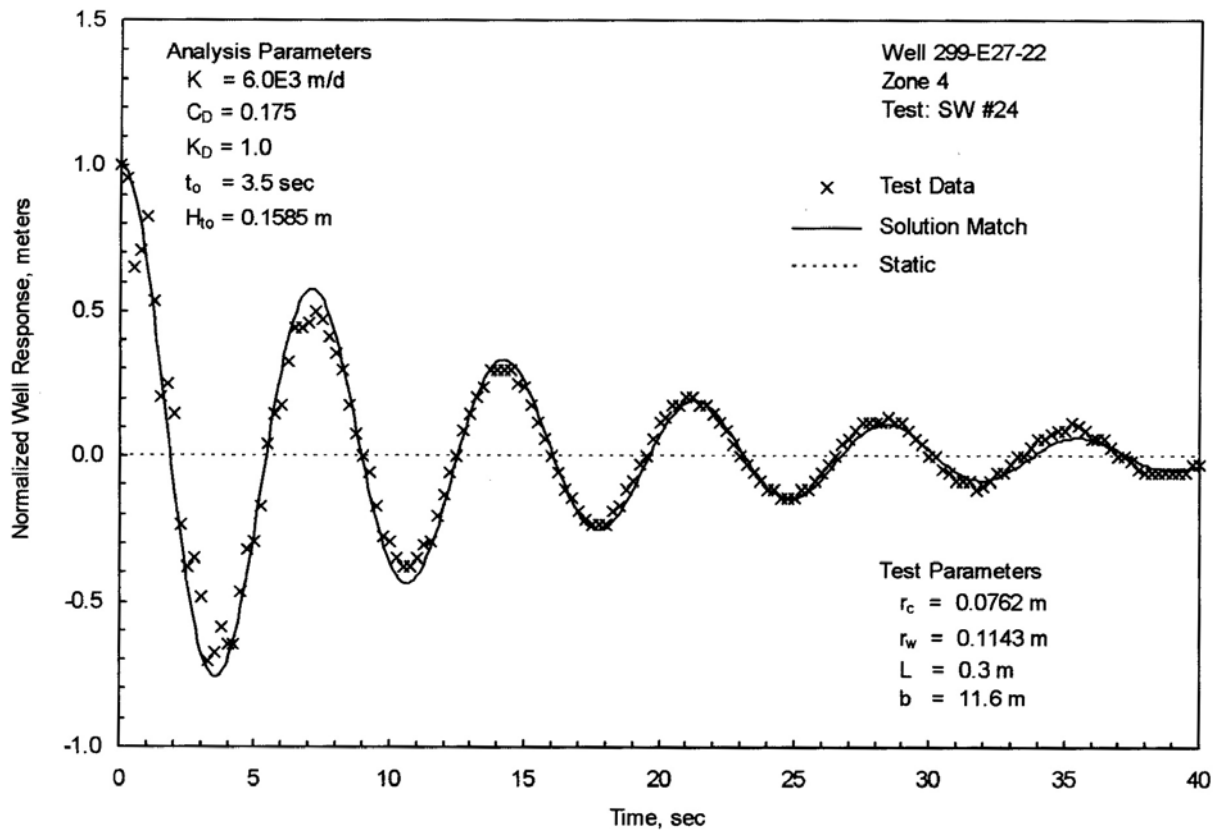
**Figure 6.** Test Zone 3 Observed Slug Testing Response Sequence, and Test History Match: Sensitivity to Varying K values (0.04, 0.4, and 4.0 m/day)



**Figure 7.** Test Zone 4 Observed Oscillatory Under-Damped Slug Withdrawal Test #23:  
Response and Analysis

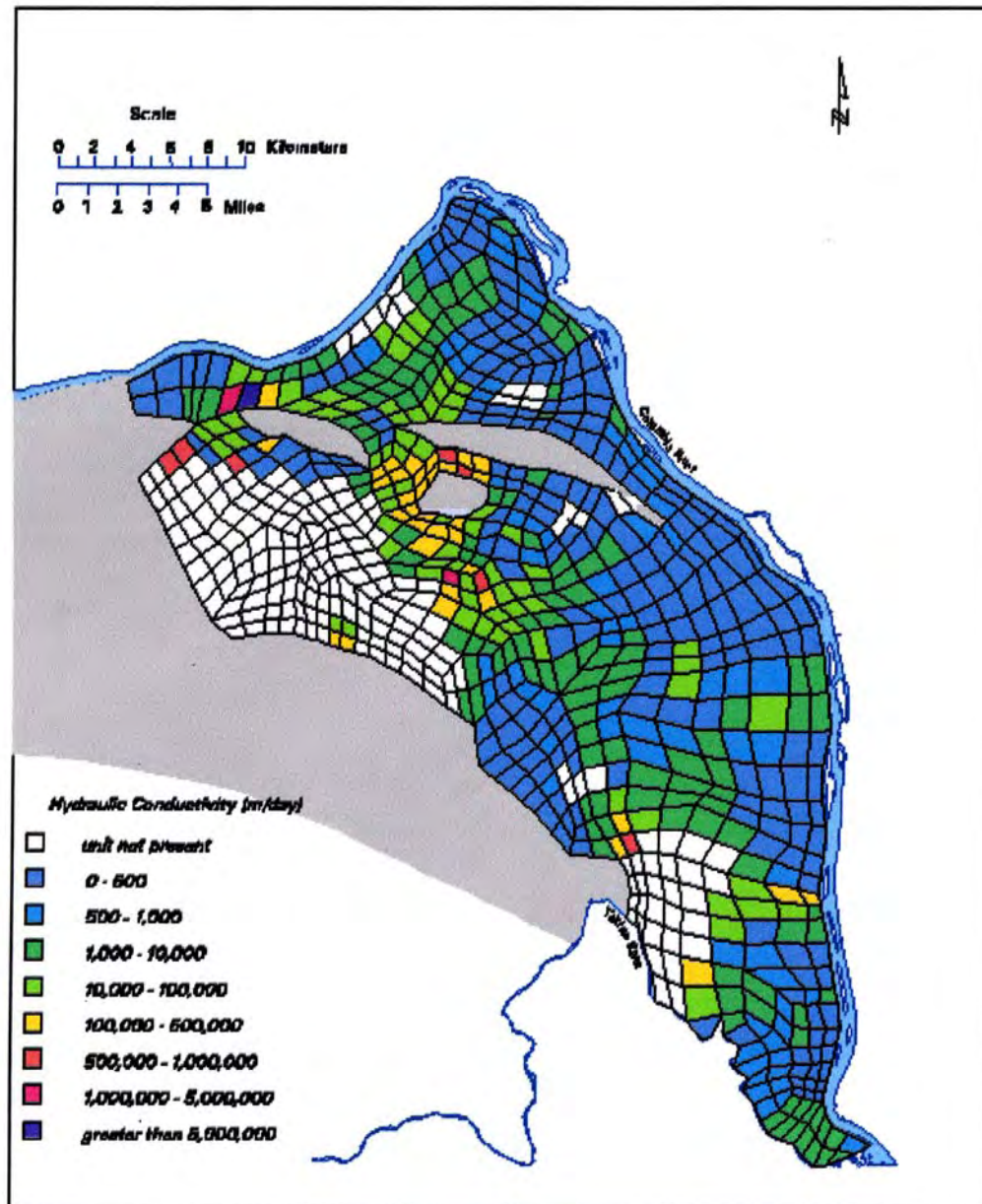


**Figure 8.** Test Zone 4 Observed Oscillatory Under-Damped Slug Withdrawal Test #24:  
Response and Analysis





**Figure 9.** Hydraulic Conductivity Values Assigned to the Hanford Formation, Based on Hanford Site Groundwater Flow, Inverse Calibration Modeling (taken from Wurstner et al. 1995).



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