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Abstract

The Portland District of the U.S. Army Corps of Engineers requested that scientists with the Pacific Northwest National Laboratory (PNNL) and the U.S. Army Engineer Research and Development Center (ERDC) conduct fish-passage studies at Bonneville Dam using hydroacoustic evaluation methods. The ERDC also contracted with MEVATEC Corporation and Dyntel to provide staff ranging from scientists to technicians for the study. This study supports the Portland-District goal of maximizing fish passage efficiency (FPE) and obtaining 95% survival for juvenile salmon passing the Bonneville Project.

This report presents results of two hydroacoustic studies of juvenile salmonids conducted in 2001 at Bonneville Dam in an extensive summary, in the main body of the report, and in appendices. Appendix E on the accompanying compact disk includes hourly estimates of forebay elevation and route-specific water discharge, fish passage, and associated variances and covariances.

One study was a project-wide evaluation of fish-passage efficiency, and the other was a more narrowly focused study of the approach, vertical distribution, and fish-guidance efficiency (FGE) of fish at Unit 15, where the Portland District extensively modified the gatewell and vertical barrier screen to improve gatewell flow and FGE. The goal of the larger of the two studies was to provide project-wide estimates of FPE, spill efficiency, and spill effectiveness for run-of-river fish passing the Bonneville Project during the 2001 out-migration. This type of study also provides estimates of the horizontal, vertical, and diel distributions of fish passage and FGE by turbine unit. These data will provide a baseline for evaluating the performance of future management efforts to improve juvenile fish passage. The goal of the second study was to assess the effect of gatewell and vertical-barrier-screen modifications on the FGE of Unit 15.

Executive Summary

The Portland District of the U.S. Army Corps of Engineers requested that scientists with the Pacific Northwest National Laboratory (PNNL) and the U.S. Army Engineer Research and Development Center (ERDC) conduct the hydroacoustic fish-passage studies described in this report. The ERDC also contracted with MEVATEC Corporation and Dyntel to provide staff ranging from scientists to technicians for the study. This study supports the Portland District goal of maximizing fish passage efficiency (FPE) and obtaining 95% survival for juvenile salmon passing the Bonneville Project. Project FPE is the percent of all juvenile salmon passing the project by non-turbine routes. Estimation of Project FPE and survival requires estimates of the proportion of juvenile salmon that pass through every major passage route.

This report presents results of two hydroacoustic studies of juvenile salmonids. One was a Project-wide study of fish-passage efficiency and the other was more narrowly focused upon the approach, vertical distribution, and fish-guidance efficiency (FGE) of fish at Unit 15, where the Portland District extensively modified the gatewell and vertical barrier screen to improve gatewell flow and FGE. The District also funded other parallel research on juvenile salmonids in 2001, including a Project-wide radio telemetry study by the U.S. Geological Survey (USGS) and a netting study of fish-guidance and orifice-passage efficiency by the National Marine Fisheries Service (NMFS) at Unit 15.

Common metrics used to describe fish passage at Bonneville Dam are listed below.

- Spill Passage Efficiency (SPE) – the proportion of total fish passing the project that pass through the spillway.

- Spill Passage Effectiveness – SPE divided by percent of total discharge going over the spillway.

- Fish Passage Efficiency (FPE) – the proportion of fish that pass through non-turbine routes i.e., juvenile bypass system and spillway.

Goals

The goal of the larger of the two studies was to provide project-wide estimates of FPE, spill efficiency, and spill effectiveness for run-of-river fish passing the Bonneville Project during the 2001 out-migration. It is the second full-project hydroacoustic study of fish passage at Bonneville Dam. The first was conducted in 2000 (Ploskey et al. 2002a). This type of study also provides estimates of the horizontal, vertical, and diel distributions of fish passage and FGE by turbine unit. These data will provide a baseline for evaluating the performance of future management efforts to improve juvenile fish passage. The goal of the second study was to assess the effect of gatewell and vertical-barrier-screen modifications on the FGE of Unit 15.

Objectives

Project FPE Evaluation

1. Estimate the proportion of smolt-sized fish that pass the project above and below in-turbine screens, sluiceway openings with water depths > 1 m, and the spillway each season.
2. Estimate spill efficiency and effectiveness by season and for spill periods.
3. Characterize the vertical and lateral distributions of smolt-sized fish passing through Powerhouses 1 and 2 and the spillway.
4. Describe day-night changes in vertical and lateral distributions of smolt-sized fish passing Powerhouses 1 and 2 and the spillway.

Unit 15 Evaluation

1. Determine average trajectories of juvenile salmon by elevation and distance upstream of trash racks through three successive hydroacoustic sample volumes aligned in a downstream-upstream direction.
2. Determine the vertical distribution of smolts from the top of the intake to the bottom of the forebay within three successive hydroacoustic sample volumes to determine how distributions change as fish approach the trash racks.
3. Use in-turbine up- and down-looking hydroacoustic beams to determine the vertical distribution of fish downstream of trash racks and to provide independent estimates of FGE from NMFS netting effort at the same unit.
4. Determine whether the distribution and behavior of fish upstream and downstream of the trash racks explain why FGE decreases from spring through summer.

Site Description and Conditions in 2001

From the Oregon shore north toward Washington, the project is composed of a navigation lock, a 10-unit Powerhouse 1, Bradford Island, an 18-gate spillway, Cascades Island, and an 8-unit Powerhouse 2. Principal passage routes include the spillway and two powerhouses, but within each powerhouse, fish passage can be through ice/trash sluiceways, turbines, or the juvenile bypass system (JBS). Smolts enter the JBS after they encounter screens in the upper part of turbine intakes and are diverted to gatewell slots and orifices opening to a bypass channel.

In a typical water year, the goal of maximizing FPE largely influences operation of the project. Large volumes of spill are presumed to be necessary to compensate for the low FGE of screens at both powerhouses, particularly in summer. In a typical year, spill volumes are limited to between 50,000 and 75,000 cfs during the day and are typically higher at night (100,000-140,000 kcfs) as long as total dissolved gas saturation does not exceed 120% (i.e., the gas cap). The Northwest had an unusually dry year in 2001 and that, combined with high generation demand, led to unusually low spill volumes. Total project discharge in spring was roughly half (46% in spring and 54% in summer) of what it was in 2000. In 2001, the project spilled 16% of the total discharge in spring and 11% in summer, down 31% and 50%, respectively, from the percent spilled in 2000. Total spill volume in 2001 was less than a quarter (23%) in spring and less than an eighth (12%) in summer of what it was in 2000.

Materials and Methods

Equipment

We sampled Powerhouse 1 turbines with four hydroacoustic systems, the spillway with three systems, and Powerhouse 2 turbines and forebay with four systems. Each system consisted of an echosounder, cables, transducers, an oscilloscope, and a computer system. An echosounder generates electric signals of specific frequency and amplitude and at the required pulse durations and repetition rates, and cables conduct those transmit signals from the echosounder to transducers and return data signals from transducers. Transducers convert voltages into sound on transmission and sound into voltages after echoes return to the transducer. Oscilloscopes were used to display echo voltages and calibration tones as a function of time, and the computer system controlled echosounder activity and recorded data to a hard disk. The 420 kHz, circular, single- or split-beam Precision Acoustic Systems (PAS) transducers were controlled by PAS 103 echosounders and Hydroacoustic Assessments' HARP software running on Pentium-class computers.

Calibrations

Before deployment, all hydroacoustic equipment was transported to Seattle, Washington, where PAS electronically checked the echosounders and transducers and calibrated the transducers using several standard transducers. After calibration, we calculated receiver gains to equalize the output voltages among transducers for on-axis targets ranging in hydroacoustic size from –56 to –36 dB $\| 4\pi m^2$. Lengths of fish corresponding to that acoustic size range would be about 1.3 and 12 inches, respectively, for fish insonified within 21° of dorsal aspect (Love 1977).

Sampling Powerhouse 1

In turbine units 1 through 10, we sampled one randomly selected intake slot out of three per unit. We mounted one upward- and one downward-angled 6° transducer in each of the selected slots to monitor guided and unguided passage, respectively. The lateral location of both transducers within the same intake was randomly selected to be on the north, center, or south side of the trash rack so that some of the lateral variation in passage within intakes would be captured in the variance estimate for the entire powerhouse.

Transducers deployed in units 5 and 10 were 6° split beams to provide target strength data for detectability modeling. Sampling the 40-ft-long extended submerged bar screen (ESBS) at Unit 8 required a different deployment of transducers. Fish passing above and below the ESBS of Unit 8 were sampled with upward- and a downward-angled, 6°, single-beam transducers to estimate guided and unguided numbers, respectively, but the down-looking transducer was mounted on the downstream side of the ESBS instead of on a trash rack. Therefore, fish passage at Unit 8 could differ from estimates at other Powerhouse 1 units for a variety of reasons, e.g., screen type, unit location, intake selected for sampling, and differences in detectability among deployments. Our modeling of and correction for differences in detectability among deployments should have minimized the last effect. Paired transducers in every intake were fast multiplexed to acquire 20 1-minute samples from each intake per hour. The pulse repetition rate was 15 pings per second for every transducer. At Powerhouse 1, we examined the vertical distribution of fish detected by split-beam transducers sampling inside Intake 10<u>b</u>.

Sampling the Spillway

Spill bays 2, 4, 5, 6, 7, 8, 10, 12, 14, and 15 were each sampled with one down-looking, 10°, single-beam transducer, and Spill Bay 17 was sampled with one down-looking, 12°, split-beam transducer.

Bays were selected to allow interpolation of fish passage to bays that were not sampled and to emphasize sampling at gates that would pass the most water according to the 1999 Fish Passage Plan. Transducers were mounted 28 ft below the tops of spill gates and aimed upstream 8° (single beams) or 15° (split-beam transducer at Bay 17). Transducers were at EL 59 ft when operators opened a gate about 3 ft, which was the maximum opening observed in 2001. The lateral location of both transducers within a bay was randomly selected to be on the north, center, or south side so that some of the lateral variation in passage within bays would be captured in the variance estimate for the entire spillway. Transducers were sampled sequentially to allow a pulse repetition rate of 30 pings per second during each of 12 1-minute samples collected by each transducer per hour.

Sampling Powerhouse 2

At Powerhouse 2, one out of three intakes at every turbine unit was randomly selected for sampling, and at Unit 15 we sampled both the b and c intakes. The lateral locations of transducers within intakes also were randomized among north, center, and south locations so that some of the lateral variation in passage through intakes would be incorporated in the total variance for the powerhouse. In each intake, we mounted a pair of transducers on the downstream side of the trash racks. One transducer of each pair was mounted near the bottom of the uppermost trash rack and aimed downward to sample unguided fish passing below the traveling screen. The second transducer of each pair was mounted near the bottom of the fourth trash rack from the top and aimed upward to sample fish passing above the screen. The two transducers deployed in Unit 18 were split beams to provide target strength data. Each transducer transmitted sound pulses at 15 pings per second, and both transducers of a pair usually were sampled simultaneously (i.e., fast multiplexed). Fast multiplexing allowed us to estimate covariances for the simultaneous samples of guided and unguided fish, and allowed us to collect 30 1-minute samples at Intake 15b and 15 1-minute samples per hour at all other intakes including 15c. Three transducers in the forebay were for sampling vertical distributions and the azimuth direction of travel of fish upstream of Intake 15b. They consisted of down-looking 6° split-beam transducers deployed on a steel beam lowered to a depth of 70 ft MSL in the trash-rack slot. They were aimed 6, 12, and 18 degrees off the upstream plane of the trash racks.

At Powerhouse 2, we examined the vertical distribution of fish detected upstream and downstream of the trash racks at Intake 15b, where the gatewell and vertical barrier screen had been modified to increase flow up into the gatewell. We also examined the direction of travel of detected fish through three split-beams to better characterize the behavior of fish approaching trash racks and the effect on FGE in spring and summer.

Fish Tracking and Filtering Criteria

Since the hydroacoustic sampling effort on Bonneville Dam was so extensive and generated such a large volume of data in 2001, we could not manually process enough data to make reliable fish-passage

estimates with available staff. Therefore, we relied on autotracking software developed over the last four years by the Corp's Fisheries Field Unit, the Corps Waterways Experiment Station (WES), and PNNL to process raw data into tracked fish observations.

During most of spring and early summer, we reviewed samples of the autotracker's performance for every deployment on a fish-by-fish basis to evaluate and fine-tune the autotracker and to develop post-processing filters for eliminating false traces from the autotracker's output. We released the autotracker to process data for a given deployment only after we determined that it was missing few of the echo patterns that we would have tracked.

Output from the autotracker was filtered extensively to reject non-fish traces that the autotracker selected. Filtering non-fish traces based upon variables like range, slope, and noise level is a critical part of using autotracking software, because the autotracker is more likely to track intermittent series of structural echoes or noise than are technicians. Filters were designed to eliminate echo traces that had a high probability of being from structure, noise, or non-target fish based upon their track statistics.

Although the autotracker was a very efficient tool, we evaluated its performance and post-processing filters in both seasons by comparing counts of fish by the software and by trained technicians. Every technician and the autotracker processed identical Powerhouse 2 data sets acquired early, mid, and late each season, but the abbreviated generation schedule at Powerhouse 1 left few options for data set selection there. We selected spillway samples from throughout the abbreviated spilling seasons. Results from the technicians provided an estimate of inter-tracker error and deployment-specific mean hourly estimates for comparison to the autotracker-based estimates.

We compared human and autotracked counts for each transducer (channel) because there are important differences in passage characteristics, ranges of interest, trace slopes and lengths, and noise conditions for each deployment site and aiming angle. Up-looking-transducer channels sampling guided fish have very different noise regimes from down-looking-transducer channels and the slopes of regression lines fitted to autotracker and mean human counts often differ too. They can even vary in opposite directions, so that up-looking-transducer channels have higher autotracked counts and down-looking transducer channels have higher human-tracked counts.

Adjustments to Fish-Passage Estimates

After regressing average technician counts on autotracker counts for each deployment, we used slopes of regression lines with intercepts forced through zero to convert autotracker counts into mean technician counts and thereby remove systematic bias in autotracker counts among deployments. Slope multipliers in spring were 0.96 (Powerhouse 1 unguided), 0.83 (Powerhouse 1 guided), 0.833 (Powerhouse 2 unguided), 0.754 (Powerhouse 2 guided), and 0.789 (spillway). Slope multipliers in summer were 0.985 (Powerhouse 1 unguided), 0.953 (Powerhouse 1 guided), 0.841 (Powerhouse 2 unguided), 0.678 (Powerhouse 2 guided), and 0.98 (spillway). Variances were multiplied by the square of the slope factors. Plots of the regressions of mean technician counts on autotracker counts are presented in the Results section of this report.

After the Anadromous Fish Evaluation Program Research Review (13-16 November), where we found that hydroacoustic estimates of fish spill efficiency and effectiveness were considerably higher than

those from radio telemetry, we examined the azimuth direction of travel of fish through the down-looking split beam at the spillway. We found that 7 to 13% of the fish in spring and 6 to 10% in summer were not moving in a downstream direction.

We decided to apply a conservative estimate of the number of fish passing through the spillway, rather than counting only the fraction of fish moving in a downstream direction. We estimated the downstream flux of fish per hour and multiplied hourly counts of fish in all spillway beams by that factor. The fish-flux factor is more conservative than multiplying by the fraction moving downstream because it subtracts the upstream fraction from the downstream fraction. For example, if 90% of detected fish are moving downstream and 10% are moving upstream, the flux factor applied would be 0.8 instead of 0.9. We consider this to be the most appropriate because upstream moving fish have the potential to be counted more than once and should be subtracted from the passage estimate. In reality, all we know is that some fish moving upstream could have been counted more than once and that the flux factor should be somewhere between 0.8 and 0.9. We could have split the difference and used 0.85, but we wanted to be certain not to overestimate spillway passage in a drought year. Flux factors applied in spring and summer are described in the Materials and Methods section of the report.

Dam Operations and Fish Passage

Bonneville Dam operators, who recorded results in a spreadsheet, provided hourly operations data, including discharge by spill bay and turbine unit. Hourly operations data were integrated with fish passage data, and fish passage was set to zero when passage routes were closed. When flow is low at a closed turbine unit or spill bay, a fish can stay in the beam much longer than when the passage route is open. A transducer samples continuously regardless of operations, and samples from closed turbine units and spill bays often include many traces that may be tracked as fish, often multiple times, when a turbine unit is off or a spill bay is closed. It is best to have operations data at 5-minute intervals so that hourly passage estimates are not inflated by multiple fish detections during the fraction of an hour when a turbine was off. For that reason, we set fish passage to zero if hourly discharge through a turbine was less than 65% of the maximum discharge on a given day. When discharge is less than 65% of the maximum discharge, there is a high probability that the turbine was off for some part of an hour. Multiple detections of just a few fish wallowing in an out of an acoustic beam when a turbine is off can greatly inflate hourly estimates of guided fish passage and bias estimates of FGE and FPE. We assumed that a turbine with < 65% of maximum discharge was off the entire hour rather than risk inflation of guided fish counts. These adjustments had little effect on overall fish-passage estimates because they were infrequent and over one half of those occurrences resulted from a turbine running < 10 minutes / hour.

Missing Data

All hydroacoustic systems were operated continuously (> 23 hours / day), except for about 15 minutes every morning when data were copied from the acquisition computer onto a portable FireWire™ hard drive or when equipment failed and data from the affected routes were not sampled. Short equipment failures lasting up to 45 minutes were not a problem because fish counts and associated variances could still be estimated from the remaining within-hour samples. Computer lock-ups usually were fixed within an hour because we had staff monitoring systems ever hour, 24 hours per day. Transducer cables failed on units 9 and 11 and both were fixed within a day, as soon as project support or divers became available.

Missing hourly sums and variances that resulted from equipment outages > 45 minutes were estimated by temporal linear interpolation for periods < 6 hours and by spatial interpolation or linear regression for periods > 6 hours. Occasionally the ratio of guided to unguided numbers at adjacent turbines with similar screens was useful for interpolating estimates of guided or unguided numbers. Regression equations relating hourly variances with hourly sums were sometimes used to estimate missing variance estimates. Two spill bays (3 and 16) were not among those sampled and were interpolated from passage estimates for other bays in their respective strata.

Detectability Modeling and Spatial Expansions

The count of every fish (1) was expanded based upon the ratio of the opening width to beam diameter at the range of detection:

$$EXP\_NUM = \frac{OW}{[MID\_R \times TAN(\frac{EBA}{2}) \times 2]}$$

where OW is opening width in m, MID_R is the mid-point range of a trace in m, TAN is the tangent, and EBA is effective beam angle in degrees.

Effective beam angle depends upon the detectability of fish of different sizes in the acoustic beam and is a function of nominal beam width, ping rate, trace criteria, and fish size, aspect, trajectory, velocity, and range. We modeled detectability for every transducer deployment to calculate effective beam angle as a function of range from a transducer. We obtained target-strength estimates from the average backscattering cross section of fish detected by split-beam transducers and flow-velocity data by 1- m depth strata from a physical or computational fluid design (CFD) model. These data and other hydroacoustic-acquisition data (e.g., beam tilt, ping rate, target-strength threshold, number of echoes, and maximum ping gaps) were entered into a detectability model. Model output consisted of effective beam angle as a function of range from a transducer.

Statistical Methods

The Material and Methods section of this report contains detailed descriptions of statistical methods used to analyze the hydroacoustic data. Dr. John Skalski developed these methods specifically for this study year.

Our estimates of variation associated with fish passage and efficiency metrics probably are conservative for two reasons. First, we took systematic 1-min samples (usually 12-15) per hour, and treated them as if they were simple random samples. This approach should overestimate the variance. Second, we estimated and added the variation among two or more turbine units to the temporal variation of each unit to provide a very conservative estimate of spatial variation resulting from sampling one out of three intakes per turbine unit.

Results and Discussion

Hydroacoustic Detectability

The motivating force behind efforts to improve detectability modeling is the desire to provide hydroacoustic estimates that are quantitative as well as relative indices to fish passage. Ratio estimators such as fish guidance efficiency only require that the hydroacoustic beams sampling guided and unguided fish have equal detectability so that the ratios of counts, not necessarily the counts themselves, are accurate. Nevertheless, accurate counts estimated by proper expansion of detected fish have the potential to provide estimates with inherent quantitative value as well as providing acceptable relative estimates.

One of the ways to check the adequacy of detectability is to regress numbers of fish per transducer hour on discharge volume and look for negative slopes that might indicate that fish were missed at higher discharge rates. This is one of the quality control checks that we perform every year, and as expected, we found no significant negative regressions between fish counts and discharge.

The closeness of our nighttime (2000-0500 hours) hydroacoustic estimates of FGE for Intake 15b at Powerhouse 2 with 1-2 hour netting estimates (2000-2100 or 2200 hours) by the NMFS indicated that the detectability of transducers sampling guided and unguided fish was similar. The 95% confidence intervals overlapped in both spring and summer indicating that respective estimates did not differ significantly. In all of spring, nighttime FGE was 73.7% for hydroacoustic gear and 74.7% for netting. For summer, nighttime FGE was 54.3% for hydroacoustics and 56% for netting.

The closeness of concurrent hydroacoustic and netting estimates of fish passage at Intake 15b in spring and summer verified that our detectability modeling and corrections to expansion factors were reasonable. In spring, the sum of all hydroacoustic and netting estimates of guided fish numbers differed by 22%, and in summer, the estimates did not differ (< 1%). The sum of all unguided fish by the two methods also were reasonably close and differed by less than 1% in spring and by about 21% in summer.

Validation of Autotracking Hydroacoustic Data

Mean hourly counts of fish by human trackers were very highly correlated with hourly autotracker counts for each deployment. This year, we used human trackers only to verify and adjust the results of the autotracker. Although the agreement among technicians tracking the same data was better than it has sometimes been, the cumulative difference in passage estimate for the lowest tracker would be only about 72.8% that of the highest tracker for the 438 channel hours we compared in spring and 68.8% for the 227 channel hours we compared in summer. The slopes of regressions were used to correct our autotracked results downward to offset the tendency of the autotracker to overestimate passage. This approach is not only more economical but also qualitatively superior to assigning technicians to process data from different deployments because of known inter-tracker bias.

Major Passage Metrics

Project and Powerhouse FPE

The drought of 2001 provided a unique opportunity to evaluate Project FPE during spill and non-spill periods in the same year. Project FPE was 15 and 35% higher during 50,000 cfs spill periods in spring and summer, respectively, than it was during non-spill periods. In 2000, continuous spill at 75,000 or 120,000 cfs throughout spring and summer and the operation of a prototype surface collector at Powerhouse 1 produced Project FPE estimates of 79% in both seasons. These estimates were 16% (spring) and 26% (summer) higher than estimates for spring and summer seasons in 2001, which included spill and non-spill periods rather than continuous spill.

Project-wide FPE was 63% in spring and 53% in summer. The FPE estimate for Powerhouse 1 declined from 49% in spring to 40% in summer, a drop of 9%. The FPE for Powerhouse 2 declined even more across seasons (>15%), with estimates of 57% and 42% in the spring and summer, respectively. Project FPE was only about 1% lower in spring and in summer than FPE calculated for Powerhouse 2 and the spillway alone (without Powerhouse 1). This was not surprising given that Powerhouse 1 passed only about 7.3% of the water and 6.9% of the fish in spring and 8.6% of the water and 7.5% of the fish in summer.

Spill Efficiency and Effectiveness

Spill efficiency estimates in spring (14%) and summer (20%) 2001 were significantly lower than estimates made in spring (44%) and summer (49%) 2000, undoubtedly because of reduced volume and duration of spill during the drought in 2001. For periods of spill, spill efficiency was 33% in spring and 58% in summer. Spill effectiveness was 0.84 in spring and 1.83 in summer. For periods of spill, spill effectiveness was 0.93 in spring and 1.6 in summer. Spill effectiveness also was about 38% lower in spring 2001 than it was the previous spring. In 2000, spill was continuous at about 75,000 cfs during the day and 120,000 cfs at night, but lack of water in 2001 limited spill to about 50,000 cfs for about 21 of 45 days in spring and 10 of 40 days in summer.

Effectiveness seems to be a meaningful metric when differences in flow proportions do not exceed about 30%, which was not the case in comparisons between summer 2000 and 2001. In summer 2001, spill effectiveness was about 55% higher than the previous year's estimate likely because the proportion of water spilled in summer 2001 was much lower than it was in 2000. The denominator in the spill-efficiency calculation (the proportion of water spilled) in summer 2000 was 0.48 whereas was it only 0.11 in summer 2001. The inverse of these proportions shows how much spill efficiency was expanded (i.e., by 2.1 in 2000 and by 9.1 in 2001) to estimate effectiveness. The multiplicative nature of the effectiveness statistic is exemplified by the effectiveness at sluiceways and surface collectors, which are always higher than estimates for a spillway because those small routes pass orders of magnitude less water than a spillway passes.

Effects of Spill Level

We found several significant relationships that suggest an optimum spill strategy for future drought years that includes night spill lasting at least 11 hours. There were positive relations between the number of hours of spill per day and FPE and spill-efficiency metrics, and we observed significantly higher fish passage through the spillway at night than during the day, even though the amount of spill was the same during each period. We observed a similar trend in 2000, but nighttime spill discharge was much higher than it was during the daytime, and we could not determine whether the pattern was driven by spill level or day versus night. With constant spill in 2001, we can confidently describe the effect as a diel pattern unrelated to spillway discharge. Spilling at night also has the advantage of eliminating fall back of adult salmonids through the spillway during the day and may reduce fish losses due to visual predators such as birds and fishes in the spillway tailrace. Spill efficiency increased linearly with the number of spill hours per day in spring. We identified two obvious levels of effect. At low-spill durations of 0 to 10 h/day, average FPE was about 54% and at high-spill durations of 11 to 24 h/day average FPE was about 71%.

Comparison with Radio Telemetry Estimates

The largest differences between hydroacoustic and radio telemetry estimates occurred in spring, including a 14% difference in Powerhouse 2 FPE during 2% spill and an 11% difference in Project FPE, but all other differences in major metrics in spring and summer were ≤ 10% (Table S.1). In general, the hydroacoustic estimates of major fish-passage metrics were higher than the radio telemetry estimates. Powerhouse 1 FGE in summer was the only exception. The radio-telemetry season started and ended later than did the hydroacoustic season so we recalculated our hydroacoustic estimates based on the USGS's data collection schedule and they did the equivalent recalculation of their data in summer so that we would be comparing the same days each season. The level of agreement between our hydroacoustic and the radio telemetry-based estimates was better for major fish-passage metrics and entire powerhouses than it was for individual units. Differences in FGE estimates for individual units are described later under Comparing FGE Estimates by Different Sampling Methods.

Spatial Trends in Fish Passage

Horizontal Distributions

The percentage of discharge through major passage routes was a good indicator of the relative percentage of fish passage among those routes in spring but was less so in the summer. In spring, about 7% of both fish passage and discharge occurred at Powerhouse 1, 14% of the fish and 16% of the flow passed through the spillway, and Powerhouse 2 passed 79% of the fish with 76% of the flow. Fish and flow percentages also matched up well at Powerhouse 1 in summer (about 8% of the fish with about 9% of the flow), but the relative proportions at the other passage routes (the spillway and Powerhouse 2) differed. For the entire summer period, the spillway passed 20% of the fish in summer with 11% of the flow and Powerhouse 2 passed about 72% of the fish with 80% of the flow. Powerhouse 1 passed about 4% of all fish in summer in about 7.5% of the total discharge. During spill days in summer, the spillway passed 58% of the fish in just 36% of the flow, while Powerhouse 2 passed 40% of the fish in 61% of the flow.

Table S.1. Comparison of Fish-Passage Metrics Estimated by Hydroacoustics (HA) and Radio Telemetry (RT) at Bonneville Dam in 2001 for May 1-June 9 in Spring and July 1-July 15 in Summer

Metric	Season and Spill Conditions	HA	RT	Difference
Project FPE[a]	Spring overall	67%	56%	11% (HA>RT)
	Spring (about 37% spill)	71%	64%	7% (HA>RT)
	Spring (about 2% spill)	56%	47%	9% (HA>RT)
PH1 FGE	Spring overall	47%	45%	2% (HA>RT)
(Excluding sluiceways)	Spring (about 37% spill)	39%	N/A[2]	
	Spring (about 2% spill)	50%	45%	5% (HA>RT)
PH1 FPE	Spring overall	N/A[1]	87%	
	Spring (about 37% spill)	N/A[1]	100%	
	Spring (about 2% spill)	N/A[1]	86%	
PH2 FPE	Spring overall	56%	46%	10% (HA>RT)
	Spring (about 37% spill)	55%	49%	6% (HA>RT)
	Spring (about 2% spill)	57%	43%	14% (HA>RT)
Spill Efficiency	Spring overall	26%	16%	10% (HA>RT)
	Spring during spill	38%	30%	8% (HA>RT)
Spill Effectiveness	Spring overall	1.21	0.70	0.51 (HA>RT)
	Spring during spill	1.13	0.86	0.27 (HA>RT)
Project FPE	Summer overall (about 3% spill)	44%	40%	4% (HA>RT)
PH1 FPE	Summer overall (about 3% spill)	N/A[b]	89%	
PH1 FGE	Summer overall (about 3% spill)	47%	57%	10% (RT>HA)
PH2 FGE & FPE	Summer overall (about 3% spill)	44%	35%	9% (HA>RT)

1 The radio telemetry FPE estimates include fish that pass by the sluiceway at Powerhouse 1, but there was no hydroacoustic sampling of Powerhouse 1 sluiceway passage so there can be direct comparison of Powerhouse 1 FPE estimates. Since the Powerhouse 2 sluiceway was closed in both seasons, Powerhouse FPE and FGE are the same for Powerhouse 2. Since the Powerhouse 1 sluiceway handled a very small proportion of the total project passage, we neglected this distinction at the project level.

2 During spring 37% spill, only four radio-tagged fish were tracked through Powerhouse 1 and they all passed by the sluiceway, which was not sampled by hydroacoustics. Powerhouse FGE is the proportion of all fish guided divided by the sum of guided and unguided (turbine) fish. In this case, Powerhouse 1 FGE would equal 0/0, which is undefined.

Lateral fish passage patterns that may normally occur during times of full loading of Powerhouse 1 could not occur in 2001 given the drought and a Powerhouse 2 priority for generation. Flow was so low in both spring and summer at Powerhouse 1 that many of the units seldom ran, particularly during periods of spill. Horizontal passage patterns at Powerhouse 1 were consistent between seasons. In spring, about 70% of the fish that passed at Powerhouse 1 passed through units 9 and 10, as did 73% of the Powerhouse 1 discharge. Fish passage and flow were low throughout the rest of Powerhouse 1, with the exception of Units 1 and 2, which passed 8% of the fish with 14% of the flow, and 9% of the fish with 7% of the flow, respectively. In summer, nearly 75% of the fish that passed Powerhouse 1 in the summer passed at units 9 and 10, along with 81% of the water. Discharge at Powerhouse 1 was very low during the summer and was mostly allocated to units 1, 9, and 10, and Unit 1 passed about 5% of the fish in about 10.6% of the flow. Of the remaining units, significant passage occurred only at Unit 6, which passed 12.6% of the fish in less than 3% of the flow.

The southern skew in the distribution of fish passage at Powerhouse 2 in both seasons was much more noticeable in 2001 than it was in 2000, and it certainly supports the management decision to build a corner collector adjacent to Unit 11. Fish passage through the south half of the second powerhouse was consistently high during both sampling seasons. About 70% of the fish passing through Powerhouse 2 passed through units 11-14, although these units discharged only slightly more than half of the water

(52.6%). Units 11-15 passed roughly similar numbers of fish per volume of water during spring and summer. Unit 17 was off-line all summer. We also observed a southern skew in the passage distribution in summer of 1996 (Ploskey et al. 1998). To better compare fish passage among the individual units of Powerhouse 2, we standardized passage by reporting the density of fish passage in fish per volume of water in both spring and summer. Density was highest at the southern and central units (units 11 through 15), ranging from 531 to 703 fish passed per M m^3 water discharged. Fish passage density was lowest at the three northern units (units 16, 17, and 18), ranging from 217 to 321 fish passed per M m^3 water discharged.

Fish passage at the spillway was slightly skewed to the south during both seasons, despite a relatively even distribution of discharge across the spillway. This was mainly due to low passage rates at bays 2 and 3, which passed far fewer fish than bays at the southern end of the spillway, although they discharged about the same amount of water as the bays to the south. Spill discharge was relatively constant in spring and summer at about 50,000 cfs, and the spill pattern (bays and gate openings) varied little. In spring, the highest proportions of the fish that passed the project at the spillway passed through Bay 6 (where 19% of all spillway passage occurred), Bay 16 (18% of spillway passage), and Bay 17 (22% of spillway passage). Spillway discharge was terminated on 15 June, 10 days into the summer sampling season. For the entire summer sampling season, 11% of all fish passage occurred at the spillway along with 20% of all discharge. During the ten days that the spillway was operating, however, the spillway passed 58% of the fish in 40% of the water.

The exceptional effectiveness of the spillway during the only 10 days of spill in early summer may be explained by a peak in the summer migration, spill at the expense of generation at some Powerhouse 2 units, and the fact that forebay elevations were falling. According to salmonid run-timing estimates by the hydroacoustics and JBS counts, the largest peak in the summer run passed the dam during these early days of summer sampling. When forebay elevations drop, the depth of a bottom ridge upstream of Cascades Island and into the Powerhouse 2 forebay is shallower than it is when pool levels are high. Sub-yearling fish migrating along the shore upstream of the Powerhouse 2 forebay may guide along the channel edge that separates the Powerhouse 2 forebay from the main channel leading to the spillway, particularly when water levels decrease. In 2001, Powerhouse 2 was the priority powerhouse and usually was fully loaded. However, during the 10 days of spill in early summer, the percent of off hours for Powerhouse 2 turbines was higher than usual (Unit 17 = 100%; Unit 15 = 46%; Unit 14 = 41%; Unit 13 = 25%; Unit 12 = 14%; and Unit 11 = 5%).

Vertical Distributions

Powerhouse 1 – Inside Intake 10b

The vertical distributions of fish at Unit 10 in spring and summer strongly suggest that installing an ESBS similar to the one installed at Unit 8 would improve FGE in spring, but the benefit would be less in summer. The elevation for classifying detected fish as guided or unguided at an ESBS would be about 21 ft MSL. According to this cutoff criterion, an ESBS would guide about 68% of the fish in spring but only about 50% in summer. In spring 2001, we classified about 47% of all fish as guided by the STS, but in summer, that percentage fell to about 36%. In the 2000 passage season we found an estimated FGE of 72% in spring that fell to 50% in summer (Ploskey et al. 2002a).

Powerhouse 2 - Upstream and Downstream of Intake 15<u>b</u>

Theoretical (expected) FGE based upon the vertical distribution of fish upstream of the trash racks at modified Unit 15 (Intake <u>b</u>) was similar to the estimated in-turbine FGE for all hours sampled in spring but not in summer. Theoretical FGE is defined as expected FGE based upon the upstream vertical distribution relative to an elevation for classifying guided and unguided fish projected upstream parallel to the intake roofline from the elevation used inside the turbine. The FGE of 50% in summer was 29% less than the theoretical FGE. In spring, fish detected 16 to 21 ft upstream of trash racks were higher in the water column than fish detected 4 to 9 ft from the racks. A similar pattern was observed in summer, but the peak in the distribution of fish 4 to 9 ft from trash racks was several ft lower in the water column than the peak for fish 4 to 9 ft from racks in spring. The downward shift in the distribution of fish approaching the trash racks was observed during the day and at night.

Two pieces of evidence indicate that fish approaching trash racks increased in depth and changed behavior, and these factors may make them more or less susceptible to being guided by a STS inside the turbine. First, peaks in vertical distributions of fish located below the elevation of the top of the intake and 4 to 9 ft from trash racks were 9 to 12 ft deeper than peaks in distributions sampled 16 to 21 ft upstream. Second, direction-of-movement and fish-detection statistics show that 70% of the relatively few detections 10 to 15 ft upstream of trash racks were moving downstream, whereas only about 54% of detections within 4 to 9 ft of trash racks were moving downstream. In short, we found both higher numbers of fish and lower vertical distributions of fish detected 4 to 9 ft from the racks than of fish detected 16 to 21 ft from the racks. These differences were consistent for both spring and summer. Higher numbers of fish close to the trash racks may indicate that fish paused in their downstream movement as they encountered physical cues relating to the presence of the racks. If fish paused just upstream of the racks, they could easily have been counted multiple times as they passed in and out of the sampling volume, resulting in higher cumulative counts.

Smaller individuals that comprise the summer smolt population likely are less able to maintain their vertical position in the water column when they pause upstream of the trash racks. Fish that pause in their downstream movement just upstream of the trash racks are not only exposed to the downstream component of flow, they also encounter strong downward water velocities. The agreement of theoretical FGE with observed in-turbine FGE during spring may indicate that the spring-migrating smolts were able to maintain both their horizontal and their vertical position in the water column as they paused before going through the trash racks. In summer, the lower vertical distribution of fish detected 4 to 9 ft upstream of the trash racks, as compared to those detected 16 to 21 ft upstream of the racks, was more exaggerated than during spring. In addition, theoretical FGE was significantly higher than observed in-turbine FGE in summer.

Temporal Trends in Fish Passage

Run Timing

The run timing curve in 2001 based on hydroacoustic estimates shows that the spring peak occurred on 21 April and the summer peaks occurred on 8 and 27 June. The JBS smolt index data at the

Bonneville Project indicated similar temporal trends as observed with hydroacoustic sampling, with peaks and troughs in general agreement.

Major Fish Passage Metrics

The 9% decline in FPE from spring to summer at Powerhouse 1 and the 26% decline at Powerhouse 2 were similar to but slightly larger than seasonal declines observed in 2000 for Powerhouse 1 (6%) and for Powerhouse 2 (19%). Powerhouse 1 FPE in 2000 was 67% and 61% in spring and summer, and these estimates were 18% and 21% higher than respective estimates in spring and summer 2001. The difference most likely resulted from the nearly continuous operation of the PSC and Unit 8 with an ESBS in 2001. In 2001, the PSC units functioned as standard STS units and Unit 8 ran less than 1 day each season because of drought prioritization of operations. Project FPE was about 57% in spring with no visually obvious trend until spill began on about 15 May when FPE began a gradual increase into early summer. The average FPE during spring spill was about 71% and 76% during the 9 days of spill in early summer. Fish passage efficiency dropped down to 34% on 16 June when spill ended, and it averaged about 40% with ± 10% fluctuations for the rest of summer.

Powerhouse 1 FPE estimates averaged 49% in spring and 40% in summer, but all daily estimates for Powerhouse 1 were much more variable than estimates for Powerhouse 2. Powerhouse 2 estimates averaged 57% in spring and 42% in summer, ranging from a high of 65% on 30 May to a low of 29% on 14 June.

Spill efficiency varied substantially from day to day but exhibited a general upward trend from 16 May, when spill began, through 15 June, the last day of spill in 2001. Spill efficiency tracked the spill proportion during the first half of the spill season but not during the second half.

Guidance Efficiency at Modified Unit 15

The spring to summer decline in FGE that we observed at Unit 15 was typical of what we have observed at most units at Bonneville Dam, but the summer FGE estimate was not as low as those from other STS-equipped units at Powerhouse 1 or 2 in the summer of 2000. It was comparable to adjacent Units 14 and 16 in 2001. The nighttime FGE of Unit 15 decreased about 20%, from 74% to 54% from spring through summer in 2001. In 2000, the summer FGE estimate for Powerhouse 1 units running STS and the summer FPE of Powerhouse 2, which had no modified units was about 30%. Daily estimates of FGE for modified intake 15b and 15c based upon all hours sampled each day decreased significantly from spring to summer but were highly variable in both seasons.

American Shad Run Timing

American shad present a problem for hydroacoustic sampling in summer. Almost 2.3 million American shad migrated up through Bonneville Dam in 2001. Shad began arriving at the dam in mid May and were present in large numbers during the third week in May before peaking on 1 June when 144,000 individuals were observed. By 6 June, 50% of all the migrating shad had already passed the dam. By 30 June, the shad migration was essentially complete with over 98% of all fish having passed by that day. The Bonneville Dam 2001 shad up migration was nearly twice as large as the 2000 run and it peaked 10 days earlier.

Diel Trends

Providing a Powerhouse 2 priority and nighttime spill could significantly improve fish-passage efficiency in spring by as much as 6% to 12% during a drought year, while minimizing fallback of adult salmonids through the spillway. Factors contributing to a 6% to 12% higher project FPE at night than during the day included significantly higher nighttime fish passage through the project, including the spillway and Powerhouse 2, and higher FGE of Powerhouse-2 turbines at night than during the day.

On an hourly basis, project-wide estimates of FPE in the springtime were higher at night than during the day, and extreme values only differed by 12%. Summertime estimates of FPE were higher at night than they were during 6 or 7 of the daytime hours, although a diel trend was not as obvious in summer as it was in spring.

Estimates of spill efficiency during the spring were low from mid-morning to early evening and were higher at night than during the day. Spill efficiency in the summer was highest from early morning to early afternoon and was at its lowest in early evening. Estimates of spill effectiveness in the spring were slightly higher in the late evening and early morning hours but changed very little throughout the day. Summertime spill effectiveness followed a similar pattern as the spill efficiency in the summer with peaks in the early morning to early afternoon and lows in the early evening.

Project-wide fish passage through all routes in the spring gradually declined through the day, began to slightly increase in the early evening, peaked at 2100 hours, and then declined again through the early morning hours. Numbers of fish spilled in the spring declined through the day then increased sharply at 2100 hours and peaked at 0100 hours. The volume of water spilled differed little among hours in the spring, but a slight increase occurred at 2300 hours, coinciding with an increase in the number of fish spilled. In the summer, the pattern of fish spilled through the day was less defined than in spring, but the decreasing trend during the day and an increase in nighttime hours was still evident. Spill passage during the summer peaked at 0300 hours. There was very little variation in hourly spillway flow in the summer.

We found no significant diel trends in FGE at Powerhouse 1 in spring or summer because variances of estimates were too high, but Powerhouse 2 FGE estimates were generally higher in late afternoon and at night than they were during the day. In spring, the estimates declined slightly from highs at 0100 to 0500 hours to lows from 1200 to 1500 hours. Total fish passage in the spring declined through the morning and into the early afternoon then slightly increased through the remaining afternoon hours then rose sharply and peaked at 2100 hours. During the summer, FGE estimates at Powerhouse 2 dipped to lows in the midmorning and early afternoon hours and peaked staying relatively constant from 1800 to 0400 hours. Total passage through Powerhouse 2 in the summer was similar to the pattern observed during spring except the initial increase started later in the afternoon and the peak occurred at 2200 hours (instead of 2100 hours as in spring).

Hydroacoustic and radio telemetry estimates of hourly trends in fish passage for the project were generally similar, except for a peak in radio telemetry data in the middle of the afternoon (1400 to 1600 hours) that was not evident in the hydroacoustic data. In summer, both hydroacoustics and radio telemetry methods documented a peak in fish passage after sunset. However, the hydroacoustic data show higher passage through the night until about 0900 hours than from 1000 to 1800 hours, whereas the

radio telemetry data show little if any trend from 0000 to 2000 hours. In summer, the radio telemetry data are for a longer period, which ended July 24, about 9 days after the end of hydroacoustic sampling.

The average hourly percentage of fish passage estimated by hydroacoustics to have passed entire structures (powerhouses or the spillway) or combinations of structures in daytime (0500-2059 hours) were within one percent of radio telemetry results for the same hours in both spring and summer.

Table S.2. Percentage of Fish Estimated by Hydroacoustics (HA) and Radio Telemetry (RT) to Have Passed Bonneville Dam Structures during an Average Daytime Hour (0500-2059 hours) in Spring and Summer of 2001. Data from non-overlapping parts of seasons have been deleted and adjusted appropriately so that the times reported here are the same for both methods. Those dates are May 1-June 9 for spring and July 1-July 15 for summer.

Season and Location	HA Percent	RT Percent	Difference
Spring PH1 Only	4.68%	3.86%	0.82 % (HA>RT)
Spring PH2 Only	3.77%	3.46%	0.31% (HA>RT)
Spring Spillway Only	3.49%	4.04%	0.55% (RT>HA)
Spring PH2 + Spillway	3.67%	3.55%	0.12% (HA>RT)
Spring Full Project	3.73%	3.56%	0.17% (HA>RT)
Summer PH1 Only	4.72%	4.17%	0.55% (HA>RT)
Summer PH2 Only	3.51%	3.18%	0.33% (RT>HA)
Summer Spillway Only	N/A	5.73%	N/A
Summer Full Project	3.58%	3.30%	0.28% (HA>RT)

Comparing the Performance of Fish-Guidance Structures

For all sample hours in spring, the FGE of submerged traveling screen (STS)-equipped units at Powerhouse 1 ranged from 22% to 57%, and this was lower than the range observed at Powerhouse 2 (35% to 72%), but in summer the performance of units at both powerhouses was similar. Therefore, provision of a Powerhouse 2 priority may have been a good management tactic in spring. Guidance efficiency ranged from 29% to 53% (FPE=40%) at Powerhouse 1 and from 11% to 54% (FPE=42%) in summer. The higher FGE of Powerhouse 2 units may have resulted from the presence of turbine intake extensions (TIEs) at every other intake and the fact that five of nine intakes that we sampled were between TIEs where passage and FGE tended to be higher. We also observed higher FGE in spring at Intake 15b (72%), which was between two TIEs, than we did at Intake 15c (59%), which was behind a TIE. The difference was less in summer (50% at 15b and 48% at 15c). There also was a tendency for FGE to be lower at the ends of Powerhouse 2 than in the middle, but since the intakes we sampled at end units of Powerhouse 2 were behind instead of between TIEs, the effect of unit location could have been masked. Unit 1 had the lowest FGE at Powerhouse 1 in both spring and summer.

In spring, the FGE of the 40-ft-long ESBS at Unit 8 (83%) was higher than that of any of the units equipped with 20-ft-long STS, except for modified Unit 15 at Powerhouse 2, but the 38% ESBS efficiency in summer was comparable to that of average STS units. Unit 8 only ran for about 8 h in spring and 5 h in summer, so its FGE estimates were based upon very small data sets and its contribution to Powerhouse 1 and Project FPE was minimal.

The 72% to 74% FGE of modified Unit 15 was higher than that of all other unmodified STS units at Powerhouse 1 and 2 in spring. In summer, it was among the three highest individual Powerhouse 2 units (50% to 54%). The FGE of Unit 15 in summer was 4% less than that observed at Unit 14 (54%) and statistically the same (50% to 51%) as that estimated for Unit 13, although it exceeded the FGE of four other operating units at Powerhouse 2. In summer, Units 2 and 6 at Powerhouse 1 also had high FGE estimates, but they only ran 2% of the season (20 and 23 hours, respectively). Most 95% confidence limits on estimates for Powerhouse 1 units were much wider than limits for Powerhouse 2 units because of abbreviated operations that reduced hydroacoustic sample sizes.

Comparing FGE Estimates by Different Sampling Methods

We had the opportunity to compare our estimates of the FGE of turbine units at Powerhouse 2 with estimates by two other methods. The USGS estimated FGE for every unit at Powerhouse 2 based upon the distribution of passage of radio-tagged fish, and the NMFS estimated FGE for modified Unit 15 by gatewell dipping and fyke netting. Comparison with radio tagging estimates of FGE could be examined for more units, but sampling with the hydroacoustics and radio telemetry was not simultaneous as it was for the hours netted at Unit 15 by the NMFS. Scott Evans (USGS) provided radio telemetry estimates and Bruce Monk (NMFS) provided gatewell and fyke-net estimates presented in this section.

All sampling methods are imperfect and each has unique advantages and disadvantages. Radio telemetry can provide data on movements of known fish and is not limited to the area near the dam. Information on travel time, large-scale trajectories, forebay residency, survivorship, and species or origin and even rearing (wild vs. hatchery) differences is potentially available. However, the power of radio telemetry is diminished when the total number of tagged fish is divided among too many treatments or passage routes, resulting in small sample sizes. Also radio telemetry provides no data on untagged animals. The NMFS continues gatewell dipping and fyke netting single units until the number of guided fish captured is adequate to provide a reliable daily FGE estimate. The average number of guided fish taken in 1 to 2 hours in 2001 was about 600 fish. This is substantially more fish than radio telemetry can detect for a single passage route in an entire season. However, netting is labor intensive and may injure or kill fish, including individuals from endangered populations; therefore, it cannot be used for more than a few hours per day at one or two intakes. The restriction of physical capture to one and at the most two or three samples per day prevents biologists from obtaining daily estimates of sample variance or increased resolution of the temporal and spatial variation in FGE.

While hydroacoustic methods can provide FGE estimates that are very comparable to physical capture based estimates, they can only provide a relative index to fish passage unless calibrated by net sampling and they cannot directly provide species-specific estimates. However, hydroacoustic methods can be economically applied to all intakes 24 h per day and provide information about variations among intakes and hours of the day. While hydroacoustic sampling requires more than the 1 to 2 hours needed by netting to obtain reliable FGE estimates, it can provide seasonal estimates for single routes that are not limited by the number of fish sampled. Fixed-aspect hydroacoustics provides estimates for untagged fish and can provide reliable estimates for individual passage routes that usually comport with estimates from more intensive netting methods.

Comparison with Netting Estimates

Concurrent hydroacoustic and netting (NMFS) samples provided FGE estimates for Intake 15b that were very similar in spring and only slightly different in summer (Figure S.1), and estimates were even closer when we estimated hydroacoustic FGE from all nighttime hours instead of just concurrent hours (Figure S.2). Hydroacoustic sampling underestimated the number of guided fish in spring and underestimated the number of unguided fish in summer, according to the lack of overlap in 95% confidence limits (Figure S.1).

Hydroacoustic estimates of FGE require longer sampling durations than the 1 to 2 hours that are commonly used to estimate FGE by netting because hydroacoustic beams sample only about 5% of the cross sectional area of an intake compared to near 100% coverage by netting. In 2001, we were able to sample throughout the night only when the NMFS was conducting orifice passage efficiency testing, and the unit was operated all night. Abbreviated operations severely limited the number of fish that could be detected by hydroacoustics and the precision and accuracy of hydroacoustic estimates. We made up for this shortcoming by using all available hours of nighttime sampling to make seasonal estimates, but the unit usually was shut down for the night after the netting effort ended. Consequently, many of the additional nighttime samples used to estimate hydroacoustic FGE came from nights of orifice-passage tests rather than nights of FGE netting. For future testing, we recommend that operators restart test units after FGE netting ends so that hydroacoustic estimates can be based upon the maximum number of nighttime samples from the same nights that FGE netting was conducted. The NMFS sampled with nets from about 2000 until 2100 or 2200 hours depending upon the number of fish they collected in the dip basket sampling the gatewell. Sampling duration was only as long as needed to obtain a reliable FGE estimate based upon catches of guided fish and knowledge of FGE ranges that were likely.
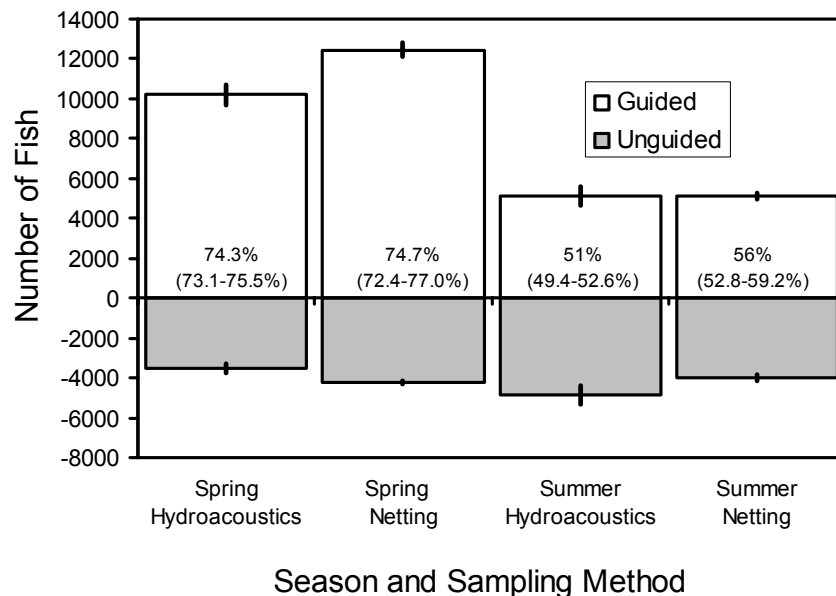

Figure S.1. Plot of the Number of Guided and Unguided Fish Estimated by Concurrent Hydroacoustic Sampling and Netting in Spring and Summer. The percentages inside bars for guided fish are estimates of FGE and numbers in parentheses are 95% confidence limits.
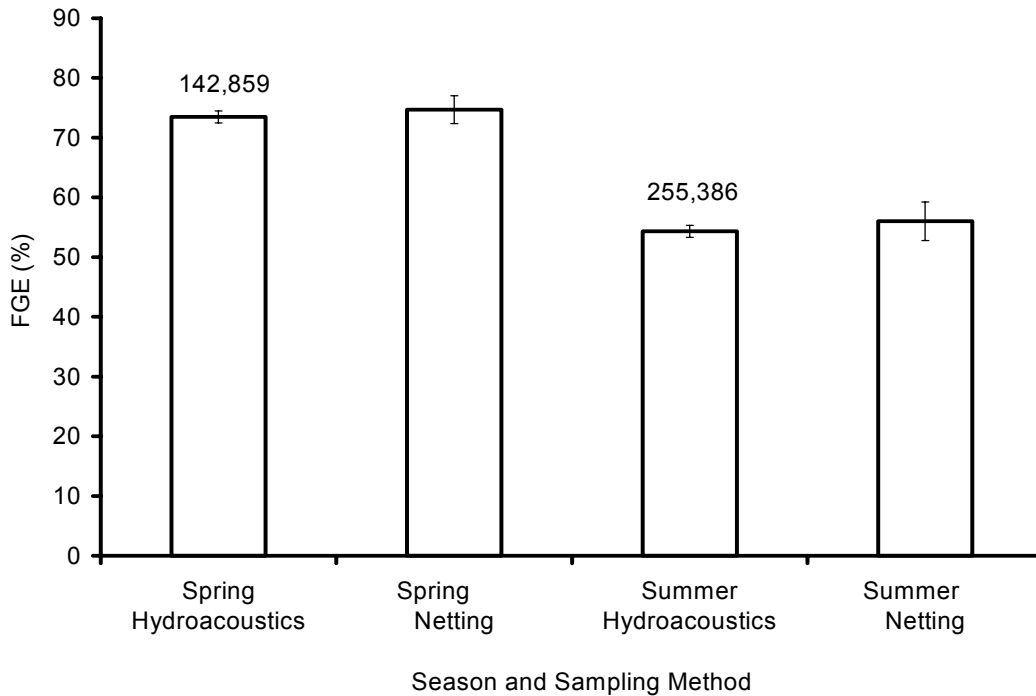
Figure S.2. Plot of FGE Estimates Made from all Nighttime Hours of Hydroacoustic Sampling (2000-0500) Compared to Estimates Based on Netting from about 2000 to 2100 or 2200 h. Vertical bars are 95% confidence limits. The expanded numbers of fish upon which FGE estimates were based are shown above the bars for hydroacoustic sampling each season.

Another problem introduced by on and off operation of a turbine unit is that hydroacoustic beams continue to sample and to record multiple traces from fish that are swimming around in the intake of the unit when it is off. At Unit 15, we carefully threw out all fish detected before or after FGE netting based upon start and end times provided by Bruce Monk (NMFS). Operations data reported at 5-minute intervals, like those available in 2000 and earlier years were much better for accurately assigning zero fish counts to samples collected when units are off.

Comparison with Radio Telemetry Estimates

Our hydroacoustic estimates are reasonably close to radio telemetry estimates, and some of the differences that exist may be attributed to the small sample sizes that are inherent in highly partitioned radio telemetry estimates. Powerhouse unit-specific FGE estimates from radio telemetry were based on from 14 (Unit 18) to 136 (Unit 14) fish in spring and from 15 (Unit 18) to 136 (Unit 14) fish in summer. Inasmuch as those numbers are composed of varying proportions of different species, it is not surprising that radio telemetry estimates sometimes differ. In contrast, unit-specific hydroacoustic estimates are based upon thousands of fish each season. The number of fish captured during 1 to 2 hours of net sampling by the NMFS effort usually is an order of magnitude larger than the number available for radio telemetry estimates for an entire season.

Similar hydroacoustic and netting estimates of FGE for Unit 15 were both 38% to 40% higher than radio telemetry estimates for the same unit in spring, and this may be a function of limited sample sizes of radio-tagged fish. The 38% FGE estimate by radio telemetry in spring was based on only 19 of 50 detected fish for the entire season, whereas netting estimates usually were based upon >10 times that number in just 1 to 2 hours of sampling. The total number of fish counted by concurrent hydroacoustic sampling and netting for spring was 14,687 and 16,651, respectively.

On the unit level, estimates by hydroacoustics were higher than estimates by radio telemetry in five of eight units (12, 13, 14, 15, and 16) in spring and in three of four units for which there were radio telemetry estimates in summer (units 12, 13, and 14; Table S.3). The worst case was a 34% difference at Unit 15 in spring, and the best case was a 1% difference at Unit 11 in spring. Unit 15 was unusual in that it was very intermittent in its operation during high passage hours due to the NMFS FGE studies there. The next largest differences were at units 12 and 14 in both spring (19% in both units) and summer (21% in both units). Hydroacoustic estimates were lower than radio telemetry estimates at units 17 and 18 in spring and at Unit 11 in summer. Estimates were only similar at Unit 11 in spring. Unit-specific differences between the two methods averaged 14.7% for eight units in spring and 13.7% for seven units (Unit 17 did not operate) in summer.

Radio telemetry estimates pooled for four adjacent units were within 11% of similarly pooled hydroacoustic estimates (Table S.3). In spring, the hydroacoustic estimates exceeded radio telemetry estimates by 9% for units 11 through 14 and by only 2% for units 15 through 18. In summer, the hydroacoustic estimates exceeded radio telemetry estimates by 8% for units 11 through 14, and by 11% for units 15 through 18.

Table S.3. Hydroacoustic (HA) and Radio Telemetry (RT) Estimates of FGE for Turbines at Bonneville Dam in 2001. Study times were made comparable for both methods by using data only from 1 May to 9 June for spring and 1 July to 15 July for summer.

Location	HA Estimate	RT Estimate	Difference
Spring			
Unit 11	50%	51%	1% (RT>HA)
Unit 12	59%	40%	19% (HA>RT)
Unit 13	67%	58%	9% (HA>RT)
Unit 14	62%	43%	19% (HA>RT)
Units 11-14	58%	49%	9% (HA>RT)
Unit 15	70%	38%	32% (HA>RT)
Unit 16	60%	48%	12% (HA>RT)
Unit 17	48%	64%	16% (RT>HA)
Unit 18	32%	42%	10% (RT>HA)
Units 15-18	51%	49%	2% (HA>RT)
All PH2	56%	46%	10% (HA>RT)
Summer			
Unit 11	26%	33%	7% (RT>HA)
Unit 12	40%	19%	21% (HA>RT)
Unit 13	48%	38%	10% (HA>RT)
Unit 14	53%	32%	21% (HA>RT)
Units11-14	39%	31%	8% (HA>RT)
Unit 15	52%	34%	18% (HA>RT)
Unit 16	53%	46%	7% (HA>RT)
Unit 17	N/A	N/A	
Unit 18	19%	7%	12% (HA>RT)
Unit 15-18	50%	39%	11% (HA>RT)
All PH2	44%	35%	9% (HA>RT)

Preface

This report was prepared by the Pacific Northwest National Laboratory (PNNL), Richland, Washington, and the Fisheries Engineering Team (FET), U.S. Army Engineer Research and Development Center (ERDC), Vicksburg, Mississippi, with support from MEVATEC Corporation, 1525 Perimeter Parkway, Suite 500, Huntsville, AL 35806, DynTel, 3530 Manor Drive, Suite 4, Vicksburg, MS 39180, the U.S. Army Corps of Engineers - Portland District, and the University of Washington, Seattle.

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Bruce Monk with the National Marine Fisheries Service graciously provided us with his 2001 netting estimates of guided and unguided fish passage for Unit 15 so we could compare them with hydroacoustic estimates from this study. Bruce also provided us with juvenile bypass screen (JBS) data on run timing of juvenile salmonids.

Acronyms and Abbreviations

cfs	cubic feet per second
CFD	computational fluid dynamics
ERDC	U.S. Army Engineer Research and Development Center
ESBS	extended submerged bar screens
FGE	fish guidance efficiency
FPE	fish passage efficiency
ft	feet
h	hour
HA	hydroacoustics
JBS	juvenile bypass system
km	kilometer
M	million
NMFS	National Marine Fisheries Service
PNNL	Pacific Northwest National Laboratory
PSC	Prototype Surface Collector
RT	radio telemetry
s	second
SPE	spill passage efficiency
STS	submerged traveling screens
TIE	turbine intake extension
USGS	U.S. Geological Survey
WES	U.S. Army Corps of Engineers Waterways Experiment Station

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1.0   Introduction

This report presents results of two hydroacoustic studies of juvenile salmonids funded by the U. S. Army Engineers – Portland District and conducted at Bonneville Dam by a team of researchers from Pacific Northwest National Laboratory (PNNL), MEVATEC, University of Washington, Dyntel, and the U.S. Army Corps of Engineers Fisheries Field Unit and Engineer Research Development Center (ERDC). One was a project-wide fish passage efficiency study and the other was a more narrowly focused study of the approach, vertical distribution, and fish guidance efficiency (FGE) of fish at Unit 15. The District extensively modified the gatewell and vertical barrier screen at Unit 15 to determine whether the changes would improve FGE. The District also funded other parallel research on juvenile salmonids in 2001, included a project-wide radio telemetry study by the U.S. Geological Survey (USGS) and a netting study of fish guidance efficiency and orifice-passage efficiency by the National Marine Fisheries Service (NMFS) at Unit 15.

1.1   Background

The U.S. Army Corps of Engineers – Portland District is striving to meet the goal, set in the 2000 Biological Opinion, of maximizing fish passage efficiency (FPE) and obtaining 95% survival for juvenile salmon passing the Bonneville Project. Project FPE is the percent of all juvenile salmon passing the project by non-turbine routes. To estimate project FPE and survival, the proportions of juvenile salmon that pass through all major routes must be estimated.

In a typical water year, the goal of maximizing FPE largely influences operation of the project. Large volumes of spill are presumed to be necessary to compensate for the low fish guidance efficiency (FGE) of screens at both powerhouses, particularly in summer. Spill volumes are, in a typical year, limited to between 50,000 and 75,000 ft^3/sec during the day and up to 120% of the gas cap set to control total dissolved gas supersaturation. The Northwest had an unusually dry year in 2001 and that, combined with high generation demand, led to unusually low spill volumes. Total project discharge in spring was roughly half (46% in spring and 54% in summer) of what it was in 2000. In 2001, the project spilled 16% of the total discharge in spring and 11% in summer, down from 31% and 50%, respectively, in 2000. Total spill volume was less than a quarter (23%) in spring and less than an eighth (12%) in summer of what it was in 2000.

Spill under 50,000 ft^3 / second creates eddies and slack water areas in the spillway tailrace. Excessive predation is assumed in the tailrace where currents do not quickly carry fish downstream. Spill levels above 75,000 ft^3 / second during the day can lead to high numbers of adult salmon falling back through the spillway, as adults exit the Bradford Island ladder and follow the shoreline around to the spillway forebay. Adult salmon do not pass through the ladder at night, and therefore spill can be increased in an attempt to reach 80% FPE for a 24-hour period. However, spill above 120,000 ft^3/second typically causes total dissolved gas (TDG) levels to exceed 120% saturation. State water-quality standard waivers allow supersaturation up to 120%. Levels of TDG above this may result in greater fish mortality than would occur if spill was reduced and more fish were passed through the turbines.

The Portland District acquired mobile hydroacoustic data on fish distributions in both powerhouse forebays at Bonneville Dam in 1996 (Ploskey et al. 1998) and 1997 (BioSonics Incorporated 1998). For Powerhouse 1, these data indicated that higher average fish densities occurred upstream of Units 4 through 6 in spring and upstream of Units 4 through 6 and 8 and 9 in summer. For Powerhouse 2, average fish densities were highest upstream of Units 11 through 13 adjacent to the south eddy and sluice chute in spring and in summer. Fish densities also were high upstream of Unit 18 in 1996 but not in 1997. Vertical distribution data showed that most fish were in the upper 15 m of the water column. The low fish guidance efficiency of many submerged traveling screens at Bonneville Dam would not be expected from an examination of the vertical distribution data collected within 10 m of the dam. If fish did not alter their vertical distribution from what was observed in forebay areas, data from 1996 and 1997 would suggest that fish guidance efficiency usually would exceed 80%. Data acquired from in-turbine sampling and from fixed up-looking transducers deployed on the bottom of the Powerhouse 2 forebay in 2000 also indicated that FGE estimates were much lower than expected from vertical distributions in the forebay.

Diel (24-hour) patterns of smolt passage are not uniform regardless of whether passage is estimated in sluiceways (Uremovich et al. 1980; Willis and Uremovich 1981) or the juvenile bypass system (JBS) (Hawkes et al. 1991; Wood et al. 1994). Diel passage through the JBS often has a bimodal distribution with a major peak occurring just after dark and a minor peak after sunrise. In contrast, passage through sluiceways usually is higher during the day than at night (Willis and Uremovich 1981). However, patterns apparently are influenced by the operation of sluice gates (Uremovich et al. 1980), flow, unit outages, and species (Willis and Uremovich 1981). Netting required to estimate FGE is intensive but because netting is limited to a few hours per day, it does not provide diel information. Diel patterns of fish passage above and below screens were estimated in spring and summer 1996 for randomly selected intakes of every turbine at Powerhouse 2 and every intake of Units 3 and 5 at Powerhouse 1. Estimates also were made in the spring and summer of 1998 and 2000. These indicate that fish passage through turbines usually is higher at night than it is during the day (Ploskey et al. 2001a; Ploskey et al. 2002a).

Available data indicate that the horizontal distribution of smolt passage among intakes is not uniform. Gatewell sampling has indicated that the number and location of operating units and sluice gates as well as the species of smolt determine lateral distributions of juvenile salmon at Powerhouse 1 (Willis and Uremovich 1981). Interactions among factors may account for a lack of consistency in measures of horizontal patterns by Uremovich et al. (1980), who found fish concentrated at units 6, 7, and 10; Willis and Uremovich (1981), who found variable patterns depending on operations; and Krcma et al. (1982), who observed most passage at units 4 through 6. Much of the FGE data collected at Powerhouse 2 with in-turbine hydroacoustics (e.g., Magne et al. 1989; Stansell et al. 1990) and netting (Gessel et al. 1988; Muir et al. 1989) are of limited value for evaluating the horizontal distribution of passage because they typically focused on one or two units at a time. The Fishery Field Unit attempted hydroacoustic sampling of juvenile salmon passing through several spillway gates in the mid 1980s. Transducers were mounted on the bottom of gates and aimed upward and out from the gate. Apparently, noise generated by sound echoing off of vortices at some gates masked echoes from juvenile salmon and prevented equalized sampling efforts among gates. BioSonics tested several methods for sampling spillway passage in 1997 (BioSonics 1998). Their best approach was to mount their transducers on piers and aim them toward the ogee just upstream of the gates. BioSonics also designed a mount to deploy transducers and estimate passage through the second powerhouse sluice chute. Transducers were placed at the bottom center of the upstream bulkhead slot and aimed vertically and slightly upstream.

Vertical distributions of juvenile salmon sampled by fixed-aspect hydroacoustics also vary seasonally and daily but this information has not been considered for improving juvenile fish passage at Powerhouse 2. For example, late spring and summer operations at Powerhouse 2 now prioritize the use of turbines 11 and 18 for adult salmon attraction. However, previous studies clearly showed that these units have the lowest FGE for juveniles passing downstream and that juvenile passage through Unit 11 is exceptionally high relative to other units at Powerhouse 2. The FGE of traveling screens was highest at units near the center of the second powerhouse. If Units 11 and 18 did not have turbines or had turbines with much more benign passage conditions than those presently installed, current operations would benefit both adults and juveniles. However, given the low FGE at units 11 and 18 in summer, 85% to 90% of the juvenile fish passing Powerhouse 2 go through turbines rather than the bypass.

In the 1980s and early 1990s, hydroacoustics also has been used on limited spatial and temporal scales to evaluate sampling potential or relative passage among a few routes. Thorne and Kuehl (1989) evaluated the effects of noise on hydroacoustic assessment of passage within several turbines of Powerhouse 1. Results showed that acoustic sampling is feasible at the units they tested. Magne et al. (1986, 1989), Magne (1987) and Stansell et al. (1990) made hydroacoustic estimates of FGE for turbine units 11 and 17 and found estimates were closer to netting estimates by the National Marine Fisheries Service (NMFS) when they sampled longer than just a few hours with hydroacoustic gear.

A corner collector is being designed for the south end of the second powerhouse. Ploskey et al. (1998) and BioSonics (1998) found high densities of fish upstream of units 11-13, and Unit 11 had the highest passage of any intake sampled in 1996. Like the Fisheries Field Unit in previous years, BioSonics found that large numbers of fish passed through the sluice chute when that route was available. However, is it not known what contribution the sluice chute or a corner collector could make to guidance at Powerhouse 2 or to project-wide FPE. Data from Ploskey et al. (1998) indicated that the combined FGE of Units 11, 12, and 13 was only 35%. However, operation of the chute increased the combined FGE to 87% after sluice passage was added to the guided fish terms. This finding could be significant because 1996 mobile hydroacoustic sampling indicated that there was a 2:1 skew in the distribution of fish toward the south end of Powerhouse 2. An important factor contributing to successful fish passage in 1998 was removal of one half of the turbine intake extensions (TIEs), which increased lateral flow toward the sluice chute. When in place, TIES reduce lateral flows along the face of the powerhouse.

At Bonneville Dam First Powerhouse, the Portland District evaluated two distinct smolt bypass approaches, surface flow bypass and extended-length submersible bar screens, from 1998 through 2000. The year 2001 was scheduled for a decision on which complement of smolt passage devices to emphasize for long-term smolt protection at Powerhouse 1. The Corps prepared a special document, called the decision document, to analyze the relative merits of surface bypass and screens at B1.

Research conducted on surface flow bypass from 1998 through 2000 was summarized by Johnson and Carlson (2000). The goal of the surface flow bypass program was to develop and evaluate surface bypass and collection prototype concepts that would lead, if justified by prototype test results, to permanent systems for improving survival of juvenile salmon. In 1998, a prototype surface collector (PSC) was installed at Units 3-6 and was extensively studied (see Johnson and Giorgi 1999 for a review). In 1999, limited research occurred to prepare for tests in 2000. In 2000, the PSC was extended from Units 3-6 to also cover Units 1-2, because a noticeable number of smolts were observed in 1998 and 1999

to move obliquely from north to south along the face of the PSC. A thorough evaluation of the PSC was conducted in 2000 as part of the Anadromous Fish Evaluation Program (AFEP). The 2000 PSC evaluation emphasized forebay fish behavior as well as PSC performance, i.e., efficiency and effectiveness. It included the following biological research (AFEP study codes in parentheses):

- fixed radio telemetry to determine species-specific PSC performance and movement patterns for yearling chinook salmon and steelhead (SBE-P-95-6)

- acoustic telemetry to study three-dimensional movement patterns and PSC performance on a species-specific basis (SBE-P-00-14)

- fixed hydroacoustics to estimate fish passage rates to determine PSC performance for the run-at-large (SBE-P-98-8a)

- multi- and split-beam hydroacoustics to assess fish movements near the PSC (SBE-P-98-8b)

- numerical modeling to integrate hydraulic data from a computational fluid dynamics model with three-dimensional fish movement data (SBE-P-00-13).

A hydroacoustic evaluation was conducted because radio telemetry only provides data on individuals of species and age classes that are chosen for study whereas hydroacoustics samples the run at large. Estimates of FPE can be made by radio telemetry, but only for tagged fish and under the assumption that tagged fish behave like untagged fish. Radio telemetry provides species-specific information, reservoir passage routes and rates, forebay delay times, and other insights that hydroacoustics cannot, but it cannot provide the robust horizontal and vertical distribution information for assessing changes in fish passage or for suggesting improvements in interception facilities. Telemetry sample sizes sometimes are too small when divided among 36 or more passage routes at a project. Hydroacoustic sampling not only provides overall measures of Project performance, but also can indicate where improvements can be made and what kind and how much of a change might be required. For example, vertical distribution data of fish passing through turbines can provide estimates of FGE for existing screens or for proposed screens or surface collectors assuming that the interception point was lower in the water column. The ability to ask such "what if" questions for run-of-river fish is a unique strength of hydroacoustic sampling. In addition, continuous hydroacoustic sampling allows for regression of performance measures (such as spill efficiency) on continuous operations data such as spill volume. These types of regressions can suggest Project operations to optimize juvenile fish passage at a project. Provision of continuous fish-passage data on run-of-river fish is a unique strength of hydroacoustic sampling.

1.2 Site Description

Estimation of FPE and quantification of any enhancement by fish guidance devices is difficult because the Bonneville Project is among the most complex on the Columbia River. From the Oregon shore north toward Washington, the project is composed of a navigation lock, a 10-unit Powerhouse 1, Bradford Island, an 18-gate spillway, Cascades Island, and an 8-unit Powerhouse 2 (Figure 1). Principal passage routes include the spillway and two powerhouses, but within each powerhouse, fish passage can be through ice/trash sluiceways, turbines, or the juvenile bypass system (JBS). Smolts enter the JBS after they encounter screens in the upper part of turbine intakes and are diverted to gatewell slots and orifices opening to a bypass channel. In 2000, Units 1-6 at Powerhouse 1 were modified to create a prototype

surface collector (PSC) for testing the efficacy of deep-slot surface collection (Ploskey et al. 2002a). The PSC was removed before the beginning of the 2001 passage seasons.
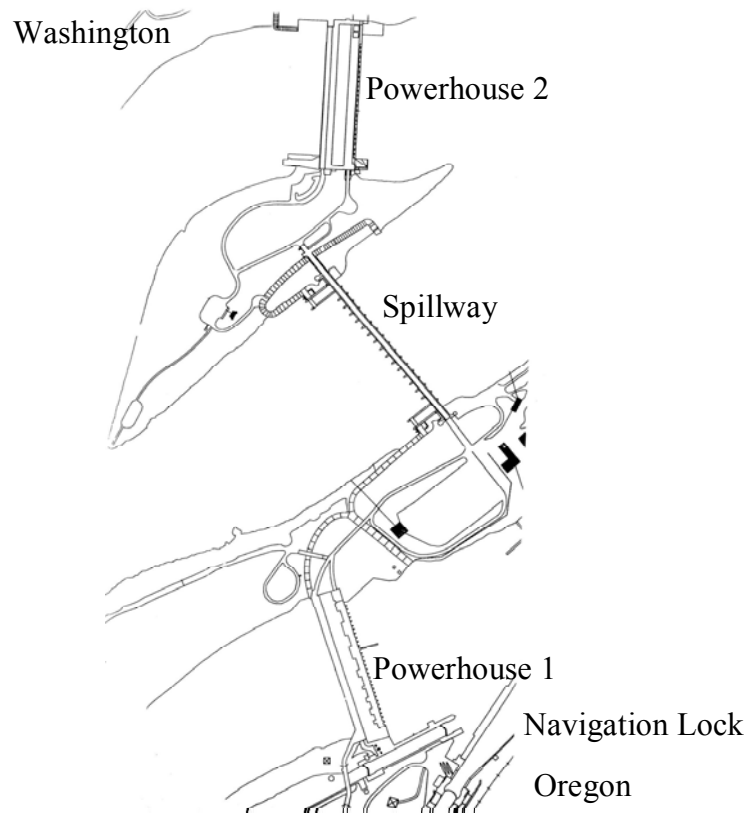
Figure 1. Plan View of the Bonneville Dam Project

1.3 Goals

The goal of the larger of the two studies was to provide project-wide estimates of FPE, spill efficiency, and spill effectiveness for run-of-river fish passing the Bonneville Project during the 2001 out-migration. It is the second full-project hydroacoustic study of fish passage at Bonneville Dam. The first was conducted in 2000 (Ploskey et al. 2002a). This type of study also provides estimates of the horizontal, vertical, and diel distributions of fish passage and FGE by turbine unit. These data will provide a baseline for evaluating the performance of future management efforts to improve juvenile fish passage. The goal of the second study was to assess the effect of gatewell and vertical-barrier-screen modifications on the FGE of Unit 15.

1.4   Objectives

Two evaluations were conducted: a project-wide evaluation and a study of Unit 15.

1.4.1   Project FPE Evaluation

1. Estimate the proportion of smolt-sized fish that pass the project above and below in-turbine screens, through sluiceway openings with water depths > 1 m, and via the spillway each season.
2. Estimate spill efficiency and effectiveness by season and for spill periods.
3. Characterize the vertical and lateral distributions of smolt-sized fish passing through Powerhouses 1 and 2 and the spillway.
4. Describe day-night changes in vertical and lateral distributions of smolt-sized fish passing Powerhouses 1 and 2 and the spillway.

1.4.2   Unit 15 Evaluation

1. Determine average trajectories of juvenile salmon by elevation and distance upstream of trash racks through three successive hydroacoustic sample volumes aligned in a downstream-upstream direction.
2. Determine the vertical distribution of smolts from the top of the intake to the bottom of the forebay within three successive hydroacoustic sample volumes to determine how distributions change as fish approach the trash racks.
3. Use in-turbine up- and down-looking hydroacoustic beams to determine the vertical distribution of fish downstream of trash racks and to provide independent estimates of FGE from the National Marine Fisheries Service (NMFS) netting effort at the same unit.
4. Determine whether the distribution and behavior of fish upstream and downstream of the trash racks explain why FGE decreases from spring through summer.

2.0   Materials and Methods

2.1   Equipment

We sampled Powerhouse 1 turbines with four hydroacoustic systems, the spillway with three systems, and Powerhouse 2 turbines and forebay with four systems. Each system consisted of an echosounder, cables, transducers, an oscilloscope, and a computer system. Each echosounder and computer was plugged into an uninterruptible power supply. An echosounder generates electric signals of specific frequency and amplitude and at the required pulse durations and repetition rates, and cables conduct those transmit signals from the echosounder to transducers and return data signals from the transducers to the echosounder. Transducers convert voltages into sound on transmission and sound into voltages after echoes return to the transducer. The oscilloscopes were used to display echo voltages and calibration tones as a function of time, and the computer system controlled echosounder activity and recorded data to a hard disk. The 420 kHz, circular, single- or split-beam Precision Acoustic Systems (PAS) transducers were controlled by PAS 103 echosounders and Hydroacoustic Assessments' HARP software running on Pentium-class computers.

2.2   Calibrations

Before deployment, all hydroacoustic equipment was transported to Seattle, Washington, where PAS electronically checked the echosounders and transducers and calibrated the transducers using several standard transducers. After calibration, we calculated receiver gains to equalize the output voltages among transducers for on-axis targets ranging in hydroacoustic size from –56 to –36 dB $\| \ 4\pi m^2$ (Appendix A). Lengths of fish corresponding to that acoustic size range would be about 1.3 and 12 inches, respectively, for fish insonified within 21° of dorsal aspect (Love 1977). Inputs for receiver-gain calculations included calibration data (i.e., echosounder source levels and 40 log [range] receiver sensitivities for specific transducers and cable lengths) and acquisition equipment data and settings (installed cable lengths, maximum output voltage, and on-axis target strengths of the smallest and largest fish of interest). In most instances, calibrated and installed cable lengths were identical. When installed cable lengths differed from calibrated cable lengths because we had insufficient cable for a deployment, we used an empirically derived correction factor to compensate for cable length effects on source levels, receiver sensitivity, and receiver gain settings.

2.3   Transducer Deployments and Sampling Schemes

This section describes hydroacoustic deployments and sampling schemes with text and figures. We also describe technical details about transducer locations and aiming angles in Appendix B.

2.3.1   Sampling Powerhouse 1

In turbine units 1-10, we sampled one randomly selected intake slot out of three per unit. We mounted one upward- and one downward-angled, 6° transducer in the selected slots to monitor guided and unguided passage, respectively (Figures 2.1 and 2.2). The lateral location of both transducers within the same intake was randomly selected to be on the north, center, or south side of the trash rack

(Appendix B) so that some of the lateral variation in passage within intakes would be captured in the variance estimate for the entire powerhouse.
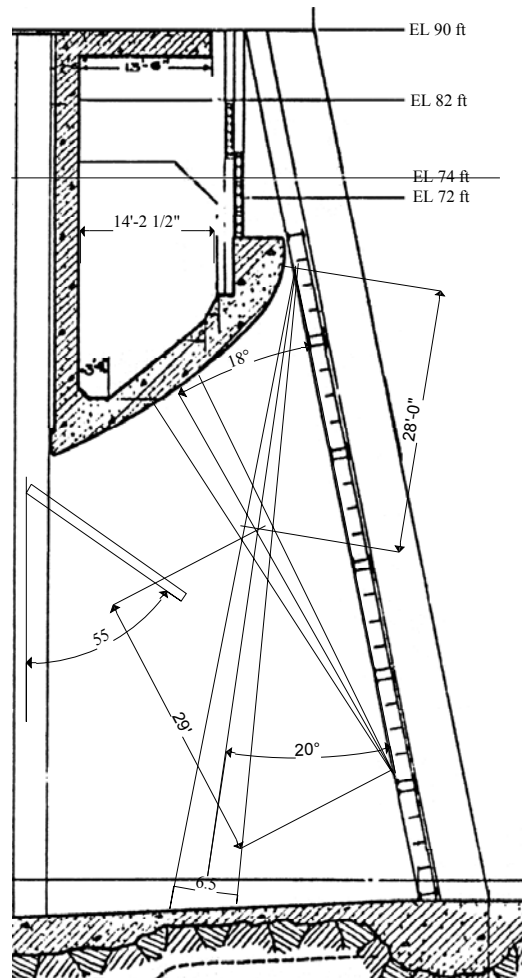
Figure 2.1. Cross Sectional View through a Powerhouse 1 Intake like those Sampled in Units 1-7, 9, and 10. The drawing shows up- and down-looking hydroacoustic beams, aiming angles, and cutoff ranges for sampling guided and unguided fish. Minimum ranges for sampling guided and unguided fish were 8.53 and 8.84 m, respectively.

Transducers deployed in units 5 and 10 were 6° split-beams to provide target strength data for detectability modeling. Sampling the 40-ft-long extended submerged bar screen (ESBS) at Unit 8 required a different deployment of transducers. Fish passing above and below the ESBS of Unit 8 were sampled with upward- and a downward-angled, 6°, single-beam transducers to estimate guided and unguided numbers, respectively, but the down-looking transducer was mounted on the downstream side of the ESBS instead of on trash racks (Figure 2.2). Therefore, fish passage at Unit 8 could differ from estimates at other Powerhouse 1 units for a variety of reasons, e.g., screen type, unit location, intake selected for sampling, and differences in detectability among deployments. Our modeling of and correction for differences in detectability among deployments should have minimized the last effect. Paired transducers in every intake were fast multiplexed to acquire 20 1-minute samples from each intake per hour. The pulse repetition rate was 15 pings per second for every transducer.
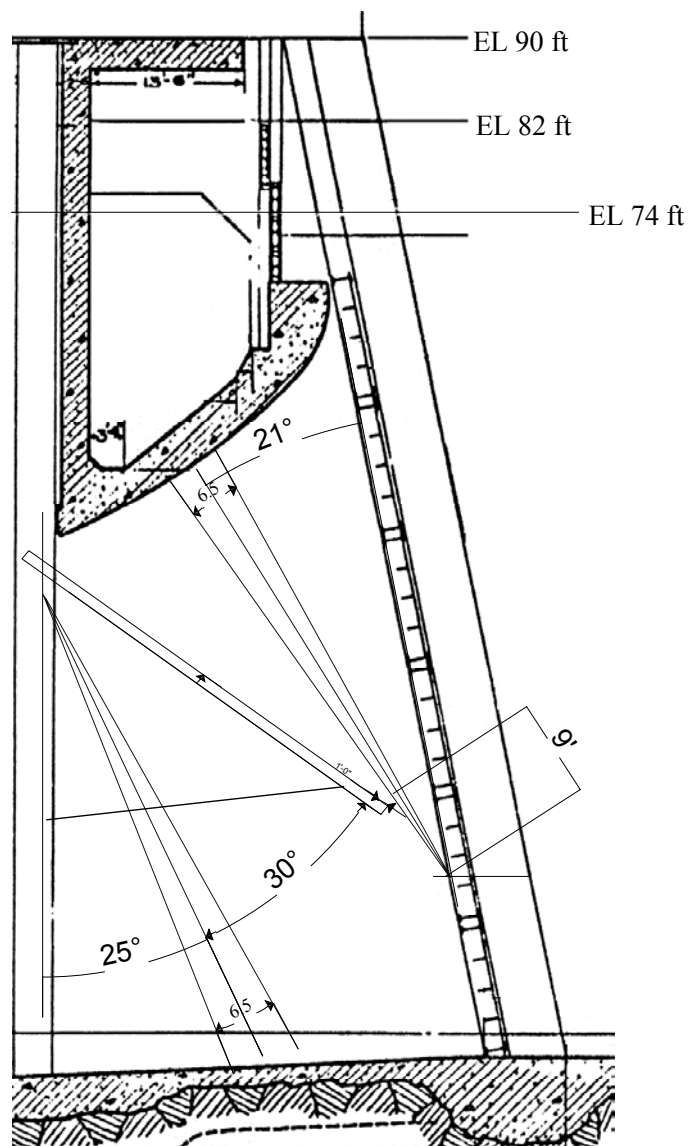
Figure 2.2. Cross-Sectional View through Intake 8b Where Up- and Down-Looking Single-Beam Transducers Were Used to Sample Guided and Unguided Fish, Respectively. Minimum ranges for sampling guided and unguided fish were 3.1 and 2.7 m, respectively.

2.3.2 Sampling the Spillway

Spill bays 2, 4, 5, 6, 7, 8, 10, 12, 14, and 15 were each sampled with one down-looking, 10°, single-beam transducer, and Spill Bay 17 was sampled with one down-looking, 12°, split-beam transducer. Bays were selected to allow interpolation of fish passage to bays that were not sampled and to emphasize sampling at gates that would pass the most water according to the 1999 Fish Passage Plan. Transducers were mounted 28 ft below the tops of spill gates and aimed upstream 8° (single beams; Figure 2.3) or 15° upstream for the split-beam transducer (Appendix B). Transducers were at EL 59 ft when operators opened a gate about 3 ft, which was the maximum opening observed in 2001. The lateral location of each

transducer within a bay was randomly selected to be on the north, center, or south side so that some of the lateral variation in passage within bays would be captured in the variance estimate for the entire spillway.

Severe drought in 2001 limited the number of spill days each season. When there was spill, it was set at about 50,000 cfs day and night. Transducers were sampled sequentially to allow a pulse repetition rate of 30 pings per second during each of 12 1-minute samples collected by each transducer per hour.
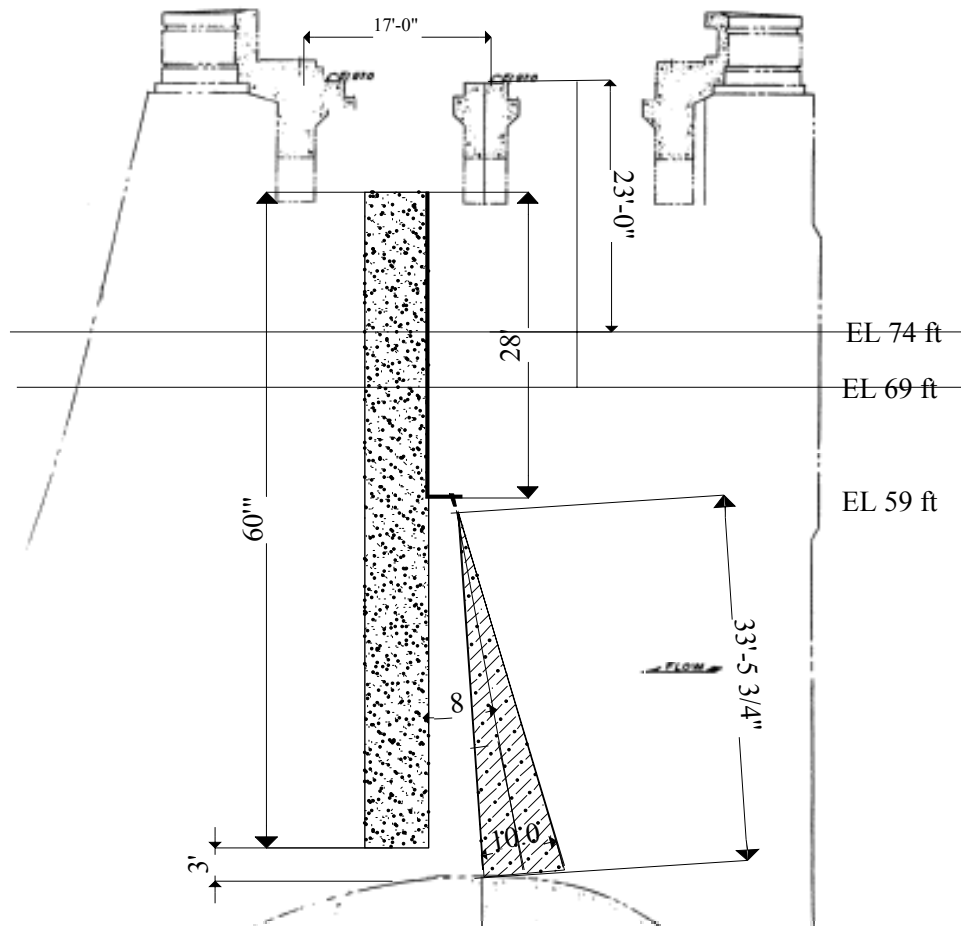
Figure 2.3. Cross-Sectional View through a Spill Bay at Bonneville Dam. The diagram shows a transducer mount on the upstream side of a spill gate and the orientation of the hydroacoustic beam. Flow was from right to left through the beam. The gate opening of about 3 ft was the maximum observed in 2001. The minimum range for sampling spilled fish was 2.4 m from the transducer.

2.3.3 Sampling Powerhouse 2

At Powerhouse 2, one out of three intakes at every turbine unit was randomly selected for sampling, and at Unit 15 we sampled both the b and c intakes. Three transceivers and computers were used to control the 18 transducers. The lateral locations of transducers within intakes also were randomized among north, center, and south locations (Appendix B). In each intake, we mounted a pair of transducers on the downstream side of the trash racks (Figure 2.4; Appendix B). One transducer of each pair was mounted near the bottom of the uppermost trash rack and aimed downward to sample unguided fish

passing below the traveling screen. The second transducer of each pair was mounted near the bottom of the fourth trash rack from the top and aimed upward to sample fish passing above the screen. The lateral location of both transducers within the same intake was randomly selected to be on the north, center, or south side of the trash rack (Appendix B). The two transducers deployed in Unit 18 were split beams to provide target strength data.
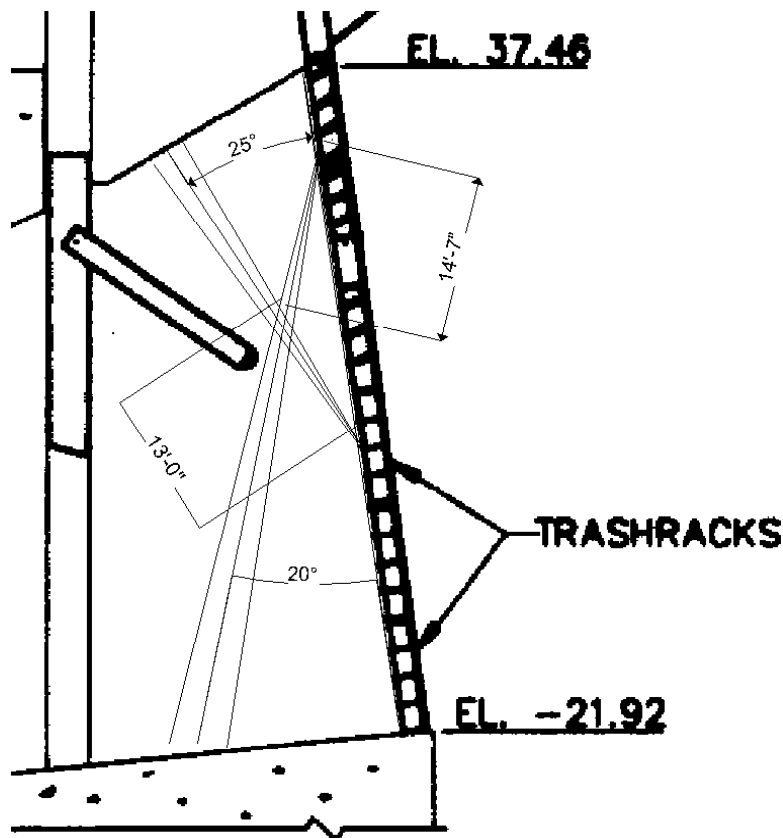
Figure 2.4. Cross-Sectional View through a Powerhouse 2 Turbine Showing Up- and Down-Looking Transducer Beams and Cutoff Ranges for Classifying Fish as Guided or Unguided. Minimum ranges for sampling guided and unguided fish were 3.96 and 4.44 m, respectively.

Each transducer transmitted sound pulses at 15 pings per second, and both transducers of a pair usually were sampled simultaneously (i.e., fast multiplexed). Fast multiplexing allowed us to estimate covariances for the simultaneous samples of guided and unguided fish and to collect 30 1-minute samples at Intake 15b and 15 1-minute samples per hour at all other intakes including 15c. We always employed simultaneous sampling on units 15 through 18. We also used simultaneous sampling for units 11 through 14 on days when the NMFS was conducting FGE testing at Unit 15, when we were not trying to operate forebay transducers upstream of Intake 15b. However, we sampled transducers of each pair in units 11 through 14 sequentially for 30 s each from 0000 through 1600 h on days when the NMFS was conducting orifice-passage efficiency (OPE) studies at Unit 15, and we were operating three forebay transducers at Intake 15b at the same time (Figure 2.5).

Slow multiplexing transducers in units 11-14 during OPE tests eliminated extensive interference of acquired signals that we encountered when we first tried fast multiplexing transducers in Units 11 through 14 and slow multiplexing forebay transducers upstream of trash racks at Intake 15b. The three transducers in the forebay (Figure 2.5) were for sampling vertical distributions and the azimuth direction of travel of fish upstream of Intake 15b. They consisted of down-looking 6° split-beam transducers deployed on a steel beam lowered to a depth of 70 ft MSL in the trash-rack slot.
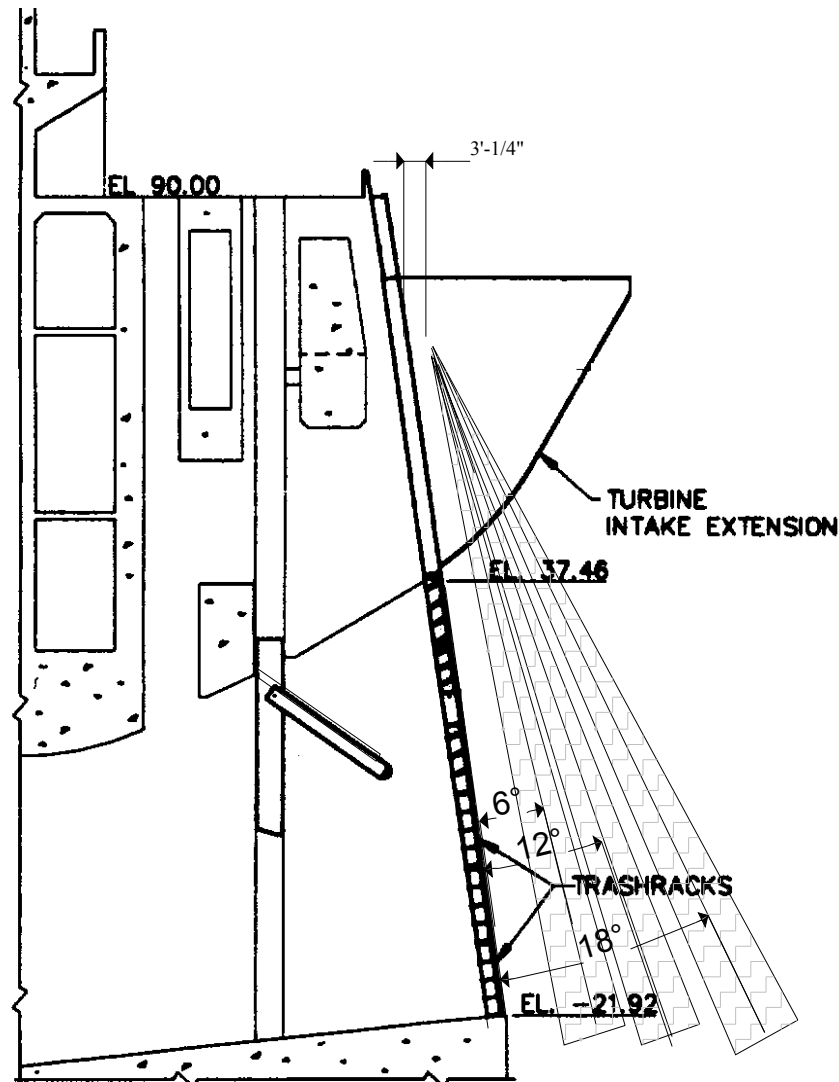
Figure 2.5. Cross-Sectional View through Intake 15b at Bonneville Dam Powerhouse 2 in Spring and Summer 2001 Showing Three Down-Looking Beams from Split-Beam Transducers

2.4 Fish Tracking and Filtering Criteria

Since the hydroacoustic sampling effort on Bonneville Dam was so extensive and generated such a large volume of data in 2001, we could not feasibly manually process enough data to make reliable fish-

passage estimates with available staff. Therefore, we relied on autotracking software developed over the last four years by the Fisheries Field Unit, the Waterways Experiment Station (WES), and PNNL to process raw data into tracked fish observations. The autotracker software tells the processing computer to:

1. Identify and remove echoes at constant range from structure.
2. Find seed echoes for candidate tracks.
   Go to every echo.
   Define a 10-ping by 1-m window centered on that echo.
   Place all echoes in the window into 5-degree angle bins.
   If any bin-count >3, flag the center echo as a candidate seed.
3. Re-examine candidate seed echoes.
   Go to every seed-echo window.
   Count echoes in all possible line features (Hough transform).
   If no echoes in the window are part of a strong line feature then drop the seed echo (to distinguish between dense noise and dense fish tracks).
4. Initiate alpha-beta tracking.
   Track forward, starting at each seed echo.
   Track backward from the same seed echo after forward tracking has ended.
   Check the track segment against criteria (core criterion; minimum and maximum gap).
5. Link track segments that are collinear into single tracks. This involves projecting the first track segment forward and the second segment backward and linking them into one fish if the ping gap ≤ 20 pings and the two segments line up and meet a track link criteria.
6. Write out track statistics (echo statistics optional).

We describe and present autotracker parameters and the settings used to process the 2001 data in Appendix C. During most of spring and early summer, we reviewed samples of the autotracker's performance for every deployment on a fish-by-fish basis to evaluate and fine-tune the autotracker and to develop post-processing filters for eliminating false traces from the autotracker's output. We released the autotracker to process data for a given deployment only after we determined that it was missing few of the echo patterns that we would have tracked.

In Appendix D, we describe criteria and present Statistical Analysis System code used to reject non-fish traces that the autotracker selected. In another part of the processing program, we eliminated fish detected at ranges less than those described in legends of Figures 2.1 through 2.3. Filtering non-fish traces based upon variables like range, slope, and noise level is a critical part of using autotracking software, because the autotracker is more likely to track intermittent series of structural echoes or noise than are technicians. Filters were designed to eliminate echo traces that had a high probability of being from structure, noise, or non-target fish based upon their track statistics.

Filtering American shad traces selected by the autotracker in summer was a difficult problem that was pervasive in 2001 because the peak of the American shad run arrived at least two weeks earlier than in most years. In echograms, shad usually can be recognized because they occur in schools, unlike salmon smolts that usually pass through beams as single traces. It is rare to detect more than one or two smolt traces in close proximity in time or space inside turbine intakes. In addition, few of the traces in these schools had ping gaps and the average number of echoes per trace often exceeded 10. In heavy shad

passage events, it was common to detect > 30 traces in a 1-min sample. Shad schools were almost never observed in down-looking beams sampling unguided fish, but they were common in up-looking beams sampling guided fish in some turbines.

Our approach to filtering shad schools was to find obvious schools of shad in echograms from up-looking split-beam transducers and statistically characterize the distribution of average target strengths of those fish. Most of the fish in those schools had target strengths > -49.2 dB (about a 4-inch-long fish when insonified about 30° off ventral aspect); thus, these were too big to likely be sub-yearling smolts. Using echo strength to filter shad detected with single-beam transducers is imperfect because large fish on the edge of a beam return lower amplitude echoes that are not adjusted for the fishes' position in the beam. After comparing the central tendency of target and echo-strength distributions, we decided to use an echo-strength filter of –51.5 dB to filter shad from single-beam samples of guided fish. This conservative setting may have filtered some larger smolts, but it reduced the probability of sample contamination by shad. Maximum target or echo strengths used to filter shad were deployment specific and depended upon the aiming angle of each transducer. We used Love's (1977) equations relating target strength to fish length and insonification angle to find corresponding maximum target strengths for 4-inch-long fish in each deployment. We are working on other ways to filter American shad from summer samples using criteria such as the density of traces in range and time and the number of consecutive echoes without gaps, but for now target strength or a roughly equivalent echo-strength is the filter of choice.

Although the autotracker was a very efficient tool, we evaluated its performance and post-processing filters in both seasons by comparing counts of fish by the software and by trained technicians. Although five of our six human trackers each had from one to three years of previous tracking experience, we did extensive training and testing on raw hydroacoustic data from previous years and from early 2001 data before the 2001 tracking season began. Every technician and the autotracker processed identical Powerhouse 2 data sets acquired early, mid, and late each season, but the abbreviated generation schedule at Powerhouse 1 left few options for data set selection there. We selected spillway samples from throughout the abbreviated spilling seasons. Fish count data, in the form of computer files that include statistics for each trace, were processed the same as are autotracked fish counts to produce temporally and spatially expanded hourly passage estimates. Results from the technicians provided an estimate of inter-tracker error and deployment-specific mean hourly estimates for comparison to the autotracker-based estimates. We used this approach because fish counts, even for the same files, can vary widely among human trackers (Ploskey et al. 2001b; 2002). Given the demonstrated wide range of interpersonal variation, we compare our autotracker's results to mean human estimates rather than to any one person's estimates.

It is important that autotracker and human-tracker quality control checks be made at the proper level, the transducer channel. We compared human and autotracked counts for each transducer (channel) because there are important differences in passage characteristics, ranges of interest, trace slopes and lengths, and noise conditions for each deployment site and aiming angle. Last year, we discovered that comparing at the system level, which involves several transducer channels with different deployments, could mask error (Ploskey et al. 2002). Up-looking-transducer channels sampling guided fish have very different noise regimes from down-looking-transducer channels and the slopes of regression lines fitted to autotracker and mean human counts often differ too. They can even vary in opposite directions, so that up-looking-transducer channels have higher autotracked counts and down-looking transducer channels

have higher human-tracked counts. In those cases, comparing at the system level would mask some of the disagreement between the humans and the autotracker.

Each tracker's output, whether from a human or from the autotracker, is processed with a channel-specific software "filter" that automatically rejects traces that do not meet specific criteria. Output files from each human or automatic tracker were post processed identically. Post-processing included deployment-specific "filtering" for trace length, trace slope, echo or target strength, structure, and other regular noise, and other characteristics described in Appendix D. The resulting filtered fish counts on each day were then summed separately by the transducer channel that was sampled. We also compared cumulative temporal deviations among trackers by cumulative counts over time.

2.5   Adjustments to Fish-Passage Estimates

After regressing average technician counts on autotracker counts for each deployment, we used slopes of regression lines with intercepts forced through zero to convert autotracker counts into mean technician counts and thereby remove systematic bias in autotracker counts among deployments. Slope multipliers in spring were 0.96 (Powerhouse 1 unguided), 0.83 (Powerhouse 1 guided), 0.833 (Powerhouse 2 unguided), 0.754 (Powerhouse 2 guided), and 0.789 (spillway). Slope multipliers in summer were 0.985 (Powerhouse 1 unguided), 0.953 (Powerhouse 1 guided), 0.841 (Powerhouse 2 unguided), 0.678 (Powerhouse 2 guided), and 0.98 (spillway). Variances were multiplied by the square of the slope factors. Plots of the regressions of mean technician counts on autotracker counts are presented in the Results section of this report.

After the Anadromous Fish Evaluation Program Research Review (13-16 November), where we found that hydroacoustic estimates of fish spill efficiency and effectiveness were considerably higher than were those from radio telemetry, we examined the azimuth direction of travel of fish through the down-looking split beam at the spillway. We found 7% to 13% of the fish in spring and 6% to 10% in summer not moving in a downstream direction. Some of the percentage of upstream-moving fish could have resulted from error in the way direction of travel was estimated this year. The azimuth estimates were based upon positions of the first and last echoes in a fish trace. This approach has some error associated with it because inaccurate phase data for one or both echoes could result in inaccurate positioning of the echoes in three-dimensional space and an error in the estimated direction of travel. Phase data can be corrupted by having fish echoes near noise echoes, structure, or other fish echoes at the same range. A better approach and the one that will be used in future years would be to determine the direction of travel based upon a line fitted to all echoes in a fish trace. This will be less susceptible to error because it will depend upon position estimates for more than just two echoes.

We decided to apply a conservative estimate of the number of fish passing through the spillway, rather than counting only the fraction of fish moving in a downstream direction. Instead, we estimated the downstream flux of fish per hour and multiplied hourly counts of fish in all spillway beams by that factor. The fish-flux factor is more conservative than multiplying by the fraction moving downstream because it subtracts the upstream fraction from the downstream fraction. For example, if 90% of detected fish are moving downstream and 10% are moving upstream, the flux factor applied would be 0.8 instead of 0.9. We consider this to be the most appropriate because upstream moving fish have the potential to be counted more than once and should be subtracted from the passage estimate. In reality, all we know is that some fish moving upstream could have been counted more than once and that the flux factor should

be somewhere between 0.8 and 0.9. We could have split the difference and used 0.85, but we wanted to be certain not to overestimate spillway passage in a drought year. Flux factors applied in spring were 0.74 from 0800 to 1700 hours, 0.86 from 2000 to 0400 hours, and 0.80 during crepuscular hours (0500-0700 hours and 1800 or 1900 hours). Flux factors applied in summer were 0.80 from 0800 to 1700 hours, 0.88 from 2000 to 0400 hours, and 0.84 during crepuscular hours (0500-0700 hours and 1800 or 1900 hours).

2.6   Dam Operations and Fish Passage

Hourly operations data, including discharge by spill bay and turbine unit, were provided by Bonneville Dam operators, who recorded results in a spreadsheet. Hourly operations data were integrated with fish passage data, and fish passage was set to zero when passage routes were closed. When flow is low at a closed turbine unit or spill bay, a fish can stay in the beam much longer than when the passage route is open. A transducer samples continuously regardless of operations, and samples from closed turbine units and spill bays often include many traces that may be tracked as fish, often multiple times, when a turbine unit is off or a spill bay is closed. It is best to have operations data at 5-minute intervals so that hourly passage estimates are not inflated by multiple fish detections during the fraction of an hour when a turbine was off. For that reason, we set fish passage to zero if hourly discharge through a turbine was less than 65% of the maximum discharge on a given day.

When discharge is less that 65% of the maximum discharge, there is a high probability that the turbine was off for some part of an hour. Multiple detections of just a few fish wallowing in and out of an acoustic beam when a turbine is off can greatly inflate hourly estimates of guided fish passage and can bias estimates of FGE and FPE. We assumed that a turbine with < 65% of maximum discharge was off the entire hour rather than risk inflation of guided fish counts. These adjustments had little effect on overall fish-passage estimates because they were infrequent and over one half of those occurrences resulted from a turbine running < 10 minutes/hour. For example, at units 9 and 10, we set hourly fish passage to zero in only 28 and 31 of 1,103 spring hours (< 3 %), respectively, based upon low hourly discharge. At Unit 14, fish passage was set to zero based upon low discharge in 17 (1.5 %) of 1,103 spring hours monitored.

Hourly rates and variances in fish passage and hourly rates of water discharge through various routes at Bonneville Dam are presented in Appendix E on the accompanying compact disk. Tables 1 and 2 of Appendix E describe the variables in the comma-separated variable files.

2.7   Missing Data

We made a special effort to make certain that missing samples were accounted for in the spring and summer data sets. First, we created a data set consisting of all possible sample locations and times each season and set an expanded fish variable to missing in every observation. Second, we merged the missing data set with the acquired data set and counts of expanded fish, if present in the acquired data, overwrote missing counts. When a sample was not acquired for whatever reason, there was nothing in the acquired data set to overwrite the missing value for expanded fish. Therefore, the observation was appropriately designated as missing and could be interpolated before data were analyzed.

All hydroacoustic systems were operated continuously (> 23 hours/day), except for about 15 minutes every morning when data were copied from the acquisition computer onto a portable FireWire™ hard

drive or when equipment failed and data from the affected routes were not collected. Short equipment failures lasting up to 45 minutes were not a problem because fish counts and associated variances could still be estimated from the remaining within-hour samples. Computer lock-ups usually were fixed within an hour because we had staff monitoring systems 24 hours per day. We had transducer cables fail on units 9 and 11 and both were fixed within a day, as soon as project support or divers became available. The failure at Unit 11 was replaced in March before the fish passage season began.

Missing hourly sums and variances that resulted from equipment outages > 45 minutes were estimated by temporal linear interpolation for periods < 6 hours and by spatial interpolation or linear regression for periods > 6 hours. Occasionally the ratio of guided to unguided numbers at adjacent turbines with similar screens was useful for interpolating estimates of guided or unguided numbers. Regression equations relating hourly variances with hourly sums were sometimes used to estimate missing variance estimates. Two spill bays (3 and 16) were not among those sampled and were interpolated from passage at the next open bay on either side to produce estimates for horizontal distribution figures.

2.8 Detectability Modeling and Spatial Expansions

The count of every fish (1) was expanded based upon the ratio of the opening width to beam diameter at the range of detection:

$$EXP\_NUM = \frac{OW}{[MID\_R \times TAN(\frac{EBA}{2}) \times 2]}$$

where OW is opening width in m, MID_R is the mid-point range of a trace in m, TAN is the tangent, and EBA is effective beam angle in degrees.

Effective beam angle depends upon the detectability of fish of different sizes in the acoustic beam and is a function of nominal beam width, ping rate, trace criteria, and fish size, aspect, trajectory, velocity, and range. We modeled detectability for every transducer deployment to determine effective beam angle as a function of range from a transducer. We obtained target-strength estimates from the average back-scattering cross section of fish detected by split-beam transducers and flow-velocity data by 1- m depth strata from a physical or computational fluid design (CFD) model. These data and other hydroacoustic-acquisition data (e.g., beam tilt, ping rate, target-strength threshold, number of echoes, and maximum ping gaps) were entered into a detectability model. Inputs to the detectability model are presented in Tables 2.1 and 2.2. Model output consisted of effective beam angle as a function of range from a transducer. Polynomials fitted to those data were substituted for EBA in Equation 1 to correct for differences in detectability by range among transducers and locations.

Polynomial regressions were used to describe the relationships between predictions of effective beam angle with range from a transducer for every type of deployment. Those equations and passage width data were used to expand the count of each detected fish and to equalize detectability among sample ranges and deployments. The coding solved a deployment-specific polynomial equation for effective beam angle based upon the range of detection of each individual fish (Appendix F), calculated the corresponding beam diameter at the same range (Equation 1), and multiplied the fish's count (i.e., one) by

the ratio of the passage width to the beam diameter. The polynomials presented in Appendix F can be used to generate the detectability curves. Sampling ranges that were used to solve for effective beam angle truncated the polynomial curves to appropriate ranges.

Table 2.1. Deployment-Specific Variables that Were Input to a Stochastic Detectability Model for Estimating Effective Beam Angle as a Function of Range from a Transducer. Constants were as follows: Blanking range = 1 m; Target Strength threshold = -56 dB; Maximum ping gap = 2. A negative tilt is upstream of vertical and a positive tilt is downstream.

Deployment	-3 dB Beam Angle	Trans-ducer Tilt from Vertical (Degrees)	Pings / Second	Mean Target Strength	TS Standard Deviation	Minimum Echo Count	Maximum Range
			Spring				
Units 1-7, 9, & 10 Down-looking	6	9	14	-44.7	4.1	4	21
Units 1-7, 9, & 10 Up-looking	6	29	14	-44.7	4.1	4	14
Unit 8 Down-looking	6	-25	14	-44.7	4.1	4	13
Unit 8 Up-looking	6	28	14	-44.7	4.1	4	13
Spill Bays 2, 5, 6, 7, 8, 10, 14, & 15 Down-looking	10	-8	30	-44.7	4.1	4	10
Spill Bays 4 & 12	10	-8	30	-44.7	4.1	7	10
Spill Bay 17 Down-looking	12	-15	30	-44.7	4.1	4	10
Units 11-18 Down-looking	6	9	15	-44.7	4.1	4	17
Units 11-18 Up-looking	6	36	15	-44.7	4.1	4	10
Upstream of Intake 15b	6	17,23,29	14	-44.7	4.1	4	31
			Summer				
Units 1-7, 9, & 10 Down-looking	6	9	14	-48	4.11	4	21
Units 1-7, 9, & 10 Up-looking	6	29	14	-48	4.11	4	14
Unit 8 Down-looking	6	-25	14	-48	4.11	4	13
Unit 8 Up-looking	6	28	14	-48	4.11	4	13
Spill Bays 2, 5, 6, 7, 8, 10, 14, & 15 Down-looking	10	-8	30	-48	4.11	4	10
Spill Bays 4 & 12	10	-8	30	-48	4.11	7	10
Spill Bay 17 Down-looking	12	-15	30	-48	4.11	4	10
Units 11-18 Down-looking	6	9	15	-48	4.11	4	17
Units 11-18 Up-looking	6	36	15	-48	4.11	4	10
Upstream of Intake 15b	6	17,23,29	14	-48	4.11	4	31

Table 2.2. Polynomial Inputs or Constants for the Detectability Model for Beam Patterns, Fish Trajectories, and Fish Speeds for Every Deployment

Deployment	Variable	Polynomial or Constants
Units 1-7 & 9 Down-looking	Beam Shape	$B = -.003330226586X^4 + .017471453954X^3 - .310142505527X^2 + .035753868397X - .004849602465$
	Trajectory	$plunge = .002373764589X^4 - .112735778158X^3 + 1.56076075983X^2 - 6.603395811676X + 36.885504201695$
	Speed	$mps = .000018623951X^4 - .001270343248X^3 + .025384265243X^2 - .103042996658X + .677731764708$
Units 1-7 & 9 Up-looking	Beam Shape	$B = -.003330226586X^4 + .017471453954X^3 - .310142505527X^2 + .035753868397X - .004849602465$
	Trajectory	$plunge = -.000308771027X^4 + .001553540498X^3 + .275668020657X^2 - 5.22697691328X - 4.1964285714$
	Speed	$mps = .000000000001X^4 + .000291396396X^3 - .003501776837X^2 - .051568234978X + 1.362891428571$
Unit 10 Down-looking	Beam Shape	$B = -.00738221648X^4 + .040217634582X^3 - .404438802016X^2 + .036170817387X - .00152995463$
	Trajectory	$plunge = .002373764589X^4 - .112735778158X^3 + 1.56076075983X^2 - 6.603395811676X + 36.885504201695$
	Speed	$mps = .000018623951X^4 - .001270343248X^3 + .025384265243X^2 - .103042996658X + .677731764708$
Unit 10 Up-looking	Beam Shape	$B = -.00738221648X^4 + .040217634582X^3 - .404438802016X^2 + .036170817387X - .00152995463$
	Trajectory	$plunge = -.000308771027X^4 + .001553540498X^3 + .275668020657X^2 - 5.22697691328X - 4.1964285714$
	Speed	$mps = .000000000001X^4 + .000291396396X^3 - .003501776837X^2 - .051568234978X + 1.362891428571$
Unit 8 Down-looking	Beam Shape	$B = -.003330226586X^4 + .017471453954X^3 - .310142606627X^2 + .035753868397X - .004849601465$
	Trajectory	$plunge = -.000086076347X^4 + .016096619208X^3 - .667377525502X^2 + 10.273234879192X - 56.813249624336$
	Speed	$mps = -.000607X^3 + .0388228X^2 - .201837X + .8758629$
Unit 8 Up-looking	Beam Shape	$B = -.003330226586X^4 + .017471453954X^3 - .310142606627X^2 + .035753868397X - .004849601465$
	Trajectory	$plunge = -28$
	Speed	$mps = .000018340049X^4 - .001702427407X^3 + .04529765004X^2 - .435040205779X + 2.2606$
Spill Bays 4 & 12 Down-looking	Beam Shape	$B = -.000479254381X^4 + .005816071612X^3 - .17653166225X^2 + .108057677967X - .001573760223$
	Trajectory	$plunge = -.08224067599X^4 + 2.06132672882X^3 - 17.20578942702X^2 + 60.665036907455X - 110.10999999990$
	Speed	$mps = -.000528205128X^4 + .010511771562X^3 - .06068467366X^2 + .517001107226X + .5129833333279999$
Spill Bays 2, 5, 6, 7, 8, 10, 14, & 15 Down-looking	Beam Shape	$B = -.000479254381X^4 + .005816071612X^3 - .17653166225X^2 + .108057677967X - .001573760223$
	Trajectory	$plunge = -.08224067599X^4 + 2.06132672882X^3 - 17.20578942702X^2 + 60.665036907455X - 110.10999999990$
	Speed	$mps = -.000528205128X^4 + .010511771562X^3 - .06068467366X^2 + .517001107226X + .5129833333279999$
Spill Bay 17 Down-looking	Beam Shape	$B = .0003634X^4 - .006977X^3 - .031845X^2 - .012959X - .005818$
	Trajectory	$plunge = -.08224067599X^4 + 2.06132672882X^3 - 17.20578942702X^2 + 60.665036907455X - 110.10999999990$
	Speed	$mps = -.000528205128X^4 + .010511771562X^3 - .06068467366X^2 + .517001107226X + .5129833333279999$
Units 11-18 Down-looking	Beam Shape	$B = -.003330226586X^4 + .017471453954X^3 - .310142505527X^2 + .035753868397X - .004849601465$
	Trajectory	$plunge = -.003360361183X^4 + .145723292012X^3 - 2.010411084854X^2 + 7.381654309909X + 26.672858617129$
	Speed	$mps = .000049630032X^4 - .001581448873X^3 + .012092068792X^2 + .071453243301X + .81122724458$
Units 11-18 Up-looking	Beam Shape	$B = -.003330226586X^4 + .017471453954X^3 - .310142505527X^2 + .035753868397X - .004849601465$
	Trajectory	$plunge = -26$
	Speed	$mps = -.000499129625X^4 + .010107508945X^3 - .072403499059X^2 + .194463002585X + 1.254298181816$
Upstream of Intake 15b	Beam Shape	$B = .011170692053X^4 - .158786483125X^3 + .231914384635X^2 - .5101118323179999X + .056466461582$
	Trajectory	$plunge = -.0004X^4 + .0183X^3 - .2178X^2 + .2152X + 20.969$
	Speed	$mps = 1.5$

2.9   Estimating Fish Passage

This section describes in detail the estimation of fish passage at Powerhouses 1 and 2 and the spillway at Bonneville Dam in 2001. These estimates of passage will be used in subsequent measures of fish passage performance. Within every hour, we sampled 12 to 30 minutes systematically depending upon location, and we assumed that these systematic samples would behave as if they were simple random samples. This approach should overestimate the variance. We also estimated and added the variation among two or more turbine units to the temporal variation of each unit to make a conservative estimate of spatial variation resulting from sampling one of three intakes per turbine unit.

Confidence intervals for individual intakes or spill bays were calculated as 1.96 times the square root of temporal variance estimate for the time frame of interest (day, week, or season). The following sub-sections describe procedures for estimating temporal variances in fish passage through individual intakes and spill bays as first steps for estimating the variance for strata of intakes or bays or for each powerhouse and the spillway.

2.9.1   Powerhouse 1 Unguided Passage

The sampling at Powerhouse 1 can be viewed as a two-stage sampling scheme. The first stage is the sampling of intake slots within a stratum composed of neighboring turbine units that were operating simultaneously. Typically, two consecutive turbine units would be grouped together to form a stratum, and it would be assumed that two of six intake slots were randomly selected for monitoring. However, the low-flow conditions of 2001 resulted in an unexpected and irregular pattern of turbine use. In many instances, the closure of a turbine unit would result in some strata no longer having the within-strata replication needed for variance estimation.

The proposed solution to the dilemma imposed by the dam operations in 2001 is to post-stratify the operational turbine units into strata according to their proximity to one another. The re-stratification at times is somewhat arbitrary, because there is no single unique way to group the locales. Priority would be given to grouping locations into the most proximal sets of locations while retaining the ability to calculate the spatial sampling variances. The resulting variance estimates can generally be considered conservative, for they often include more between-intake variance than expected under the original sampling design.

Based on load demands and equipment use, the number and location of operational turbine units varied over time. Table 2.3 below illustrates some of the turbine unit configurations observed in 2001 and the subsequent post-stratification used in the data analyses for Powerhouse 1.

Table 2.3. Stratification Scheme for Estimating among Intake Variance Components at Powerhouse 1

Possible Loading/Units Operations										Stratification		
1	2	3	4	5	6	7	8	9	10	Stratum #1	Stratum #2	Stratum #3
1	2	3				7			10	1, 2, 3	7, 10	
1									10	1, 10		
1	2								10	1, 2, 10		
1	2	3							10	1, 2	3, 10	
1	2	3		5		7			10	1, 2	3, 5	7, 10
1	2	3		5	6	7			10	1, 2, 3	5, 6	7, 10
									10	10		

Hence, the number of strata and sampling effort within strata varied over time.
The unguided fish passage at Powerhouse 1(TU) will be estimated by the quantity

$$\widehat{TU} = \sum_{i=1}^{D}\sum_{j=1}^{23}\sum_{k=1}^{K_{ij}}\left[\frac{A_{ijk}}{a_{ijk}}\left[\sum_{l=1}^{a_{ijk}}\widehat{TU}_{ijkl}\right]\right] \tag{1}$$

where

$\widehat{TU}_{ijkl}$ = estimated fish passage in the lth intake slot ($l = 1,\ldots,a_{ijk}$) within the kth turbine stratum
($k = 1,\ldots K_{ij}$) during the jth hour ($j = 1,\ldots,24$) on the ith day ($i = 1,\ldots,D$);

a_{ijk} = number of intake slots actually sampled in the kth turbine stratum ($k = 1,\ldots K_{ij}$) during the
jth hour ($j = 1,\ldots,24$) on the ith day ($i = 1,\ldots,D$);

A_{ijk} = total number of intake slots within the kth turbine stratum ($k = 1,\ldots K_{ij}$) during the jth hour
($j = 1,\ldots,24$) on the ith day ($i = 1,\ldots,D$);

K_{ij} = number of turbine strata created during the jth hour ($j = 1,\ldots,24$) on the ith day ($i = 1,\ldots,D$).

Because of the varying power loads over time, the number of spatial strata (i.e., K_{ij}) formed by post-
stratification of adjacent turbine units may vary between hours ($j = 1,\ldots,24$) and days ($i = 1,\ldots,D$).

The estimate of $\widehat{TU}_{ijkl}$ is based on the assumption of simple random sampling within a slot-hour, in
which case

$$\widehat{TU}_{ijkl} = \frac{B_{ijkl}}{b_{ijkl}}\sum_{g=1}^{b_{ijkl}}z_{ijklg} \ . \tag{2}$$

Combining Equations (1) and (2), the overall estimate of unguided fish passage at Powerhouse 1
during D days can be expressed as

$$\widehat{TU} = \sum_{i=1}^{D}\sum_{j=1}^{23}\sum_{k=1}^{K_{ij}}\left[\frac{A_{ijk}}{a_{ijk}}\left[\frac{B_{ijkl}}{b_{ijkl}}\sum_{g=1}^{b_{ijkl}}z_{ijklg}\right]\right] \tag{3}$$

where

z_{ijklg} = expanded fish count in the gth sampling unit ($g = 1,\ldots,b_{ijkl}$) in the lth intake slot ($l = 1,\ldots,a_{ijk}$) within the kth turbine stratum ($k = 1,\ldots K_{ij}$) during the jth hour ($j = 1,\ldots,23$) on the ith day ($i = 1,\ldots,D$);

b_{ijkl} = number of sampling units actually observed in the lth intake slot ($l = 1,\ldots,a_{ijk}$) within the kth turbine stratum ($k = 1,\ldots K_{ij}$) during the jth hour ($j = 1,\ldots,23$) on the ith day ($i = 1,\ldots,D$);

B_{ijkl} = total number of sampling units within the lth intake slot ($l = 1,\ldots,a_{ijk}$) within the kth turbine stratum ($k = 1,\ldots K_{ij}$) during the jth hour ($j = 1,\ldots,23$) on the ith day ($i = 1,\ldots,D$).

Nominally, $B_{ijkl} = 60\ \forall ijkl$ and $b_{ijkl} = 15$ or 20, depending on location. Based on the assumption of simple random sampling

$$\widehat{Var}\left(\widehat{TU}_{ijkl}\right) = \frac{B_{ijkl}^2\left(1 - \frac{b_{ijkl}}{B_{ijkl}}\right)s_{z_{ijkl}}^2}{b_{ijkl}} \tag{4}$$

where

$$s_{z_{ijkl}}^2 = \frac{\sum_{g=1}^{b_{ijkl}}\left(z_{ijklg} - \overline{z_{ijkl}}\right)^2}{\left(b_{ijkl} - 1\right)} \qquad \text{and where}$$

$$\overline{z_{ijkl}} = \frac{1}{b_{ijkl}}\sum_{g=1}^{b_{ijkl}} z_{ijklg}\ .$$

The variance of $\widehat{TU}$ can then be extended by the formula

$$\widehat{Var}\left(\widehat{TU}\right) = \sum_{i=1}^{D}\sum_{j=1}^{24}\sum_{k=1}^{K_{ij}}\left[\frac{A_{ijk}^2\left(1 - \frac{a_{ijk}}{A_{ijk}}\right)s_{\widehat{TU}_{ijk}}^2}{a_{ijk}} + \frac{A_{ijkl}\sum_{l=1}^{a_{ijk}}\widehat{Var}\left(\widehat{TU}_{ijkl}\right)}{a_{ijk}}\right] \tag{5}$$

where

$$s_{\widehat{TU}_{ijk}}^2 = \frac{\sum_{l=1}^{a_{ijk}}\left(\widehat{TU}_{ijkl} - \widehat{\overline{TU}}_{ijk}\right)^2}{\left(a_{ijk} - 1\right)},$$

$$\widehat{\overline{TU}}_{ijk} = \frac{1}{a_{ijk}}\sum_{l=1}^{a_{ijk}}\widehat{TU}_{ijkl}\ .$$

2.9.2 Powerhouse 1 Guided Passage

The post-stratification used in estimating unguided passage at Powerhouse 1 is the same as used to estimate guided passage at Powerhouse 1. Hence, the estimator for guided fish passage at Powerhouse 1 can be written as

$$\widehat{TG} = \sum_{i=1}^{D} \sum_{j=1}^{23} \sum_{k=1}^{K_{ij}} \left[\frac{A_{ijk}}{a_{ijk}} \left[\frac{B_{ijkl}}{b_{ijkl}} \sum_{g=1}^{b_{ijkl}} y_{ijklg} \right] \right] \tag{6}$$

where

y_{ijklg} = expanded fish passage in the gth sampling unit ($g = 1, \ldots, b_{ijkl}$) in the lth intake slot ($l = 1, \ldots, a_{ijk}$) within the kth turbine stratum ($k = 1, \ldots K_{ij}$) during the jth hour ($j = 1, \ldots, 23$) on the ith day ($i = 1, \ldots, D$).

The estimated variance of $\widehat{TG}$ can then be expressed as

$$\widehat{Var}\left(\widehat{TG}\right) = \sum_{i=1}^{D} \sum_{j=1}^{24} \sum_{k=1}^{K_{ij}} \left[\frac{A_{ijk}^2 \left(1 - \dfrac{a_{ijk}}{A_{ijk}}\right) s_{\widehat{TG}_{ijk}}^2}{a_{ijk}} + \frac{A_{ijkl} \displaystyle\sum_{l=1}^{a_{ijk}} \widehat{Var}\left(\widehat{TG}_{ijkl}\right)}{a_{ijk}} \right] \tag{7}$$

where

$$\widehat{Var}\left(\widehat{TG}_{ijkl}\right) = \frac{B_{ijkl}^2 \left(1 - \dfrac{b_{ijkl}}{B_{ijkl}}\right) s_{y_{ijkl}}^2}{b_{ijkl}},$$

$$s_{y_{ijkl}}^2 = \frac{\displaystyle\sum_{g=1}^{b_{ijkl}} \left(y_{ijklg} - \overline{y}_{ijkl}\right)^2}{\left(b_{ijkl} - 1\right)},$$

$$\overline{y}_{ijkl} = \frac{1}{b_{ijkl}} \sum_{g=1}^{b_{ijkl}} y_{ijklg},$$

and where

$$s_{\widehat{TG}_{ijk}}^2 = \frac{\displaystyle\sum_{l=1}^{a_{ijk}} \left(\widehat{TG}_{ijkl} - \widehat{\overline{TG}}_{ijk}\right)^2}{\left(a_{ijk} - 1\right)},$$

$$\widehat{\overline{TG}}_{ijk} = \frac{1}{a_{ijk}} \sum_{l=1}^{a_{ijk}} \widehat{TG}_{ijkl}.$$

Because the z_{ijklg} and the y_{ijklg} within a turbine intake are measured simultaneously, they are correlated as will be the estimators $\widehat{TU}$ and $\widehat{TG}$. The covariances between $\widehat{TG}$ and $\widehat{TU}$ can then be estimated by the quantity

$$\widehat{Cov}\left(\widehat{TU},\widehat{TG}\right)=\sum_{i=1}^{D}\sum_{j=1}^{23}\sum_{k=1}^{K_{ij}}\left[\frac{A_{ijk}^{2}\left(1-\dfrac{a_{ijk}}{A_{ijk}}\right)\widehat{Cov}\left(\widehat{TU}_{ijk},\widehat{TG}_{ijk}\right)}{a_{ijk}}+\frac{A_{ijkl}\displaystyle\sum_{l=1}^{a_{ijk}}\widehat{Cov}\left(\widehat{TU}_{ijkl},\widehat{TG}_{ijkl}\right)}{a_{ijk}}\right] \qquad 8)$$

where

$$\widehat{Cov}\left(\widehat{TU}_{ijk},\widehat{TG}_{ijk}\right)=\frac{\displaystyle\sum_{l=1}^{a_{ijk}}\left(\widehat{TU}_{ijkl}-\overline{\widehat{TU}}_{ijkl}\right)\left(\widehat{TG}_{ijkl}-\overline{\widehat{TG}}_{ijkl}\right)}{\left(a_{ijk}-1\right)}$$

and where

$$\widehat{Cov}\left(\widehat{TU}_{ijkl},\widehat{TG}_{ijkl}\right)=\frac{B_{ijkl}^{2}\left(1-\dfrac{b_{ijkl}}{B_{ijkl}}\right)Cov\left(z_{ijklg},y_{ijklg}\right)}{b_{ijkl}}$$

and where

$$Cov\left(z_{ijklg},y_{ijklg}\right)=\frac{\displaystyle\sum_{g=1}^{b_{ijkl}}\left(z_{ijklg}-\overline{z}_{ijkl}\right)\left(y_{ijklg}-\overline{y}_{ijkl}\right)}{\left(b_{ijkl}-1\right)}.$$

2.9.3 Spillway Passage

During spring 2001, hydroacoustic transducers were placed in spill bays 2, 4, 5, 6, 7, 8, 10, 12, 14, 15, and 17. In practice, only spill bays 2, 3, 4, 6, 10, 12, 16, and 17 were operated for spill at various times during the study because of drought conditions. We classified spillway sampling into four spill-bay strata (Table 2.4).

Table 2.4. Groups of Spill bays Selected to Form Strata for Calculating Spill Passage and Variances

Stratum	Spill bays	No. of Bays	No. Monitored	Sampling Fraction
1	2, 3, 4	3	2	2/3
2	6	1	1	1.0
3	10	1	1	1.0
4	12, 16, 17	3	3	2/3

Hence, the sampling at the Bonneville spillway was designed as a stratified two-stage sampling regime. The first stage of sampling was the selection of spill bays within the spatial strata. In two of the four strata (i.e., 2 and 3), the first-stage sampling of spill bays was 100%. The second stage of sampling was a random sample of time intervals within a spill-bay hour.

Total spillway passage was estimated by the formula

$$\hat{S} = \sum_{g=1}^{4} \left[\frac{H_g}{h_g} \sum_{i=1}^{h_g} \sum_{j=1}^{D} \sum_{k=1}^{23} \frac{T_{gijk}}{t_{gijk}} \sum_{l=1}^{t_{gijk}} p_{gijkl} \right] \qquad (9)$$

where

p_{gijkl} = expanded fish passage in the lth sampling interval $\left(l = 1, \ldots, t_{gik} \right)$ during the kth hour $\left(k = 1, \ldots, 23 \right)$ in the jth day $\left(j = 1, \ldots, D \right)$ at the ith spill bay $\left(i = 1, \ldots, h_g \right)$ in the gth stratum $\left(g = 1, \ldots, 4 \right)$;

T_{gijk} = possible number of sampling units within an hour (i.e., nominally $T_{gijk} = 60$);

t_{gijk} = actual number of samples drawn within the kth hour $\left(k = 1, \ldots, 23 \right)$ in the jth day $\left(j = 1, \ldots, D \right)$ at the ith spill bay $\left(i = 1, \ldots, h_g \right)$ in the gth stratum $\left(g = 1, \ldots, 4 \right)$ (i.e., nominally $t_{gijk} = 10$ or 12);

H_g = number of operating (open) spill bays within the gth spillway stratum;

h_g = number of operating (open) spill bays actually sampled within the gth spillway stratum.

The variance of $\hat{S}$ was estimated by the quantity

$$\widehat{Var}\left(\hat{S} \right) = \sum_{g=1}^{4} \frac{H_g^2 \left(1 - \frac{h_g}{H_g} \right) s_{\hat{S}_g}^2}{h_g} + \sum_{g=1}^{4} \left[\frac{H_g \sum_{j=1}^{h_g} \widehat{Var}\left(\hat{S}_{gi} \right)}{h_g} \right] \qquad (10)$$

where

$$s_{\hat{S}_g}^2 = \frac{\sum_{j=1}^{h_g} \left(\hat{S}_{gi} - \bar{\hat{S}}_g \right)^2}{\left(h_g - 1 \right)},$$

$$\bar{\hat{S}}_g = \frac{\sum_{i=1}^{h_g} \hat{S}_{gi}}{h_g},$$

$$\hat{S}_{gi} = \sum_{j=1}^{D} \sum_{k=1}^{23} \frac{T_{gijk}}{t_{gijk}} \sum_{l=1}^{t_{gijk}} p_{gijkl},$$

and where

$$Vâr\left(\hat{S}_{g_i}\right) = \sum_{j=1}^{D}\sum_{k=1}^{23}\left[T_{gijk}^2\left(1-\frac{t_{gijk}}{T_{gijk}}\right)\frac{s_{p_{gijk}}^2}{t_{gijk}}\right],$$

$$s_{p_{gijk}}^2 = \frac{\sum_{l=1}^{t_{gijk}}\left(p_{gijkl}-\overline{p_{gijk}}\right)^2}{\left(t_{gijk}-1\right)},$$

$$\overline{p}_{gijk} = \frac{\sum_{l=1}^{t_{gijk}}p_{gijkl}}{t_{gijk}}.$$

Note for strata 2 and 3, $H_g = h_g$ and the first term in Equation (10) goes to zero.

2.9.4 Powerhouse 2 Unguided Passage

The same two-stage sampling scheme used to estimate fish passage at Powerhouse 1 was used to estimate fish passage at Powerhouse 2, units 11 through 18. Nominally, two consecutive turbine units (e.g., 11-12, 13-14, …) were combined to form a stratum with 2 or 6 intake slots selected for monitoring. In reality, a single intake slot among the three within a turbine intake were randomly selected. Very occasionally, unit shutdowns because of load demands required further post-stratification to ensure within-stratum replication of turbine slots. Under these circumstances, the turbine units at Powerhouse 2 were grouped into three or fewer strata. To accommodate all circumstances, the estimators and variances will be expressed generically.

Using the fish counts from the down-looking transducers, total unguided fish passage at Powerhouse 2 was estimated by the quantity

$$\widehat{HU} = \sum_{i=1}^{D}\sum_{j=1}^{23}\sum_{k=1}^{K_{ij}}\left[\frac{C_{ijk}}{c_{ijk}}\left[\frac{D_{ijkl}}{d_{ijkl}}\sum_{g=1}^{d_{ijkl}}x_{ijklg}\right]\right] \tag{11}$$

where

x_{ijklg} = expanded fish passage in the gth sampling unit ($g = 1,\ldots,b_{ijkl}$) in the lth intake slot ($l = 1,\ldots,a_{ijk}$) within the kth turbine stratum ($k = 1,\ldots K_{ij}$) during the jth hour ($j = 1,\ldots,23$) on the ith day ($i = 1,\ldots,D$);

d_{ijkl} = number of sampling units actually observed in the lth intake slot ($l = 1,\ldots,a_{ijk}$) within the kth turbine stratum ($k = 1,\ldots K_{ij}$) during the jth hour ($j = 1,\ldots,23$) on the ith day ($i = 1,\ldots,D$);

D_{ijkl} = total number of sampling units within the lth intake slot ($l = 1,\ldots,a_{ijk}$) within the kth turbine stratum ($k = 1,\ldots K_{ij}$) during the jth hour ($j = 1,\ldots,23$) on the ith day ($i = 1,\ldots,D$);

c_{ijk} = number of intake slots actually sampled in the kth turbine stratum ($k = 1,\ldots K_{ij}$) during the jth hour ($j = 1,\ldots,23$) on the ith day ($i = 1,\ldots,D$);

C_{ijk} = total number of intake slots within the kth turbine stratum ($k = 1, \ldots K_{ij}$) during the jth hour ($j = 1, \ldots, 23$) on the ith day ($i = 1, \ldots, D$);

K_{ij} = number of turbine strata created during the jth hour ($j = 1, \ldots, 23$) on the ith day ($i = 1, \ldots, D$).

Nominally, $K_{ij} = 4 \; \forall ij$, $C_{ijk} = 6 \; \forall ijk$, $c_{ijk} = 2 \; \forall_{ijk}$, and $D_{ijkl} = 60 \; \forall ijkl$. Depending on location, $d_{ijkl} = 15$ or 20.

The variance of $\widehat{HU}$ can then be estimated by the formula

$$\widehat{Var}\left(\widehat{HU}\right) = \sum_{i=1}^{D}\sum_{j=1}^{23}\sum_{k=1}^{K_{ij}}\left[\frac{C_{ijk}^{2}\left(1 - \frac{c_{ijk}}{C_{ijk}}\right)s_{\widehat{HU}_{ijk}}^{2}}{c_{ijk}} + \frac{C_{ijk}\sum_{l=1}^{c_{ijk}}\widehat{Var}\left(\widehat{HU}_{ijkl}\right)}{c_{ijk}} \right] \tag{12}$$

where

$$\widehat{Var}\left(\widehat{HU}_{ijkl}\right) = \frac{D_{ijkl}^{2}\left(1 - \frac{d_{ijkl}}{D_{ijkl}}\right)s_{x_{ijkl}}^{2}}{d_{ijkl}} ,$$

$$s_{x_{ijkl}}^{2} = \frac{\sum_{g=1}^{d_{ijkl}}\left(x_{ijklg} - \bar{x}_{ijkl}\right)^{2}}{\left(d_{ijkl} - 1\right)} ,$$

$$\bar{x}_{ijkl} = \frac{1}{d_{ijkl}}\sum_{g=1}^{d_{ijkl}}x_{ijklg} ,$$

and where

$$s_{\widehat{HU}_{ijk}}^{2} = \frac{\sum_{l=1}^{a_{ijk}}\left(\widehat{HU}_{ijkl} - \widehat{\overline{HU}}_{ijk}\right)^{2}}{\left(a_{ijk} - 1\right)} ,$$

$$\widehat{\overline{HU}}_{ijk} = \frac{1}{a_{ijk}}\sum_{l=1}^{a_{ijk}}\widehat{HU}_{ijkl} .$$

2.9.5 Powerhouse 2 Guided Passage

The same two-stage sampling scheme used to estimate unguided passage (HU) at Powerhouse 2 is used to simultaneously sample guided passage (HG) at Powerhouse 2. Hence, the estimator for guided fish passage at Powerhouse 2 can be written as

$$\widehat{HG} = \sum_{i=1}^{D}\sum_{j=1}^{23}\sum_{k=1}^{K_{ij}}\left[\frac{C_{ijk}}{c_{ijk}}\left[\frac{D_{ijkl}}{d_{ijkl}}\sum_{g=1}^{d_{ijkl}}w_{ijklg} \right] \right] \tag{13}$$

where

w_{ijklg} = expanded fish passage in the gth sampling unit ($g = 1,\ldots,b_{ijkl}$) in the lth intake slot ($l = 1,\ldots,a_{ijk}$) within the kth turbine stratum ($k = 1,\ldots K_{ij}$) during the jth hour ($j = 1,\ldots,23$) on the ith day ($i = 1,\ldots,D$).

The estimated variance of $\widehat{HG}$ can then be expressed as

$$\widehat{Var}\left(\widehat{HG}\right) = \sum_{i=1}^{D}\sum_{j=1}^{23}\sum_{k=1}^{K_{ij}}\left[\frac{C_{ijk}^2\left(1-\dfrac{c_{ijk}}{C_{ijk}}\right)s_{\widehat{HG}_{ijk}}^2}{c_{ijk}} + \frac{C_{ijk}\displaystyle\sum_{l=1}^{c_{ijk}}\widehat{Var}\left(\widehat{HG}_{ijkl}\right)}{c_{ijk}}\right] \tag{14}$$

where

$$\widehat{Var}\left(\widehat{HG}_{ijkl}\right) = \frac{D_{ijkl}^2\left(1-\dfrac{d_{ijkl}}{D_{ijkl}}\right)s_{w_{ijkl}}^2}{d_{ijkl}},$$

$$s_{w_{ijkl}}^2 = \frac{\displaystyle\sum_{g=1}^{d_{ijkl}}\left(w_{ijklg}-\overline{w}_{ijkl}\right)^2}{\left(d_{ijkl}-1\right)},$$

$$\overline{w}_{ijkl} = \frac{1}{d_{ijkl}}\sum_{g=1}^{d_{ijkl}}w_{ijklg},$$

and where

$$s_{\widehat{HG}_{ijk}}^2 = \frac{\displaystyle\sum_{l=1}^{c_{ijk}}\left(\widehat{HG}_{ijkl}-\widehat{\widehat{HG}}_{ijk}\right)^2}{\left(c_{ijk}-1\right)},$$

$$\widehat{\widehat{HG}}_{ijk} = \frac{1}{c_{ijk}}\sum_{l=1}^{c_{ijk}}\widehat{HG}_{ijkl}.$$

The response variables x_{ijklg} and w_{ijklg} are measured simultaneously in the same water volume by the fast multiplex transducers and, as such, are correlated. Hence, the estimates of fish passage $\widehat{HU}$ and $\widehat{HG}$ for Powerhouse 2 are correlated. Their covariance can be estimated by the quantity

$$\widehat{Cov}\left(\widehat{HU},\widehat{HG}\right) = \sum_{i=1}^{D}\sum_{j=1}^{23}\sum_{k=1}^{K_{ij}}\left[\frac{C_{ijk}^2\left(1-\dfrac{c_{ijk}}{C_{ijk}}\right)\widehat{Cov}\left(\widehat{HU}_{ijk},\widehat{HG}_{ijk}\right)}{c_{ijk}} + \frac{C_{ijk}\displaystyle\sum_{l=1}^{c_{ijk}}\widehat{Cov}\left(\widehat{HU}_{ijkl},\widehat{HG}_{ijkl}\right)}{c_{ijk}}\right] \tag{15}$$

where

$$\widehat{Cov}\left(\widehat{HU}_{ijk},\widehat{HG}_{ijk}\right)=\frac{\sum_{l=1}^{c_{ijk}}\left(\widehat{HU}_{ijkl}-\widehat{\overline{HU}}_{ijk}\right)\left(\widehat{HG}_{ijkl}-\widehat{\overline{HG}}_{ijk}\right)}{\left(c_{ijk}-1\right)}$$

and where

$$\widehat{Cov}\left(\widehat{HU}_{ijkl},\widehat{HG}_{ijkl}\right)=\frac{D_{ijkl}^{2}\left(1-\frac{d_{ijkl}}{D_{ijkl}}\right)\widehat{Cov}\left(x_{ijklg},w_{ijklg}\right)}{d_{ijkl}},$$

$$\widehat{Cov}\left(x_{ijklg},w_{ijklg}\right)=\frac{\sum_{g=1}^{d_{ijkl}}\left(x_{ijklg}-\overline{x}_{ijkl}\right)\left(w_{ijklg}-\overline{w}_{ijkl}\right)}{\left(d_{ijkl}-1\right)}.$$

It should be noted that formulas (5), (7), and (8) for Powerhouse 1 are analogous to formulas (12), (13), and (14) for Powerhouse 2. The estimators $\widehat{TU}$ and $\widehat{TG}$ are also analogous to the estimators $\widehat{HU}$ and $\widehat{HG}$, respectively.

2.10 Estimating Passage Performance

Estimates of fish passage through the powerhouses and the spillway will be used to estimate measures of project-wide passage performance. This section presents the estimators and associated variance estimators.

2.10.1 Spill Efficiency (SY)

The spill efficiency at the Bonneville Project was estimated by the quotient

$$\widehat{SY}=\frac{\hat{S}}{\left[\widehat{TU}+\widehat{TG}+\widehat{HU}+\widehat{HG}+\hat{S}\right]}=\frac{\hat{S}}{\widehat{NS}+\hat{S}} \tag{16}$$

where the numerator is the estimated spill-bay passage and the denominator is total project passage. The variance of $\widehat{SE}$ was estimated by

$$\widehat{Var}\left(\widehat{SY}\right)=\widehat{SY}^{2}\left(1-\widehat{SY}\right)^{2}\left[\frac{\widehat{Var}\left(\hat{S}\right)}{\hat{S}^{2}}+\frac{\widehat{Var}\left(\widehat{NS}\right)}{\widehat{NS}^{2}}\right] \tag{17}$$

where

$$\widehat{NS}=\widehat{TU}+\widehat{TG}+\widehat{HU}+\widehat{HG},$$

and where

$$\widehat{Var}\left(\widehat{NS}\right)=\widehat{Var}\left(\widehat{TU}\right)+\widehat{Var}\left(\widehat{TG}\right)+\widehat{Var}\left(\widehat{HU}\right)+\widehat{Var}\left(\widehat{HG}\right)+2\,\widehat{Cov}\left(\widehat{TU},\widehat{TG}\right)$$
$$+2\,\widehat{Cov}\left(\widehat{HU},\widehat{HG}\right).$$

2.10.2 Spill Effectiveness (SE)

The spill effectiveness at the Bonneville Project was estimated by the quantity

$$\widehat{SE} = \frac{\left(\dfrac{\hat{S}}{V_S}\right)}{\dfrac{\left(\widehat{NS} + \hat{S}\right)}{V_T}} = \widehat{SY} \cdot \frac{V_T}{V_S} \tag{18}$$

Where

V_S = volume of water spilled,

V_T = total volume of water passing the dam during the period of inference.

The variance of $\widehat{SE}$ can be estimated by

$$\widehat{Var}\left(\widehat{SE}\right) = \left(\frac{V_T}{V_S}\right)^2 \cdot \widehat{Var}\left(\widehat{SY}\right). \tag{19}$$

2.10.3 Project-Wide Fish Passage Efficiency

The project-wide FPE was estimated by the quotient

$$\widehat{FPE} = \frac{\left[\hat{S} + \widehat{TG} + \widehat{HG}\right]}{\left[\widehat{TU} + \widehat{TG} + \widehat{HU} + \widehat{HG} + \hat{S}\right]} \tag{20}$$

where the numerator is the estimated spillway and bypass guided passage and the denominator is total project passage; it is alternatively expressed as

$$\widehat{FPE} = \frac{\hat{G}}{\hat{G} + \hat{U}} \tag{21}$$

where

$$\hat{G} = \hat{S} + \widehat{TG} + \widehat{HG},$$
$$\hat{U} = \widehat{TU} + \widehat{HU}.$$

The variance of $\widehat{FPE}$ can then be estimated by

$$\widehat{Var}\left(\widehat{FPE}\right) = \widehat{FPE}^2 \left(1 - \widehat{FPE}\right)^2 \left[\frac{\widehat{Var}\left(\hat{G}\right)}{\hat{G}^2} + \frac{\widehat{Var}\left(\hat{U}\right)}{\hat{U}^2} - \frac{2\,\widehat{Cov}\left(\hat{G}, \hat{U}\right)}{\hat{G} \cdot \hat{U}}\right] \tag{22}$$

and where

$$\widehat{Var}\left(\hat{G}\right) = \widehat{Var}\left(\hat{S}\right) + \widehat{Var}\left(\widehat{TG}\right) + \widehat{Var}\left(\widehat{HG}\right),$$
$$\widehat{Var}\left(\hat{U}\right) = \widehat{Var}\left(\widehat{TU}\right) + \widehat{Var}\left(\widehat{HU}\right),$$
$$\widehat{Cov}\left(\hat{G}, \hat{U}\right) = \widehat{Cov}\left(\widehat{TU}, \widehat{TG}\right) + \widehat{Cov}\left(\widehat{HU}, \widehat{HG}\right).$$

2.10.4 Powerhouse 1 Fish Passage Efficiency (FPE)

For Powerhouse 1, FPE was estimated by the quantity

$$\widehat{FPE}_1 = \frac{\widehat{TG}}{\widehat{TG} + \widehat{TU}}$$

(23)

with associated variance estimator

$$\widehat{Var}\left(\widehat{FPE}_1\right) = \widehat{FPE}_1^2 \left(1 - \widehat{FPE}_1\right)^2 \left[\frac{\widehat{Var}\left(\widehat{TG}\right)}{\widehat{TG}^2} + \frac{\widehat{Var}\left(\widehat{TU}\right)}{\widehat{TU}^2} - \frac{2\,\widehat{Cov}\left(\widehat{TU},\widehat{TG}\right)}{\widehat{TU}\cdot\widehat{TG}}\right].$$

(24)

2.10.5 Powerhouse 2 Fish Passage Efficiency (FPE)

For Powerhouse 2, FPE was estimated by the quantity

(25)

$$\widehat{FPE}_2 = \frac{\widehat{HG}}{\widehat{HG} + \widehat{HU}}$$

with associated variance estimator

(26)

$$\widehat{Var}\left(\widehat{FPE}_2\right) = \widehat{FPE}_2^2 \left(1 - \widehat{FPE}_2\right)^2 \left[\frac{\widehat{Var}\left(\widehat{HG}\right)}{\widehat{HG}^2} + \frac{\widehat{Var}\left(\widehat{HU}\right)}{\widehat{HU}^2} - \frac{2\,\widehat{Cov}\left(\widehat{HU},\widehat{HG}\right)}{\widehat{HU}\cdot\widehat{HG}}\right].$$

3.0 Results

3.1 Hydroacoustic Detectability

In spring, most effective beam angles were within one degree of or above the nominal (-3 dB) beam angles (see Appendix B for nominal angles) for each transducer at minimum sampling ranges (Figure 3.1). Exceptions included the transducer sampling guided fish at Unit 8 and spillway transducers at bays 4 and 12. Smaller effective beam angles translate into bigger spatial expansion factors. In summer, curves for effective-beam angle by range had similar shapes to those modeled for spring, although angles at all ranges were narrower in summer than they were in spring (compare Figure 3.1 with Figure 3.2) because mean target strength estimates were lower in summer.
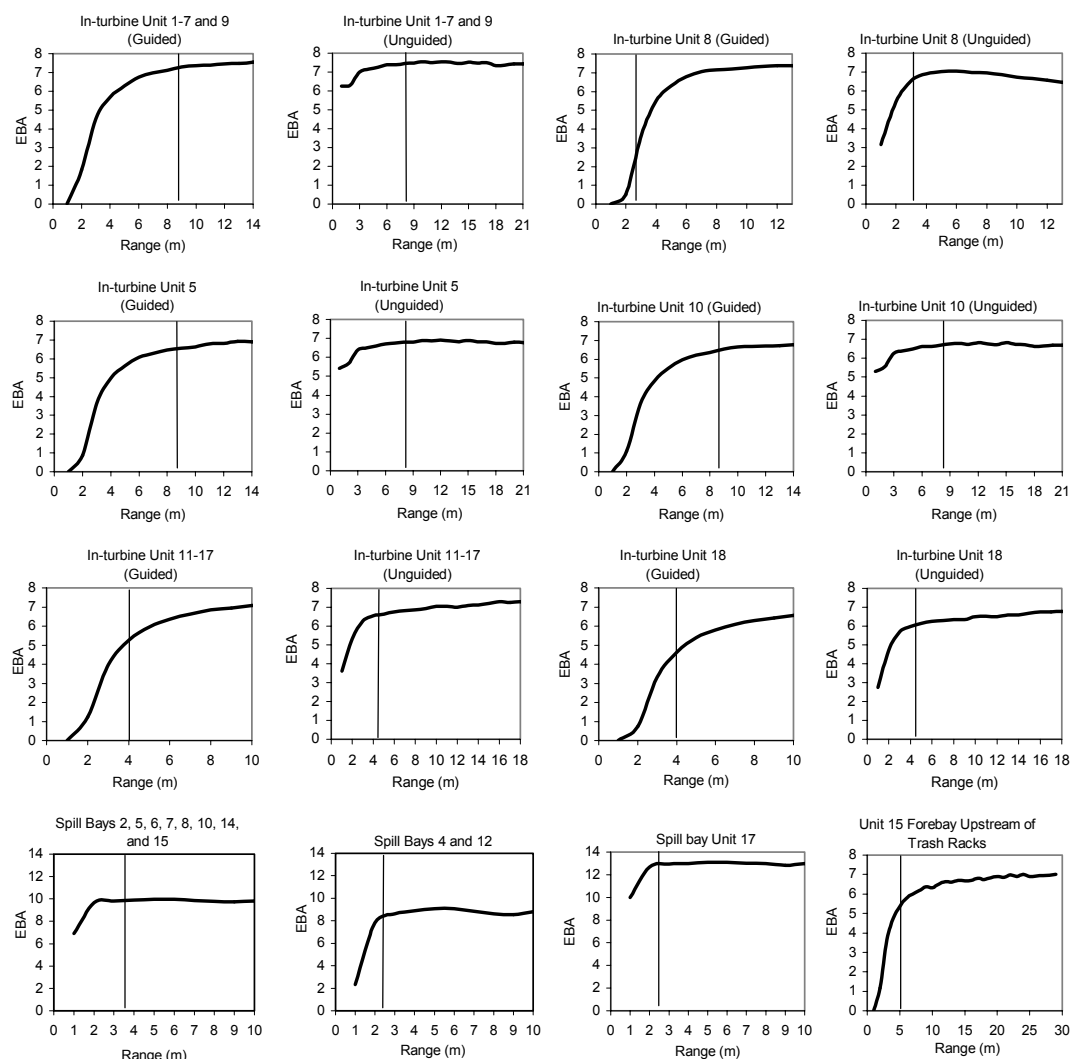
Figure 3.1. Plots of Effective Beam Angle (EBA) as a Function of Range from Transducers Deployed at Bonneville Dam in Spring 2001. Minimum sampling ranges are indicated by vertical bars. Note that both x and y scales vary among plots.
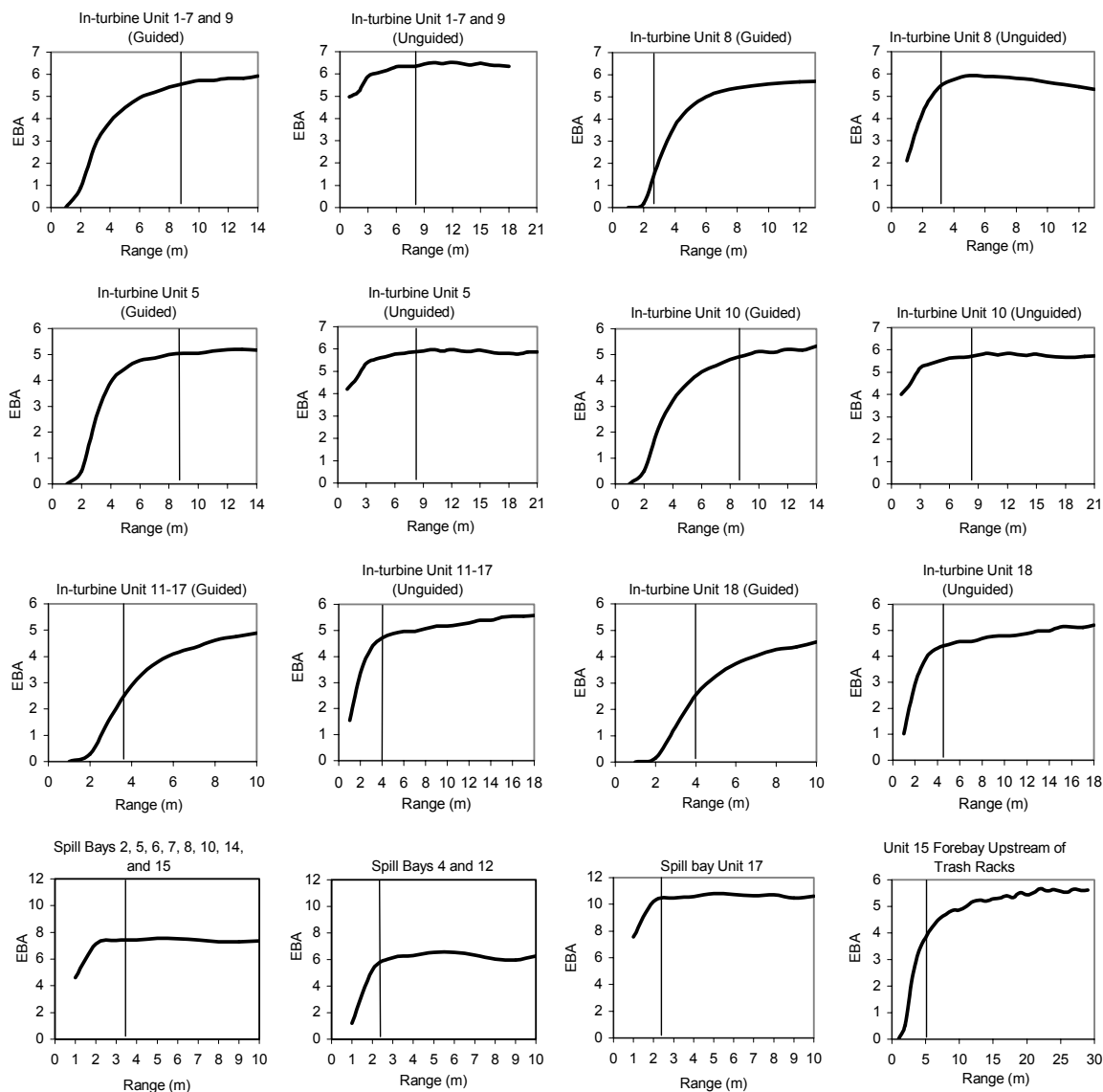
Figure 3.2. Plots of Effective Beam Angle (EBA) as a Function of Range from Transducers Deployed at Bonneville Dam in Summer 2001. Minimum sampling ranges are indicated by vertical bars. Note that both x and y scales vary among plots.

3.2 Validation of Autotracking Hydroacoustic Data

3.2.1 Inter-Tracker Error and Human versus Autotracker Comparisons

In our comparisons among six different human trackers, we found levels of inter-tracker error that could have led to biased results if the same human trackers had processed different passage routes consistently. Figure 3.3 demonstrates the possible cumulative effects of differences among human trackers, and the general tendency of the autotracker to produce estimates that are slightly higher than are those produced by an average human tracker.
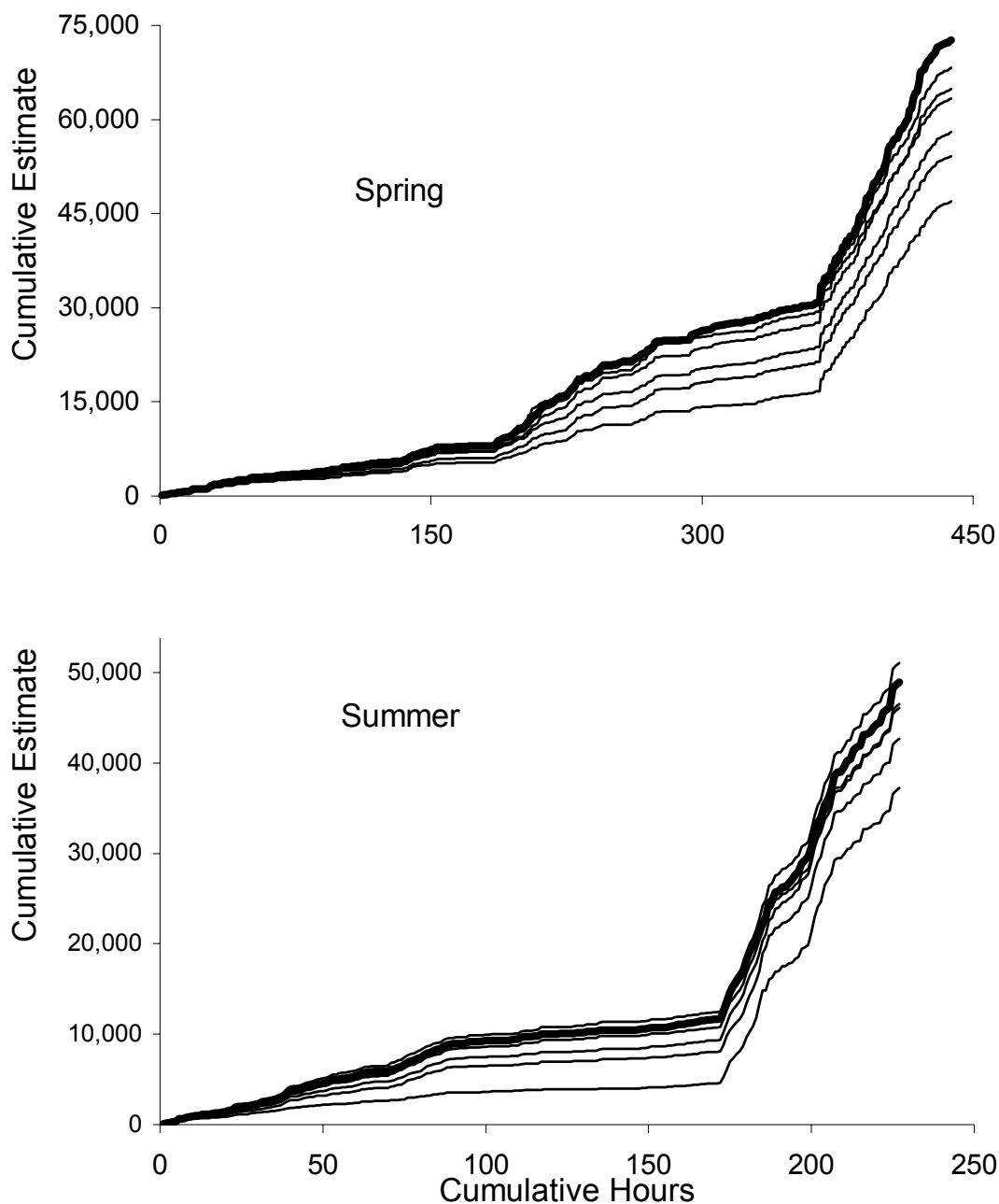
Figure 3.3. Cumulative Differences among Human Trackers in Spring and Summer. Estimates are spatially and temporally expanded fish counts. The heavy line represents the autotracker-based estimates, and the light lines, some of which may be obscured, are cumulative estimates based on fish counts made by individual human trackers.

Figures 3.3 and 3.5 present scatter plots of regression of mean fish counts by technicians on auto-tracker counts of the same data in spring and summer, respectively. Regression coefficients are high, indicating a generally good agreement between the autotracker results and the mean human results, although the 95% confidence bounds on the human estimates can be large, especially on those for guided passage.
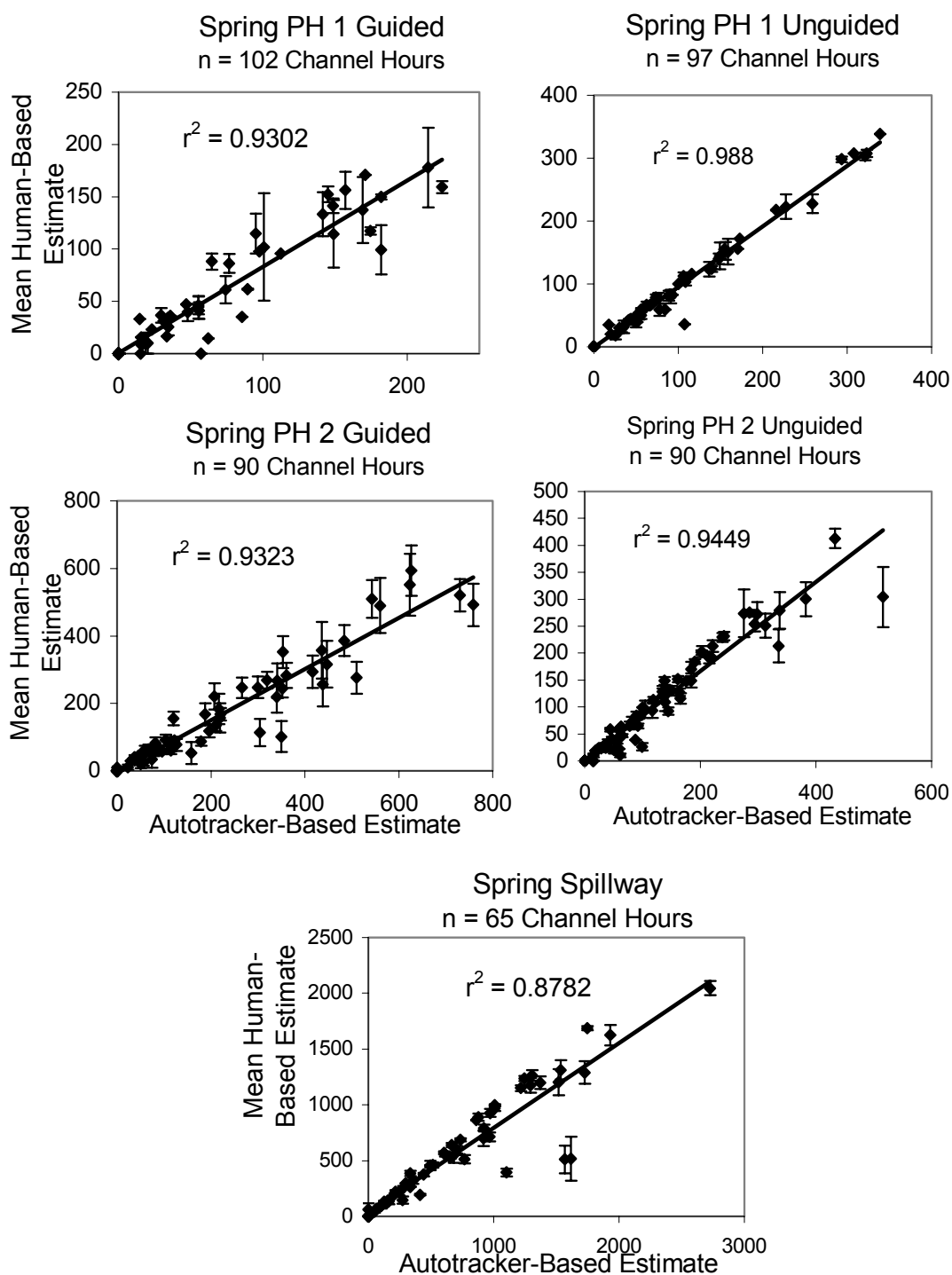
Figure 3.4. Regressions of Mean Human-Tracker Derived Hourly Passage Estimates and Autotracker-Derived Hourly Passage Estimates by Location (structure) and Deployment (passage route) in Spring. Bars indicate 95% confidence limits.
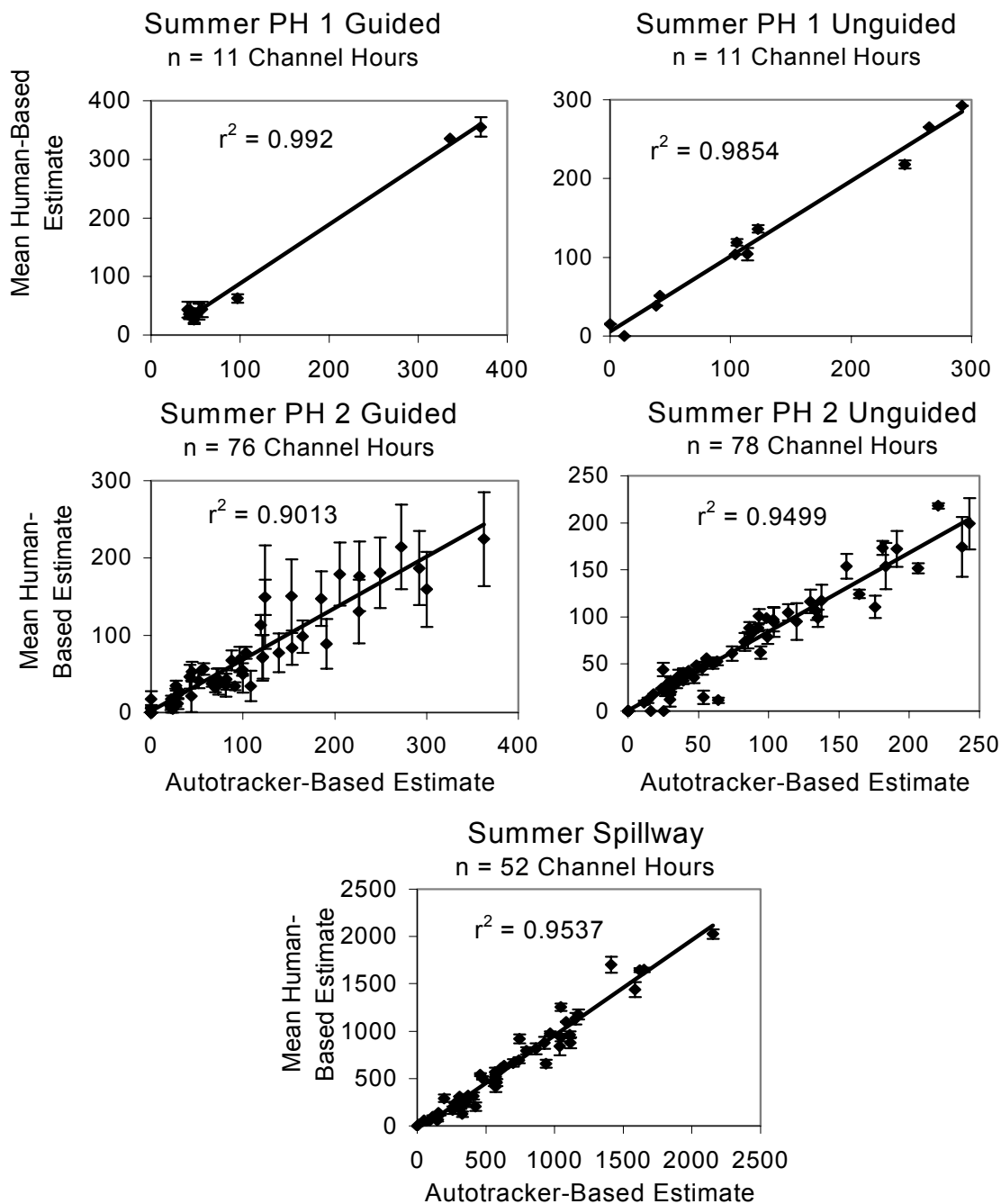
Figure 3.5. Regressions of Mean Human Tracker-Derived Hourly Passage Estimates and Autotracker-Derived Hourly Passage Estimates by Location (structure) and Deployment (passage route) in Summer. Bars indicate 95% confidence limits.

3.2.2 Regression Line Slopes for Autotracker Correction

Since the autotracker counts tend to be somewhat higher than are the mean human-derived counts, we forced the regressions in Figures 3.4 and 3.5 (above) through the origin in order to get estimates for the

magnitudes of those biases (Figure 3.6). The slopes in those figures are the values that we used to adjust our passage estimates.
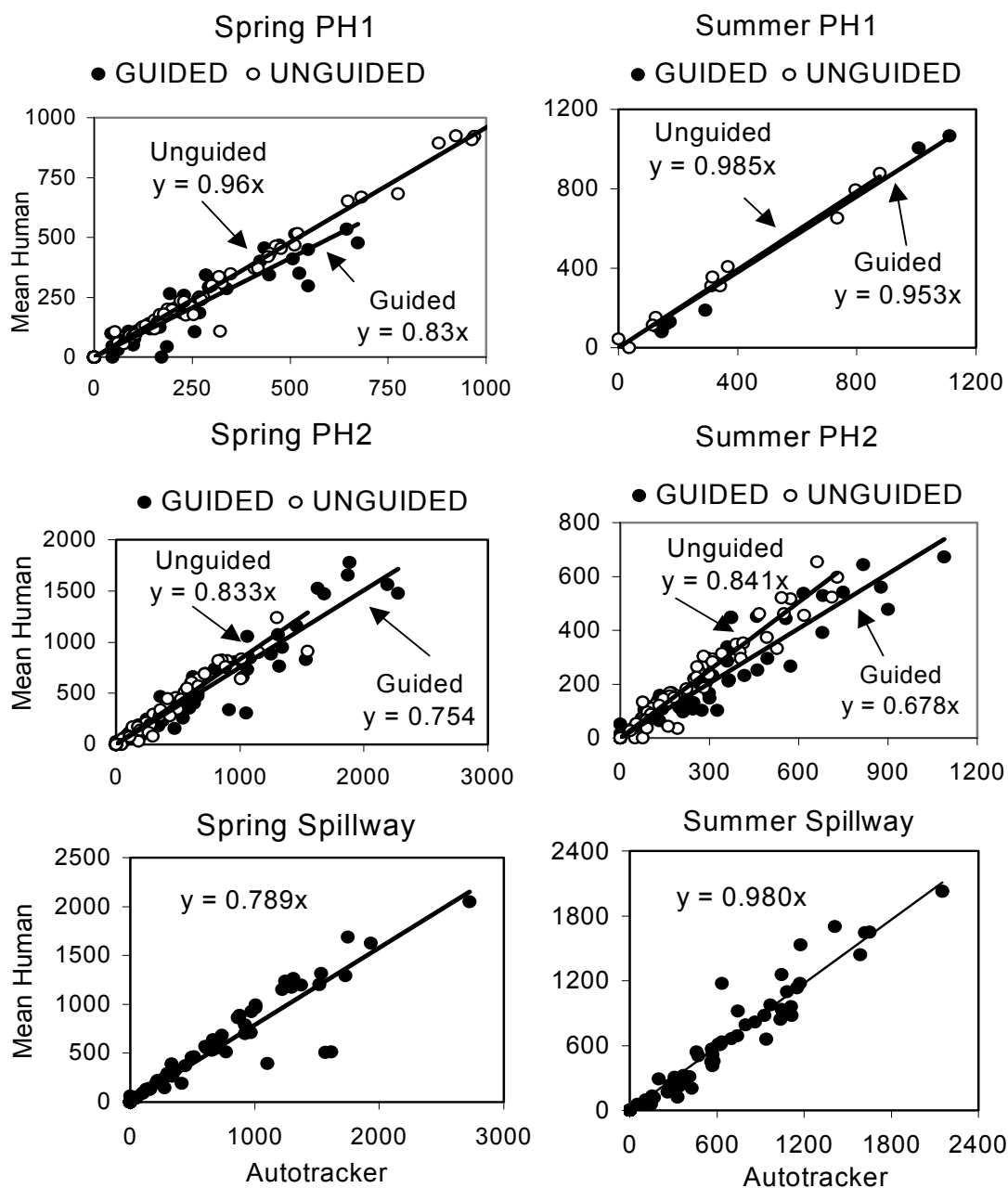
Figure 3.6. Regressions of Autotracker-Based Expanded Hourly Estimates and Mean Human-Based Expanded Hourly Estimates. These same data appear in Figure 3.5 and 3.6 except that the regression lines have been forced through the origins of the graphs. The slopes of these regression lines are the values with which passage estimates were adjusted.

3.3   Major Passage Metrics

3.3.1   Project and Powerhouse FPE

Project-wide FPE estimates are presented in Figure 3.7. Project-wide FPE was 63% in spring and 53% in summer. During spill periods, the summertime FPE estimate was slightly higher than the estimate for spring. The opposite was true during non-spill periods, when the FPE estimate was higher in spring than in summer. The FPE estimate for Powerhouse 1 declined from 49% with a 95% confidence interval (CI) of 4.3% in spring to 40% (CI = 3.6%) in summer, a drop of 9%. The FPE for Powerhouse 2 declined even more across seasons (>15%), with estimates of 57% (CI = 1%) and 42% (CI = 1%) in the spring and summer, respectively. The FPE for powerhouse 2 and the spillway (excluding Powerhouse 1) was 64% in spring and 54% in summer. These estimates were both 1% lower than for the entire project.
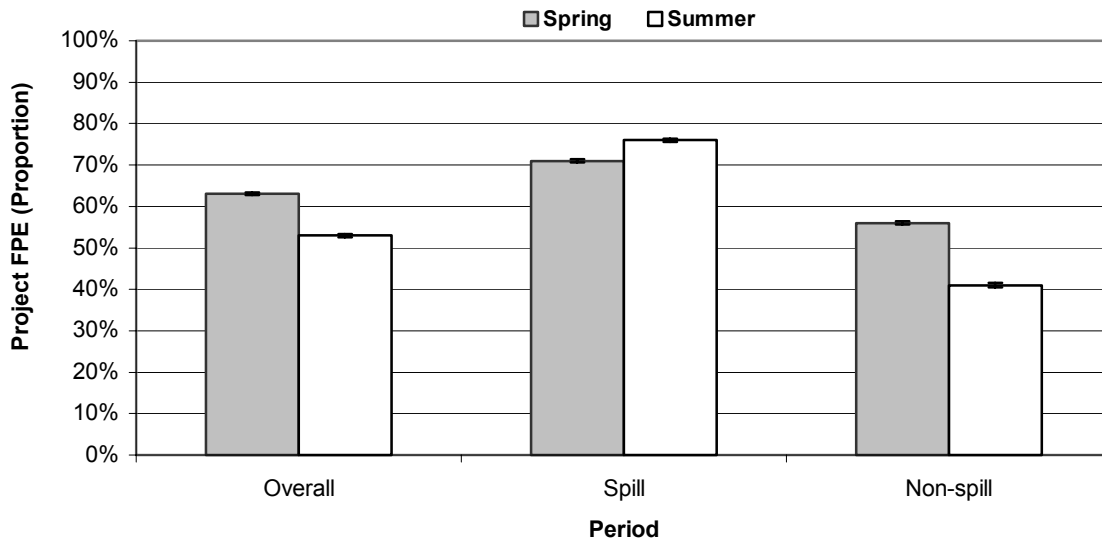
Figure 3.7. Project-Wide Fish Passage Efficiency Estimates for Spring and Summer Seasons at Bonneville Dam in 2001. Estimates are presented by spill and no-spill periods, and overall. Error bars represent 95% confidence intervals.

3.3.2   Spill Efficiency and Effectiveness

Spill efficiency was 14% (CI = 0.4%) in spring and 20% (CI = 0.6) in summer. For periods of spill, spill efficiency was 33 %(CI = 1%) in spring and 58% (CI = 1.2%) in summer. Spill effectiveness was 0.84 (CI = 0.01) in spring and 1.83 (CI = 0.02) in summer. For periods of spill, spill effectiveness was 0.93 (CI = 0.02) in spring and 1.6 (CI = 0.02) in summer.

3.3.3   Effects of Spill Level

We plotted estimates of FPE and spill efficiency on the number of hours of spill per day in spring 2001 (Figure 3.8). Spill discharge was nearly constant at about 50,000 cfs during hours or

days when water was spilled in spring and summer 2001, and therefore we could not examine the effect of spill discharge or fraction on major passage metrics. In summer, there was only 10 days of 50,000 cfs spill and only one of those days had less than 24 hours of spill.
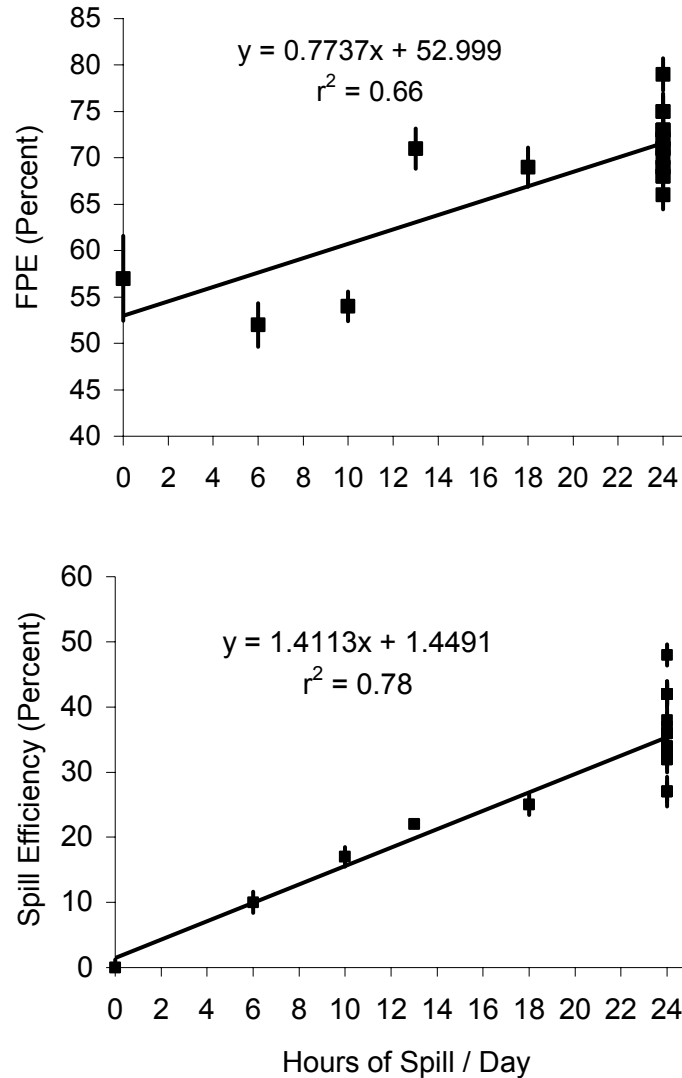
Figure 3.8. Plot of Project FPE and Spill Efficiency on Hours of Spill per Day at Bonneville Dam in 2001

3.3.4 Comparison with Radio Telemetry Estimates

We recalculated hydroacoustic estimates based on the USGS's data collection schedule during their radio telemetry study so that we would be comparing the same days in spring and summer. In general, the hydroacoustic estimates are higher than are the radio telemetry estimates (Table 3.8). Powerhouse 1 FGE in summer is the only exception. The largest difference is that

for Powerhouse 2 FPE and FGE, which differs by 14%. Spring Project FPE is 11% higher by hydroacoustics than by radio telemetry. Otherwise, the estimates are within 10% or less.

Even during "no spill" conditions spill bays 1 and 18 each discharged attraction flow for adult salmonids (about 2 % of project discharge in spring and about 3% in summer) and a few radio tagged fish could and did pass there when no other bays were open. There was no hydroacoustic sampling of those end spill bays.

Table 3.1. Comparison of Fish-Passage Metrics Estimated by Hydroacoustics (HA) and Radio Telemetry (RT) at Bonneville Dam in 2001. Data from non-overlapping parts of seasons have been deleted and adjusted so that time periods reported here are the same for both methods. Those dates are May 1-June 9 for spring and July 1-July 15 for summer. Some hydroacoustic FGEs are slightly different than those reported elsewhere because the times have been adjusted to match those for radio telemetry.

Metric	Season and Spill Conditions	HA	RT	Difference
Project FPE[a]	Spring overall	67%	56%	11% (HA>RT)
	Spring (about 37% spill)	71%	64%	7% (HA>RT)
	Spring (about 2% spill)	56%	47%	9% (HA>RT)
PH1 FGE	Spring overall	47%	45%	2% (HA>RT)
	Spring (about 37% spill)	39%	N/A[2]	
	Spring (about 2% spill)	50%	45%	5% (HA>RT)
PH1 FPE	Spring overall	N/A[a]	87%	
	Spring (about 37% spill)	N/A[a]	100%	
	Spring (about 2% spill)	N/A[a]	86%	
PH2 FGE & FPE	Spring overall	56%	46%	10% (HA>RT)
	Spring (about 37% spill)	55%	49%	6% (HA>RT)
	Spring (about 2% spill)	57%	43%	14% (HA>RT)
Spill Efficiency	Spring overall	26%	16%	10% (HA>RT)
	Spring during spill	38%	30%	8% (HA>RT)
Spill Effectiveness	Spring overall	1.21	0.70	0.51 (HA>RT)
	Spring during spill	1.13	0.86	0.27 (HA>RT)
Project FPE	Summer overall (about 3% spill)	44%	40%	4% (HA>RT)
PH1 FPE	Summer overall (about 3% spill)	N/A[b]	89%	
PH1 FGE	Summer overall (about 3% spill)	47%	57%	10% (RT>HA)
PH2 FGE & FPE	Summer overall (about 3% spill)	44%	35%	9% (HA>RT)

[a] The radio telemetry FPE estimates include fish that pass by the sluiceway at Powerhouse 1. There was no hydroacoustic sampling of Powerhouse 1 sluiceway passage and so there can be no hydroacoustic estimate made to compare directly with the radio telemetry Project or Powerhouse 1 FPE estimates. Since the Powerhouse 2 sluiceway was closed in both seasons FPE = FGE for both hydroacoustic and radio telemetry data at Powerhouse 2. Since the Powerhouse 1 sluiceway handled a very small proportion of the total project passage we neglected this distinction at the project level.

(b) During spring 37% spill, only four radio-tagged fish were tracked through Powerhouse 1 and they all passed by the sluiceway, which was not sampled by hydroacoustics. Powerhouse FGE is the proportion of all fish guided divided by the sum of guided and unguided (turbine) fish. In this case Powerhouse 1 FGE would equal 0/0, which is undefined.

3.4   Spatial Trends in Fish Passage

3.4.1   Horizontal Distributions

We estimate that just over 6.15 M fish passed the project during the 46 spring days that we sampled, with nearly 80% (4.9 M fish) passing at Powerhouse 2, about 14% (0.84 M fish) passing by spill, and about 7% (0.42 M fish) passing Powerhouse 1 (Figure 3.9). Project flow was similar to fish passage, with 76% of discharge occurring at Powerhouse 2, about 16% at the spillway, and about 7% at Powerhouse 1 (Figure 3.10). The density of fish passage, in the number of fish per million cubic meters of water (fish/M m^3), was highest at Powerhouse 2 (474 fish/M m^3), followed by Powerhouse 1 (428 fish/M m^3) and the spillway (384 fish/M m^3).

About 70% of the 0.42 M fish that passed at Powerhouse 1 passed through Units 9 and 10 (Figure 3.9), as did 73% of the Powerhouse 1 discharge (Figure 3.10). Fish passage and flow were low throughout the rest of Powerhouse 1, with the exception of Units 1 and 2, which passed 8% of the fish with 14% of the flow, and 9% of the fish with 7% of the flow, respectively.

Fish passage at Powerhouse 2 was noticeably skewed towards the south half of the powerhouse (Figure 3.9). About 70% of the fish passing through Powerhouse 2 passed through Units 11 through 14, although these units only discharged slightly more than half of the water (52.6%; Figure 3.10).
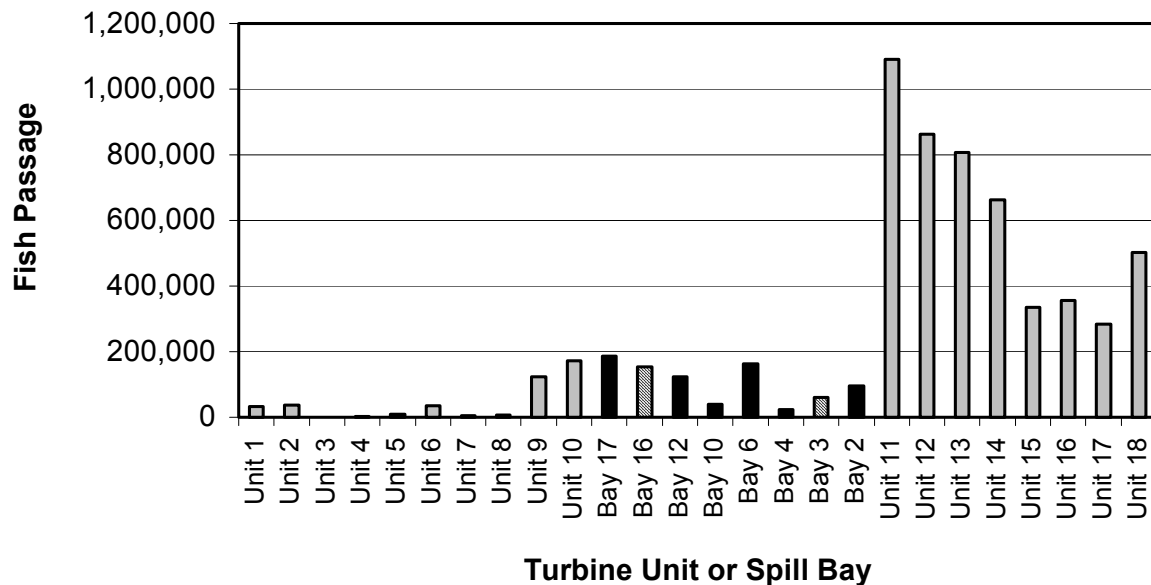
Figure 3.9. Horizontal Distribution of Fish Passage through Turbines (gray bars) and Spill Bays (black or striped bars) in Spring. Spill bays 1 and 18 that were opened only 4 inches and other bays that were closed all season (bays 5, 7-9, 11, and 13-15) are not displayed. Estimates for spill bays 3 and 16 were interpolated from those of the nearest operating spill bays.

The highest proportions of the fish that passed the project at the spillway passed through Bay 6 (where 19% of all spillway passage occurred), Bay 16 (18% of spillway passage), and Bay 17 (22% of spillway passage; Figure 3.9). Passage was distributed unevenly across the spillway but was somewhat skewed towards the south side. Spill discharge was relatively constant in spring and summer at about 50,000 cfs, and the spill pattern (bays and gate openings) varied little (Figure3.10).
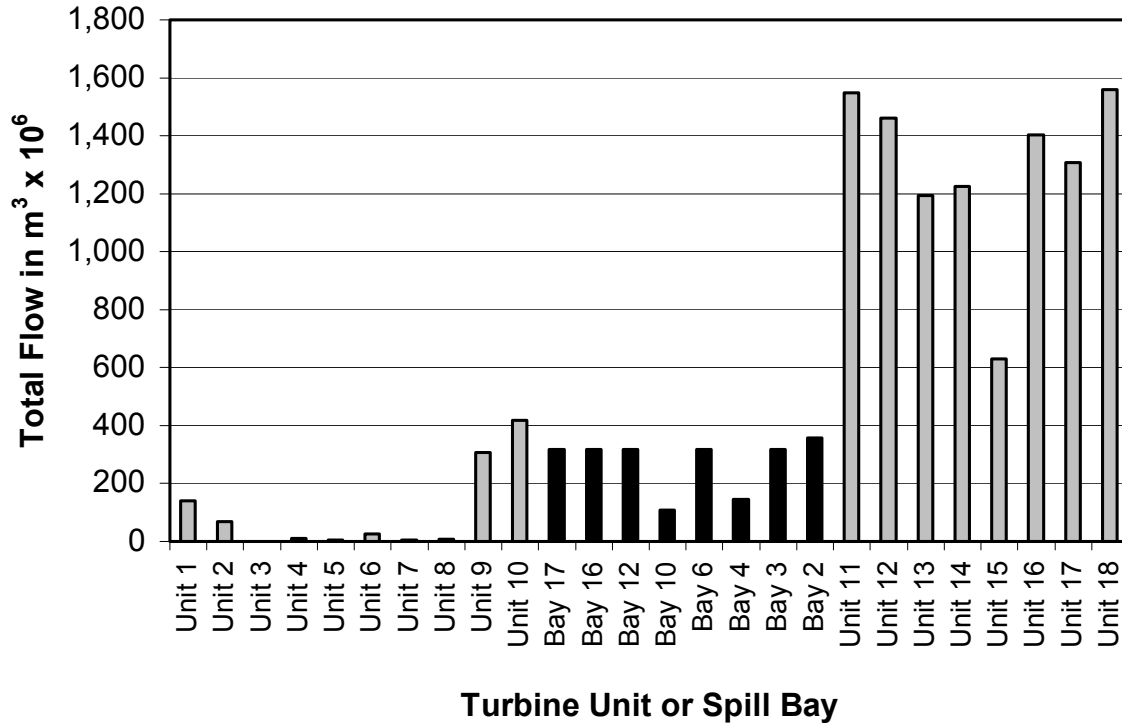
Figure 3.10. Horizontal Distribution of Discharge through Turbines (gray bars) and Spill Bays (black bars) in Spring. Spill bays 1 and 18 that were opened only 4 inches and other bays that were closed all season (bays 5, 7-9, 11, and 13-15) are not displayed.

In summer, we estimate that 5.1 M fish passed Bonneville Dam during the 40 days we sampled. Of these, 3.7 M or about 72% of total project passage passed at Powerhouse 2, along with 80% of project discharge (Figures 3.11 and3.12). The Spillway passed 1 M fish or about 20% of the project total in about 11% of project discharge. Powerhouse 1 passed about 4% of all fish in summer (0.4 M fish) in about 7.5% of the total discharge.

Nearly 75% of the fish that passed Powerhouse 1 in the summer passed at Unit 9 and Unit 10, along with 81% of the water (Figure 3.11 and 3.12). Discharge at Powerhouse 1 was very low during the summer and was mostly allocated to Units 1, 9, and 10 (Figure 3.12), and Unit 1 passed about 5% of the fish in about 10.6% of the flow. Of the remaining units, significant passage occurred only at Unit 6, which passed 12.6% of the fish in less than 3% of the flow.
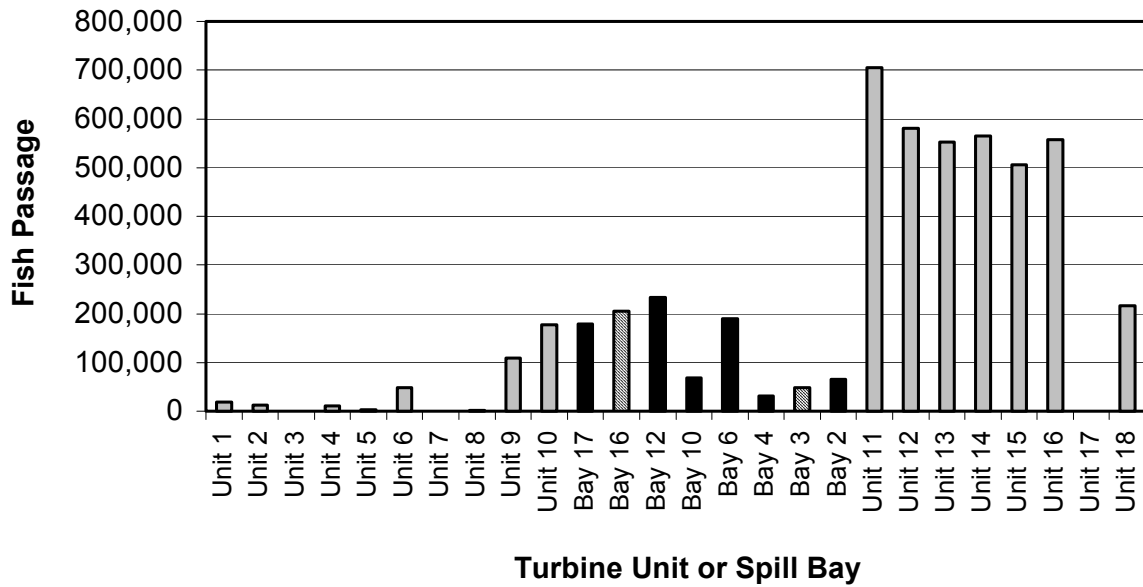
Figure 3.11. Horizontal Dstribution of Fish Passage through Turbines (gray bars) and Spill Bays (black or striped bar) in Summer. Spill bays 1 and 18 that were opened only 4 inches and other bays that were closed all season (bays 5, 7-9, 11, and 13-15) are not displayed. Estimates for spill bays 3 and 16 were interpolated from those of the nearest operating spill bays. Turbine unit 17 did not operate in summer.
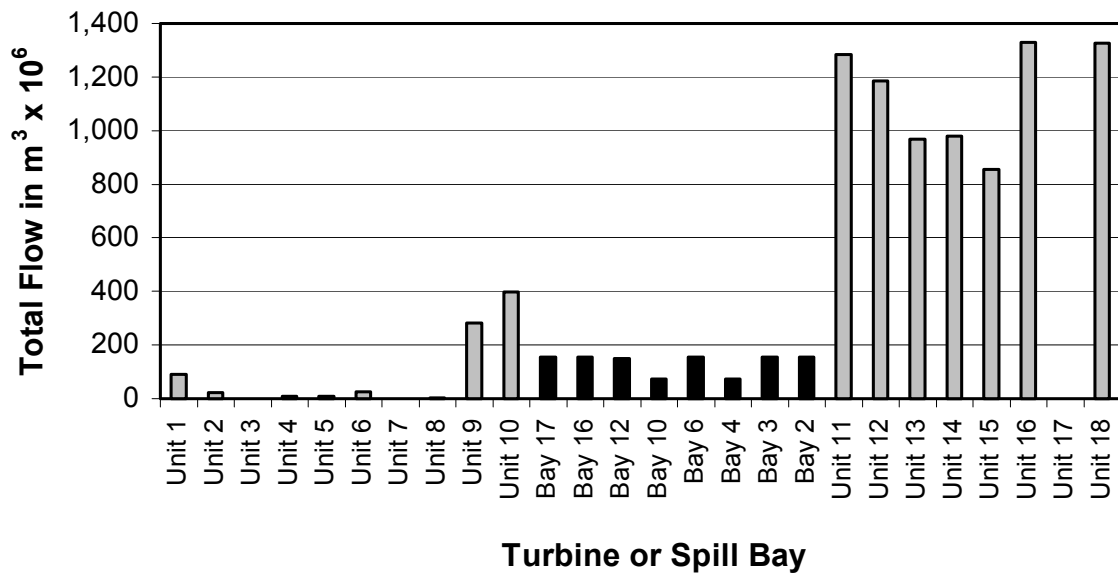
Figure 3.12. Horizontal Distribution of Discharge through Turbines (gray bars) and Spill Bays (black bars) in Summer. Spill bays 1 and 18 that were opened only 4 inches and other bays that were closed all season (bays 5, 7-9, 11, and 13-15) are not displayed. Turbine unit 17 did not operate in summer.

To better compare fish passage among the individual units of Powerhouse 2, we standardized passage by reporting the density of fish passage in fish per volume of water in both spring (Figure 3.13) and summer (Figure 3.14). Density was highest at the southern and central units (Units 11 through 15), ranging from 531 to 703 fish passed per M m^3 water discharged. Fish passage density was lowest at the three northern units (Units 16, 17, and 18), ranging from 217 to 321 fish passed per M m^3 water discharged.
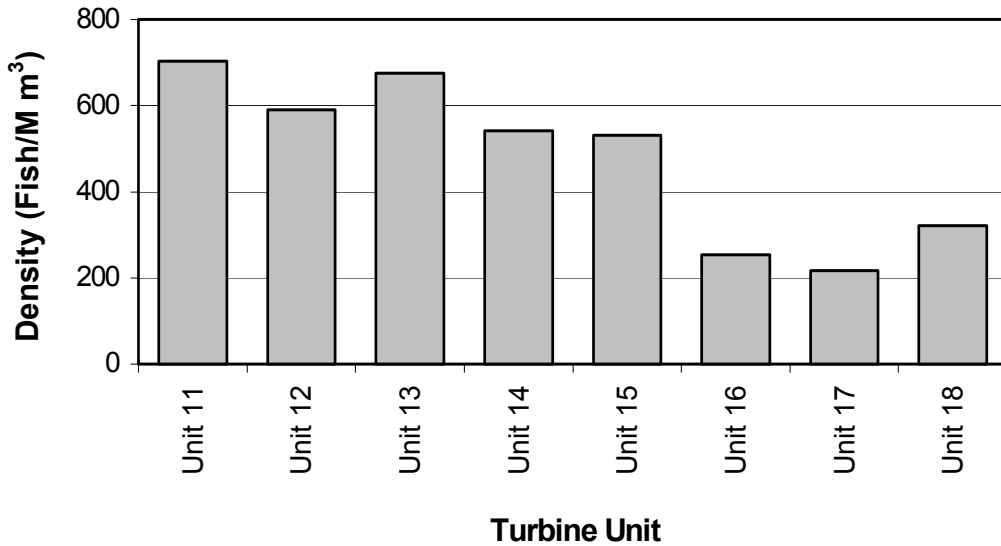
Figure 3.13. Horizontal Distribution of Fish Passage Density, in Fish per Millions of Cubic Meters of Water by Turbine Unit at Powerhouse 2 in Spring
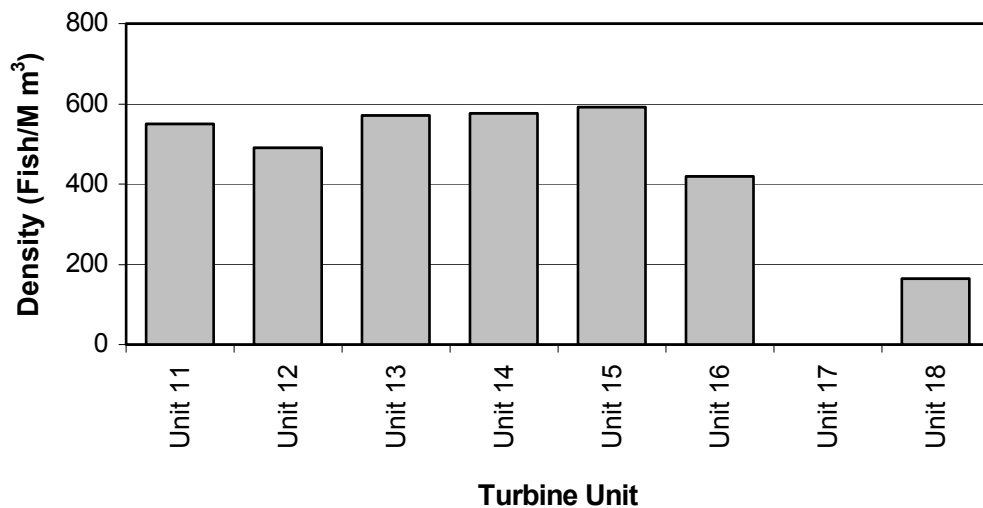
Figure 3.14. Horizontal Distribution of Fish Passage Density, in Fish per Million Cubic Meters of Water, at Powerhouse 2 in Summer

Spillway discharge was terminated on Julian date 166, 10 days into the summer sampling season. For the entire summer sampling season, 11% of all fish passage occurred at the spillway along with 20% of all discharge. During the ten days that the spillway was operating, however, the spillway passed 58% of the fish in 40% of the water (Figure 3.15 and Figure 3.16).
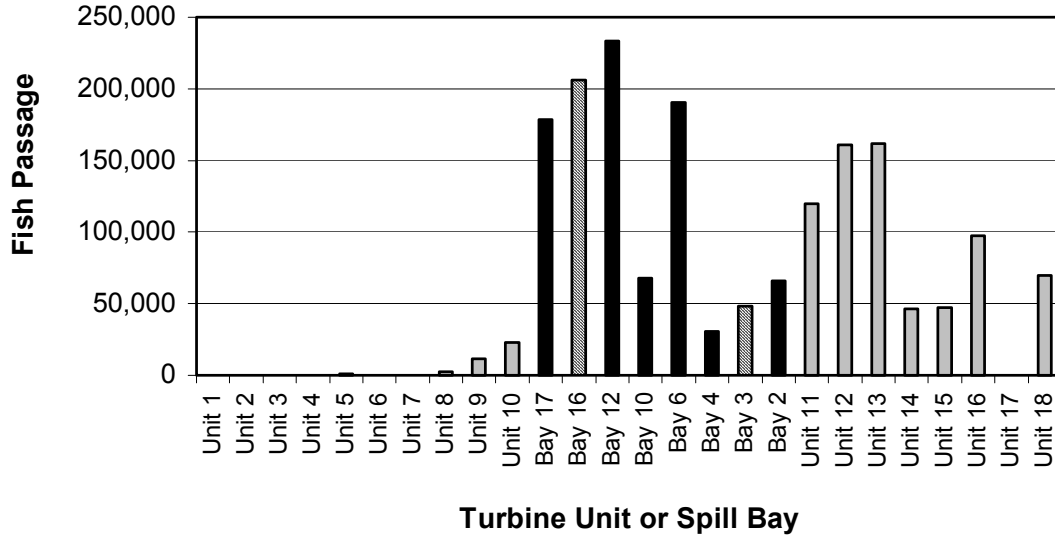
Figure 3.15. Horizontal Distribution of Fish Passage at Turbines (gray bars) and Spill Bays (black or striped bars) during the Ten Days that Spill Occurred in Summer. Spill bays 1 and 18 that were opened only 4 inches and other bays (bays 5, 7-9, 11, and 13-15) that were closed all season are not displayed. Estimates for spill bays 3 and 16 were interpolated from those of the nearest operating spill bays. Turbine Unit 17 did not operate in summer.
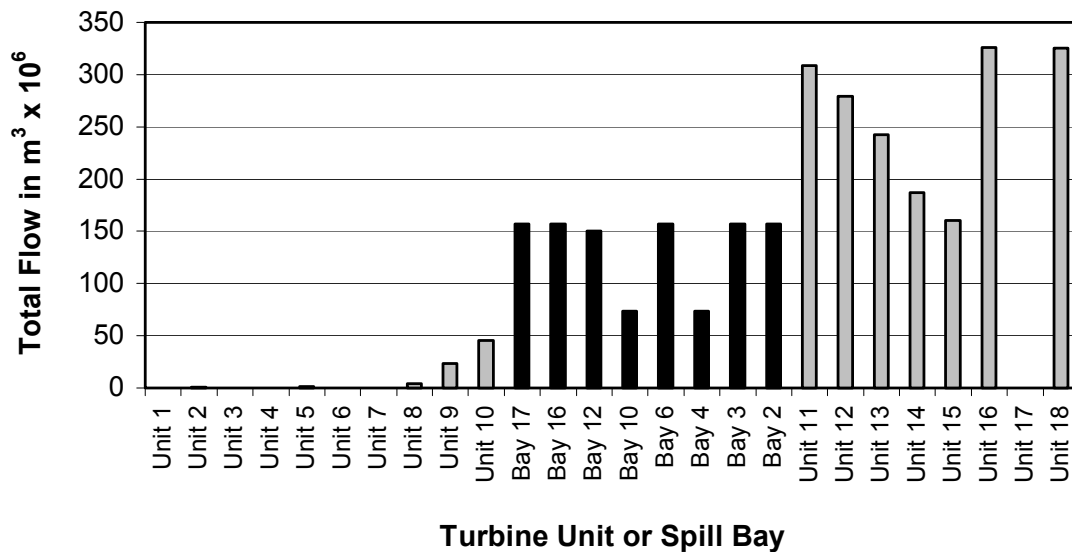
Figure 3.16. Horizontal Distribution of Discharge at Turbines (gray bars) and Spill Bays (black bars) during the Ten Days that Spill Occurred in Summer. Spill bays 1 and 18 that were opened only 4 inches and other bays that were closed all season (bays 5, 7-9, 11, and 13-15) are not displayed. Turbine Unit 17 did not operate in summer.

3.4.2 Vertical Distributions

3.4.2.1 Powerhouse 1 – Inside Intake 10b

At powerhouse 1, we examined the vertical distribution of fish detected by split-beam transducers sampling inside Intake 10B. In spring, we classified about 47% of all fish as guided by the STS (Figure 3.17), but in summer, that percentage fell to about 36% (Figure 3.18).
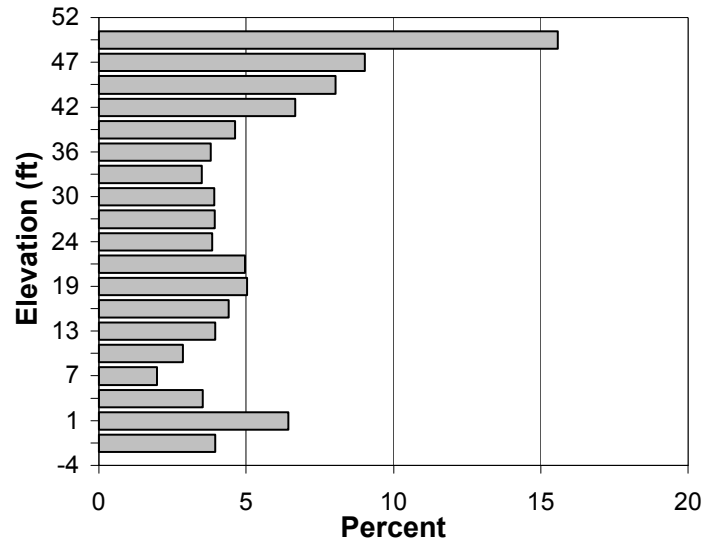
Figure 3.17. Vertical Distribution of Smolt-Sized Fish Detected inside Intake 10b at Powerhouse 1 in Spring 2001
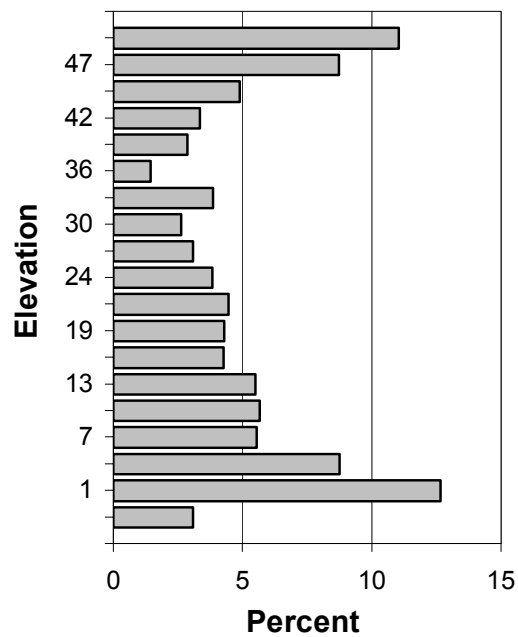
Figure 3.18. Vertical Distribution of Smolt-Sized Fish Detected inside Intake 10b in Summer 2001

3.4.2.2 Powerhouse 2 - Upstream and Downstream of Intake 15<u>b</u>

At Powerhouse 2, we examined the vertical distribution of fish detected upstream and downstream of the trash racks at Intake 15<u>b</u>, where the gatewell and vertical barrier screen had been modified to increase flow up into the gatewell. We also examined the direction of travel of detected fish through three split-beams to better characterize the behavior of fish approaching trash racks and the effect on FGE in spring and summer.

Theoretical (expected) FGE based upon the vertical distribution upstream and downstream of the trash racks at modified Unit 15 (Intake <u>b</u>) was similar to the observed in-turbine FGE for all hours sampled in spring but not in summer (Figure 3.19). Theoretical FGE is defined as expected FGE based upon the upstream vertical distribution relative to an elevation for classifying guided and unguided fish projected upstream parallel to the intake roofline from the elevation used inside the turbine. The FGE of 50% in summer was 29% less than the theoretical FGE. In spring, fish detected 16 to 21 ft upstream of trash racks were higher in the water column than fish detected 4 to 9 ft from the racks (Figure 3.20). A similar pattern was observed in summer (Figure 3.21), but the peak in the distribution of fish 4 to 9 ft from trash racks was several feet lower in the water column than the peak for fish 4 to 9 ft from racks in spring (compare Figures 3.20 and 3.21). The downward shift in the distribution of fish approaching the trash racks was observed during the day and at night (Figure 3.21).
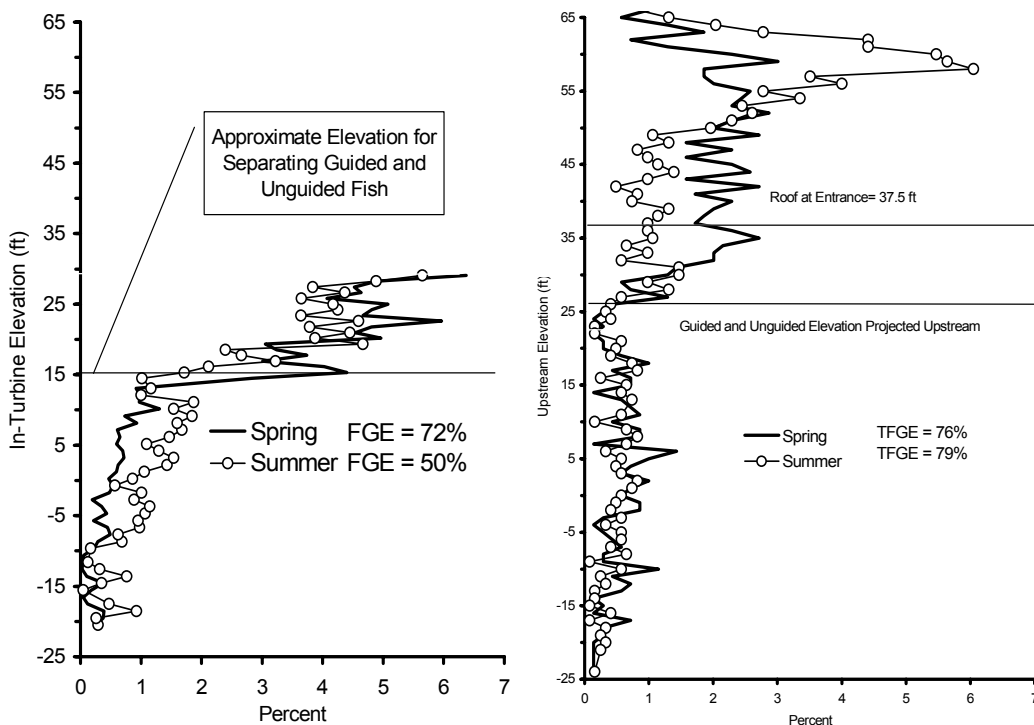
Figure 3.19. Vertical Distributions Upstream (right) and Downstream of the Trash Racks at Modified Unit 15 (Intake b). Theoretical FGE is defined as expected FGE based upon the upstream vertical distribution in spring and summer relative to an elevation for classifying guided and unguided fish projected upstream parallel to the intake roof line from the elevation used inside the turbine.
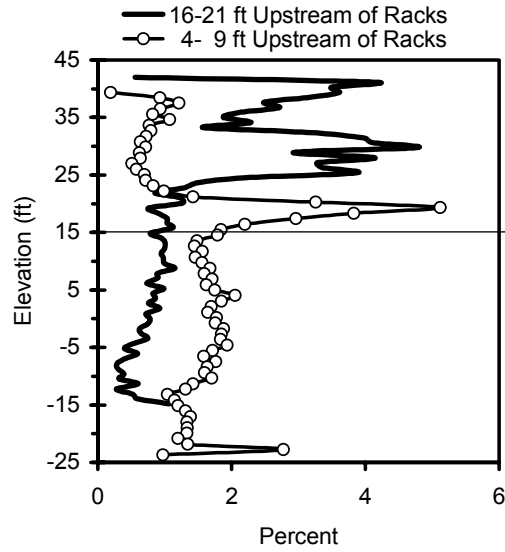
Figure 3.20. Vertical Distributions of Fish 4 to 9 and 16 to 21 ft Upstream of Intake 15<u>b</u> Trash Racks in Spring
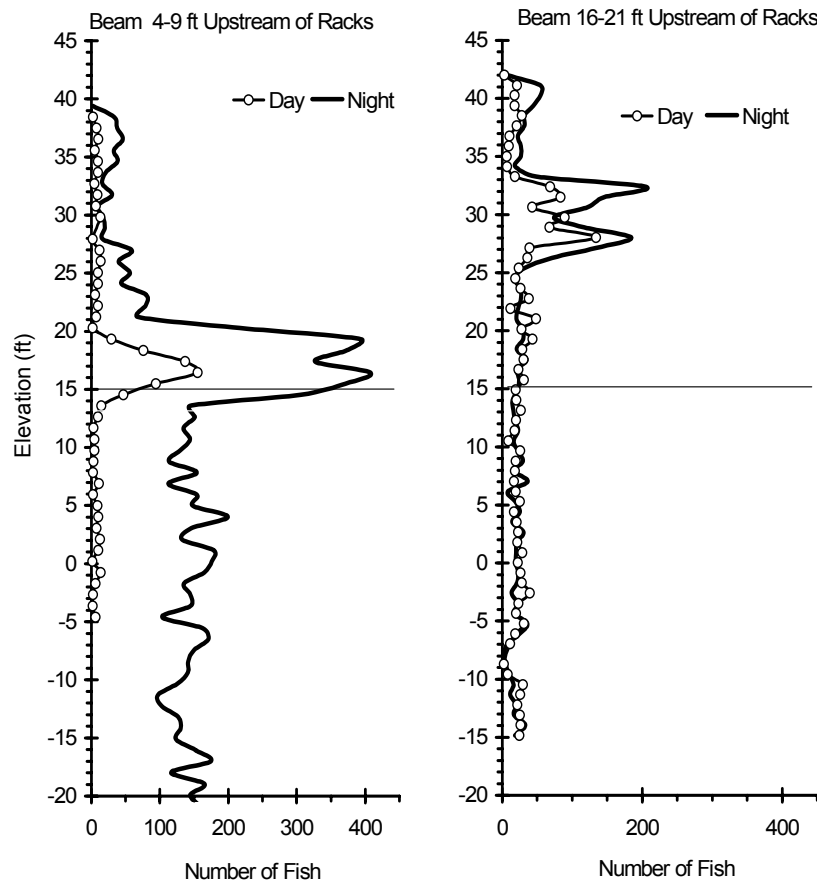
Figure 3.21. Vertical Distributions of Fish 4 to 9 and 16 to 21 ft Upstream of Trash Racks at Intake 15<u>b</u> in Summer

The azimuth direction of travel of fish and the number of detections in each of the three successive split beams differed considerably. In spring and summer, 16% and 17% more fish were moving downstream when passing through the beam sampling 10 to 15 ft upstream of trash racks, than when passing through the beam 4 to 9 ft from trash racks (Figures 3.22 and 3.23). In addition, the number of fish detections was much higher in the downstream and upstream beams, particularly the beam nearest the trash racks, than the number detected in the center beam. Near the trash racks, only 54% to 55% of the fish were moving downstream.
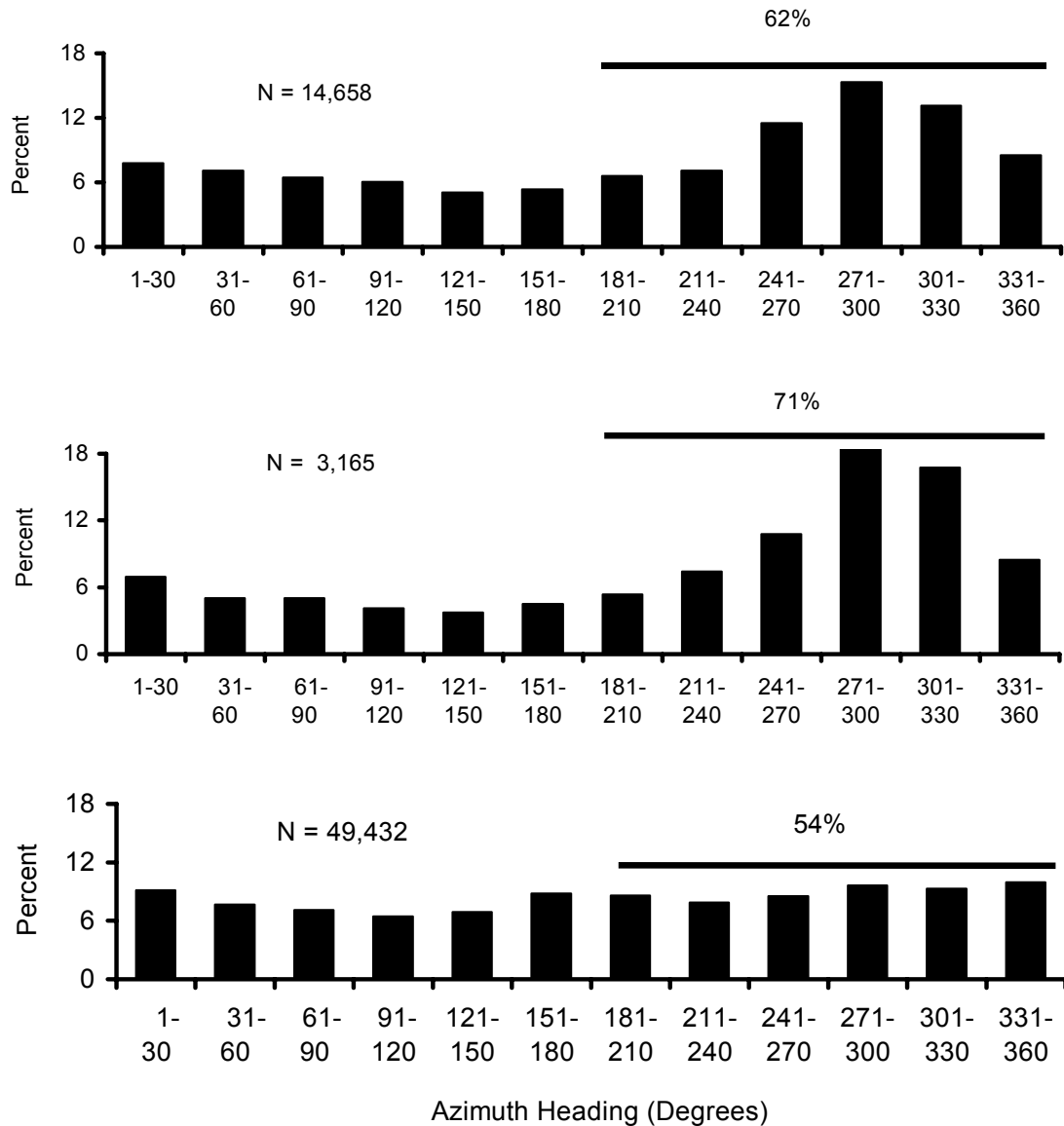
Figure 3.22. Distribution of Azimuth Headings of Fish Approaching Trash Racks at Intake 15b in Spring. Data were from down-looking, 6° split beams sampling about 4 to 9 ft (bottom plot), 10 to 15 ft (middle plot), or 16 to 21 ft (top plot) upstream of trash racks.
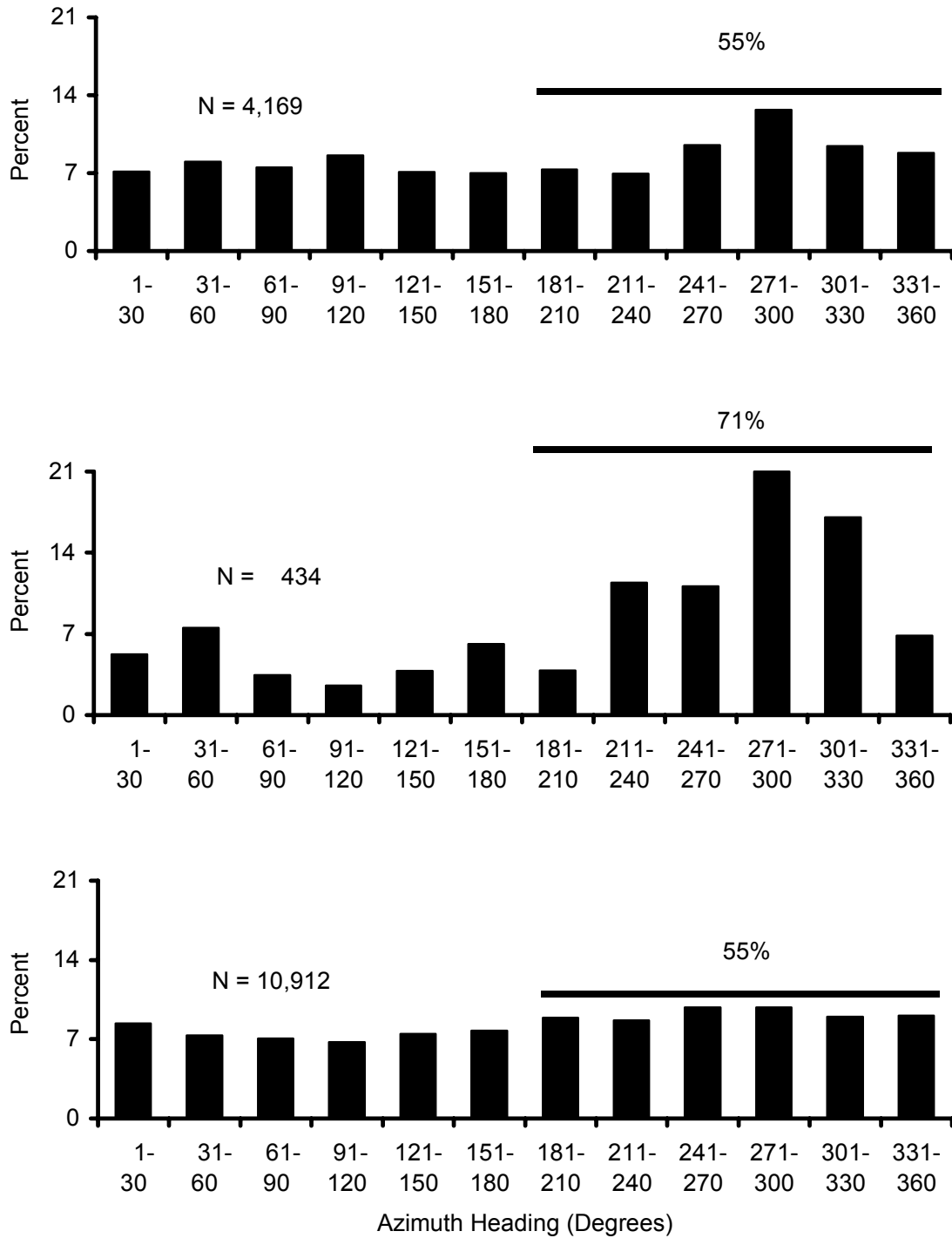
Figure 3.23. Distribution of Azimuth Headings of Fish Approaching Trash Racks at Intake 15b in Summer. Data were from down-looking, 6° split beams sampling about 4-9 ft (bottom plot), 10-15 ft (middle plot), or 16-21 ft (top plot) upstream of trash racks.

3.5   Temporal Trends in Fish Passage

3.5.1   Seasonal Trends

3.5.1.1 Run Timing

The run timing curve in 2001 based on hydroacoustic estimates shows that the spring peak occurred on 21 April and the summer peaks occurred on 8 and 27 June (Figure 3.24). During spring, the Juvenile Bypass System (JBS) smolt index data at the Bonneville Project indicated temporal trends similar to those observed with hydroacoustic sampling, with peaks and troughs in general agreement. Although there is some agreement between the two sampling methods in the summer, the peaks detected with hydroacoustics on 8 and 27 June were not reflected in the JBS sampling. The ratio of percentages there was good agreement between the two estimates except for a few dates where larger deviations were apparent.
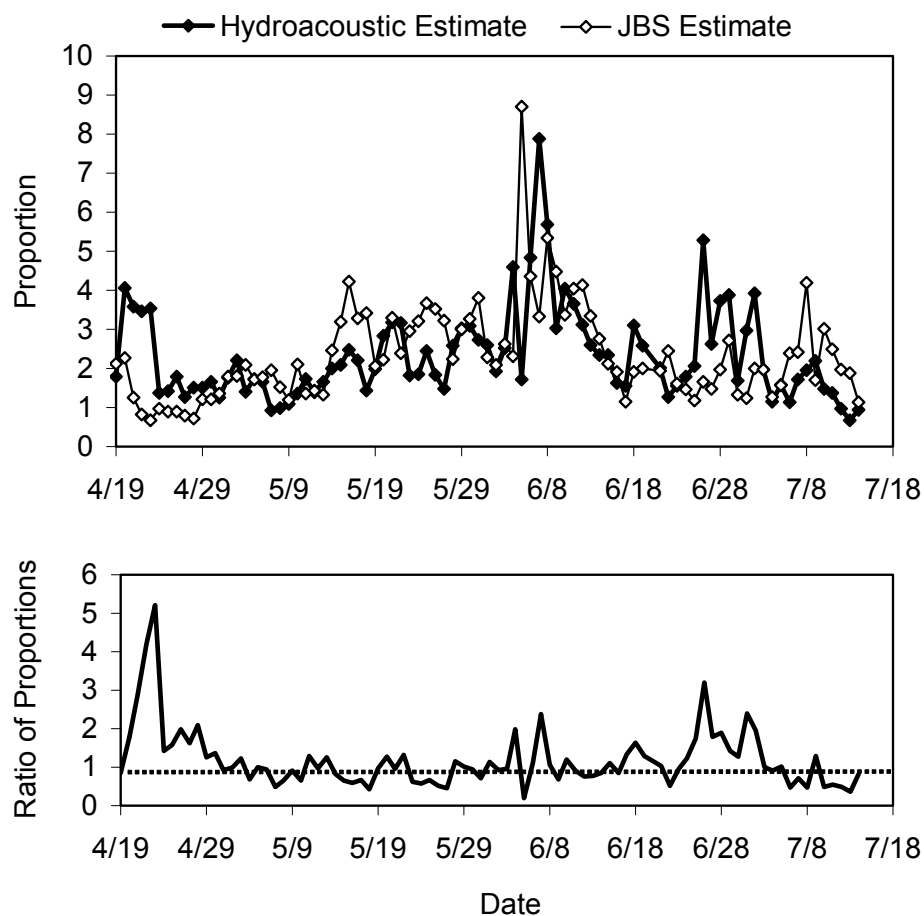
Figure 3.24. Patterns of Run Timing through the Spring and Summer Seasons at Bonneville Dam in 2001 Estimated with Hydroacoustics and by Sampling a Smolt Trap in the Juvenile Bypass System (upper plot) and the Ratio of the Two Estimated Proportions (lower plot)

3.5.1.2 Major Fish-Passage Metrics

Project FPE was about 57% in spring with no visually obvious trend until spill began on about 15 May when FPE began a gradual increase into early summer (Figure 3.25). The average FPE during spring spill was about 71% and 76% during the 9 days of spill in early summer. Fish passage efficiency dropped down to 34% on 16 June when spill ended, and it averaged about 40% with ± 10% fluctuations for the rest of summer.
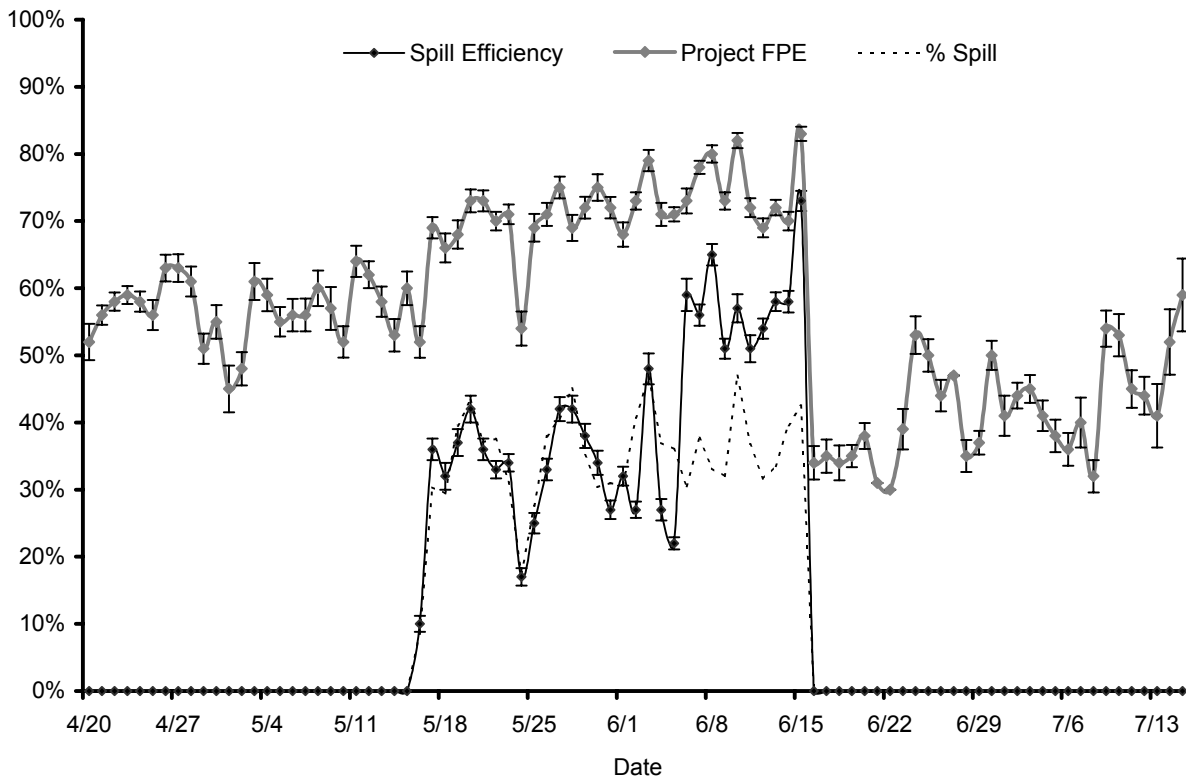
Figure 3.25. Estimated Project FPE and Spill Efficiency, and Proportion of Water Spilled at Bonneville in 2001. Error bars represent 95% confidence limits.

Powerhouse 1 FPE estimates averaged 49% in spring and 40% in summer, but all daily estimates for Powerhouse 1 were much more variable than estimates for Powerhouse 2 (Figure 3.26). Powerhouse 2 estimates averaged 57% in spring and 42% in summer, ranging from a high of 65% on 30 May to a low of 0.29% on 14 June.

Spill efficiency varied considerably from day to day but exhibited a general upward trend from 16 May, when spill began, through 15 June, the last day of spill in 2001 (Figure 3.25). Spill efficiency tracked the spill proportion during the first half of the spill season but not the second half. Daily spill effectiveness estimates varied from an initial high of 1.3 on 6 May to a low of 0.6 on 26 May before increasing to the spill period high of 1.96 on 29 May (Figure 3.27). As daily discharge over the spillway increased, spill effectiveness decreased. Conversely, as spill discharge decreased, spill effectiveness increased. However, the peak in spill effectiveness on 29 May was not the result of a substantial drop in spill discharge, as discharge volume remained relatively constant to the previous day's discharge.
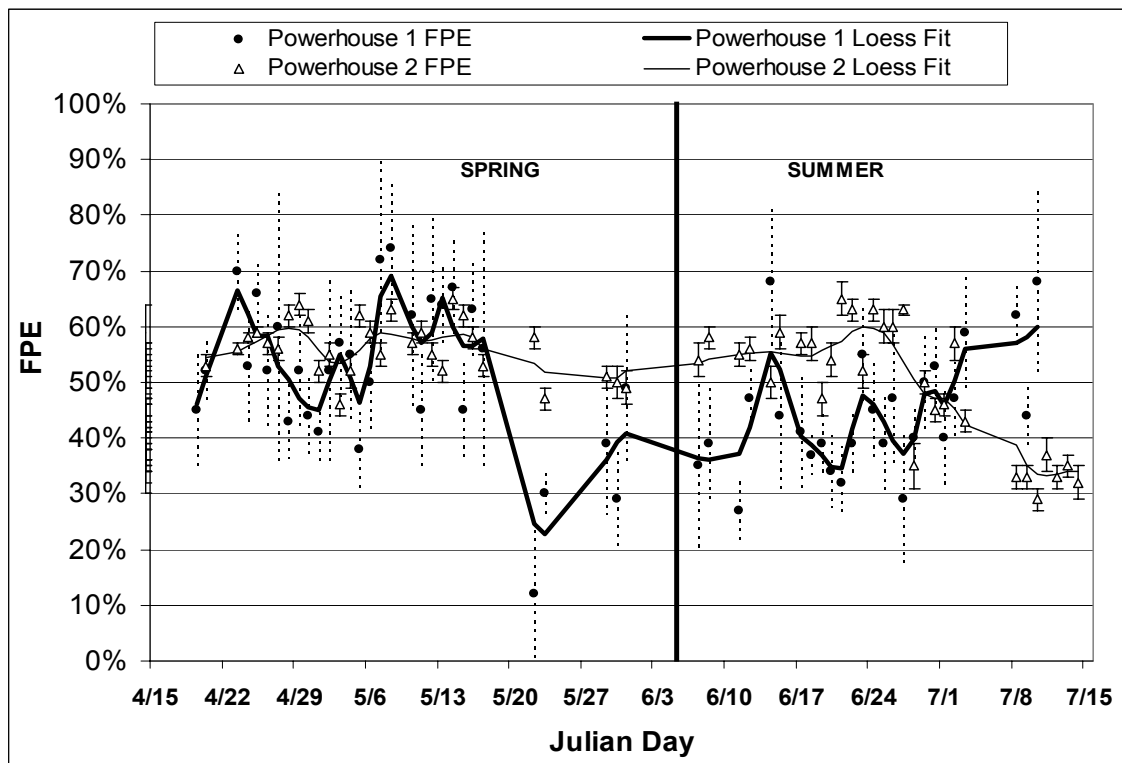
Figure 3.26. Daily Fish Passage Efficiency Estimates for both Powerhouses at Bonneville Dam in 2001. Error bars represent 95% confidence limits.
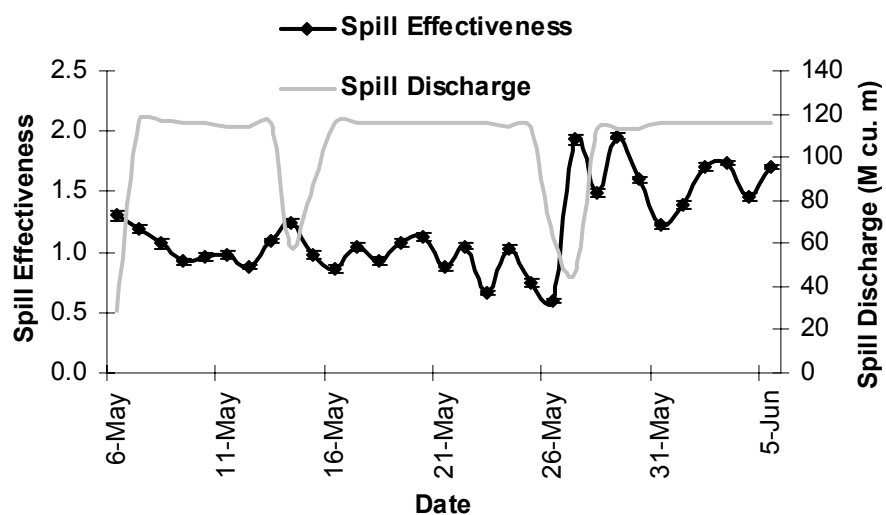
Figure 3.27. Daily Spill Effectiveness Estimates and Spill Discharge during the Limited Spill Period at Bonneville Dam in 2001. Error bars represent 95% confidence intervals.

3.5.1.3 Guidance Efficiency at Modified Unit 15

Daily estimates of FGE for modified intake 15b and 15c based upon all hours sampled each day decreased significantly from spring to summer but were highly variable in both seasons (Figure3.28). Generally FGE estimates for each intake trended downward through the spring and into the second week in June, then trended upward through the remaining sampling period before dipping again at the very end of the summer.

Mean FGE for Intake 15b was significantly higher than for Intake 15c in spring (72.0% vs. 59.0%) and in summer (50% vs. 44%). In spring, there were 32 days for which we had FGE estimates for both intakes 15b and 15c, and a paired t-test comparing the mean FGEs for each found the difference significant (p = 0.00078). In summer, there were 31 days with estimates for both intakes and again the difference was significant (p = 0.00166). Intake 15b was between two turbine intake extensions (TIEs) and Intake 15c was behind an extension. Although there was agreement between intake FGE estimates for some days (e.g., on 1 and 2 June the estimates were within 1% of one another), there were also days with large disparity between the intake FGE estimates (on 24 April the FGE for Intake 15b was 35% greater than for Intake 15c). In spring, there were 32 days for which we had FGE estimates for both intakes 15b and 15c and paired t-tests comparing the mean FGEs for each found the difference significant (p = 0.00078. In summer there were 31 days with estimates for both intakes and again the difference was significant (p = 0.00166). In both cases, the FGE of Intake 15b was higher than that of 15c.
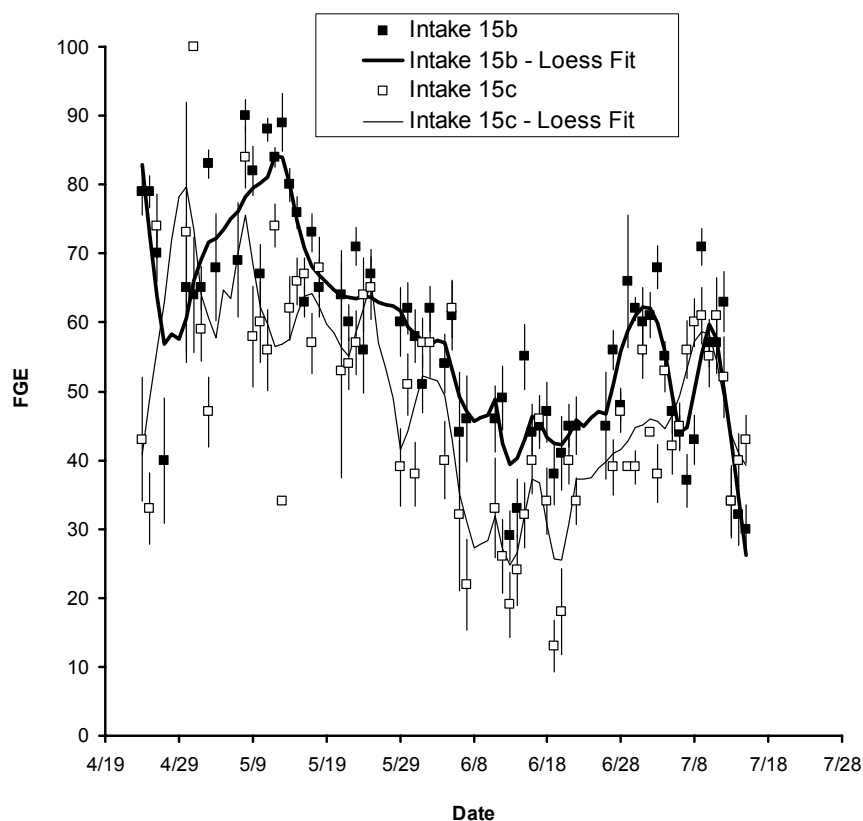
Figure 3.28. Estimates of Fish Guidance Efficiency (FGE) throughout Spring and Summer at Intake 15b and 15c at Bonneville Dam in 2001. Error bars represent 95% confidence intervals.

3.5.1.4 American Shad Run Timing

American shad present a problem for hydroacoustic sampling in summer. Almost 2.3 million American shad migrated up through Bonneville Dam in 2001. Shad began arriving at the dam in mid May and showed up in large numbers during the third week in May (> 50,000 / day) before peaking on 1 June when 144,000 individuals were observed (Figure 3.29). By 6 June, 50% of all the migrating shad had already passed the dam. By 30 June, the shad migration was essentially complete with over 98% of all fish having passed by that day. Nearly twice as many shad passed through Bonneville Dam in 2001 as passed in 2000.
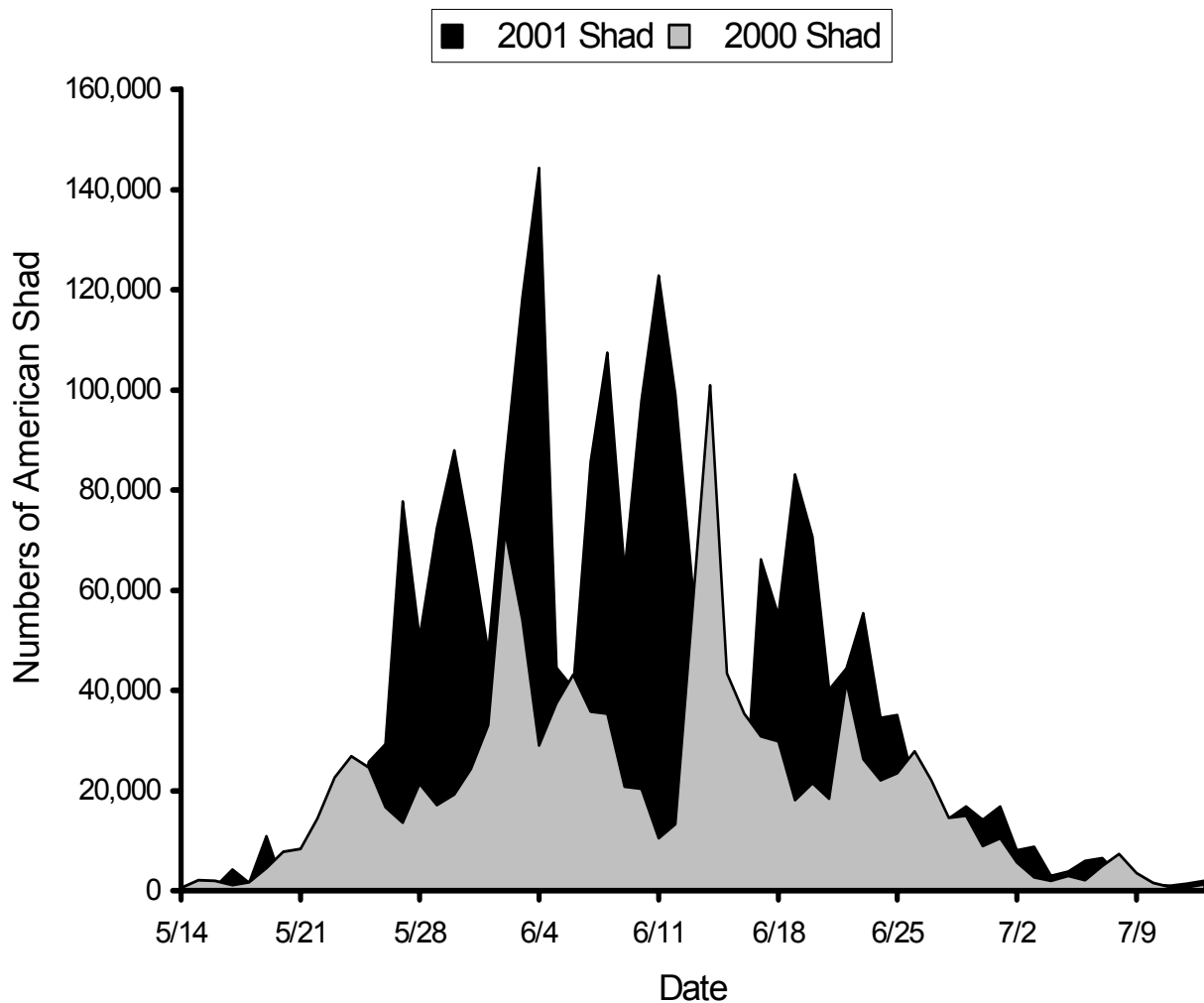
Figure 3.29. Run Timing of Up-Migrating American Shad through the Bonneville Project in 2000 and 2001

3.5.2 Diel Trends

3.5.2.1 Project-Wide Estimates and Spill

On an hourly basis, project-wide estimates of FPE in the springtime were higher at night than during the day, and extreme values only differed by 12% (Figure 3.30). Summertime estimates of FPE were higher at night than they were during 6 or 7 of the daytime hours, although a diel trend was not as obvious in summer as it was in spring.

Estimates of spill efficiency during the spring were low from mid-morning to early evening and were higher at night than they were during the day (Figure 3.30). Spill efficiency in the summer was highest from early morning to early afternoon and bottomed out in the early evening. Estimates of spill effectiveness in the spring were slightly higher in the late evening and early morning hours but changed very little throughout the day (Figure 3.30). Summertime spill effectiveness followed a pattern similar to that of summer spill efficiency with peaks in the early morning to early afternoon and lows in the early evening.
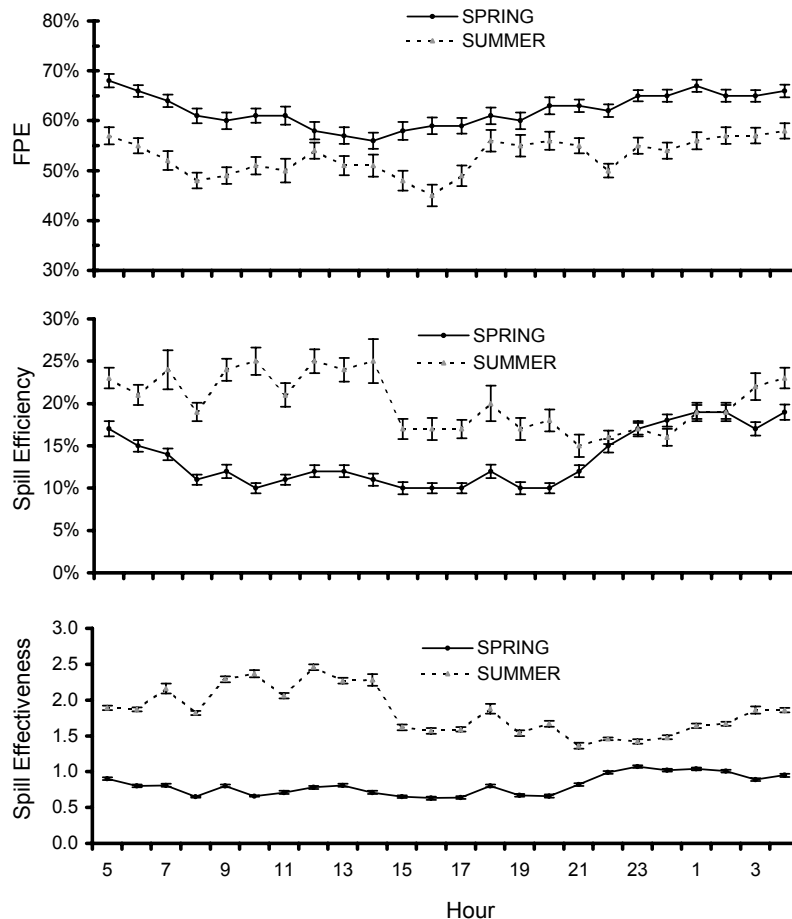
Figure 3.30. Diel Patterns of Fish Passage Efficiency, Spill Efficiency, and Spill Effectiveness during the Spring and Summer at Bonneville Dam in 2001

    Project-wide fish passage through all routes in the spring gradually declined through the day, began to slightly increase in the early evening, and peaked at 2100 then declined again through the early morning hours (Figure 3.31). During daylight hours, total project passage and total flow through the Project exhibited an inverse relationship in the spring. During nighttime hours, total project passage followed total project flow (i.e., as flow decreased, passage decreased). In the summer, total project passage through the day followed a pattern similar to spring except there was a slight increase in passage at 0800, the gradual decline lasted longer into the day, and the peak occurred an hour later (at 2200). As in spring, the relationship between total project passage and flow through the Project in the summer was inverse during daylight hours and direct during nighttime hours.
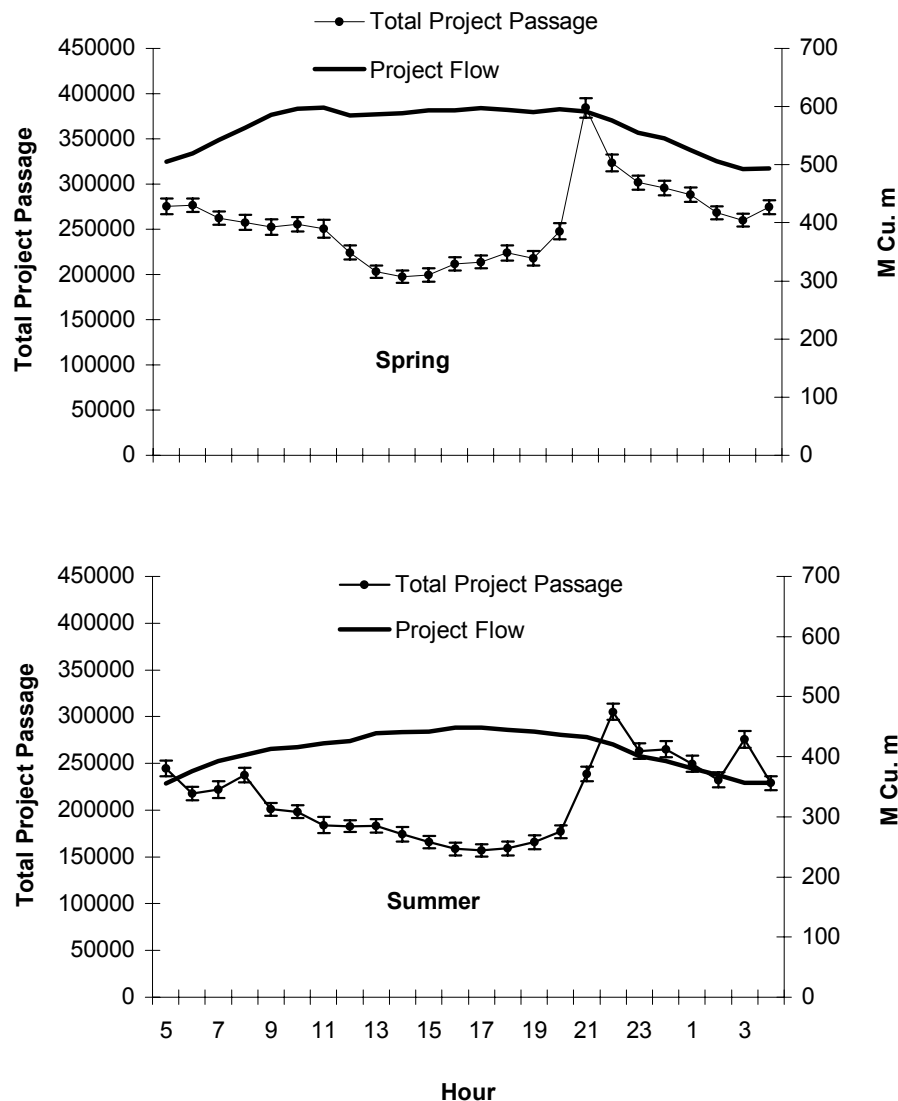
Figure 3.31. Estimates of Diel Trend in Total Fish Passage and Discharge in Spring (top) and Summer through Bonneville Dam in 2001. Error bars represent 95% confidence intervals.

Numbers of fish spilled in the spring declined through the day then increased sharply at 2100 and peaked at 0100 (Figure 3.32). The volume of water spilled differed little among hours in the spring, but a slight increase occurred at 2300, coinciding with an increase in the number of fish spilled. In the summer, the pattern of fish spilled through the day was less defined than in spring, but the decreasing trend during the day and an increase in nighttime hours was still evident. Spill passage during the summer peaked at 0300. There was very little variation in hourly spillway flow in the summer.
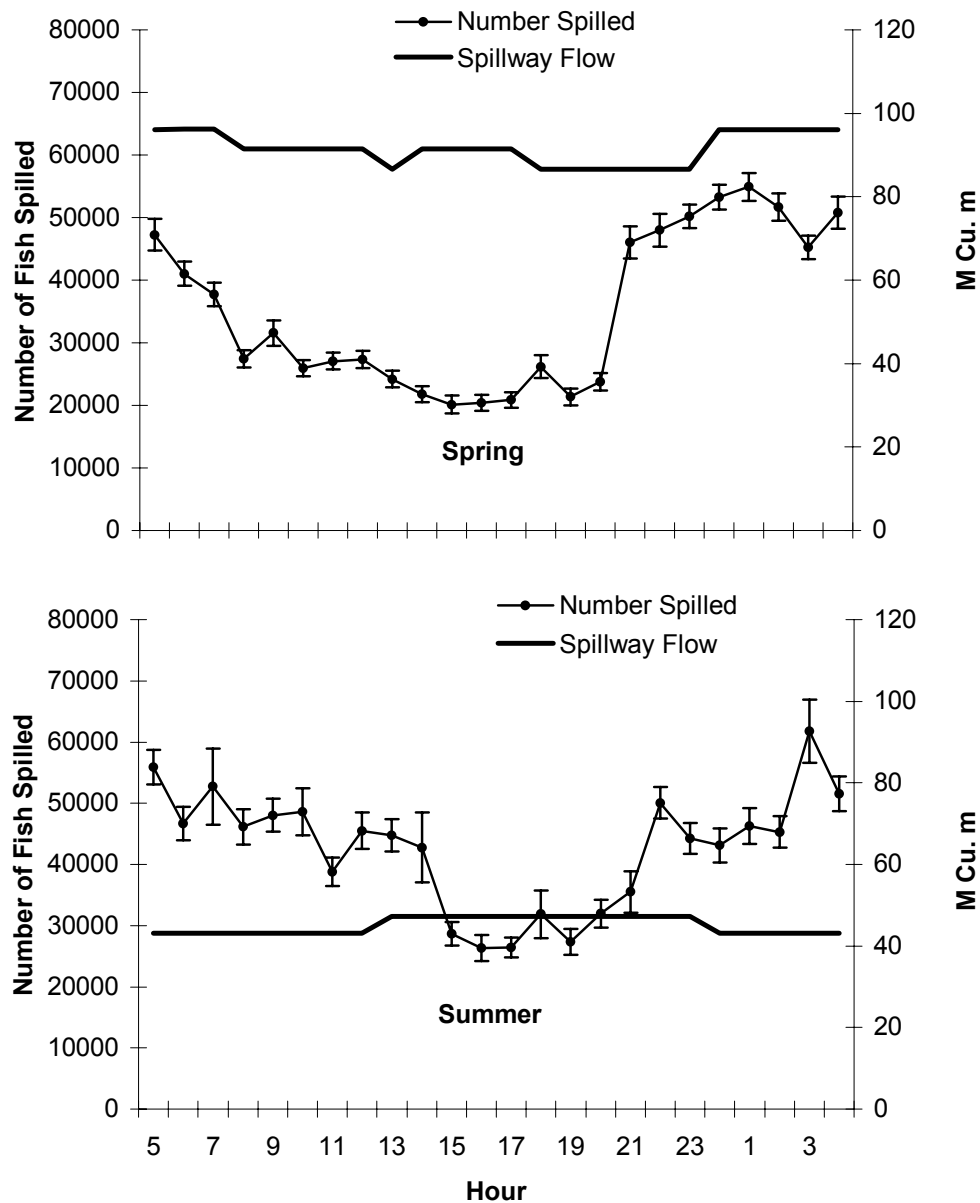
Figure 3.32. Estimates of Diel Trend in Spilled Fish and Discharge over the Spillway in Spring (top) and Summer through Bonneville Dam in 2001. Error bars represent 95% confidence intervals.

3.5.2.2 Fish Guidance Efficiency and Passage at Turbines

We found no significant diel trends in FGE at Powerhouse 1 in spring or summer because variances of estimates were too high (Figure 3.33). Total fish passage (guided + unguided) through Powerhouse 1 in the spring was bimodal, with peaks during late morning and early evening hours. Powerhouse 1 FGE estimates in the summer were highest from 0100 to 0600 hours and generally were lowest during late afternoon and early evening hours although these estimates did not differ significantly, as indicated by overlapping 95% confidence intervals. Total passage through Powerhouse 1 in the summer was higher from about 1600 through 2200 hours than it was during the rest of the day.
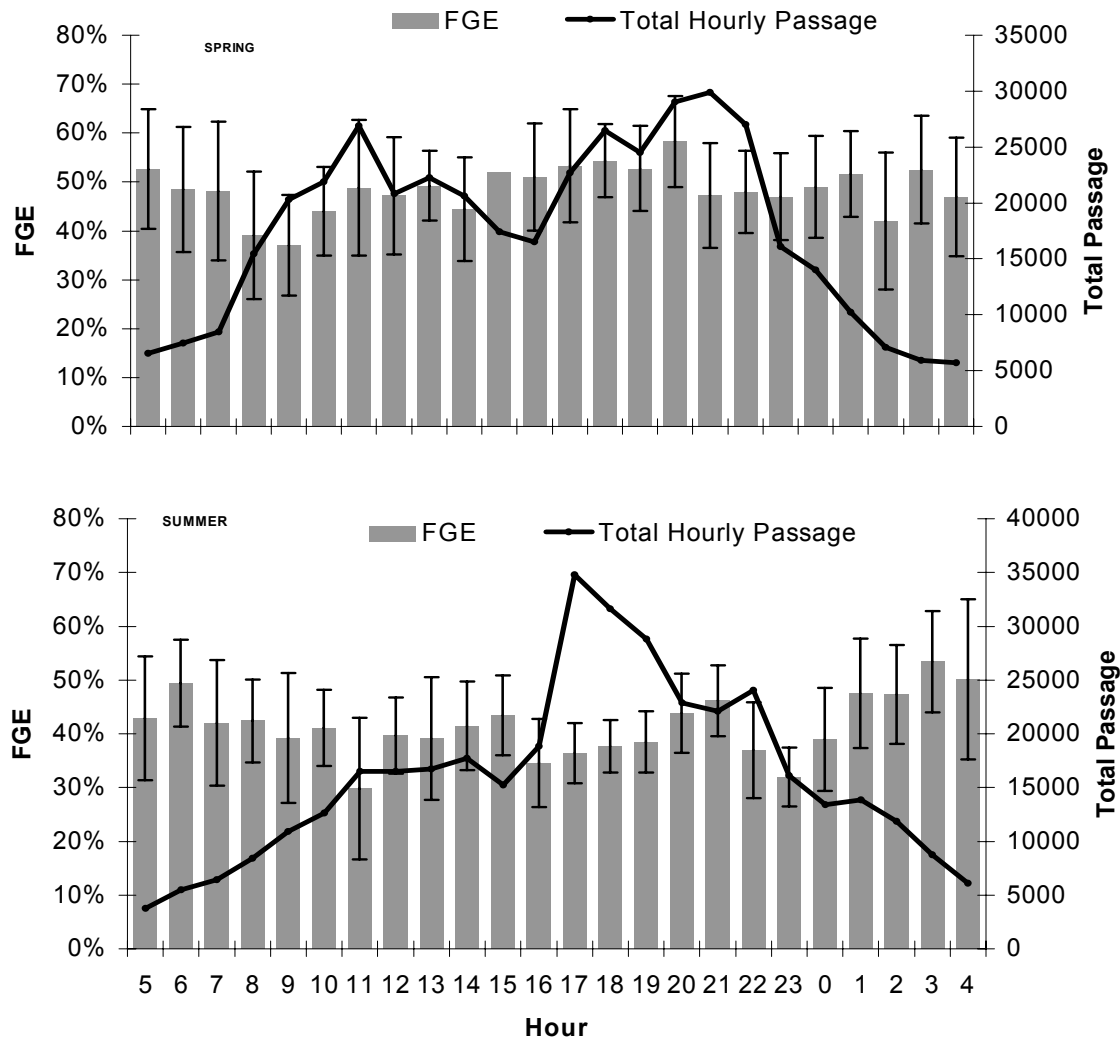
Figure 3.33. Diel Estimates of Fish Guidance Efficiency and Total Fish Passage for Powerhouse 1 during Spring (top) and Summer at Bonneville Dam in 2001. Error bars represent 95% confidence limits.

Powerhouse 2 FGE estimates were generally higher in late afternoon and at night than they were during the day (Figure 3.34). In spring, the estimates declined slightly from highs at 0100 to 0500 to lows from 1200 to 1500. Total fish passage in the spring declined through the morning and into the early

afternoon then slightly increased through the remaining afternoon hours then rose sharply and peaked at 2100. During the summer, FGE estimates at Powerhouse 2 dipped to lows in the midmorning and early afternoon hours and peaked staying relatively constant from 1800 to 0400. Total passage through Powerhouse 2 in the summer was similar to the pattern observed during spring except the initial increase started later in the afternoon and the peak occurred at 2200 (instead of 2100 as in spring).
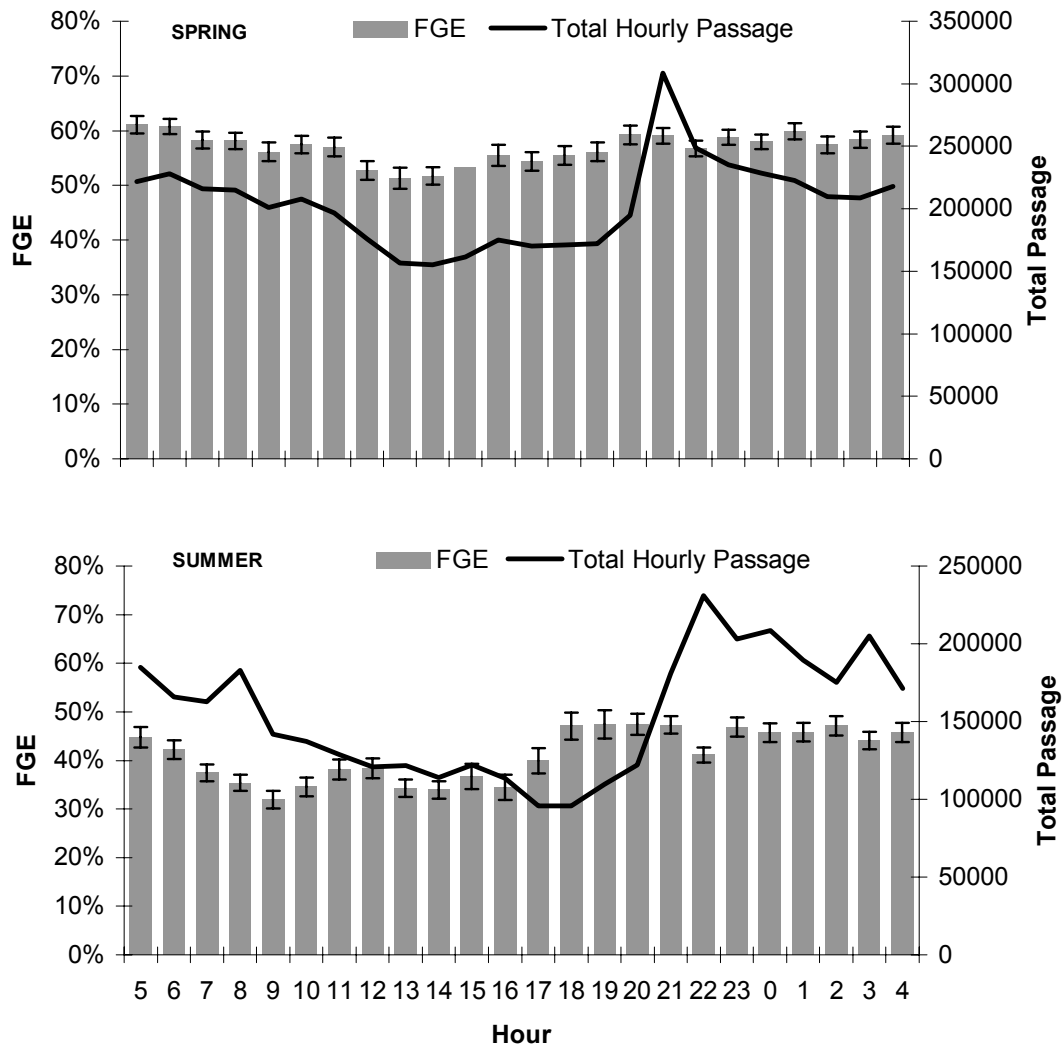
Figure 3.34. Diel Estimates of Fish Guidance Efficiency and Total Fish Passage for Powerhouse 2 during Spring (top) and Summer at Bonneville Dam in 2001. Error bars represent 95% confidence limits.

3.5.2.3 Compared to Radio Telemetry Estimates

Hydroacoustic and radio telemetry estimates of hourly trends in fish passage for the project were generally similar in both seasons (Figures 3.35and3.36), except for a peak in radio telemetry data in the middle of the afternoon (1400 to 1600 hours) in both seasons that was not evident in the hydroacoustic

data. The hydroacoustic season was modified to match the radio telemetry spring season. In both spring and summer, both hydroacoustics and radio telemetry methods documented a peak in fish passage after sunset. Scott Evans of USGS provided radio telemetry data for Figures 3.35 and3.36.
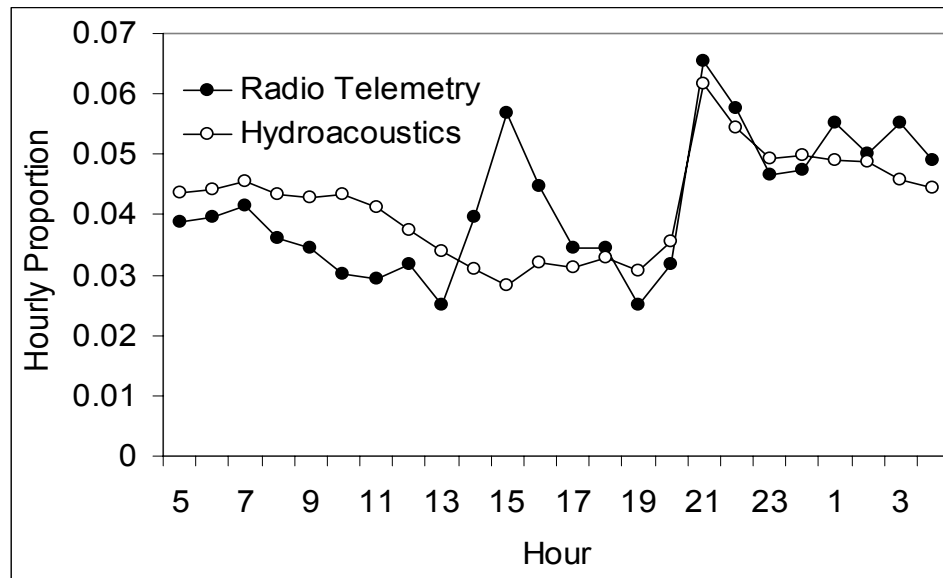
Figure 3.35. Diel Passage Based on Hydroacoustic and Radio Telemetry Sampling at Bonneville Dam in 2001 during the Spring (5/1-6/9) when both Radio Telemetry and Hydroacoustic Studies Were Ongoing
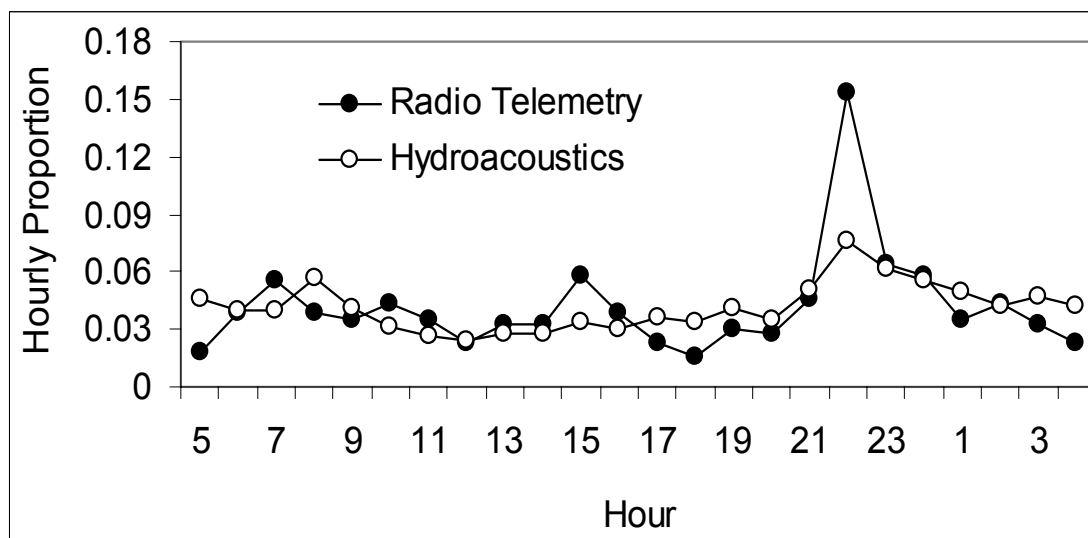
Figure 3.36. Diel Passage Based on Hydroacoustic and Radio Telemetry Data at Bonneville Dam in 2001 during the summer, when both Radio Telemetry and Hydroacoustic Studies Were Ongoing

The average hourly percentage of fish passage estimated by hydroacoustics to have passed entire structures (powerhouses or the spillway) or combinations of structures in daytime (0500 to 2059 hours) were within one percent of radio telemetry results for the same hours in both spring and summer (Table 3.2).

Table 3.2. Percentage of Fish Estmated by Hydroacoustics (HA) and Radio Telemetry (RT) to Have Passed Bonneville Dam Structures during an Average Daytime Hour (0500 to 2059 hours) in Spring and Summer of 2001. Data from non-overlapping parts of seasons have been deleted and adjusted appropriately so that the times reported here are the same for both methods. Those dates are May 1-June 9 for spring and July 1-July 15 for summer.

Season and Location	HA Percent	RT Percent	Difference
Spring PH1 Only	4.68%	3.86%	0.82 % (HA>RT)
Spring PH2 Only	3.77%	3.46%	0.31% (HA>RT)
Spring Spillway Only	3.49%	4.04%	0.55% (RT>HA)
Spring PH2 + Spillway	3.67%	3.55%	0.12% (HA>RT)
Spring Full Project	3.73%	3.56%	0.17% (HA>RT)
Summer PH1 Only	4.72%	4.17%	0.55% (HA>RT)
Summer PH2 Only	3.51%	3.18%	0.33% (RT>HA)
Summer Spillway Only	N/A	5.73%	N/A
Summer Full Project	3.58%	3.30%	0.28% (HA>RT)

3.6 Fish Guidance Efficiencies

3.6.1 Background

Fish guidance efficiency is the ratio of the estimated number of fish passing a turbine by a non-turbine route ("guided" fish) to the estimated number of all of the fish passing that turbine ("guided" + "unguided" fish). Fish passage efficiency is the same calculation done on the scale of a powerhouse or the entire project. Based upon historical information, FPE and FGE are expected to be lower in summer than in spring. Results of the efficiency evaluations of fish-guidance structures are presented in the following order: 1) the STS versus the ESBS at Powerhouse 1; 2) Powerhouse 1 versus Powerhouse 2 STS; 3) Modified Unit 15 STS versus other Powerhouse 2 STS.

3.6.2 Comparing Performance of Fish-Guidance Structures

In spring, the FGE of the ESBS at Unit 8 was higher than that of all STS-equipped units, except for modified Unit 15 at Powerhouse 2, but in summer, the FGE of Unit 15 was higher than that of the ESBS and the combined FGE of all other unmodified STS units (Figure3.37). Despite an impressive FGE in spring, Unit 8 only ran for about 8 h, so its contribution to FPE was minimal. It only ran 5 h in summer. The FGE of the modified Unit 15 was higher than that of STS-equipped units at Powerhouse 1 and Powerhouse 2, which had similar ranges in FPE, in most of spring and all but the end of summer (Figure 3.38). Spring FGE was significantly higher than summer FGE, particularly for Unit 15 and other Powerhouse 2 units (Figure 3.37 and 3.38).
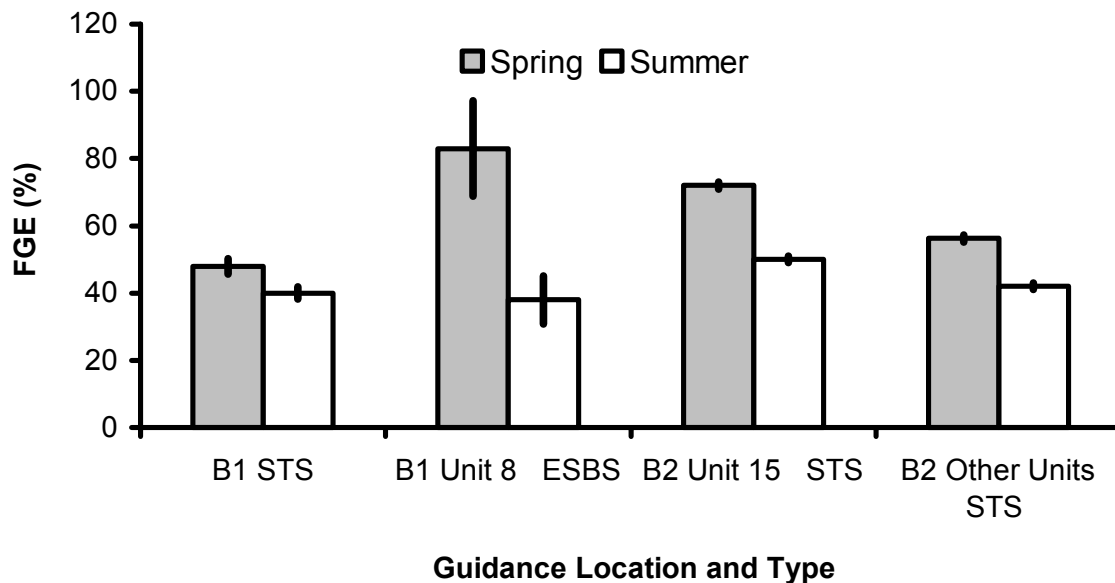
Figure 3.37. Comparison of FGE among Combinations of Location and Fish-Guidance Devices or Conditions. Unit 15 had extensive structural modifications to a gatewell and vertical barrier screen to increase flow up the gatewell slot. Error bars are 95% confidence limits and estimates with overlapping bars are not considered different.
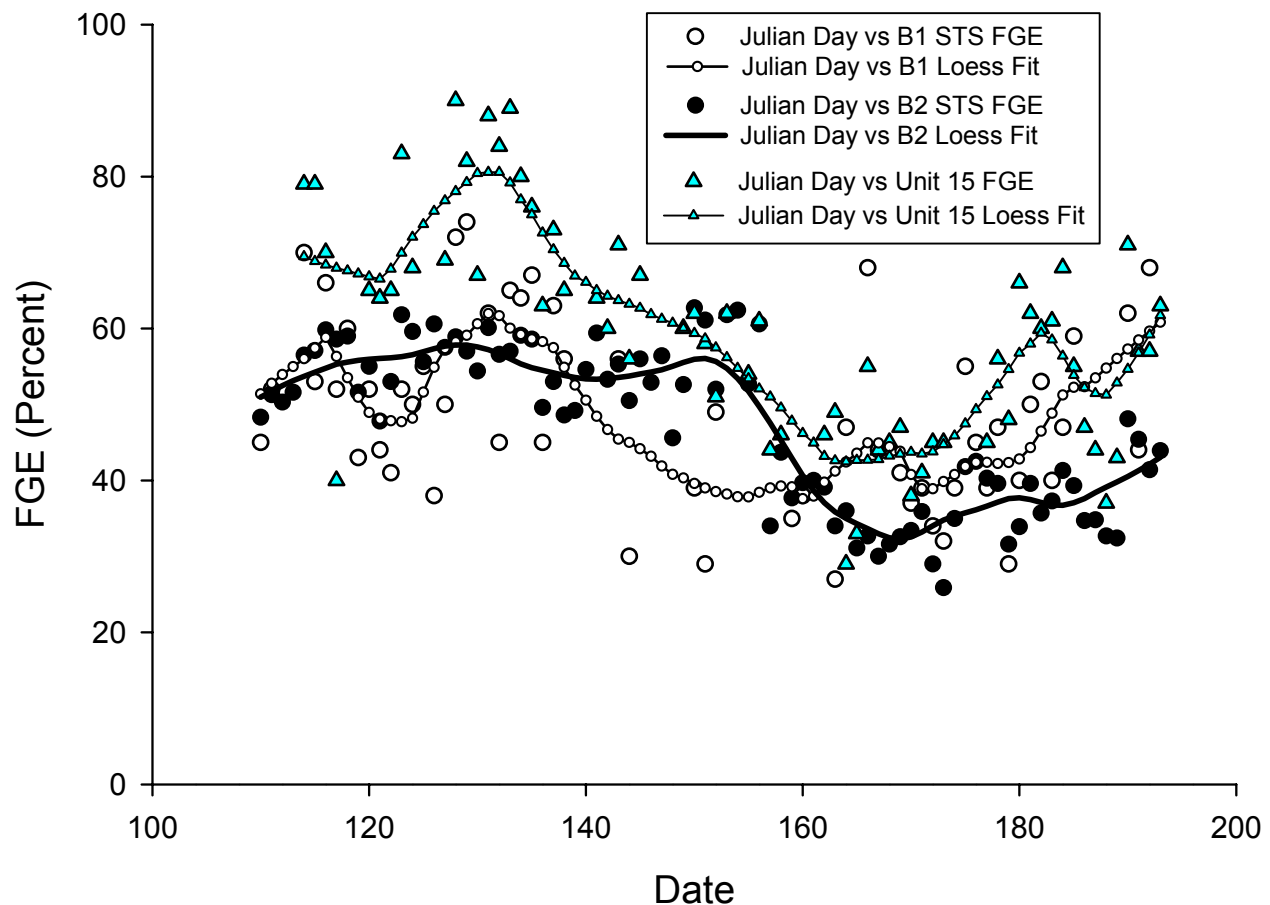
Figure 3.38. Comparison of FGE among Types of Units with STS's at Powerhouse 1, Powerhouse 2, and at Modified Unit 15 by Date

The FGE of individual units (Figure3.39) was more variable than that estimated for units with similar guidance devices or passage conditions (Figure 3.37). For example, the FGE of Unit 15 in summer actually was 4% less than that observed at Unit 14 and statistically the same as that estimated for Unit 13, although it exceeded the FGE of all other Powerhouse 2 units (Figure 3.39). In summer, units 2 and 6 also had high FGE estimates, but they only ran 2% of the time (20 and 23 hours, respectively). The 95% confidence limits associated with estimates at Powerhouse 1 units were wider than those at Powerhouse 2.

There was a tendency for FGE to be higher at intakes between turbine intake extensions (TIEs) than at intakes behind TIEs. For example, randomly sampled intakes that happened to be between TIEs at units 12, 13, 14, and 15 had higher FGEs than estimated for Unit 11 and 18 in spring and summer and at Unit 16 in summer. Intakes at units 11, 16, and 17 were behind TIEs. We also observed higher FGE at Intake 15<u>b</u>, which was between two TIEs than we did at Intake 15<u>c</u>, which was behind a TIE, although the difference was much greater in spring than in summer (Figure 3.40). Intake 15<u>b</u> also passed significantly more fish than did Intake 15<u>c</u> in both seasons, and FGE was higher in spring than in summer at both

intakes. Exceptions to the trend of higher FGEs at intakes between TIEs included the intake sampled at Unit 16 in spring, which had a high FGE despite being behind a TIE and the intake at Unit 17, which produced a below-average FGE in spring despite being between two TIEs. The lowest FGEs were recorded at an intake behind a TIE at Unit 18 in spring and summer, and an intake behind a TIE at Unit 11 had the next-to-the-lowest FGE in summer. There was a trend for FGE to be higher at units near the center than at the ends of Powerhouse 2. Unit 1, which is located at one end of Powerhouse 1 had the lowest FGE of all units at that Powerhouse in both spring and summer.
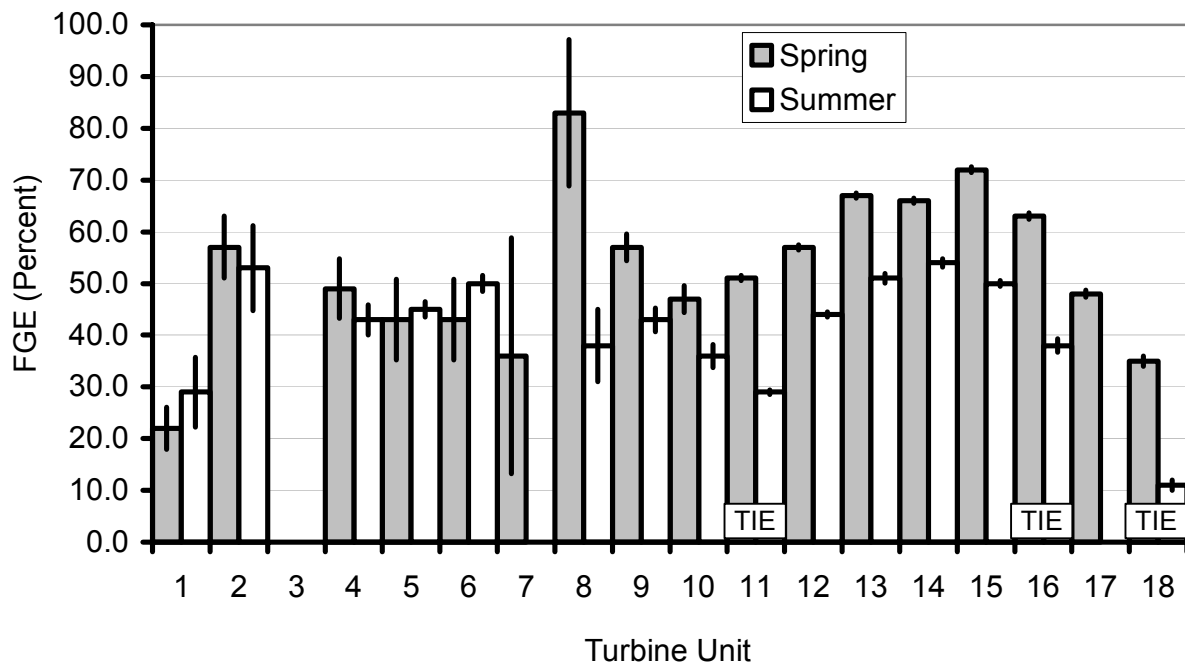
Figure 3.39. Estimates of FGE and 95% Confidence Limits for Turbine Units at Bonneville Dam in Spring and Summer
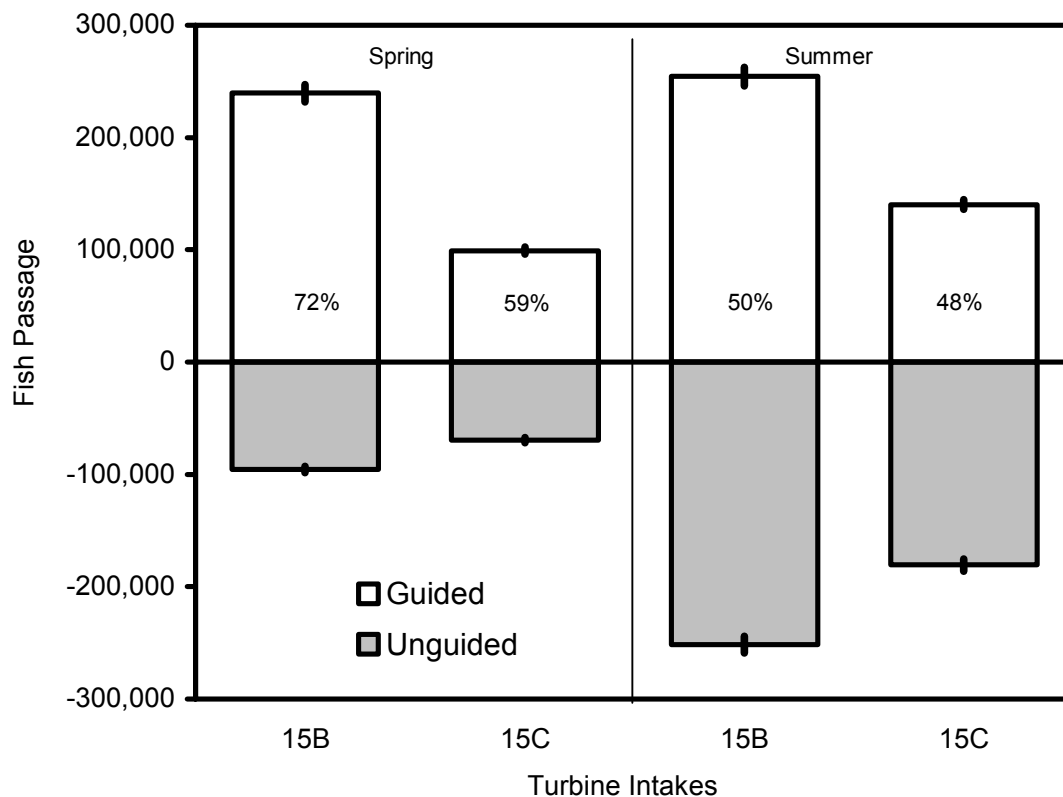
Figure 3.40. Estimates of the Number of Guided and Unguided Fish and FGE at Intakes 15<u>b</u> (between TIEs) and 15<u>c</u> (behind a TIE) during all Hours the Turbine Was Operated in Spring. The 95% confidence limits on FGE estimates were about 1%. Vertical bars show 95% confidence limits on passage estimates.

3.6.3 Comparing FGE Estimates by Different Sampling Methods

We had the opportunity to compare our estimates of the FGE of turbine units at Powerhouse 2 with estimates by two other methods. The USGS estimated FGE for every unit at Powerhouse 2 based upon the distribution of passage of radio-tagged fish, and the NMFS estimated FGE for modified Unit 15 by gatewell dipping and fyke netting. Comparison with radio tagging estimates of FGE could be examined for more units, but sampling with the hydroacoustics and radio telemetry was not simultaneous as it was for the hours netted at Unit 15 by the NMFS. Scott Evans (USGS) provided radio telemetry estimates and Bruce Monk (NMFS) provided gatewell and fyke-net estimates presented in this section.

3.6.3.1 Comparison with Gatewell Dipping and Fyke Netting Estimates

We sampled continuously at Unit 15, while the NMFS sampled with nets from about 2000 until 2100 or 2200 depending upon the number of fish they collected in the dip basket sampling the gatewell. Sampling duration was only as long as needed to obtain a reliable FGE estimate based upon catches of guided fish and knowledge of FGE ranges that were likely.

By season, our concurrent estimates of FGE were similar to those made by netting, as were estimates of number of guided and unguided fish (Figure 3.41). Hydroacoustics underestimated the number of guided fish in spring and underestimated the number of unguided fish in summer, according to the lack of overlap in 95% confidence limits. In spring, the FGE estimates were very similar, but in summer, hydroacoustic estimates were about 5% lower than netting estimates.
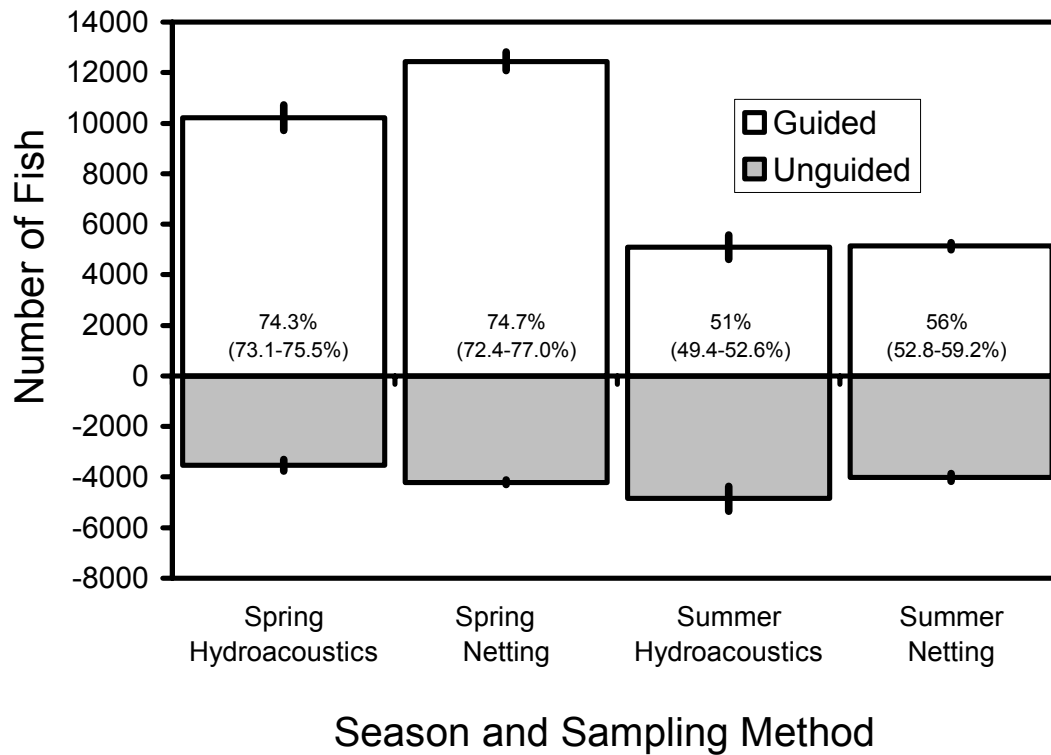
Figure 3.41. Plot of the Number of Guided and Unguided Fish Estimated by Concurrent Hydroacoustic and Net Sampling at Unit 15 in Spring and Summer. The percentages inside bars for guided fish are estimates of FGE and numbers in parentheses are 95% confidence limits.

We also were able to make estimates based upon all hours that we sampled and during which the turbines operated (day and night) and we compared them to netting estimates (Figure 3.42). In both cases, hydroacoustic estimates were lower than the respective netting estimates. This result surprised us because we expected that detecting more fish would improve our estimates.

Investigating further, we compared estimates based upon all nighttime hours (2000 through 0500 hours) sampled by hydroacoustics with netting estimates made from 2000 to 2100 or 2200 hours and the agreement between the two improved considerably (Figure 3.43). The 95% confidence intervals overlapped in both spring and summer.
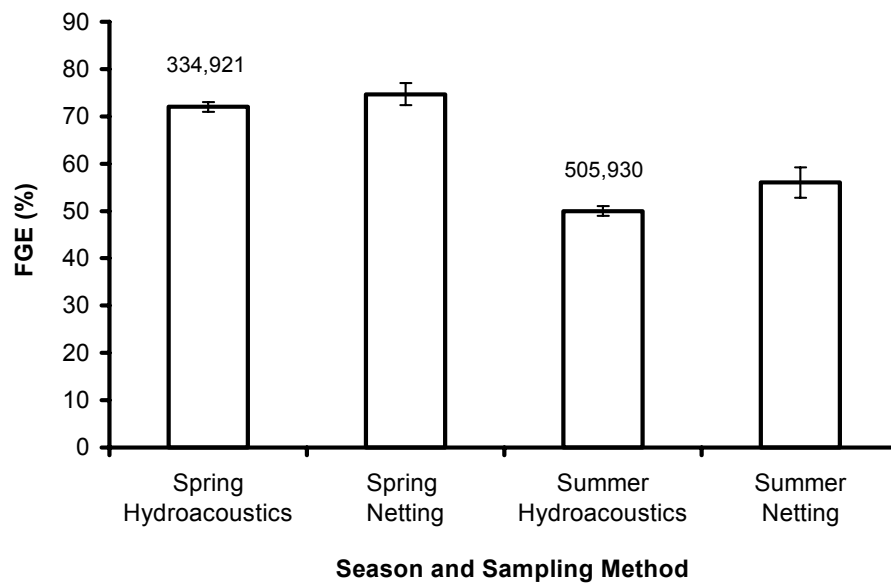
Figure 3.42. Plot of FGE Estimates Made from all Hours of Hydroacoustic Sampling Compared to Estimates Based upon Netting from about 2000 to 2100 or 2200 h. Vertical bars are 95% confidence limits. The expanded numbers of fish upon which FGE estimates were based are shown above the bars for hydroacoustic sampling each season.
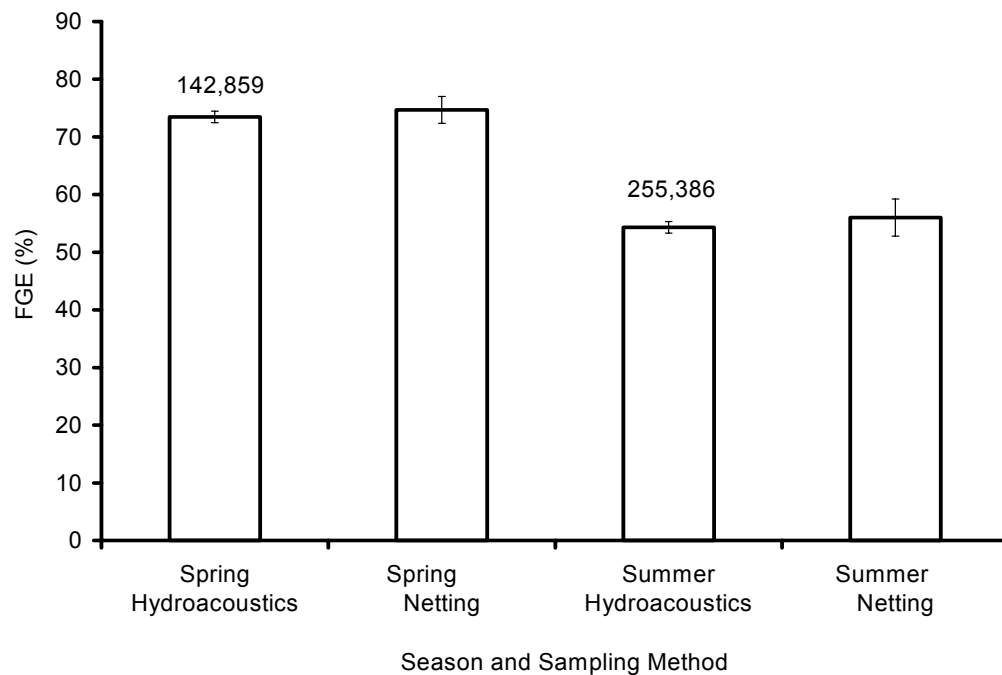
Figure 3.43. Plot of FGE Estimates Made from all Nighttime Hours of Hydroacoustic Sampling (2000-0500) Compared to Estimates Based upon Netting from about 2000 to 2100 or 2200 h. Vertical bars are 95% confidence limits. The expanded numbers of fish upon which FGE estimates were based are shown above the bars for hydroacoustic sampling each season.

3.6.3.2 Comparison with Radio Telemetry Estimates

The radio telemetry study also produced unit-specific estimates of FGE for Powerhouse 2, and those estimates and hydroacoustic estimates are presented in Table 3.3. On the unit level, estimates by hydroacoustics were higher than estimates by radio telemetry in five of eight units (12, 13, 14, 15, and 16) in spring and in three of four units for which there were radio telemetry estimates in summer (units 12, 13, and 14). Hydroacoustic estimates were lower than radio telemetry estimates at units17 and 18 in spring and at Unit 11 in summer. Estimates were only similar at Unit 11 in spring.

Radio telemetry estimates pooled for four adjacent units were within 10% of similarly pooled hydroacoustic estimates (Table 3.3). In spring, the hydroacoustic estimates exceeded radio telemetry estimates by 9% for units 11 through 14 and by only 2% for units 15 through 18. In summer, the hydroacoustic estimates exceeded radio telemetry estimates by 8% for units 11 through 14, and no radio telemetry estimates were available for units 15 through 18.

The comparison of estimates at Unit 15 is of particular interest because NMFS' netting study estimate is available. The hydroacoustic estimate of 72% for all hours of the day in spring was within 3% of NMFS estimate for sampling at 2000 to 2100 or 2200 hour, but it was 34% higher than the radio telemetry estimate. Similarly, NMFS' netting estimate was 37% higher than the radio telemetry estimate.

Table 3.3. Hydroacoustic (HA) and Radio Telemetry (RT) Estimates of FGE for Turbines at Bonneville Dam Powerhouse 2 in 2001. For this comparison, only data from 1 May to 9 June for spring and 1 July to 15 July for summer were used, so these hydroacoustic FGEs differ slightly from those reported elsewhere.

Location	HA Estimate	RT Estimate	Difference
Spring			
Unit 11	50%	51%	1% (RT>HA)
Unit 12	59%	40%	19% (HA>RT)
Unit 13	67%	58%	9% (HA>RT)
Unit 14	62%	43%	19% (HA>RT)
Units 11-14	58%	49%	9% (HA>RT)
Unit 15	70%	38%	32% (HA>RT)
Unit 16	60%	48%	12% (HA>RT)
Unit 17	48%	64%	16% (RT>HA)
Unit 18	32%	42%	10% (RT>HA)
Units 15-18	51%	49%	2% (HA>RT)
All PH2	56%	46%	10% (HA>RT)
Summer			
Unit 11	26%	33%	7% (RT>HA)
Unit 12	40%	19%	21% (HA>RT)
Unit 13	48%	38%	10% (HA>RT)
Unit 14	53%	32%	21% (HA>RT)
Units11-14	39%	31%	8% (HA>RT)
Unit 15	52%	34%	18% (HA>RT)
Unit 16	53%	46%	7% (HA>RT)
Unit 17	N/A	N/A	
Unit 18	19%	7%	12% (HA>RT)
Unit 15-18	50%	39%	11% (HA>RT)
All PH2	44%	35%	9% (HA>RT)

4.0   Discussion

4.1   Hydroacoustic Detectability

The motivating force behind efforts to improve detectability modeling is the desire to provide hydroacoustic estimates that are quantitative as well as relative indices to fish passage. Ratio estimators such as fish guidance efficiency only require that the hydroacoustic beams sampling guided and unguided fish have equal detectability so that the ratios of counts, not necessarily the counts themselves, are accurate. Combining counts from different locations such as powerhouses and a spillway also requires equal detectability so that counts from different locations are comparable, although the counts themselves may not be accurate. Nevertheless, accurate counts estimated by proper expansion of detected fish have the potential to provide estimates with inherent quantitative value as well as providing acceptable relative estimates.

One of the ways to check the adequacy of detectability is to regress numbers of fish per transducer hour on discharge volume and to look for negative slopes that might indicate lower detectability. Lower detectability may result if fish speed through the beam faster at high than at low discharge and return fewer than the minimum number of echoes. This is one of the quality control checks that we perform every year, and as expected, we found no significant regressions between fish counts and discharge. We know from work in 2000 that our ping rate of 30 pings per second at the spillway was adequate for detecting fish at the highest possible spill levels, and the drought and limited spill rates of 50,000 cfs in 2001 assured that spillway detectability was adequate.

We had some concern that detectability at Powerhouse 2 might be a problem because of the Powerhouse 2 priority and drought-limited discharge through Powerhouse 1 and the spillway. We compared expanded hydroacoustic counts of guided and unguided fish at Intake 15<u>b</u> with estimates from netting by the NMFS to evaluate the reasonableness of our detectability modeling and the resulting spatial expansion factors. The closeness of concurrent hydroacoustic and netting estimates of fish passage for all of the spring and summer seasons (Figure 3.41) provided independent verification that our detectability modeling and corrections to expansion factors were reasonable for Powerhouse 2. In spring, the sum of all hydroacoustic and netting estimates of guided fish numbers differed by only 22%, and in summer, the estimates did not differ (< 1%). The sum of all unguided fish by the two methods also were reasonably close and differed by less than 1% in spring and by about 21% in summer. The bias in hydroacoustic estimates of guided and unguided fish passage relative to netting estimates can be much worse. For example, Ploskey and Carlson (1999) reported ratios of differences for netting to hydroacoustic counts ranging from 2 to 11 for guided fish and from 10 to 13 for unguided fish, although FGE estimates were closer because of error compensation in the ratio estimator (Ploskey and Carlson 1999).

4.2   Validation of Autotracking Hydroacoustic Data

For the past four years we have been evaluating and dealing with inter-individual differences in human hydroacoustic analysis. Over that time, it has become clear that individuals are substantially and consistently different in their results when given the same large data set to analyze. Out of a pool of trackers, even when trained together over several weeks, some individuals consistently produce

substantially lower-than-average fish counts and some produce substantially higher-than-average fish counts. Failure to recognize individual bias and assign different passage routes to different trackers has the potential to produce biased and perhaps very biased estimates. That potential is especially clear for ratio estimates. Although this year the agreement among our trackers was better than it has sometimes been, the cumulative difference in passage estimate for the lowest tracker was only about 72.8% that of the highest tracker for the 438 channel hours we compared in spring and 68.8% for the 227 channel hours we compared in summer (Figure 3.3). The degree by which individuals disagree is at least partly related to noise. Up-looking deployments that sample guided fish and shallow water routes (sluiceways, surface collector entrances) are more problematic than are down-looking deployments sampling the spillway or unguided fish in turbines (Ploskey et al. 2001a; Ploskey et al. 2002).

The high coefficients of determination for regressions of human-based counts on autotracker counts for each deployment (Figures 3.4 and 3.5) indicate that the estimates comport very well. This year we used human trackers only to verify and adjust the results of the autotracker. The slopes of regression lines in Figure 3.6 were used to correct our autotracked results downward to offset the tendency of the autotracker to overestimate passage. We consider this method of evaluation and correction, when based on large samples of data analyzed and compared at the level of channel hour, to be an adequate method of quality control and assurance for our autotracked estimates. This approach is not only more economical but qualitatively superior to manual tracking by individual humans.

4.3 Major Passage Metrics

4.3.1 Project and Powerhouse FPE

The drought of 2001 provided a unique opportunity to evaluate Project FPE during spill and non-spill periods in the same year. Project FPE was 15% and 35% higher during 50,000 cfs spill periods in spring and summer, respectively, than it was during non-spill periods. In 2000, continuous spill at 75,000 or 120,000 cfs throughout spring and summer and the operation of a prototype surface collector at Powerhouse 1 produced Project FPE estimates of 79% in both seasons. These estimates were 16% (spring) and 26% (summer) higher than estimates for spring and summer seasons in 2001, which included spill and non-spill periods rather than continuous spill.

Project FPE was only about 1% lower in spring and in summer than FPE calculated for Powerhouse 2 and the spillway, without Powerhouse 1. This was not surprising given that Powerhouse 1 passed only about 7.3% of the water and 6.9% of the fish in spring and 8.6% of the water and 7.5% of the fish in summer.

4.3.2 Spill Efficiency and Effectiveness

Spill efficiency estimates in spring (14%) and summer (20%) 2001 were significantly lower than estimates made in spring (44%) and summer (49%) 2000, undoubtedly because of reduced volume and duration of spill during the drought in 2001. Spill effectiveness also was about 38% lower in spring 2001 than it was the previous spring. In 2000, spill was continuous at about 75,000 cfs during the day and 120,000 cfs at night, but lack of water in 2001 limited spill to about 50,000 cfs for about 21 of 45 days in spring and 10 of 40 days in summer. About 5% of the reduction in spill efficiency between 2000 and 2001 could be the result of our conservative choice of a flux factor to correct spill passage estimates for

fish direction of travel in spring and summer, but that still leaves a spring and summer decrease of 33% and 24 %, respectively from 2000 to 2001.

The fish-flux factor that we used was more conservative than multiplying by the fraction moving downstream because it subtracted the upstream fraction from the downstream fraction. For example, if 90% of detected fish are moving downstream and 10% are moving upstream, the flux factor applied was 0.8 instead of 0.9. In reality, all we know is that some fish moving upstream could have been counted more than once and that the flux factor should be somewhere between 0.8 and 0.9. We could have split the difference and used 0.85, but we wanted to be certain not to overestimate spillway passage in a drought year.

Effectiveness seems to be a meaningful metric when differences in flow proportions do not exceed about 30%, which was not the case in comparisons between summer 2000 and 2001. In summer 2001, spill effectiveness was about 55% higher than the previous year's estimate, likely because the proportion of water spilled in summer 2001 was much lower than it was in 2000. The denominator in the spill-efficiency calculation (the proportion of water spilled) in summer 2000 was 0.48 whereas it was only 0.11 in summer 2001. The inverse of these proportions represents how much spill efficiency is expanded (i.e., by 2.1 in 2000 and by 9.1 in 2001. The inflation of the effectiveness statistic can be observed in estimates of effectiveness at sluiceways and surface collectors, which are always higher than estimates for a spillway because these small routes pass orders of magnitude less water than a spillway passes. For this reason, we believe that efficiency is a more meaningful metric than effectiveness, which can be inflated by very low spill proportions.

Another possible explanation for the high spill effectiveness in 2001 is the early and large run of American shad (Figure 3.29) that could have contaminated spillway samples, but we did not observe a lot of evidence of shad schools in the summer echograms that we processed for quality control. In echograms, shad usually can be recognized because they occur in dense schools, often high in the water column. In contrast, juvenile salmon usually pass through hydroacoustic beams as single traces. With reduced spill, it is possible that shad could visit spill bays and wallow through the upper one half of hydroacoustic beams without threat of fallback in spill. Although we apply target and echo strength filters to reduce detection of fish larger than smolts, it would be impossible to eliminate false detections with single beams because even a large fish detected far off the axis of a single beam can return smolt-sized echoes. We usually do not have evidence of shad contamination of spillway or in-turbine samples until late June or July when weak, spent shad begin to fall back downstream.

4.3.3 Effects of Spill Level

We found several significant relationships that suggest an optimum spill strategy for future drought years that includes night spill lasting at least 11 hours. There were positive relations between the number of hours of spill per day and FPE and spill-efficiency metrics (Figure3.8), and we observed significantly higher fish passage through the spillway at night than during the day (Figure 3.32), even though the amount of spill was the same during each period. We observed a similar trend in 2000, but nighttime spill discharge was much higher than it was during the daytime, and we could not determine whether the pattern was driven by spill level or day versus night. With constant spill in 2001, we can confidently describe the effect as a diel pattern unrelated to spillway discharge. Spill efficiency increased linearly with the number of spill hours per day in spring. Although we plotted a linear relation for FPE

(Figure 3.8), there really were only two obvious levels of effect that could be classified at low-spill durations of 0-10 h/day that produced an average FPE of about 54% and high-spill durations of 11 to 24 h/day that produced an average FPE of about 71% (Figure 4.1). We were only able to examine the effect of hours of spill per day because spill was constant at about 50,000 cfs on days when spill occurred. Spilling at night also has the advantage of eliminating fallback of adult salmonids through the spillway during the day and may reduce fish losses due to visual predators such as birds and fishes in the spillway tailrace.

4.3.4 Comparison with Radio Telemetry and Netting Estimates

The level of agreement between our hydroacoustic and the radio telemetry-based estimates by our USGS colleagues was better for major fish-passage metrics and entire powerhouses than it was for individual units. At the level of the individual turbine unit (Table 3.3), the agreement was sometimes very poor. The worst case was a 34% difference at Unit 15 in spring, and the best case was a 1% difference at Unit 11 in spring. Unit 15 was unusual in that it was very intermittent in its operation during high passage hours due to the NMFS studies there. The next largest differences were at units 12 and 14 in both spring (19% both seasons) and summer (21% both seasons). Unit-specific differences between the two methods averaged 14.7% for eight units in spring and 13.7% for 7 units (Unit 17 did not operate) in summer.
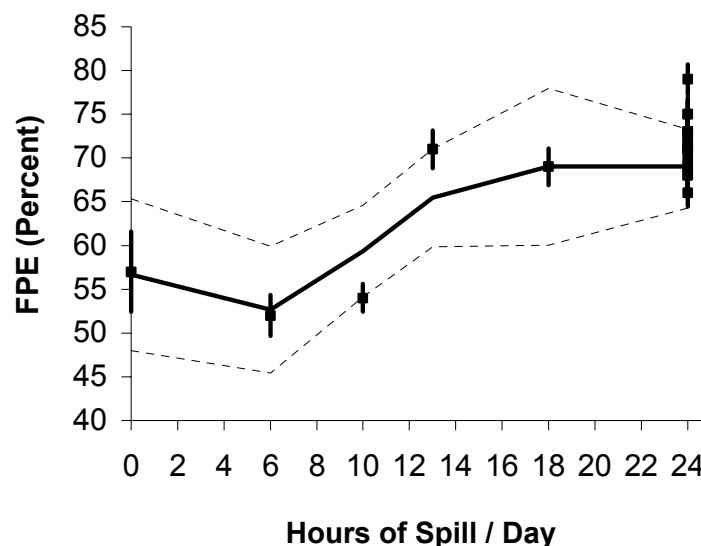
Figure 4.1. Relation between Fish Passage Efficiency (FPE) and Hours of Spill per Day in Spring 2001. The solid line was Loess fitted to points and the dashed lines represent 95% confidence intervals on the fitted line. Vertical bars represent 95% confidence intervals on individual estimates of FPE.

Across the entire project or a powerhouse or spillway structure differences were somewhat smaller (Table 3.1). The worst case was a 14% difference for Powerhouse 2 FPE during low spill in spring. The next greatest difference is for Project FPE in spring, and all other differences are 10% or less. Diel passage estimates for the two methods (Figure 3.35 with Figure 3.36) are very similar, with the notable exception of mid afternoons (1400-1600 hrs), especially in spring. Further pooling samples into daytime versus total passage further reduces differences in some cases (Table 3.2). Hydroacoustic and radio-

telemetry estimates at Powerhouse 1 still differed by 21.4% in spring and 13.2% in summer, but Powerhouse 1 had an unusually limited generation schedule. The only other differences that were greater than 10% were the spillway in spring (15.6%) and Powerhouse 2 (10.4%).

We believe that our hydroacoustic estimates are reasonably close to those of the USGS radio telemetry workers and that a good part of the differences that exist can be attributed to the small sample sizes that are inherent in highly partitioned radio telemetry estimates. Powerhouse unit-specific FGE estimates from radio telemetry were based on from 14 (Unit 18) to 136 (Unit 14) fish in spring and from 15 (Unit 18) to 136 (Unit 14) fish in summer. When you consider that those numbers are composed of varying number of different species, it is not surprising that radio telemetry estimates sometimes differ. In contrast, unit-specific hydroacoustic estimates are based upon thousands of fish each season.

All sampling methods are imperfect and each has unique advantages and disadvantages. Radio telemetry can provide data on movements of known fish and is not limited to the dam itself. Information on travel time, large-scale trajectories, forebay residency, survivorship, species or origin and even rearing (wild versus hatchery) differences is potentially available. However, the power of radio telemetry is diminished when the number of tagged fish is divided among too many treatments or passage routes, and it provides no data on untagged animals. In contrast, the NMFS continues gatewell dipping and fyke netting single units until the number of fish sampled is believed to be sufficient to provide a reliable species-specific FGE estimate. The number of fish captured during 1 to 2 hours of net sampling by the NMFS effort usually is an order of magnitude larger than the number available for radio telemetry estimates for an entire season. However, netting is labor intensive and may injure or kill fish, including individuals from endangered populations; therefore, it cannot be used for more than a few hours per day at one or two intakes. The restriction of physical capture to one and at the most two or three samples per day prevents biologists from obtaining daily estimates of sample variance or increased resolution of the temporal and spatial variation in FGE.

While hydroacoustic methods provide FGE estimates that are very comparable to physical capture-based estimates, they can only provide a relative index to fish passage unless calibrated by net sampling and cannot directly provide species-specific estimates. However, hydroacoustic methods can be economically applied to all intakes 24 h per day, and provide information about variations among intakes and hours of the day. While hydroacoustic sampling requires more than the 1 to 2 hours needed by netting to obtain reliable FGE estimates, it can provide seasonal estimates for single routes that are not limited by the number of fish sampled. Fixed-aspect hydroacoustics provides estimates for unidentified and untagged fish and can provide estimates for individual passage routes that usually comport with estimates from more intensive netting methods.

4.4 Spatial Trends in Fish Passage

4.4.1 Horizontal Distributions

The proportion of discharge through major passage routes was a good indicator of the relative percentage of fish passage among those routes in spring but was less so in the summer. In spring, about 7% of both fish passage and discharge occurred at Powerhouse 1, 14% of the fish and 16% of the flow passed through the spillway, and Powerhouse 2 passed 79% of the fish with 76% of the flow. Fish and flow percentages also matched up well at Powerhouse 1 in summer (about 8% of the fish with about 9%

of the flow), but the relative proportions at the other passage routes (the spillway and Powerhouse 2) differed. For the entire summer period, the spillway passed 20% of the fish in summer with 11% of the flow and Powerhouse 2 passed about 72% of the fish with 80% of the flow. During spill days in summer, the spillway passed 58% of the fish in just 36% of the flow, while Powerhouse 2 passed 40% of the fish in 61% of the flow.

The exceptional effectiveness of the spillway during the 10 days of spill in early summer may be explained by a peak in the summer migration, spill at the expense of generation at some Powerhouse 2 units, and the fact that forebay elevations were falling (Figure 4.2). According to salmonid run-timing estimates by the hydroacoustics and JBS counts (Figure 3.24), the largest peak in the summer run passed the dam during these early days of summer sampling. When forebay elevations drop (as in Figure 4.2), the depth of a bottom ridge upstream of Cascades Island and into the Powerhouse 2 forebay is shallower than it is when pool levels are high. Subyearling fish migrating along the shore upstream of the Powerhouse 2 forebay may guide along the channel edge that separates the Powerhouse 2 forebay from the main channel leading to the spillway, particularly when water levels decrease. In 2001, Powerhouse 2 was the priority powerhouse and usually was fully loaded. However, during the 10 days of spill in early summer, the percent of off-hours for Powerhouse 2 turbines was higher than usual (Unit 17 = 100%; Unit 15 = 46%; Unit 14 = 41%; Unit 13 = 25%; Unit 12 = 14%; and Unit 11 = 5%).
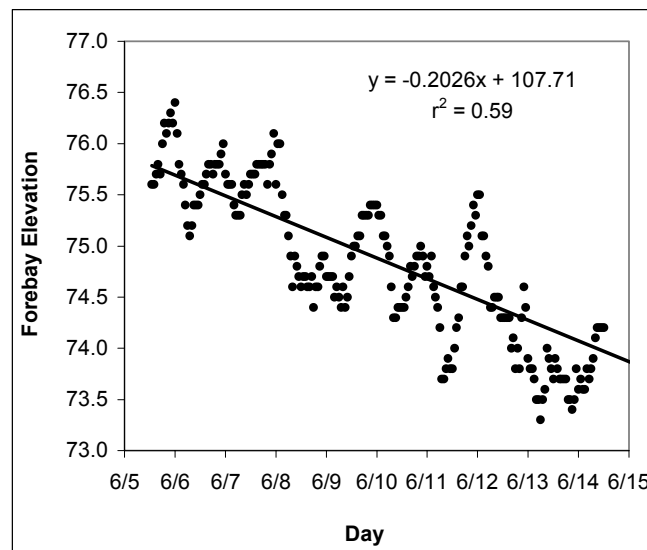
Figure 4.2. Plot of Bonneville Dam Forebay Elevation during the First 9 Days of Summer when Spill was Occurring in 2001.

Lateral fish passage patterns that may normally occur during times of full loading of Powerhouse 1 could not occur in 2001 given the drought and a Powerhouse 2 priority for generation. Flow was so low in both spring and summer at Powerhouse 1 that many of the units seldom ran, particularly during periods of spill. Horizontal passage patterns at Powerhouse 1 were consistent between seasons, the majority of both fish passage and discharge occurring through Unit 9 and Unit 10.

Fish passage at the spillway was slightly skewed to the south during both seasons, despite a relatively even distribution of discharge across the spillway. This was mainly due to low passage rates at Bays 2,

which passed far fewer fish than bays at the southern end of the spillway, although they discharged about the same amount of water as the bays to the south.

The southern skew in the distribution of fish passage at Powerhouse 2 in both seasons was much more noticeable in 2001 than it was in 2000, and it certainly supports the management decision to build a corner collector adjacent to Unit 11. Fish passage through the south half of the second powerhouse was consistently high during both sampling seasons. About 70% of the fish passing through Powerhouse 2 passed through units 11 to 14, although these units discharged only slightly more than half of the water (52.6%). Not only was the total number of fish passing higher at units 11 to 15 than at units 16 through 18, but fish density or concentration of fish also was higher. Units 11 to 15 passed roughly similar numbers of fish per volume of water during spring and summer. Unit 17 was off-line all summer. We also observed a southern skew in the passage distribution in summer 1996 (Ploskey et al. 1998).

Individual turbine FGE at Powerhouse 2 was lowest at the two units operating nearest each end of the powerhouse during spring and summer. The low turbine FGE values estimated at Units 17 and 18 in spring and Units 16 and 18 in summer did not affect powerhouse FGE as much as the low turbine FGE values at Units 11 and 12 because fish passage densities at the north units were low. The two units at the south end of the powerhouse, on the other hand, passed many fish at relatively high densities with poor guidance and so had a larger negative contribution to total powerhouse FGE.

4.4.2 Vertical Distributions

4.4.2.1 Powerhouse 1 -- Unit 10

The vertical distributions of fish at Unit 10 in spring and summer strongly suggest that installing an ESBS similar to the one installed at Unit 8 would improve FGE in spring, but the benefit would be less in summer. The elevation for classifying detected fish as guided or unguided was about 21 ft MSL. According to Figure 3.19 an ESBS and this cutoff criterion, an ESBS would guide about 68% of the fish in spring but only about 50% in summer. In spring 2001, we classified about 47% of all fish as guided by the STS, but in summer, that percentage fell to about 36%. In the 2000 passage season we found an estimated FGE of 72% in spring that fell to 50% in summer (Ploskey et al. 2002a).

4.4.2.2 Upstream and Downstream of Modified Unit 15

Two pieces of evidence indicate that fish approaching trash racks increased in depth and changed behavior, and these factors may make them more or less susceptible to being guided by a STS inside the turbine. First, peaks in vertical distributions of fish located below the elevation of the top of the intake and 4 to 9 ft from trash racks were 9 to 12 ft deeper than peaks in distributions sampled 16 to 21 ft upstream (Figures 3.21 and 3.22). Second, direction-of-movement and fish-detection statistics show that 70% of the relatively few detections 10 to 15 ft upstream of trash racks were moving downstream, whereas only about 54% to 55% of many detections within 4 to 9 ft of trash racks were moving downstream.

In short, we found lower numbers and deeper distributions of fish detected 4 to 9 ft from the racks than of fish detected 16 to 21 ft from the racks. These differences were consistent for both spring and summer. Higher numbers of fish close to the trash racks may indicate that fish paused in their

downstream movement as they encounter physical cues relating to the presence of the racks. If fish paused just upstream of the racks, they could easily have been counted multiple times as they passed in and out of the sampling volume, resulting in higher cumulative counts. Horizontal fish movement was oriented fairly randomly close to the trash racks, while movement was oriented more downstream farther upstream of the racks.

Smaller individuals that make up the summer smolt population likely are less able to maintain their vertical position in the water column when they pause upstream of the trash racks. Fish that pause in their downstream movement just upstream of the trash racks are not only exposed to the downstream component of flow, they also encounter strong downward water velocities. The agreement of theoretical FGE with observed in-turbine FGE during spring may indicate that the spring-migrating smolts were able to maintain both their horizontal and their vertical position in the water column as they paused before going through the trash racks. In summer, the lower vertical distribution of fish detected 4-9 ft upstream of the trash racks, as compared to those detected 16-21 ft upstream of the racks, was more exaggerated than during spring. In addition, theoretical FGE was significantly higher than observed in-turbine FGE in summer (Figure 3.19). Our analysis of theoretical FGE is based on the hypothesis that fish detected in front of the trash racks at Intake 15<u>b</u> will follow the flow lines that parallel the roof of the intake ceiling into the intake.

4.5   Temporal Trends in Fish Passage

4.5.1   Seasonal Trends

4.5.1.1 Run Timing

Run timing estimated by hydroacoustics compared favorably with the estimate based upon sampling the juvenile bypass facility at Powerhouse 2 by the NMFS. Most major peaks in the run-timing distributions occur at similar times, although size and duration of those peaks were not identical.

American shad present a problem for hydroacoustic sampling in summer. Almost 2.3 million American shad migrated up through Bonneville Dam in 2001. Shad began arriving at the dam in mid May and were present in large numbers during the third week in May before peaking on 1 June when 144,000 individuals were observed. By 6 June, 50% of all the migrating shad had already passed the dam. By 30 June, the shad migration was essentially complete with over 98% of all fish having passed by that day. The Bonneville Dam 2001 shad up migration was nearly twice as large as the 2000 run and it peaked 10 days earlier.

4.5.1.2 Major Fish Passage Metrics

The 9% decline in FPE from spring to summer at Powerhouse 1 and the 26% decline at Powerhouse 2 were similar to but slightly larger than seasonal declines observed in 2000 for Powerhouse 1 (6%) and for Powerhouse 2 (19%). Powerhouse 1 FPE in 2000 was 67% in spring and 61% in summer, and these estimates were 18% and 21% higher than respective estimates in spring and summer 2001. The difference most likely resulted from the nearly continuous operation of the PSC and Unit 8 with an ESBS in 2001. In 2001, the PSC units functioned as standard STS units and Unit 8 ran less than 1 day each season, because of drought prioritization of operations.

4.5.1.3 Guidance Efficiency at Modified Unit 15

The spring to summer decline in FGE that we observed at Unit 15 was typical of what we have observed at most units at Bonneville Dam, but the summer FGE estimate was not as low as those from other STS-equipped units at Powerhouse 1 or 2 in the summer of 2000. It was comparable to adjacent Units 14 and 16 in 2001. The nighttime FGE of Unit 15 decreased about 20% from 74 to 54 from spring through summer in 2001. In 2000, the summer FGE estimate for Powerhouse 1 units running STS and the summer FPE of Powerhouse 2, which had no modified units was about 30%.

4.5.2 Diel Trends

Providing a Powerhouse 2 priority and nighttime spill could significantly improve fish-passage efficiency in spring by as much as 6% to 12% during a drought year, while minimizing fallback of adult salmonids through the spillway. Factors contributing to a 6% to 12% higher project FPE at night than during the day included significantly higher nighttime fish passage through the project (Figure 3.31), including the spillway (Figure 3.32) and Powerhouse 2 (Figure 3.34), and higher FGE of Powerhouse-2 turbines at night (Figure 3.34) than during the day.

We have no definitive explanation for the higher spill efficiency and spill effectiveness observed from morning through early afternoon in summer, except to note that those observations were based on only 10 days of spill in summer. If American shad contaminated samples at the spillway in early summer, they might be expected to do so at night and in early morning, when most are not actively migrating upstream, as they do in the afternoon and evening (Figure 4.3). However, we observed few incidences of shad contamination of samples at the spillway in the echograms that we processed manually for quality control and assurance.
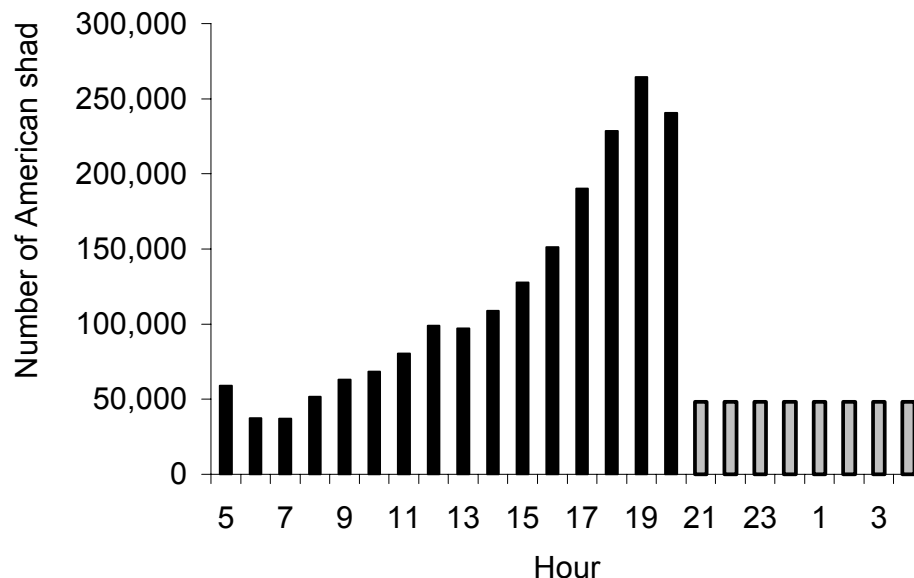
Figure 4.3. Diel Pattern of Shad Passage through Bonneville Dam in Summer 2001. Gray bars are hourly estimates produced by dividing the difference between the total season count and the sum of the hourly counts from 0500 to 2000 hours by eight.

4.6   Fish Guidance Efficiencies

4.6.1   Comparing Performance of Fish-Guidance Structures

Modification of Unit 15 increased the FGE of this unit relative to all other unmodified units (Unit 8 with an ESBS excluded) in spring and summer (Figure 3.39), and its FGE was among the highest for individual Powerhouse 2 units summer (Figure 3.40). It is important to note that FGE estimates for different units were not computed for exactly the same days and hours because units ran at different times. Therefore, time of day and day-to-day variation in FGE are a part of these estimates and comparisons. Unit 8 had a 40-ft-long ESBS while the gatewell and vertical barrier screen at Unit 15 were modified to improve flow up the gatewell and improve FGE. As in 2000, the FGE of the ESBS in summer was no better than that of STS during the same season. We considered FGE estimates for Intake 15b to be more reliable than those did for 15c (which were lower) because we sampled more minutes per hour and confidence intervals were tighter. Intake 15b passed 2.42 times more fish than did Intake 15c in both seasons so the Intake 15b estimate provided a closer approximation to FGE for the entire unit than did the estimate for Intake 15c.

Provision of a Powerhouse 2 priority in spring was a good management tactic because Powerhouse 2 units tended to provide higher FGE than do those at Powerhouse 1 units in spring. The FGE was similar and low for both powerhouses in summer. The higher FGE of Powerhouse 2 units may have resulted from the presence of TIES at every other intake, and the fact that five of nine intakes that we sampled were between TIES where passage and FGE tended to be higher. We also observed higher FGE in spring at Intake 15b, which was between two TIES, than we did at Intake 15c, which was behind a TIE (Figure 3.41). There also was a tendency for FGE to be lower at the ends of Powerhouse 2 than in the middle, but since the intakes we sampled at end units of Powerhouse 2 were behind instead of between TIES, the effect of unit location could have been masked. Unit 1 had the lowest FGE at Powerhouse 1 in both spring and summer.

4.6.2   Comparing FGE Estimates by Different Sampling Methods

Our estimates of FGE compared very well with netting estimates by the NMFS in both seasons, particularly when we estimated FGE from all nighttime hours sampled instead of just hours of concurrent sampling (Figure 4.1). Hydroacoustic estimates of FGE require longer sampling durations than the 1 to 2 hours that are commonly used to estimate FGE by netting, because hydroacoustic beams sample only about 5% of the cross-sectional area of an intake compared to near 100% coverage by netting. For example, Ploskey and Carlson (1999) observed that the precision of hydroacoustic estimates of FGE at John Day Dam increased by 50%, and the r^2 of a correlation line between hydroacoustic and netting estimates increased by 19%, when the hydroacoustic sampling duration was extended from the typical netting duration of 1-2 h to 4 h. In 2001, we were able to sample throughout the night only when the NMFS was conducting orifice passage efficiency testing, and the unit was operated all night. On most nights of netting to estimate FGE, Unit 15 was shut down after netting and was not restarted until the next FGE test the following night. This type of on and off operation, as depicted in Figure 4.4, severely limited the number of fish that could be detected by hydroacoustics and the precision and accuracy of hydroacoustic estimates. We made up for this shortcoming by using all available hours of nighttime sampling to make seasonal estimates, but it would have been preferable for hydroacoustic sampling to run the unit throughout the night after FGE netting ends.
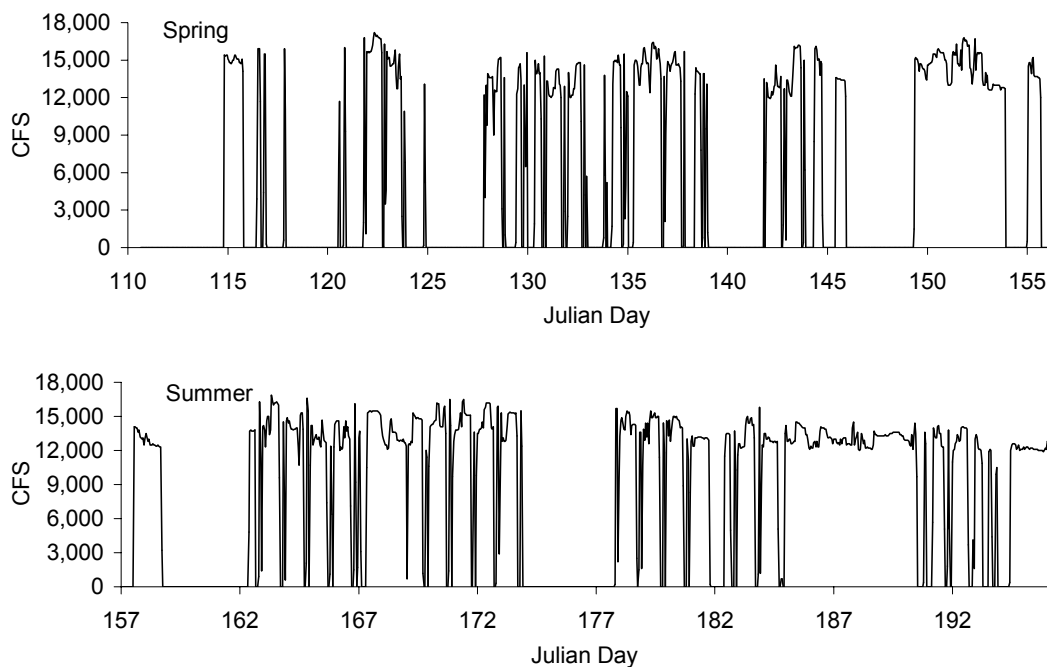
Figure 4.4. Patterns of Discharge of Modified Unit 15 in Spring and Summer 2001 showing the Frequency of On and Off Periods

Another problem introduced by excessive on and off operation of a turbine unit is that hydroacoustic beams continue to sample and fish that are swimming around in the unit when it is off are detected, often many times. At Unit 15, we carefully threw out all fish detected before or after FGE netting based upon start and end times provided by Bruce Monk (NMFS). In addition, we threw out all fish detected during hours in which the Unit 15 discharged < 65% of its maximum discharge because the operations data available in 2001 was only for whole hours. Operations data reported at 5-minute intervals, like those available in 2000 and earlier years, were much better for accurately assigning zero fish counts to samples collected when units are off.

We have two recommendations for FGE testing in 2002 to provide better hydroacoustic FGE estimates. First, we recommend that the test unit be run as much as possible instead of having it run solely for FGE and orifice passage netting. Second, we recommend that on and off times be recorded with the dam operations data or at least that discharge be recorded at 5-minute intervals instead of hourly.

Similar hydroacoustic and netting estimates of FGE for Unit 15 were 32.0 and 36.7% higher, respectively, than were radio telemetry estimates for the same unit in spring, and this may be a function of limited sample sizes in radio tagged data for individual units. The 38% FGE estimate by radio telemetry in spring was based upon only 19 guided fish of 50 (total) for the entire season, whereas netting estimates usually were based upon > 10 times that number in 1 to 2 hours of sampling. The number of fish counted by concurrent hydroacoustic sampling (14,687) and netting (16,651) also were similar. Dispersion expected for 19 of 50 fish based upon the binomial distribution (i.e., 25% to 53%; Cliff Pereira – Personal Communication) does not account for the magnitude of observed differences between the low radio-telemetry estimate and the higher and concordant netting and hydroacoustic estimates.

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Appendix A

Transducer Calibrations and Receiver Gains

Appendix A

Transducer Calibrations and Receiver Gains

Appendix A-1. Calibration Data and Calculated Receiver Gains for Single-Beam and Split-Beam Transducers Deployed at Powerhouse 1 to Provide Equal Detectability for On-Axis Targets Ranging in Acoustic Size from –56 to –36 dB. Results for split-beam transducers are presented for the x phase, y phase, and the mean of x and y phases.

Echo-sounder Letter and Channel Number	Trans-ducer Number and Phase (if split beams)	Difference in Cable Length Between Calibrated Cable and Installed Cable (ft)	Receiver Gain Adjusted for Difference in Cable Length (dB)	Source Level Adjusted for Difference in Cable Length (dB)	Receiver Sensitivity Adjusted for Difference in Cable Length (dB)	Target Strengthof Smallest On-axis Target (dB)	Voltage of Smallest On-axis Target (dB)	Voltage of Smallest On-axis Target at 20 dB per Volt (V)	Turbine Intake
C-8	8	-2	3.14	215.04	-112.18	-56	50	2.5	4A
C-7	7	-2	2.42	215.42	-111.84	-56	50	2.5	4A
C-6	6	-2	3.76	214.86	-112.62	-56	50	2.5	3C
C-5	5	-2	2.23	215.45	-111.68	-56	50	2.5	3C
C-4	4	-2	3.12	215.08	-112.20	-56	50	2.5	2A
C-3	3	-2	4.55	214.37	-112.92	-56	50	2.5	2A
C-2	2	-2	3.01	215.09	-112.10	-56	50	2.5	1B
C-1	1	-1	2.79	215.15	-111.94	-56	50	2.5	1B
D-8	19	-2	2.23	215.63	-111.86	-56	50	2.5	9C
D-7	18	-2	1.91	215.65	-111.56	-56	50	2.5	9C
D-6	17	-2	2.19	215.63	-111.82	-56	50	2.5	8B
D-5	13	-2	3.73	214.91	-112.64	-56	50	2.5	8B
D-4	12	-2	3.74	214.92	-112.66	-56	50	2.5	7A
D-3	11	-1	3.23	215.11	-112.34	-56	50	2.5	7A
D-2	10	-2	2.75	215.23	-111.98	-56	50	2.5	6C
D-1	9	0	3.02	215.09	-112.11	-56	50	2.5	6C
A-1	105 (x)	0	10.53	214.04	-108.57	-56	60	3.0	10B
A-1	105 (y)	0	10.47	214.08	-108.55	-56	60	3.0	10B
A-1	105	0	10.50	214.06	-108.56	-56	60	3.0	10B
A-0	53 (x)	0	10.29	214.16	-108.45	-56	60	3.0	10B
A-0	53 (y)	0	10.29	214.20	-108.49	-56	60	3.0	10B
A-0	53	0	10.29	214.18	-108.47	-56	60	3.0	10B
X-1	412 (x)	0	4.14	215.17	-103.31	-56	60	3.0	5B
X-1	412 (y)	0	4.14	215.17	-103.31	-56	60	3.0	5B
X-1	412	0	4.14	215.17	-103.31	-56	60	3.0	5B
X-0	413 (x)	0	4.17	215.14	-103.31	-56	60	3.0	5B
X-0	413 (y)	0	4.14	215.15	-103.29	-56	60	3.0	5B
X-0	413	0	4.16	215.15	-103.30	-56	60	3.0	5B

Appendix A-2. Calibration Data and Calculated Receiver Gains for Single-Beam and Split-Beam Transducers Deployed at the Spillway to Provide Equal Detectability for On-Axis Targets Ranging in Acoustic Size from –56 to –36 dB. Results for split-beam transducers are presented for the x phase, y phase, and the mean of x and y phases.

Echo-sounder Letter and Channel Number	Trans-ducer Number and Phase (if split beams)	Difference in Cable Length Between Calibrated Cable and Installed Cable (ft)	Receiver Gain Adjusted for Difference in Cable Length (dB)	Source Level Adjusted for Difference in Cable Length (dB)	Receiver Sensitivity Adjusted for Difference in Cable Length (dB)	Target Strength of Smallest On-axis Target (dB)	Voltage of Smallest On-axis Target (dB)	Voltage of Smallest On-axis Target at 20 dB per Volt (V)	Spill Bay
P-1	49	-300	9.44	210.66	-104.10	-56	60	3.0	8.0
P-3	50	0	4.04	213.77	-101.81	-56	60	3.0	12.0
P-2	51	-200	7.13	212.60	-103.73	-56	60	3.0	10.0
P-5	54	0	3.24	214.29	-101.53	-56	60	3.0	15.0
P-4	56	0	4.69	213.74	-102.43	-56	60	3.0	14.0
Q-1	42	0	4.06	213.71	-101.77	-56	60	3.0	2.0
Q-2	43	0	4.08	213.97	-102.05	-56	60	3.0	4.0
Q-3	44	0	3.93	213.56	-101.49	-56	60	3.0	5.0
Q-4	45	0	3.83	213.96	-101.79	-56	60	3.0	6.0
Q-5	48	0	5.58	212.09	-101.67	-56	60	3.0	7.0
O-0	120 (x)	0	15.27	209.76	-109.03	-56	60	3.0	17.0
O-0	120 (y)	0	15.34	209.69	-109.03	-56	60	3.0	17.0
O-0	120	0	15.31	209.73	-109.03	-56	60	3.0	17.0

Appendix A-3. Calibration Data and Calculated Receiver Gains for Single and Split-Beam Transducers to Provide Equal Detectability for On-Axis Targets Ranging from –56 to –36 dB in Acoustic Size at Powerhouse 2. Results for split-beam transducers are presented for the x phase, y phase, and the mean of x and y phases.

Echo-sounder Letter and Channel Number	Trans-ducer Number and Phase (if split beams)	Difference in Cable Length Between Calibrated Cable and Installed Cable (ft)	Receiver Gain Adjusted for Difference in Cable Length (dB)	Source Level Adjusted for Difference in Cable Length (dB)	Receiver Sensitivity Adjusted for Difference in Cable Length (dB)	Target Strength of Smallest On-axis Target (dB)	Voltage of Smallest On-axis Target (dB)	Voltage of Smallest On-axis Target at 20 dB per Volt (V)	Turbine Intake
G-2	28	0	3.60	215.03	-112.63	-56	50	2.5	11C
G-1	40	-2	1.73	216.01	-111.74	-56	50	2.5	11C
G-3	44	0	2.85	215.32	-112.17	-56	50	2.5	12A
G-4	35	25	2.01	215.92	-111.92	-56	50	2.5	12A
G-6	42	0	2.17	215.70	-111.87	-56	50	2.5	13B
G-5	39	-31	1.86	215.55	-111.41	-56	50	2.5	13B
G-8	38	-24	2.29	215.60	-111.89	-56	50	2.5	14C
G-7	36	5	2.94	215.39	-112.32	-56	50	2.5	14C
H-6	57	2	3.69	215.01	-112.70	-56	50	2.5	16B
H-5	58	0	1.02	216.39	-111.41	-56	50	2.5	16B
H-7	59	0	3.67	214.98	-112.65	-56	50	2.5	17B
H-8	60	0	2.60	215.43	-112.03	-56	50	2.5	17B
H-1	61	-1	2.60	215.46	-112.06	-56	50	2.5	15B
H-2	63	0	4.10	214.89	-112.99	-56	50	2.5	15B
H-3	56	3	4.08	214.85	-112.93	-56	50	2.5	15C
H-4	29	0	1.61	215.96	-111.57	-56	50	2.5	15C
I-0	51 (x)	0	7.03	214.66	-105.69	-56	60	3.0	18B
I-0	51 (y)	0	6.83	214.66	-105.49	-56	60	3.0	18B
I-0	51	0	6.93	214.66	-105.59	-56	60	3.0	18B
I-10	52 (x)	0	9.18	213.87	-107.05	-56	60	3.0	18B
I-10	52 (y)	0	9.20	213.87	-107.07	-56	60	3.0	18B
I-10	52	0	9.19	213.87	-107.06	-56	60	3.0	18B
R-0	414 (x)	0	0.00	0.00	0.00	-56	-56	-2.8	15B upstream
R-0	414 (y)	0	0.00	0.00	0.00	-56	-56	-2.8	15B upstream
R-0	414	0	0.00	0.00	0.00	-56	-56	-2.8	15B upstream
R-1	415 (x)	0	0.00	0.00	0.00	-56	-56	-2.8	15B upstream
R-1	415 (y)	0	0.00	0.00	0.00	-56	-56	-2.8	15B upstream
R-1	415	0	0.00	0.00	0.00	-56	-56	-2.8	15B upstream
R-2	416 (x)	0	0.00	0.00	0.00	-56	-56	-2.8	15B upstream
R-2	416 (y)	0	0.00	0.00	0.00	-56	-56	-2.8	15B upstream
R-2	416	0	0.00	0.00	0.00	-56	-56	-2.8	15B upstream

Appendix B

Detailed Transducer Locations and Aiming Angles

Appendix B

Detailed Transducer Locations and Aiming Angles

Appendix B-1. Transducer Locations at Powerhouse 1 in 2001. Angle refers to the angle off the trash-rack or extended- submerged-bar-screen (ESBS) plane. Abbreviations are as follows: SB = split-beam; (D) = downstream; Rack = trash rack, where Rack 1 is the uppermost of six trash racks, and its top is at Elevation 69 ft MSL.

System Letter	Channel	Trans- ducer	Beam Angle	Intake or Bay	Structure	Location on Placement on Structure	Elevation (ft)	Aim	Angle (Degrees)
C	1	1	6	1B	Rack 1	4.4 ft below top; 11.0 ft S of N Side	64.6	Down	20 (D)
C	2	2	6	1B	Rack 5	Bottom Shelf; 11.0 ft S of N Side	11.0	Up	18 (D)
C	3	3	6	2A	Rack 1	4.4 ft below top; 13.2 ft S of N Side	64.6	Down	20 (D)
C	4	4	6	2A	Rack 5	Bottom Shelf; 13.2 ft S of N Side	11.0	Up	18 (D)
C	5	5	6	2C	Rack 1	4.4 ft below top; 8.8 ft S of N Side	64.6	Down	20 (D)
C	6	6	6	2C	Rack 5	Bottom Shelf; 8.8 ft S of N Side	11.0	Up	18 (D)
C	7	7	6	4A	Rack 1	4.4 ft below top; 11.0 ft S of N Side	64.6	Down	20 (D)
C	8	8	6	4A	Rack 5	Bottom Shelf; 11.0 ft S of N Side	11.0	Up	18 (D)
X	0	413	SB 6	5B	Rack 1	4.4 ft below top; 13.2 ft S of N Side	64.6	Down	20 (D)
X	1	412	SB 6	5B	Rack 5	Bottom Shelf; 13.2 ft S of N Side	11.0	Up	18 (D)
D	1	9	6	6C	Rack 1	4.4 ft below top; 8.8 ft S of N Side	64.6	Down	20 (D)
D	2	10	6	6C	Rack 5	Bottom Shelf; 8.8 ft S of N Side	11.0	Up	18 (D)
D	3	11	6	7A	Rack 1	4.4 ft below top; 11.0 ft S of N Side	64.6	Down	20 (D)
D	4	12	6	7A	Rack 5	Bottom Shelf; 11.0 ft S of N Side	11.0	Up	18 (D)
D	5	13	6	8B	Rack 5	7.6 ft below top; 11.0 ft S of N Side	14.0	Up	21 (D)
D	6	17	6	8B	ESBS	2.0 ft below pivot; 13.0 ft S of N Side	39.2	Down	30 (D)
D	7	18	6	9C	Rack 1	4.4 ft below top; 8.8 ft S of N Side	64.6	Down	20 (D)
D	8	19	6	9C	Rack 5	Bottom Shelf; 8.8 ft S of N Side	11.0	Up	18 (D)
A	0	53	SB 6	10B	Rack 1	4.4 ft below top; 8.8 ft S of N Side	64.6	Down	20 (D)
A	1	105	SB 6	10B	Rack 5	Bottom Shelf; 8.8 ft S of N Side	11.0	Up	18 (D)

Appendix B-2. Transducer Locations at the Spillway in 2001. Spillway transducer elevations depend
upon gate position and are presented for a 3 ft opening, the maximum observed in 2001.
Angle is the angle of the center of the transducer beam off the spill-gate. Abbreviations
are as follows: SB = split-beam; (U) = upstream.

System Number	Channel	Trans-ducer	Beam Angle	Intake or Bay	Structure	Location on Placement on Structure	Elevation (ft)	Aim	Angle (Degrees)
Q	1	42	10	2	Spill Gate	28 ft below the top; 28.5 ft S of N side	59.0	Down	8 (U)
Q	2	43	10	4	Spill Gate	28 ft below the top; 17.1 ft S of N side	59.0	Down	8 (U)
Q	3	44	10	5	Spill Gate	28 ft below the top; 37.0 ft S of N side	59.0	Down	8 (U)
Q	4	45	10	6	Spill Gate	28 ft below the top; 28.5 ft S of N side	59.0	Down	8 (U)
Q	5	48	10	7	Spill Gate	28 ft below the top; 37.1 ft S of N side	59.0	Down	8 (U)
P	1	49	10	8	Spill Gate	28 ft below the top; 17.1 ft S of N side	59.0	Down	8 (U)
P	2	51	10	10	Spill Gate	28 ft below the top; 40.0 ft S of N side	59.0	Down	8 (U)
P	3	50	10	12	Spill Gate	28 ft below the top; 25.6 ft S of N side	59.0	Down	8 (U)
P	4	56	10	14	Spill Gate	28 ft below the top; 36.8 ft S of N side	59.0	Down	8 (U)
P	5	54	10	15	Spill Gate	28 ft below the top; 28.5 ft S of N side	59.0	Down	8 (U)
O	0	120	SB 12	17	Spill Gate	28 ft below the top; 25.5 ft S of N side	59.0	Down	15 (U)

Appendix B-3. Transducer Locations at Powerhouse 2 in 2001. Angle refers to the angle off the trash-rack plane. Abbreviations are as follows: SB = split-beam; (D) = downstream; (U) = upstream; Beam = a horizontal beam lowered into the trash-rack slot; Rack = trash rack, where Rack 1 is the uppermost of six trash racks, and its top is at Elevation 38 ft MSL.

System Number	Channel	Trans-ducer	Beam Angle	Intake or Bay	Structure	Location on on Structure	Elevation (ft)	Aim	Angle (Degrees)
G	1	40	6.5	11C	Rack 1	18.5' S of N Side of rack	30.7	Down	20 (D)
G	2	28	6.5	11C	Rack 4	18.5' S of N Side of rack	4.5	Up	25 (D)
G	3	44	6.5	12A	Rack 1	8.17' S of N side of rack	30.7	Down	20 (D)
G	4	35	6.5	12A	Rack 4	8.17' S of N side of rack	4.5	Up	25 (D)
G	5	39	6.5	13B	Rack 1	13' S of N side of rack	30.7	Down	20 (D)
G	6	42	6.5	13B	Rack 4	13' S of N side of rack	4.5	Up	25 (D)
G	7	36	6.5	14C	Rack 1	13' S of N side of rack	30.7	Down	20 (D)
G	8	38	6.5	14C	Rack 4	13' S of N side of rack	4.5	Up	25 (D)
H	1	61	6.5	15B	Rack 1	18.5' S of N Side of rack	30.7	Down	20 (D)
H	2	63	6.5	15B	Rack 4	18.5' S of N Side of rack	4.5	Up	25 (D)
H	3	56	6.5	15C	Rack 1	8.17' S of N side of rack	30.7	Down	20 (D)
H	4	29	6.5	15C	Rack 4	8.17' S of N side of rack	4.5	Up	25 (D)
H	5	58	6.5	16B	Rack 1	13' S of N side of rack	30.7	Down	20 (D)
H	6	57	6.5	16B	Rack 4	13' S of N side of rack	4.5	Up	25 (D)
H	7	59	6.5	17B	Rack 1	13' S of N side of rack	30.7	Down	20 (D)
H	8	60	6.5	17B	Rack 4	13' S of N side of rack	4.5	Up	25 (D)
I	0	51	6	18B	Rack 1	19.75' S of N Side of rack	30.7	Down	20 (D)
I	10	52	6	18B	Rack 4	19.75' S of N Side of rack	4.5	Up	25 (D)
R	0	414	SB 6	15B	Beam	Variable laterally	70 ft	Down	6 (U)
R	1	415	SB 6	15B	Beam	Variable laterally	70 ft	Down	12 (U)
R	2	416	SB 6	15B	Beam	Variable laterally	70 ft	Down	18 (U)

Appendix C

Autotracker Definitions and Settings

Appendix C

Autotracker Definitions and Settings

Appendix C-1. Definitions of Autotracking Software Parameters Used for Processing Hydroacoustic Data from Bonneville Dam in 2001. Values of parameters that did not vary among deployments are set in the Parameter column.

Parameter	Definition
Block Size	Maximum number of ping of data to process as a sample
Maximum Range	Range (cm) to end autotracking
Minimum Range	Range (cm) to begin autotracking
Structure Threshold = 0.075	Fraction of possible echoes in a range bin that triggers assignment as structure
Range noise = 0.2 decimeters	Range (decimeters) uncertainty in the position of an echo in range for initial binning of echoes
Vertical Gate Size	Maximum range about the predicted postion of the next echo in which an encounter echo will be added to a fish track
Maximum Ping Gap = 2	Maximum ping gap before the tracker will quit trying to add echoes to a track segment. This does not preclude linking segments.
Alpha = 0.6	Parameter used in an Alpha-Beta tracking formula; Beta was calculated from Alpha as follows: $\text{Beta} = 2(2 - \text{Alpha}) - 4(1 - \text{Alpha})^{0.5}$
Link Gate	Range (cm) over which two colinear tracked segments will be linked
Maximum Echo or Target Strength = 36 dB	Largest acoustic size acceptible for autotracking. This may be based upon echo strength (dB) from single beams or target strength (dB) from split beams
Minimum Echo or Target Strength = 56 dB	Smallest acoustic size acceptible for tracking. Also known as the on-axis strength of an echo.
Noise Level = 5	Number of times an echo will be expanded to define noise regions in a noise-characterization routine
Range to Start Bottom Detect	Sets the range at which a bottom detection routine will begin. If this parameter exceeds Maximum Range, then no bottom detection routine is implemented.
Bottom Count Threshold = 0.3	Threshold for classifying a range bin as bottom based upon the fraction of pings within a range bin that exceed some amplitude threshold. This can be important for up-looking transducers aimed to the waters surface which can flucturate.
Bottom Amplitude Threshold = -33 dB	Acoustic amplitude (dB) required for a of an echo to be considered as a bottom echo.
Segment Link Gate = 20	Maximum number of pings allowed between colinear track segments.

Appendix C-2. Autotracking Software Settings Used for Bonneville Dam Data in 2001

System (Channe) & Aiming Direction	Data Block Size (pings)	Max. Range (cm)	Min. Range (cm)	Vertical Gate Size (cm)	Link Gate (cm)	Range to Start Bottom Detect (cm)
A (0) Up	2000	1330	810	6	20	3600
A (1) Down	2000	2000	830	15	40	3600
C (1) Down	2000	2020	810		40	3600
C (2) Up	2000	1340	830	6	20	3600
C (3) Down	2000	2020	810	15	40	3600
C (4) Up	2000	1350	830	6	20	3600
C (5) Down	2000	2020	810	15	40	3600
C (6) Up	2000	1350	830	6	20	3600
C (7) Down	2000	2030	810	15	40	3600
C (8) Up	2000	1350	830	6	20	3600
D (1) Down	2000	2020	810	15	40	3600
D (2) Up	2000	1350	830	6	20	3600
D (3) Down	2000	2010	810	15	40	3600
D (4) Up	2000	1350	830	6	20	3600
D (5) Up	2000	1280	270	6	20	3600
D (6) Up	2000	1240	310	15	40	3600
D (7) Down	2000	2020	810	15	40	3600
D (8) Up	2000	1390	830	6	20	3600
X (1) Down	2000	1330	810	15	40	3600
X (2) Up	2000	2020	830	6	20	3600
O (0) Down	2000	1300	0	15	40	1050
P (1) Down	2000	1300	0	15	40	1050
P (2) Down	2000	1300	0	15	40	1050
P (3) Down	2000	1300	0	15	40	1050
P (4) Down	2000	1300	0	15	40	1050
P (5) Down	2000	1300	0	15	40	1050
Q (1) Down	2000	1300	0	15	40	1050
Q (2) Down	2000	1300	0	15	40	1050
Q (3) Down	2000	1300	0	15	40	1050
Q (4) Down	2000	1300	0	15	40	1050
Q (5) Down	2000	1300	0	15	40	1050
G (1) Down	2000	1630	520	15	40	3600
G (2) Up	2000	930	328	6	20	3600
G (3) Down	2000	1640	520	15	40	3600
G (4) Up	2000	930	328	6	20	3600
G (5) Down	2000	1640	520	15	40	Bottom
G (6) Up	2000	930	328	6	20	Detect
G (7) Down	2000	1640	520	15	40	3600
G (8) Up	2000	930	328	6	20	3600
H (1) Down	1000	1650	520	15	40	3600
H (2) Up	1000	930	328	6	20	3600
H (3) Down	2000	1650	520	15	40	3600
H (4) Up	2000	920	328	6	20	3600
H (5) Down	2000	1650	520	15	40	3600
H (6) Up	2000	920	328	6	20	3600
H (7) Down	2000	1650	520	15	40	3600
H (8) Up	2000	930	328	6	20	3600
I (0) Down	2000	1610	520	15	40	3600
I (10) Up	2000	1040	328	6	20	3600
R (0) Down	2000	2990	0	15	40	3600
R (1) Down	2000	3030	0	15	40	3600
R (2) Down	2000	3130	0	15	40	3600

Appendix D

Statistical Analysis System Code for Filtering Echo Traces Selected by Autotracking Softwar

Appendix D

Statistical Analysis System Code for Filtering Echo Traces Selected by Autotracking Software

Appendix D-1. Definitions of Variables Used for Filtering Echo Traces Selected by Autotracking Software in 2001

Parameter	Definition
System	Corresponds to an echosounder and associated transducers. Echosounder channels and transducer locations are described in Appendix B.
Channel	Corresponds to a single transducer attached to one specific echosounder channel.
First Ping	The absolute ping number for the first echo in an a series of echoes forming an echo trace.
Last Ping	The absolute ping number for the last echo in an a series of echoes forming an echo trace. Last Ping / Group Size is the total number of pings in an echo trace.
Group Size	Describes the number transducers sampled simultaneously (1=slow multiplex; 2=fast multiplex)
Mean Target Strength	The average echo amplitude of a fish trace in dB. This would be echo strength for fish detected by single beam transducers. Maximum echo-strength thresholds were set 2.3 dB lower than target-strength thresholds based upon empirical data from the two types of distributions.
Echo Count	The number of echoes in a series forming an echo trace.
Linearity1	The mean cm deviation of echoes from a line fit through a series of echoes forming a trace.
Linearity2	The mean cm deviation of echoes from a parabola fit through a series of echoes forming a trace.
Noise Count Average	The number of noise echoes in a window around an echo trace. The window began 5 pings before the first echo and ended 5 pings after the last echo in the trace and was $\pm$ 0.5 m in range.
Slope	The change in range of an echo trace through time. Units are cm / ping.
Mid Range	The average of the ranges of the first and last echoes in an echo trace.

Appendix D-2. Statistical Analysis System (SAS) Code for Filtering Out Echo Traces that Did Not Meet Fish Trace Criteria in Spring 2001. Minimum ranges for sampling guided, unguided, and spilled fish, which are presented in legends of Figures 1-4, were implemented elsewhere in the processing program.

```
IF SYSTEM='A' THEN DO;
    IF CHANNEL EQ 0 THEN DO; *uplooker;
       IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -37) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
          (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
          ((Linearity2 / Echo_Count) >= 0.3) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          (Slope >= 3.35 OR Slope <= -3.35)
       THEN DELETE;
    END;
    IF CHANNEL EQ 1 THEN DO; *downlooker;
       IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -37) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
          ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
          ((Linearity2 / Echo_Count) > 0.45) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
          ((Slope > 10.5 OR SLOPE < -10.5) AND Mid_Range >  8.5) OR
          (Mid_Range  < 10.60 AND Slope < 3.0) OR
          (Mid_Range >= 10.60 AND Mid_Range <= 17.50 AND Slope < 2.0) OR
          (Mid_Range > 17.50 AND Mid_Range < 19.00 AND Slope < 1.5) OR
          (Mid_Range >= 19.00 AND Slope <= 0)
       THEN DELETE;
    END;
 END;
 IF SYSTEM='C' THEN DO;
    IF CHANNEL EQ 1 THEN DO; ***B slot; *downlooker;
       IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -39.33) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
          ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
          ((Linearity2 / Echo_Count) > 0.45) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
          ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
          (Mid_Range  < 10.60 AND Slope < 3.0) OR
          (Mid_Range >= 10.60 AND Mid_Range <=17.50 AND Slope < 2.0) OR
          (Mid_Range > 17.50 AND Mid_Range < 19.00 and Slope < 1.5) OR
          (Mid_Range >= 19.00 AND Slope <= 0)
       THEN DELETE;
    END;
    IF CHANNEL EQ 2 THEN DO; ***B slot;
       IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -39.33) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
          (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
          ((Linearity2 / Echo_Count) >= 0.3) OR
          (Slope >= 3.35 OR Slope <= -3.35) OR
          (Mid_Range >= 13.50)
       THEN DELETE;
    END;
    IF CHANNEL EQ 3 THEN DO; ***A slot; *downlooker;
       IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -39.33) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
          ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
          ((Linearity2 / Echo_Count) > 0.45) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
          ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
          (Mid_Range  < 10.60 AND Slope < 3.0) OR
```

```
          (Mid_Range >= 10.60 AND Mid_Range <=17.50 AND Slope < 2.0) OR
          (Mid_Range > 17.50 AND Mid_Range < 19.00 and Slope < 1.5) OR
          (Mid_Range >= 19.00 AND Slope <= 0)
       THEN DELETE;
    END;
    IF CHANNEL EQ 4 THEN DO; ***A slot;
       IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -39.33) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
          (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
          ((Linearity2 / Echo_Count) >= 0.3) OR
          (Slope >= 3.35 OR Slope <= -3.35) OR
          (Mid_Range >= 13.50)
       THEN DELETE;
    END;
    IF CHANNEL EQ 5 THEN DO; ***C slot; *downlooker;
       IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -39.33) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
          ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
          ((Linearity2 / Echo_Count) > 0.45) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
          ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
          (Mid_Range  < 10.60 AND Slope < 3.0) OR
          (Mid_Range >= 10.60 AND Mid_Range <=17.50 AND Slope < 2.0) OR
          (Mid_Range > 17.50 AND Mid_Range < 19.00 and Slope < 1.5) OR
          (Mid_Range >= 19.00 AND Slope <= 0)
       THEN DELETE;
    END;
    IF CHANNEL EQ 6 THEN DO; ***C slot;
       IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -39.33) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
          (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
          ((Linearity2 / Echo_Count) >= 0.3) OR
          (Slope >= 3.35 OR Slope <= -3.35) OR
          (Mid_Range >= 13.50)
       THEN DELETE;
    END;
    IF CHANNEL EQ 7 THEN DO; ***A slot; *downlooker;
       IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -39.33) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
          ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
          ((Linearity2 / Echo_Count) > 0.45) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
          ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
          (Mid_Range  < 10.60 AND Slope < 3.0) OR
          (Mid_Range >= 10.60 AND Mid_Range <=17.50 AND Slope < 2.0) OR
          (Mid_Range > 17.50 AND Mid_Range < 19.00 and Slope < 1.5) OR
          (Mid_Range >= 19.00 AND Slope <= 0)
       THEN DELETE;
    END;
    IF CHANNEL EQ 8 THEN DO; ***A slot;
       IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -39.33) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
          (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
          ((Linearity2 / Echo_Count) >= 0.3) OR
          (Slope >= 3.35 OR Slope <= -3.35) OR
          (Mid_Range >= 13.50)
       THEN DELETE;
    END;
END;
IF SYSTEM='D' THEN DO;
```

```
IF CHANNEL EQ 1 THEN DO; *downlooker;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -39.33) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
    ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
    ((Linearity2 / Echo_Count) > 0.45) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
    ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
    (Mid_Range  < 10.60 AND Slope < 3.0) OR
    (Mid_Range >= 10.60 AND Mid_Range <= 17.50 AND Slope < 2.0) OR
    (Mid_Range > 17.50 AND Mid_Range < 19.00 AND Slope < 1.5) OR
    (Mid_Range >= 19.00 AND Slope <= 0) OR
    (First_Range >= 18.60 AND First_Range <= 18.80 AND Last_Range >= 18.60 AND Last_Range <= 18.80)
  THEN DELETE;
END;
IF CHANNEL EQ 2 THEN DO;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -39.33) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
    (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
    ((Linearity2 / Echo_Count) >= 0.3) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    (Slope >= 3.35 OR Slope <= -3.35)
  THEN DELETE;
END;
IF CHANNEL EQ 3 THEN DO; *downlooker;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -39.33) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
    ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
    ((Linearity2 / Echo_Count) > 0.45) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
    ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
    (Mid_Range  < 10.60 AND Slope < 3.0) OR
    (Mid_Range >= 10.60 AND Mid_Range <=17.50 AND Slope < 2.0) OR
    (Mid_Range > 17.50 AND Mid_Range < 19.00 AND Slope < 1.5) OR
    (Mid_Range >= 19.00 AND Slope <= 0) OR
    (Mid_Range > 16.30 AND Echo_Count/((Last_Ping / 2 + 1) - First_Ping / 2) < 1.1) AND (Echo_Count >= 10 AND
((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    (First_Range >= 19.50)
  THEN DELETE;
END;
IF CHANNEL EQ 4 THEN DO;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -39.33) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
    (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
    ((Linearity2 / Echo_Count) >= 0.3) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    (Slope >= 3.35 OR Slope <= -3.35)
  THEN DELETE;
END;
IF CHANNEL EQ 5 THEN DO; *uplooker;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -39.33) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
    (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.25)) OR
    ((Linearity2 / Echo_Count) >= 0.25) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    (Slope >= 3.35 OR Slope <= -3.35) OR
    (Mid_Range > 12.20 And Slope > -0.25 AND Slope < 0.25)
  THEN DELETE;
END;
IF CHANNEL EQ 6 THEN DO; *downlooker;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -39.33) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
    (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.25)) OR
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          ((Linearity2 / Echo_Count) >= 0.25) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          (Slope >= 5 OR Slope <= -5) OR
          ((Mid_Range >= 11.35) AND (Slope > -1 OR Slope < 1)) OR
          (First_Range >= 11.30 And First_Range <= 11.70 AND Last_Range >= 11.30 AND Last_Range <= 11.70) OR
          (First_Range >= 12.00 And First_Range <= 12.20 AND Last_Range >= 12.00 AND Last_Range <= 12.20)
      THEN DELETE;
    END;
  IF CHANNEL EQ 7 THEN DO; *downlooker;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -39.33) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
        ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
        ((Linearity2 / Echo_Count) > 0.45) OR
        (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
        ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
        (Mid_Range  < 10.60 AND Slope < 3.0) OR
        (Mid_Range >= 10.60 AND Mid_Range <=17.50 AND Slope < 2.0) OR
        (Mid_Range > 17.50 AND Mid_Range < 19.00 AND Slope < 1.5) OR
        (Mid_Range >= 19.00 AND Slope <= 0) OR
        (First_Range >= 12.75 AND First_Range <= 12.90 AND Last_Range >= 12.75 AND Last_Range <= 12.90) OR
        (First_Range >= 14.70 AND First_Range <= 14.85 AND Last_Range >= 14.70 AND Last_Range <= 14.85) OR
        (First_Range >= 18.15 AND First_Range <= 18.35 AND Last_Range >= 18.15 AND Last_Range <= 18.35)
      THEN DELETE;
  END;
  IF CHANNEL EQ 8 THEN DO;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -39.33) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
        (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
        ((Linearity2 / Echo_Count) >= 0.3) OR
        (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        (Slope >= 3.35 OR Slope <= - 3.35) OR
        (Mid_Range > 13.30 AND ((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.03) OR
        (First_Range >=12.60 And First_Range <= 12.90 And Last_Range >= 12.60 AND Last_Range <= 12.90) OR
        (First_Range >=12.08 And First_Range <= 12.44 And Last_Range >= 12.08 AND Last_Range <= 12.44)
      THEN DELETE;
  END;
END;
IF SYSTEM='G' THEN DO;
  IF CHANNEL EQ 1 THEN DO; *downlooker;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -39.33) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
        ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
        ((Linearity2 / Echo_Count) > 0.6) OR
        (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
        ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
        (Mid_Range  < 8.50 AND Slope < 4.0) OR
        (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
        (Mid_Range > 14.00 AND Slope < 2.5)
      THEN DELETE;
  END;
  IF CHANNEL EQ 2 THEN DO;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -39.33) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.3)) OR
        (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.34)) OR
        ((Linearity2 / Echo_Count) >= 0.34) OR
        (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        (Slope >= 3.35 OR Slope <= -3.35)
      THEN DELETE;
  END;
  IF CHANNEL EQ 3 THEN DO; *downlooker;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -39.33) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
        ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
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        ((Linearity2 / Echo_Count) > 0.6) OR
        (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
        ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
        (Mid_Range  < 8.50 AND Slope < 4.0) OR
        (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
        (Mid_Range > 14.00 AND Slope < 2.5) OR
        (First_Range >=5.3 And First_Range <= 6.0 And Last_Range >= 5.3 AND Last_Range <= 6.0)
      THEN DELETE;
    END;
    IF CHANNEL EQ 4 THEN DO;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -39.33) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
        (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.34)) OR
        ((Linearity2 / Echo_Count) >= 0.34) OR
        (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        (Slope >= 3.35 OR Slope <= -3.35)
      THEN DELETE;
    END;
    IF CHANNEL EQ 5 THEN DO; *downlooker;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -39.33) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
        ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
        ((Linearity2 / Echo_Count) > 0.6) OR
        (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
        ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
        (Mid_Range  < 8.50 AND Slope < 4.0) OR
        (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
        (Mid_Range > 14.00 AND Slope < 2.5)
      THEN DELETE;
    END;
    IF CHANNEL EQ 6 THEN DO;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -39.33) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
        (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.34)) OR
        ((Linearity2 / Echo_Count) >= 0.34) OR
        (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        (Slope >= 3.35 OR Slope <= -3.35)
      THEN DELETE;
    END;
    IF CHANNEL EQ 7 THEN DO; *downlooker;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -39.33) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
        ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
        ((Linearity2 / Echo_Count) > 0.6) OR
        (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
        ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
        (Mid_Range  < 8.50 AND Slope < 4.0) OR
        (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
        (Mid_Range > 14.00 AND Slope < 2.5)
      THEN DELETE;
    END;
    IF CHANNEL EQ 8 THEN DO;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -39.33) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
        (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.34)) OR
        ((Linearity2 / Echo_Count) >= 0.34) OR
        (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        (Slope >= 3.35 OR Slope <= -3.35)
      THEN DELETE;
    END;
  END;
IF SYSTEM='H' THEN DO;
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IF CHANNEL EQ  1 THEN DO; *downlooker;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -39.33) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
    ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
    ((Linearity2 / Echo_Count) > 0.6) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
    ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
    (Mid_Range  < 8.50 AND Slope < 4.0) OR
    (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
    (Mid_Range > 14.00 AND Slope < 2.5) OR
    (First_Range >= 5.56 AND Last_Range <= 5.85) OR
    (First_Range >= 13.62 AND Last_Range <= 13.88) OR
    (First_Range >=15.69 AND Last_Range <= 15.88)
      THEN DELETE;
END;
IF CHANNEL EQ 2 THEN DO;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -39.33) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
    (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.34)) OR
    ((Linearity2 / Echo_Count) >= 0.34) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    (Slope >= 3.35 OR Slope <= -3.35)
  THEN DELETE;
END;
IF CHANNEL EQ 3 THEN DO; *downlooker;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -39.33) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
    ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
    ((Linearity2 / Echo_Count) >= 0.6) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
    ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
    (Mid_Range  < 8.50 AND Slope < 4.0) OR
    (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
    (Mid_Range > 14.00 AND Slope < 2.5) OR
    (Echo_Count / ((Last_Ping / 2 + 1) - First_Ping / 2) < 0.7) OR
    (First_Range >= 13.70 AND Last_Range <= 13.88) OR
    (First_Range >= 14.71 AND Last_Range <= 14.93) OR
    (First_Range >= 15.40 AND Last_Range <= 15.78)
  THEN DELETE;
END;
IF CHANNEL EQ 4 THEN DO;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -39.33) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
    (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.34)) OR
    ((Linearity2 / Echo_Count) >= 0.34) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    (Slope >= 3.35 OR Slope <= -3.35)
  THEN DELETE;
END;
IF CHANNEL EQ 5 THEN DO; *downlooker;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -39.33) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
    ((Echo_Count >= 5 AND Echo_Count <= 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
    ((Linearity2 / Echo_Count) > 0.6) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
    ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
    (Mid_Range  < 8.50 AND Slope < 4.0) OR
    (Mid_Range >= 8.50 AND Mid_Range <=13.00 AND Slope < 2.7) OR
    (Mid_Range > 13.00 AND Slope < 2.5) OR

    (First_Range >= 13.53 AND Last_Range <= 13.78) OR
    (First_Range >= 15.03 AND Last_Range <= 15.15)
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      THEN DELETE;
    END;
    IF CHANNEL EQ 6 THEN DO;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -39.33) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
        (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.34)) OR
        ((Linearity2 / Echo_Count) >= 0.34) OR
        (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        (Slope >= 3.35 OR Slope <= -3.35)
      THEN DELETE;
    END;
    IF CHANNEL EQ 7 THEN DO; *downlooker;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -39.33) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
        ((Echo_Count >= 5 AND Echo_Count <= 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
        ((Linearity2 / Echo_Count) > 0.6) OR
        (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
        ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
        (Mid_Range  < 8.50 AND Slope < 4.0) OR
        (Mid_Range >= 8.50 AND Mid_Range <=13.00 AND Slope < 2.7) OR
        (Mid_Range > 13.00 AND Slope < 2.5) OR
        (First_Range >= 13.70 AND Last_Range <= 13.99)
      THEN DELETE;
    END;
    IF CHANNEL EQ 8 THEN DO;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -39.33) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
        (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.34)) OR
        ((Linearity2 / Echo_Count) >= 0.34) OR
        (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        (Slope >= 3.35 OR Slope <= -3.35)
      THEN DELETE;
    END;
  END;
IF SYSTEM='I' THEN DO;
  IF CHANNEL EQ 0 THEN DO; *downlooker;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -37) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
      ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
      ((Linearity2 / Echo_Count) >= 0.6) OR
      (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
      ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
      ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
      (Mid_Range  < 8.50 AND Slope < 4.0) OR
      (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
      (Mid_Range > 14.00 AND Slope < 2.5) OR
      (First_Range >= 14.35 AND First_Range <= 14.65) AND (Last_Range >= 14.35 AND Last_Range <= 14.65) OR
      (First_Range >= 14.90 AND First_Range <= 15.25) AND (Last_Range >= 14.90 AND Last_Range <= 15.25)
    THEN DELETE;
  END;
  IF CHANNEL EQ 10 THEN DO;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -37) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
      (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.34)) OR
      ((Linearity2 / Echo_Count) >= 0.34) OR
      (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
      (Slope >= 3.35 OR Slope <= -3.35) OR
      (First_Range > 5.00 AND First_Range <= 5.80) AND  (Last_Range > 5.00 AND Last_Range <= 5.80) OR
      (First_Range > 8.80 AND First_Range < 8.90) AND  (Last_Range > 8.80 AND Last_Range < 8.90) OR
      (First_Range > 8.85 AND First_Range < 9.25) AND (Last_Range > 8.85 AND Last_Range < 9.25)
    THEN DELETE;
  END;
END;
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IF SYSTEM='O' THEN DO; *downlooker;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength > -37) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
    ((Echo_Count >= 5 AND Echo_Count <= 6) AND ((Linearity1 / Echo_Count) > 0.5)) OR
    (Linearity2 > 4) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    ((((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.05) AND (Mid_Range > 2.40 AND Mid_Range < 8.50)) OR
    ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
    ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
    (Mid_Range < 2.400) OR
    (Mid_Range >=2.40 AND Mid_Range <=8.00 AND Slope < 1.5) OR
    (Mid_Range > 10.20)
  THEN DELETE;
END;

IF SYSTEM='P' THEN DO; *downlooker;
  IF CHANNEL EQ 1 THEN DO; *closed ;
  END;
  IF CHANNEL EQ 2 THEN DO;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -39.33) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
      ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >=0.5)) OR
      (Linearity2 > 4) OR
      (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
      ((((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.05) AND (Mid_Range >2.40 AND Mid_Range < 8.50)) OR
      ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
      ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
      (Mid_Range  < 2.400) OR
      (Mid_Range >=2.40 AND Mid_Range <=8.00 AND Slope < 1.5) OR
      (Mid_Range > 9.60)
    THEN DELETE;
  END;
  IF CHANNEL EQ 3 THEN DO;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -39.33) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
      ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >=0.5)) OR
      (Linearity2 > 4) OR
      (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
      ((((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.05) AND (Mid_Range > 2.40 AND Mid_Range < 8.50)) OR
      ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.50) OR
      ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.50) OR
      (Mid_Range < 2.400) OR
      (Mid_Range >= 2.40 AND Mid_Range <=8.00 AND Slope < 1.5) OR
      (Mid_Range > 10.35) OR
      (Echo_Count < 7)
    THEN DELETE;
  END;
  IF CHANNEL EQ 4 THEN DO;*closed ;
  END;
  IF CHANNEL EQ 5 THEN DO;*closed ;
  END;
END;

IF SYSTEM='Q' THEN DO; *downlooker;
  IF CHANNEL EQ 1 THEN DO;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -39.33) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
      ((Echo_Count >= 5 AND Echo_Count <= 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
      (Linearity2 > 4) OR
      (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
      ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
      ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
      (Mid_Range < 2.400) OR
      (Mid_Range >=2.40 AND Mid_Range <=8.00 AND Slope < 1.5) OR
      (Mid_Range > 10.80) OR
      ((First_Range >= 4.05 AND First_Range <= 4.35) AND (Last_Range >= 4.05 AND Last_Range <= 4.35)) OR
```

```
          ((First_Range >= 4.15 AND First_Range <= 4.60) AND (Last_Range >= 4.15 AND Last_Range <= 4.60)) OR
          ((First_Range >= 9.20 AND First_Range <= 9.45) AND (Last_Range >= 9.20 AND Last_Range <= 9.45)) OR
          ((First_Range >= 9.40 AND First_Range <= 9.65) AND (Last_Range >= 9.40 AND Last_Range <= 9.65)) OR
          ((First_Range >= 9.60 AND First_Range <= 9.90) AND (Last_Range >= 9.60 AND Last_Range <= 9.90)) OR
          ((First_Range >= 9.75 AND First_Range <= 9.95) AND (Last_Range >= 9.75 AND Last_Range <= 9.95))
       THEN DELETE;
    END;
   IF CHANNEL EQ 2 THEN DO;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
         (Mean_Target_Strength  > -39.33) OR
         (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
         ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
         (Linearity2 > 4) OR
         ((Noise_Count_Average / ((Echo_Count + 10) * 5)) > 0.04) OR
         ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.50) OR
         ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.50) OR
         (Mid_Range < 2.400) OR
         (Mid_Range >=2.40 AND Mid_Range <=8.00 AND Slope < 1.5) OR
         (Mid_Range > 9.75) OR
         ((First_Range >= 4.30 AND First_Range <= 5.65) AND (Last_Range >= 4.30 And Last_Range <= 5.65)) OR
         ((First_Range >= 6.00 AND First_Range <= 6.40) AND (Last_Range >= 6.00 And Last_Range <= 6.40)) OR
         ((First_Range >= 8.05 AND First_Range <= 8.25) AND (Last_Range >= 8.05 And Last_Range <= 8.25)) OR
         ((First_Range >= 8.35 AND First_Range <= 8.55) AND (Last_Range >= 8.35 And Last_Range <= 8.55)) OR
         ((First_Range >= 9.25 AND First_Range <= 9.45) AND (Last_Range >= 9.25 And Last_Range <= 9.45)) OR
         (Echo_Count < 7)
       THEN DELETE;
    END;
   IF CHANNEL EQ 3 THEN DO; *closed ;
    END;
   IF CHANNEL EQ 4 THEN DO;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
         (Mean_Target_Strength  > -39.33) OR
         (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
         ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
         (Linearity2 > 4) OR
         ((Noise_Count_Average / ((Echo_Count + 10) * 5)) > 0.045) OR
         ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
         ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
         (Mid_Range < 2.400) OR
         (Mid_Range >=2.40 AND Mid_Range <=8.00 AND Slope < 1.5) OR
         (Mid_Range > 10.20)
       THEN DELETE;
    END;
   IF CHANNEL EQ 5 THEN DO; *closed ;
    END;
 END;
IF SYSTEM='R' THEN DO; *downlooker;
   IF ((Noise_Count_Average / ((Echo_Count + 10) * 5)) > 0.04) THEN DELETE;
   IF Mean_Target_Strength  > -39.33 THEN DELETE;
   IF NUM_PING GT 60 THEN DELETE;
   IF CHANNEL EQ 0 THEN DO;
     IF Slope GT -1 AND Slope LT 1 THEN DELETE;
    END;
   IF CHANNEL EQ 1 THEN DO;
     IF Slope GT -1 AND Slope LT 1 THEN DELETE;
     IF Mid_Range GT 24.5 THEN DELETE;
    END;
   IF CHANNEL EQ 2 THEN DO;
     IF Slope GT -0.05 AND Slope LT 0.05 THEN DELETE;
    END;
 END;

IF SYSTEM='X' THEN DO;
   IF CHANNEL EQ 0 THEN DO; *uplooker;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
         (Mean_Target_Strength  > -37) OR
         (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
         (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
         ((Linearity2 / Echo_Count) >= 0.3) OR
         (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
```

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```
        (Slope >= 3.35 OR Slope <= -3.35) OR
        (Mid_Range >= 13.55)
    THEN DELETE;
END;
IF CHANNEL EQ 1 THEN DO; *downlooker;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -37) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
        ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
        ((Linearity2 / Echo_Count) > 0.45) OR
        ((((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045)) OR
        ((Slope > 11.5 OR Slope < -11.5) AND Mid_Range <= 8.5) OR
        ((Slope > 10.5 OR Slope < -10.5) AND Mid_Range >  8.5) OR
        (Mid_Range  < 10.60 AND Slope < 3.0) OR
        (Mid_Range >= 10.60 AND Mid_Range <= 17.50 AND Slope < 2.0) OR
        (Mid_Range > 17.50 AND Mid_Range < 19.00 AND Slope < 1.5) OR
        (Mid_Range >= 19.00 AND Slope <= 0) OR
        (First_Range >=10.57 And First_Range <= 10.81 And Last_Range >= 10.57 AND Last_Range <= 10.81)
    THEN DELETE;
```

Appendix D-3. Statistical Analysis System Code for Filtering Out Echo Traces that Did Not Meet Fish Trace Criteria in Summer 2001. Minimum ranges for sampling guided, unguided, and spilled fish, which are presented in legends of Figures 1-4, were implemented elsewhere in the processing program.

```
***Call a fish a fish;
IF (First_Ping NE . AND First_Range NE .) THEN FISH=1;
***Enter channel specific structural, trace quality, target or echo strength, and noise filters to eliminate bad tracks;
IF SYSTEM='A' THEN DO; ***Ready for 2001;
  IF CHANNEL EQ 0 THEN DO; *Uplooker aimed about 29 degrees downstream of vertical;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -49.2) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
      (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.25)) OR
      ((Linearity2 / Echo_Count) >= 0.25) OR
      (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
      (Slope >= 3.35 OR Slope <= -3.35)
    THEN DELETE;
  END;
  IF CHANNEL EQ 1 THEN DO; *Downlooker aimed 9 degrees downstream of vertical;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -45.1) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
      ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
      ((Linearity2 / Echo_Count) > 0.45) OR
      (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
      ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
      ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
      (Mid_Range  < 10.60 AND Slope < 3.0) OR
      (Mid_Range >= 10.60 AND Mid_Range <= 17.50 AND Slope < 2.0) OR
      (Mid_Range > 17.50 AND Mid_Range < 19.00 AND Slope < 1.5) OR
      (Mid_Range >= 19.00 AND Slope <= 0)
    THEN DELETE;
  END;
END;

IF SYSTEM='C' THEN DO; ***Ready for 2001;
  IF CHANNEL EQ 1 THEN DO; ***B slot; *Downlooker aimed 9 degrees downstream of vertical;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -47.4) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
      ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
      ((Linearity2 / Echo_Count) > 0.45) OR
      (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
      ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
      ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
      (Mid_Range  < 10.60 AND Slope < 3.0) OR
      (Mid_Range >= 10.60 AND Mid_Range <=17.50 AND Slope < 2.0) OR
      (Mid_Range > 17.50 AND Mid_Range < 19.00 and Slope < 1.5) OR
      (Mid_Range >= 19.00 AND Slope <= 0)
    THEN DELETE;
  END;
  IF CHANNEL EQ 2 THEN DO; ***B slot; *Uplooker aimed about 29 degrees downstream of vertical;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -51.5) OR
      (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
      (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.25)) OR
      ((Linearity2 / Echo_Count) >= 0.25) OR
      (Slope >= 3.35 OR Slope <= -3.35) OR
      (Mid_Range >= 13.50)
    THEN DELETE;
  END;
  IF CHANNEL EQ 3 THEN DO; ***A slot; *Downlooker aimed 9 degrees downstream of vertical;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -47.4) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
      ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
      ((Linearity2 / Echo_Count) > 0.45) OR
```

```
                (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
                ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
                ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
                (Mid_Range  < 10.60 AND Slope < 3.0) OR
                (Mid_Range >= 10.60 AND Mid_Range <=17.50 AND Slope < 2.0) OR
                (Mid_Range > 17.50 AND Mid_Range < 19.00 and Slope < 1.5) OR
                (Mid_Range >= 19.00 AND Slope <= 0)
         THEN DELETE;
   END;
   IF CHANNEL EQ 4 THEN DO; ***A slot; *Uplooker aimed about 29 degrees downstream of vertical;
      IF ((((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
             (Mean_Target_Strength  > -51.5) OR
             (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
             (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
             (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.25)) OR
             ((Linearity2 / Echo_Count) >= 0.25) OR
             (Slope >= 3.35 OR Slope <= -3.35) OR
             (Mid_Range >= 13.50)
         THEN DELETE;
   END;
   IF CHANNEL EQ 5 THEN DO; ***C slot; *Downlooker aimed 9 degrees downstream of vertical;
      IF ((((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
              (Mean_Target_Strength  > -47.4) OR
             (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
             ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
             ((Linearity2 / Echo_Count) > 0.45) OR
             (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
             ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
             ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
             (Mid_Range  < 10.60 AND Slope < 3.0) OR
             (Mid_Range >= 10.60 AND Mid_Range <=17.50 AND Slope < 2.0) OR
             (Mid_Range > 17.50 AND Mid_Range < 19.00 and Slope < 1.5) OR
             (Mid_Range >= 19.00 AND Slope <= 0)
         THEN DELETE;
   END;
   IF CHANNEL EQ 6 THEN DO; ***C slot; *Uplooker aimed about 29 degrees downstream of vertical;
      IF ((((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
             (Mean_Target_Strength  > -51.5) OR
             (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
             (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
             (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.25)) OR
             ((Linearity2 / Echo_Count) >= 0.25) OR
             (Slope >= 3.35 OR Slope <= -3.35) OR
             (Mid_Range >= 13.50)
         THEN DELETE;
   END;
   IF CHANNEL EQ 7 THEN DO; ***A slot; *Downlooker aimed 9 degrees downstream of vertical;
      IF ((((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
              (Mean_Target_Strength  > -47.4) OR
             (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
             ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
             ((Linearity2 / Echo_Count) > 0.45) OR
             (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
             ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
             ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
             (Mid_Range  < 10.60 AND Slope < 3.0) OR
             (Mid_Range >= 10.60 AND Mid_Range <=17.50 AND Slope < 2.0) OR
             (Mid_Range > 17.50 AND Mid_Range < 19.00 and Slope < 1.5) OR
             (Mid_Range >= 19.00 AND Slope <= 0)
         THEN DELETE;
   END;
   IF CHANNEL EQ 8 THEN DO; ***A slot; *Uplooker aimed about 29 degrees downstream of vertical;
      IF ((((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
             (Mean_Target_Strength  > -51.5) OR
             (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
             (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
             (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.25)) OR
             ((Linearity2 / Echo_Count) >= 0.25) OR
             (Slope >= 3.35 OR Slope <= -3.35) OR
             (Mid_Range >= 13.50)
```

```
        THEN DELETE;
      END;
    END;

    IF SYSTEM='D' THEN DO; ***Ready for 2001;
      IF CHANNEL EQ 1 THEN DO; *Downlooker aimed 9 degrees downstream of vertical;
        IF ((((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -47.4) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
          ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
          ((Linearity2 / Echo_Count) > 0.45) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
          ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
          (Mid_Range  < 10.60 AND Slope < 3.0) OR
          (Mid_Range >= 10.60 AND Mid_Range <= 17.50 AND Slope < 2.0) OR
          (Mid_Range > 17.50 AND Mid_Range < 19.00 AND Slope < 1.5) OR
          (Mid_Range >= 19.00 AND Slope <= 0) OR
          (First_Range >= 18.60 AND First_Range <= 18.80 AND Last_Range >= 18.60 AND Last_Range <= 18.80)
        THEN DELETE;
      END;
      IF CHANNEL EQ 2 THEN DO; *Uplooker aimed about 29 degrees downstream of vertical;
        IF ((((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -51.5) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
          (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.25)) OR
          ((Linearity2 / Echo_Count) >= 0.25) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          (Slope >= 3.35 OR Slope <= -3.35)
        THEN DELETE;
      END;
      IF CHANNEL EQ 3 THEN DO; *Downlooker aimed 9 degrees downstream of vertical;
        IF ((((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -47.4) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
          ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
          ((Linearity2 / Echo_Count) > 0.45) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
          ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
          (Mid_Range  < 10.60 AND Slope < 3.0) OR
          (Mid_Range >= 10.60 AND Mid_Range <=17.50 AND Slope < 2.0) OR
          (Mid_Range > 17.50 AND Mid_Range < 19.00 AND Slope < 1.5) OR
          (Mid_Range >= 19.00 AND Slope <= 0) OR
          (Mid_Range > 16.30 AND Echo_Count/((Last_Ping / 2 + 1) - First_Ping / 2) < 1.1) AND (Echo_Count >= 10 AND
((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          (First_Range >= 19.50)
        THEN DELETE;
      END;
      IF CHANNEL EQ 4 THEN DO; *Uplooker aimed about 29 degrees downstream of vertical;
        IF ((((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -51.5) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
          (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.25)) OR
          ((Linearity2 / Echo_Count) >= 0.25) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          (Slope >= 3.35 OR Slope <= -3.35)
        THEN DELETE;
      END;
      IF CHANNEL EQ 5 THEN DO; *Uplooker aimed about 32 degrees downstream of vertical;
        IF ((((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -51.5) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
          (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.25)) OR
          ((Linearity2 / Echo_Count) >= 0.25) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          (Slope >= 3.35 OR Slope <= -3.35) OR
          (Mid_Range > 12.20 And Slope > -0.25 AND Slope < 0.25)
        THEN DELETE;
      END;
```

```
IF CHANNEL EQ 6 THEN DO; *Downlooker aimed about 25 degrees upstream of vertical;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -47.4) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
    (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.25)) OR
    ((Linearity2 / Echo_Count) >= 0.25) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    (Slope >= 5 OR Slope <= -5) OR
    ((Mid_Range >= 11.35) AND (SLOPE > -1 OR SLOPE < 1)) OR
    (First_Range >= 11.30 And First_Range <= 11.70 AND Last_Range >= 11.30 AND Last_Range <= 11.70) OR
    (First_Range >= 12.00 And First_Range <= 12.20 AND Last_Range >= 12.00 AND Last_Range <= 12.20)
  THEN DELETE;
END;
IF CHANNEL EQ 7 THEN DO; *Downlooker aimed 9 degrees downstream of vertical;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -47.4) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
    ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
    ((Linearity2 / Echo_Count) > 0.45) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
    ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
    (Mid_Range  < 10.60 AND Slope < 3.0) OR
    (Mid_Range >= 10.60 AND Mid_Range <=17.50 AND Slope < 2.0) OR
    (Mid_Range > 17.50 AND Mid_Range < 19.00 AND Slope < 1.5) OR
    (Mid_Range >= 19.00 AND Slope <= 0) OR
    (First_Range >= 12.75 AND First_Range <= 12.90 AND Last_Range >= 12.75 AND Last_Range <= 12.90) OR
    (First_Range >= 14.70 AND First_Range <= 14.85 AND Last_Range >= 14.70 AND Last_Range <= 14.85) OR
    (First_Range >= 18.15 AND First_Range <= 18.35 AND Last_Range >= 18.15 AND Last_Range <= 18.35)
  THEN DELETE;
END;
IF CHANNEL EQ 8 THEN DO; *Uplooker aimed about 29 degrees downstream of vertical;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -51.5) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
    (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.25)) OR
    ((Linearity2 / Echo_Count) >= 0.25) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    (Slope >= 3.35 OR Slope <= - 3.35) OR
    (Mid_Range > 13.30 AND ((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.03) OR
    (First_Range >=12.60 And First_Range <= 12.90 And Last_Range >= 12.60 AND Last_Range <= 12.90) OR
    (First_Range >=12.08 And First_Range <= 12.44 And Last_Range >= 12.08 AND Last_Range <= 12.44)
  THEN DELETE;
END;
END;

IF SYSTEM='G' THEN DO; ***Ready for 2001;
  IF CHANNEL EQ 1 THEN DO; *Downlooker aimed 9 degrees downstream of vertical;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -47.4) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
      ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
      ((Linearity2 / Echo_Count) > 0.6) OR
      (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
      ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
      ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
      (Mid_Range  < 8.50 AND Slope < 4.0) OR
      (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
      (Mid_Range > 14.00 AND Slope < 2.5)
    THEN DELETE;
  END;
  IF CHANNEL EQ 2 THEN DO; *Uplooker aimed about 36 degrees downstream of vertical;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -51.5) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
      (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
      ((Linearity2 / Echo_Count) >= 0.3) OR
      (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
      (Slope >= 3.35 OR Slope <= -3.35)
    THEN DELETE;
```

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END;
IF CHANNEL EQ 3 THEN DO; *Downlooker aimed about 9 degrees downstream of vertical;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -47.4) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
    ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
    ((Linearity2 / Echo_Count) > 0.6) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
    ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
    (Mid_Range  < 8.50 AND Slope < 4.0) OR
    (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
    (Mid_Range > 14.00 AND Slope < 2.5) OR
    (First_Range >=5.3 And First_Range <= 6.0 And Last_Range >= 5.3 AND Last_Range <= 6.0)
  THEN DELETE;
END;
IF CHANNEL EQ 4 THEN DO; *Uplooker aimed about 36 degrees downstream of vertical;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -51.5) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
    (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
    ((Linearity2 / Echo_Count) >= 0.3) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    (Slope >= 3.35 OR Slope <= -3.35)
  THEN DELETE;
END;
IF CHANNEL EQ 5 THEN DO; *Downlooker aimed about 9 degrees downstream of vertical;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -47.4) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
    ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
    ((Linearity2 / Echo_Count) > 0.6) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
    ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
    (Mid_Range  < 8.50 AND Slope < 4.0) OR
    (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
    (Mid_Range > 14.00 AND Slope < 2.5)
  THEN DELETE;
END;
IF CHANNEL EQ 6 THEN DO; *Uplooker aimed about 36 degrees downstream of vertical;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -51.5) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
    (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
    ((Linearity2 / Echo_Count) >= 0.3) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    (Slope >= 3.35 OR Slope <= -3.35)
  THEN DELETE;
END;
IF CHANNEL EQ 7 THEN DO; *Downlooker aimed about 9 degrees downstream of vertical;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -47.4) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
    ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
    ((Linearity2 / Echo_Count) > 0.6) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
    ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
    (Mid_Range  < 8.50 AND Slope < 4.0) OR
    (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
    (Mid_Range > 14.00 AND Slope < 2.5)
  THEN DELETE;
END;
IF CHANNEL EQ 8 THEN DO; *Uplooker aimed about 36 degrees downstream of vertical;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength  > -51.5) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
    (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
    ((Linearity2 / Echo_Count) >= 0.3) OR
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              (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
              (Slope >= 3.35 OR Slope <= -3.35)
          THEN DELETE;
      END;
  END;
IF SYSTEM='H' THEN DO; *Ready for 2001;
   IF CHANNEL EQ  1 THEN DO; *Downlooker aimed about 9 degrees downstream of vertical;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -47.4) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
          ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
          ((Linearity2 / Echo_Count) > 0.6) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
          ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
          (Mid_Range  < 8.50 AND Slope < 4.0) OR
          (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
          (Mid_Range > 14.00 AND Slope < 2.5) OR
          (First_Range >= 5.56 AND Last_Range <= 5.85) OR
          (First_Range >= 13.62 AND Last_Range <= 13.88) OR
          (First_Range >=15.69 AND Last_Range <= 15.88)
      THEN DELETE;
   END;
   IF CHANNEL EQ 2 THEN DO; *Uplooker aimed about 36 degrees downstream of vertical;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -51.5) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
          (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
          ((Linearity2 / Echo_Count) >= 0.3) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          (Slope >= 3.35 OR Slope <= -3.35)
      THEN DELETE;
   END;
   IF CHANNEL EQ 3 THEN DO; *Downlooker aimed about 9 degrees downstream of vertical;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -47.4) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
          ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
          ((Linearity2 / Echo_Count) >= 0.6) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
          ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
          (Mid_Range  < 8.50 AND Slope < 4.0) OR
          (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
          (Mid_Range > 14.00 AND Slope < 2.5) OR
          (Echo_Count / ((Last_Ping / 2 + 1) - First_Ping / 2) < 0.7) OR
          (First_Range >= 13.70 AND Last_Range <= 13.88) OR
          (First_Range >= 14.71 AND Last_Range <= 14.93) OR
          (First_Range >= 15.40 AND Last_Range <= 15.78)
      THEN DELETE;
   END;
   IF CHANNEL EQ 4 THEN DO; *Uplooker aimed about 36 degrees downstream of vertical;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -51.5) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
          (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
          ((Linearity2 / Echo_Count) >= 0.3) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          (Slope >= 3.35 OR Slope <= -3.35)
      THEN DELETE;
   END;
   IF CHANNEL EQ 5 THEN DO; *Downlooker aimed about 9 degrees downstream of vertical;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
          (Mean_Target_Strength  > -47.4) OR
          (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
          ((Echo_Count >= 5 AND Echo_Count <= 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
          ((Linearity2 / Echo_Count) > 0.6) OR
          (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
          ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
          ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
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                (Mid_Range  < 8.50 AND Slope < 4.0) OR
                (Mid_Range >= 8.50 AND Mid_Range <=13.00 AND Slope < 2.7) OR
                (Mid_Range > 13.00 AND Slope < 2.5) OR
                (First_Range >= 13.53 AND Last_Range <= 13.78) OR
                (First_Range >= 15.03 AND Last_Range <= 15.15)
           THEN DELETE;
        END;
        IF CHANNEL EQ 6 THEN DO; *Uplooker aimed about 36 degrees downstream of vertical;
             IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
                (Mean_Target_Strength  > -51.5) OR
                (Mean_Target_Strength  > -52.6 AND Echo_Count > 6) OR
                (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
                (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
                ((Linearity2 / Echo_Count) >= 0.3) OR
                (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
                (Slope >= 3.35 OR Slope <= -3.35)
           THEN DELETE;
        END;
        IF CHANNEL EQ 7 THEN DO; *Downlooker aimed about 9 degrees downstream of vertical;
          IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
                (Mean_Target_Strength  > -47.4) OR
                (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
                ((Echo_Count >= 5 AND Echo_Count <= 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
                ((Linearity2 / Echo_Count) > 0.6) OR
                (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
                ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
                ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
                (Mid_Range  < 8.50 AND Slope < 4.0) OR
                (Mid_Range >= 8.50 AND Mid_Range <=13.00 AND Slope < 2.7) OR
                (Mid_Range > 13.00 AND Slope < 2.5) OR
                (First_Range >= 13.70 AND Last_Range <= 13.99)
           THEN DELETE;
        END;
        IF CHANNEL EQ 8 THEN DO; *Uplooker aimed about 36 degrees downstream of vertical;
          IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
                (Mean_Target_Strength  > -51.5) OR
                (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
                (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
                ((Linearity2 / Echo_Count) >= 0.3) OR
                (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
                (Slope >= 3.35 OR Slope <= -3.35)
           THEN DELETE;
        END;
    END;

    IF SYSTEM='I' THEN DO; *Ready for 2001;
      IF CHANNEL EQ 0 THEN DO; *Downlooker aimed about 9 degrees downstream of vertical;
        IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
                (Mean_Target_Strength  > -45.1) OR
                (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
                ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.6)) OR
                ((Linearity2 / Echo_Count) > 0.6) OR
                (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
                ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
                ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
                (Mid_Range  < 8.50 AND Slope < 4.0) OR
                (Mid_Range >= 8.50 AND Mid_Range <=14.00 AND Slope < 2.7) OR
                (Mid_Range > 14.00 AND Slope < 2.5) OR
                (First_Range >= 14.35 AND First_Range <= 14.65) AND (Last_Range >= 14.35 AND Last_Range <= 14.65) OR
                (First_Range >= 14.90 AND First_Range <= 15.25) AND (Last_Range >= 14.90 AND Last_Range <= 15.25)
           THEN DELETE;
        END;
      IF CHANNEL EQ 10 THEN DO; *Uplooker aimed about 36 degrees downstream of vertical;
        IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
                (Mean_Target_Strength  > -49.2) OR
                (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
                (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.3)) OR
                ((Linearity2 / Echo_Count) >= 0.3) OR
                (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
                (Slope >= 3.35 OR Slope <= -3.35) OR
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        (First_Range > 5.00 AND First_Range <= 5.80) AND  (Last_Range > 5.00 AND Last_Range <= 5.80) OR
        (First_Range > 8.80 AND First_Range < 8.90) AND  (Last_Range > 8.80 AND Last_Range < 8.90) OR
        (First_Range > 8.85 AND First_Range < 9.25) AND (Last_Range > 8.85 AND Last_Range < 9.25)
      THEN DELETE;
    END;
END;

*Ready for 2001;
IF SYSTEM='O' THEN DO; *Downlooker aimed about 15 degrees upstream of vertical;
  IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
    (Mean_Target_Strength > -45.1) OR
    (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
    ((Echo_Count >= 5 AND Echo_Count <= 6) AND ((Linearity1 / Echo_Count) > 0.5)) OR
    (Linearity2 > 4) OR
    (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
    ((((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.05) AND (Mid_Range > 2.40 AND Mid_Range < 8.50)) OR
    ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
    ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
    (Mid_Range < 2.400) OR
    (Mid_Range >=2.40 AND Mid_Range <=8.00 AND Slope < 1.5) OR
    (Mid_Range > 10.20)
  THEN DELETE;
END;

*Ready for 2001;
IF SYSTEM='P' THEN DO; *Downlookers aimed about 8 degrees upstream of vertical;
  IF CHANNEL EQ 1 THEN DO; *closed ;
  END;
  IF CHANNEL EQ 2 THEN DO;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -47.4) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
      ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >=0.5)) OR
      (Linearity2 > 4) OR
      (((Noise_Count_Average) / ((Echo_Count + 10) * 5) > 0.045) OR
      ((((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.05) AND (Mid_Range >2.40 AND Mid_Range < 8.50)) OR
      ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
      ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
      (Mid_Range  < 2.400) OR
      (Mid_Range >=2.40 AND Mid_Range <=8.00 AND Slope < 1.5) OR
      (Mid_Range > 9.60)
    THEN DELETE;
  END;
  IF CHANNEL EQ 3 THEN DO;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -47.4) OR
      (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
      ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >=0.5)) OR
      (Linearity2 > 4) OR
      (((Noise_Count_Average) / ((Echo_Count + 10) * 5) > 0.045) OR
      ((((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.05) AND (Mid_Range > 2.40 AND Mid_Range < 8.50)) OR
      ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.50) OR
      ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.50) OR
      (Mid_Range < 2.400) OR
      (Mid_Range >= 2.40 AND Mid_Range <=8.00 AND Slope < 1.5) OR
      (Mid_Range > 10.35) OR
      (Echo_Count < 7)
    THEN DELETE;
  END;
  IF CHANNEL EQ 4 THEN DO;*closed ;
  END;
  IF CHANNEL EQ 5 THEN DO;*closed ;
  END;
END;

*Ready for 2001;
IF SYSTEM='Q' THEN DO; *Downlookers aimed about 8 degrees upstream of vertical;
  IF CHANNEL EQ 1 THEN DO;
    IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
      (Mean_Target_Strength  > -47.4) OR
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                (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
                ((Echo_Count >= 5 Echo_Count <= 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
                (Linearity2 > 4) OR
                (((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
                ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
                ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE > 8.5) OR
                (Mid_Range < 2.400) OR
                (Mid_Range >=2.40 AND Mid_Range <=8.00 AND Slope < 1.5) OR
                (Mid_Range > 10.80) OR
                ((First_Range >= 4.05 AND First_Range <= 4.35) AND (Last_Range >= 4.05 AND Last_Range <= 4.35))   OR
                ((First_Range >= 4.15 AND First_Range <= 4.60) AND (Last_Range >= 4.15 AND Last_Range <= 4.60))   OR
                ((First_Range >= 9.00 AND First_Range <= 9.35) AND (Last_Range >= 9.00 AND Last_Range <= 9.35)) OR
                ((First_Range >= 9.40 AND First_Range <= 9.65) AND (Last_Range >= 9.40 AND Last_Range <= 9.65))


        THEN DELETE;
    END;
    IF CHANNEL EQ 2 THEN DO;
        IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
            (Mean_Target_Strength  > -47.4) OR
            (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
            ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
            (Linearity2 > 4) OR
            ((Noise_Count_Average / ((Echo_Count + 10) * 5)) > 0.045) OR
            ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.50) OR
            ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.50) OR
            (Mid_Range < 2.400) OR
            (Mid_Range >=2.40 AND Mid_Range <=8.00 AND Slope < 1.5) OR
            ((First_Range >= 4.30 AND First_Range <= 5.65) AND (Last_Range >= 4.30 And Last_Range <= 5.65)) OR
            ((First_Range >= 6.00 AND First_Range <= 6.40) AND (Last_Range >= 6.00 And Last_Range <= 6.40)) OR
            ((First_Range >= 8.05 AND First_Range <= 8.25) AND (Last_Range >= 8.05 And Last_Range <= 8.25)) OR
            ((First_Range >= 8.35 AND First_Range <= 8.55) AND (Last_Range >= 8.35 And Last_Range <= 8.55)) OR
            ((First_Range >= 9.25 AND First_Range <= 9.45) AND (Last_Range >= 9.25 And Last_Range <= 9.45)) OR
            (Mid_Range > 9.75) OR
            (Echo_Count < 7)
        THEN DELETE;
    END;
    IF CHANNEL EQ 3 THEN DO; *closed ;
    END;
    IF CHANNEL EQ 4 THEN DO;
        IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
            (Mean_Target_Strength  > -47.4) OR
            (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
            ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
            (Linearity2 > 4) OR
            ((Noise_Count_Average / ((Echo_Count + 10) * 5)) > 0.045) OR
            ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
            ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
            (Mid_Range < 2.400) OR
            (Mid_Range >=2.40 AND Mid_Range <=8.00 AND Slope < 1.5) OR
            (Mid_Range > 10.20)
        THEN DELETE;
    END;
    IF CHANNEL EQ 5 THEN DO; *closed ;
    END;
END;

IF SYSTEM='R' THEN DO;
    IF ((Noise_Count_Average / ((Echo_Count + 10) * 5)) > 0.045) THEN DELETE;
    IF MEAN_TARGET_STRENGTH GT -45.1 THEN DELETE;
    IF NUM_PING GT 60 THEN DELETE;
    IF CHANNEL EQ 0 THEN DO; *Downlooker aimed about 6 degrees upstream of trash racks;
        IF SLOPE GT -1 AND SLOPE LT 1 THEN DELETE;
    END;
    IF CHANNEL EQ 1 THEN DO; *Downlooker aimed about 12 degrees upstream of trash racks;
        IF SLOPE GT -1 AND SLOPE LT 1 THEN DELETE;
        IF Mid_Range GT 24.5 THEN DELETE;
    END;
    IF CHANNEL EQ 2 THEN DO; *Downlooker aimed about 18 degrees upstream of trash racks;
        IF SLOPE GT -0.05 AND SLOPE LT 0.05 THEN DELETE;
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    END;
  END;

  *Ready for 2001;
  IF SYSTEM='X' THEN DO;
    OAx=2057; *These are the average values for the two transducers.
         *Both transducers lost phase information, so something was lost from the sounder.;
    OAy=2054;
    OBx=2063;
    OBy=2053;
    SAx=279.5;
    SAy=278;
    SBx=-119950;
    SBy=-122150;
    BPF2y=((SAy*((YANGLE1+YANGLE2)/2)+OAy-OBy)**2)/-SBy;
    BPF2x=((SAx*((XANGLE1+XANGLE2)/2)+OAx-OBx)**2)/-SBx;
    BPF2 =(BPF2y**2+BPF2x**2)**0.5;
    Mean_Target_Strength=Mean_Target_Strength-BPF2;
    IF CHANNEL EQ 0 THEN DO; *Uplooker aimed about 29 degrees downstream of vertical;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -51.5) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.25)) OR
        (Echo_Count = 5 AND ((Linearity1 / Echo_Count) >= 0.25)) OR
        ((Linearity2 / Echo_Count) >= 0.25) OR
        ((((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045) OR
        (Slope >= 3.35 OR Slope <= -3.35) OR
        (Mid_Range >= 13.55)
      THEN DELETE;
    END;
    IF CHANNEL EQ 1 THEN DO; *Downlooker aimed 9 degrees downstream of vertical;
      IF (((Last_Ping / Group_Size + 1) - First_Ping / Group_Size) > 60) OR
        (Mean_Target_Strength  > -47.4) OR
        (Echo_Count = 4 AND ((Linearity1 / Echo_Count) > 0.4)) OR
        ((Echo_Count = 5 OR Echo_Count = 6) AND ((Linearity1 / Echo_Count) >= 0.5)) OR
        ((Linearity2 / Echo_Count) > 0.45) OR
        (((((Noise_Count_Average) / ((Echo_Count + 10) * 5)) > 0.045)) OR
        ((Slope > 11.5 OR Slope < -11.5) AND MID_RANGE <= 8.5) OR
        ((SLOPE > 10.5 OR SLOPE < -10.5) AND MID_RANGE >  8.5) OR
        (Mid_Range  < 10.60 AND Slope < 3.0) OR
        (Mid_Range >= 10.60 AND Mid_Range <= 17.50 AND Slope < 2.0) OR
        (Mid_Range > 17.50 AND Mid_Range < 19.00 AND Slope < 1.5) OR
        (Mid_Range >= 19.00 AND Slope <= 0) OR
        (First_Range >=10.57 And First_Range <= 10.81 And Last_Range >= 10.57 AND Last_Range <= 10.81)
      THEN DELETE;
    END;
  END;
  OUTPUT TRACKED;
END;
RUN;
```

D.22

Appendix E

List of Appendix E Tables and Definitions of Variables in Headings of Hourly Fish Passage, Flow, and Forebay Elevation Data on an Accompanying Disk

Appendix E

List of Appendix E Tables

Appendix E-1. List of Appendix Tables on the Accompanying Disk

Table	Description
Appendix E-1	List of Appendix E Tables on an Accompanying Disk
Appendix E-2	Definitions of variables in headings of Appendix E tables on the accompanying disk.
Appendix E-3	Hourly estimates of fish passage (sums, variances, and covariances), unit discharge, and forebay elevation for Powerhouse 1 in spring 2001.
Appendix E-4	Hourly estimates of fish passage (sums, variances, and covariances), unit discharge, and forebay elevation for Powerhouse 1 in summer 2001.
Appendix E-5	Hourly estimates of fish passage (sums and variances) and spill-bay discharge for the spillway in spring 2001.
Appendix E-6	Hourly estimates of fish passage (sums and variances) and spill-bay discharge for the spillway in summer 2001.
Appendix E-7	Hourly estimates of fish passage (sums, variances, and covariances), unit discharge, and forebay elevation for Powerhouse 2 in spring 2001.
Appendix E-8	Hourly estimates of fish passage (sums, variances, and covariances), unit discharge, and forebay elevation for Powerhouse 2 in summer 2001.

Appendix E-2. Definitions of Variables in Headings of Appendix E Tables on the Accompanying Disk

Variable	Definition
Begins with S	Hourly sum of spatially and temporally expanded estimates of fish passage
Begins with V	Hourly sum of temporally expanded variances
Begins with C	Hourly sum of temporally expanded covariances for guided and unguided fish at powerhouses
Ends with M3H	Discharge in millions of cubic meters
Contains INT	Interpolated hourly estimates (applies only to spill bays 3 and 16)
Contains I1BG	Intake 1B guided
Contains I1BU	Intake 1B unguided
Contains I2AG	Intake 2A guided
Contains I2AU	Intake 2B unguided
Contains I3CG	Intake 3C guided
Contains I3CU	Intake 3C unguided
Contains I4AG	Intake 4A guided
Contains I4AU	Intake 4A unguided
Contains I5BG	Intake 5B guided
Contains I5BU	Intake 5B unguided
Contains I6CG	Intake 6C guided
Contains I6CU	Intake 6C unguided
Contains I7AG	Intake 7A guided
Contains I7AU	Intake 7A unguided
Contains I8BG	Intake 8B guided
Contains I8BU	Intake 8B unguided
Contains I9CG	Intake 9C guided
Contains I9CU	Intake 9C unguided
Contains I10BG	Intake 10B guided
Contains I10BU	Intake 10B unguided
Contains I11CG	Intake 11C guided
Contains I11CU	Intake 11C unguided
Contains I12AG	Intake 12A guided
Contains I12AU	Intake 12A unguided
Contains I13BG	Intake 13B guided
Contains I13BU	Intake 13B unguided
Contains I14BG	Intake 14B guided
Contains I14BU	Intake 14B unguided
Contains I15BG	Intake 15B guided
Contains I15BU	Intake 15B unguided
Contains I15CG	Intake 15C guided
Contains I15CU	Intake 15C unguided
Contains I16BG	Intake 16B guided
Contains I16BU	Intake 16B unguided
Contains I17BG	Intake 17B guided
Contains I17BU	Intake 17B unguided
Contains I18BG	Intake 18B guided
Contains I18BU	Intake 18B unguided
Contains SB2	Spillway bay 2
Contains SB3	Spillway bay 3
Contains SB4	Spillway bay 4
Contains SB5	Spillway bay 5
Contains SB6	Spillway bay 6
Contains SB7	Spillway bay 7
Contains SB8	Spillway bay 8
Contains SB10	Spillway bay 10
Contains SB12	Spillway bay 12
Contains SB14	Spillway bay 14
Contains SB15	Spillway bay 15
Contains SB16	Spillway bay 16
Contains SB17	Spillway bay 17

Appendix F

Statistical Analysis System Code for Estimating Effective Beam Angle based Upon Range from a Transducer

Appendix F

Statistical Analysis System Code for Estimating Effective Beam Angle based Upon Range from a Transducer

Appendix F-1. **Definitions of Variables and Operators**

Variable or Operator	Definition
*	Begins a comment when placed first in a statement or is a multiplication operator within statements
**	Exponential operator
+	Addition operator
-	Subtraction operator
;	End of statement
.	Missing value symbol
LT	Less than operator
System	Corresponds to an echosounder and associated transducers. Echosounder channels and transducer locations are described in Appendix B.
Channel	Corresponds to a single transducer attached to one specific echosounder channel.
Mid_Range	The average of the ranges of the first and last echoes in an echo trace.
N_Angle	Nominal beam angle measured at the –3dB point
E_Angle	Effective beam angle estimated from a polynomial derived during detectability modeling
Angle	Effective beam angle based upon nominal beam angle (if E_Angle is missing) or the effective beam angle

F.2

Statistical Analysis System (SAS) Code for Calculating Effective Beam Angle Based upon Range from Transducers in Spring 2001

```
*Assign transducer names and calculate effective beam angle from Mid_Range;
**************************************************************************************;
* *Mid_Range**   ;
IF SYSTEM='A' THEN DO;
  IF CHANNEL=0 THEN DO; *Uplooker at Unit 10;
    N_ANGLE=6; *Nominal beam angle (-3dB angle);
    E_ANGLE=-0.0003746*Mid_Range**4 + 0.0195369*Mid_Range**3 - 0.3727782*Mid_Range**2 + 3.1195962*Mid_Range - 3.0815278;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
  END;
  IF CHANNEL=1 THEN DO; *Downlooker;
    N_ANGLE=6; *Nominal beam angle (-3dB angle);
    E_ANGLE=-0.0000405*Mid_Range**4 + 0.0026055*Mid_Range**3 - 0.0603130*Mid_Range**2 + 0.5836378*Mid_Range + 4.7763538;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
  END;
END;
IF (SYSTEM='C' AND (CHANNEL EQ 1 OR CHANNEL EQ 3 OR CHANNEL EQ 5 OR CHANNEL EQ 7))OR
   (SYSTEM='D' AND (CHANNEL EQ 1 OR CHANNEL EQ 3 OR CHANNEL EQ 7))THEN DO;
    N_ANGLE=6; *Nominal beam angle (-3dB angle); *DOWNLOOKER at Units 1, 2, 3, 4, 6, 7, and 9;
    E_ANGLE=-0.0000316*Mid_Range**4 + 0.0020959*Mid_Range**3 - 0.0502114*Mid_Range**2 + 0.5032047*Mid_Range + 5.7394944;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF (SYSTEM='C' AND (CHANNEL EQ 2 OR CHANNEL EQ 4 OR CHANNEL EQ 6 OR CHANNEL EQ 8))OR
   (SYSTEM='D' AND (CHANNEL EQ 2 OR CHANNEL EQ 4 OR CHANNEL EQ 8))THEN DO;
    N_ANGLE=6; *Nominal beam angle (-3dB angle); *UPLOOKER Units 1, 2, 3, 4, 6, 7, and 9;
    E_ANGLE=-0.0005754*Mid_Range**4 + 0.0279356*Mid_Range**3 - 0.4926121*Mid_Range**2 + 3.7846213*Mid_Range - 3.4503064;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF SYSTEM='D' THEN DO; *MAIN UNIT;
  IF CHANNEL=5 THEN DO; *Uplooker at Unit 8;
    N_ANGLE=6;
    E_ANGLE=-0.0004118*Mid_Range**4 + 0.0219099*Mid_Range**3 - 0.4276005*Mid_Range**2 + 3.6287775*Mid_Range - 3.9287092;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
  END;
  IF CHANNEL=6 THEN DO; *Downlooker at Unit 8;
    N_ANGLE=6;
    E_ANGLE=-0.0004940*Mid_Range**4 + 0.0233753*Mid_Range**3 - 0.3913853*Mid_Range**2 + 2.6109529*Mid_Range + 1.2743215;
```

```
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
  END;
END;
IF SYSTEM='O' THEN DO; *Downlooker at Spill bay 17;
  N_ANGLE=10;
  E_ANGLE=-0.0014583*Mid_Range**4 + 0.0526578*Mid_Range**3 - 0.6548105*Mid_Range**2 + 3.2577928*Mid_Range + 7.7069431;
  IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF SYSTEM='P' OR SYSTEM='Q' THEN DO; *Downlookers at spill bays 8, 10, 14, 15, 2, 5, 6, and 7;
  N_ANGLE=10;
  E_ANGLE=-0.0014580*Mid_Range**4 + 0.0528453*Mid_Range**3 - 0.6570207*Mid_Range**2 + 3.2510723*Mid_Range + 4.6469364;
  IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF (SYSTEM='P' AND CHANNEL=3) OR (SYSTEM='Q' AND CHANNEL=2) THEN DO; *Downlooker at spill bays 12 and 4;
  N_ANGLE=10;
  E_ANGLE= 0.0036436*Mid_Range**5 - 0.1108587*Mid_Range**4 + 1.2931812*Mid_Range**3 - 7.2245644*Mid_Range**2 +
              19.3212369*Mid_Range - 10.8636667;
  IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF SYSTEM='I' THEN DO;
  IF CHANNEL=10 THEN DO; *Uplooker at Unit 18;
    N_ANGLE=6;
    E_ANGLE=-0.0002857*Mid_Range**4 + 0.0161378*Mid_Range**3 - 0.3270895*Mid_Range**2 + 2.9071900*Mid_Range - 3.0138994;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
  END;
  IF CHANNEL=0 THEN DO; *Downlooker at Unit 18;
    N_ANGLE=6;
    E_ANGLE=-0.0001427*Mid_Range**4 + 0.0084217*Mid_Range**3 - 0.1741949*Mid_Range**2 + 1.4989812*Mid_Range + 2.0136265;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
  END;
END;
IF (SYSTEM='G' AND (CHANNEL EQ 2 OR CHANNEL EQ 4 OR CHANNEL EQ 6 OR CHANNEL EQ 8)) OR
  (SYSTEM='H' AND (CHANNEL EQ 2 OR CHANNEL EQ 4 OR CHANNEL EQ 6 OR CHANNEL EQ 8)) THEN DO;
    *Uplookers at units 11, 12, 13, 14, 15, 16, and 17;
    N_ANGLE=6.5;
    E_ANGLE=-0.0001185*Mid_Range**4 + 0.0086176*Mid_Range**3 - 0.2229570*Mid_Range**2 + 2.4378017*Mid_Range - 2.0871320;
              *Effective beam angle (from 2001 detectability modeling);
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF (SYSTEM='G' AND (CHANNEL EQ 1 OR CHANNEL EQ 3 OR CHANNEL EQ 5 OR CHANNEL EQ 7)) OR
```

```
   (SYSTEM='H' AND (CHANNEL EQ 1 OR CHANNEL EQ 3 OR CHANNEL EQ 5 OR CHANNEL EQ 7)) THEN DO;
      *Downlookers at units 11, 12, 13, 14, 15, 16, and 17;
      N_ANGLE=6.5;
      E_ANGLE=-0.0001262*Mid_Range**4 + 0.0074729*Mid_Range**3 - 0.1554771*Mid_Range**2 + 1.3516580*Mid_Range + 2.9217253;
                *Effective beam angle (from 2001 detectability modeling);
      IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF SYSTEM='R' AND CHANNEL EQ 0 THEN DO; *1st Downlooker upstream of Intake 15b;
      N_ANGLE=6;
      E_ANGLE=-0.0001132*Mid_Range**4 + 0.0081442*Mid_Range**3 - 0.2078268*Mid_Range**2 + 2.2352430*Mid_Range - 1.8956107;
      IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF SYSTEM='R' AND CHANNEL EQ 1 THEN DO; *2nd Downlooker upstream of Intake 15b;

      N_ANGLE=6;
      E_ANGLE=-0.0001220*Mid_Range**4 + 0.0086234*Mid_Range**3 - 0.2155319*Mid_Range**2 + 2.2584577*Mid_Range - 1.6517694;
      IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF SYSTEM='R' AND CHANNEL EQ 2 THEN DO; *3rd Downlooker upstream of Intake 15b;

      N_ANGLE=6;
      E_ANGLE=-0.0001222*Mid_Range**4 + 0.0086013*Mid_Range**3 - 0.2127203*Mid_Range**2 + 2.1871434*Mid_Range - 1.1267870;
      IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;

IF SYSTEM='X' THEN DO;
   IF CHANNEL EQ 0 THEN DO; *uplooker at Unit 5;
      N_ANGLE=6;
      E_ANGLE=-0.0000178*Mid_Range**5 + 0.0004271*Mid_Range**4 + 0.0067419*Mid_Range**3 - 0.2884562*Mid_Range**2 +
                2.9351549*Mid_Range - 3.0309238;
      IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
   END;
   IF CHANNEL EQ 1 THEN DO; *downlooker at Unit 5;
      N_ANGLE=6;
      E_ANGLE= 0.0000027*Mid_Range**5 - 0.0002102*Mid_Range**4 + 0.0064627*Mid_Range**3 - 0.0978366*Mid_Range**2 +
                0.7253817*Mid_Range + 4.7598874 ;
      IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
   END;
END;
```

Appendix F-3. Statistical Analysis System (SAS) Code for Calculating Effective Beam Angle Based upon Range from a Transducer in Summer 2001

```
*Assign transducer names and calculate effective beam angle;
******************************************************************************;
* *Mid_Range**  ;
IF SYSTEM='A' THEN DO;
  IF CHANNEL=0 THEN DO; *Uplooker at Unit 10;
    N_ANGLE=6; *Nominal beam angle (-3dB angle);
    E_ANGLE=-0.0001040*Mid_Range**4 + 0.0072551*Mid_Range**3 - 0.1776161*Mid_Range**2 + 1.8695036*Mid_Range - 2.0218137;

    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
  END;
  IF CHANNEL=1 THEN DO; *downlooker at Unit 10;
    N_ANGLE=6; *Nominal beam angle (-3dB angle);
    E_ANGLE=-0.0000553*Mid_Range**4 + 0.0034783*Mid_Range**3 - 0.0780310*Mid_Range**2 + 0.7277080*Mid_Range + 3.4213323;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
  END;
END;
IF (SYSTEM='C' AND (CHANNEL EQ 1 OR CHANNEL EQ 3 OR CHANNEL EQ 5 OR CHANNEL EQ 7))OR
  (SYSTEM='D' AND (CHANNEL EQ 1 OR CHANNEL EQ 3 OR CHANNEL EQ 7))THEN DO; *Downlooker Units 1, 2, 3, 4, 6, 7, and 9;
    N_ANGLE=6; *Nominal beam angle (-3dB angle); *DOWNLOOKER;
    E_ANGLE=-0.0000386*Mid_Range**4 + 0.0025442*Mid_Range**3 - 0.0601729*Mid_Range**2 + 0.5926396*Mid_Range + 4.4116049;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF (SYSTEM='C' AND (CHANNEL EQ 2 OR CHANNEL EQ 4 OR CHANNEL EQ 6 OR CHANNEL EQ 8))OR
  (SYSTEM='D' AND (CHANNEL EQ 2 OR CHANNEL EQ 4 OR CHANNEL EQ 8))THEN DO; *Uplooker Units 1, 2, 3, 4, 6, 7, and 9;
    N_ANGLE=6; *Nominal beam angle (-3dB angle); *UPLOOKER;
    E_ANGLE=-0.0002324*Mid_Range**4 + 0.0127909*Mid_Range**3 - 0.2602051*Mid_Range**2 + 2.3614581*Mid_Range - 2.3551021;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF SYSTEM='D' THEN DO; *MAIN UNIT;
  IF CHANNEL=5 THEN DO; *Uplooker at Unit 8;
    N_ANGLE=6;
    E_ANGLE=-0.0001290*Mid_Range**4 + 0.0089621*Mid_Range**3 - 0.2187747*Mid_Range**2 + 2.2541737*Mid_Range - 2.6229044;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
  END;
  IF CHANNEL=6 THEN DO; *Downlooker at Unit 8;
    N_ANGLE=6;
```

```
      E_ANGLE= -0.0004732*Mid_Range**4 + 0.0224982*Mid_Range**3 - 0.3793284*Mid_Range**2 + 2.5495810*Mid_Range + 0.2314783;
      IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
    END;
  END;
IF SYSTEM='O' THEN DO; *Downlooker at Spill bay 17;
    N_ANGLE=10;
    E_ANGLE= -0.0013942*Mid_Range**4 + 0.0509931*Mid_Range**3 - 0.6424398*Mid_Range**2 + 3.2511507*Mid_Range + 5.2349284;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF (SYSTEM='P' AND CHANNEL NE 3) OR (SYSTEM='Q' AND CHANNEL NE 2) THEN DO; *Downlookers at spill bays 8, 10, 14, 15, 2, 5, 6,
                and 7;
    N_ANGLE=10;
    E_ANGLE=-0.0014064*Mid_Range**4 + 0.0509348*Mid_Range**3 - 0.6320100*Mid_Range**2 + 3.1236695*Mid_Range + 2.4016384;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF (SYSTEM='P' AND CHANNEL EQ 3) OR (SYSTEM='Q' AND CHANNEL EQ 2) THEN DO; *Downlookers at spill bays 12 and 4;
    N_ANGLE=10;
    E_ANGLE=0.0018058*Mid_Range**5 - 0.0525090*Mid_Range**4 + 0.5934379*Mid_Range**3 - 3.3193546*Mid_Range**2 +
                9.3739533*Mid_Range - 6.1593333;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF SYSTEM='I' THEN DO;
  IF CHANNEL=10 THEN DO; *Uplooker at Unit 18;
    N_ANGLE=6;
    E_ANGLE=0.0002954*Mid_Range**4 - 0.0069716*Mid_Range**3 - 0.0000848*Mid_Range**2 + 1.0032224*Mid_Range - 1.3114219;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
  END;
  IF CHANNEL=0 THEN DO; *Downlooker at Unit 18;
    N_ANGLE=6;
    E_ANGLE= -0.0001359*Mid_Range**4 + 0.0081012*Mid_Range**3 - 0.1698118*Mid_Range**2 + 1.4910183*Mid_Range + 0.2731265;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
  END;
END;
IF (SYSTEM='G' AND (CHANNEL EQ 2 OR CHANNEL EQ 4 OR CHANNEL EQ 6 OR CHANNEL EQ 8)) OR
  (SYSTEM='H' AND (CHANNEL EQ 2 OR CHANNEL EQ 4 OR CHANNEL EQ 6 OR CHANNEL EQ 8)) THEN DO;
    *Uplookers at units 11, 12, 13, 14, 15, 16, and 17;
    N_ANGLE=6.5;
    E_ANGLE=-0.0000567*Mid_Range**4 + 0.0043644*Mid_Range**3 - 0.1226479*Mid_Range**2 + 1.5237704*Mid_Range - 1.7154795;
    IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
```

F.7

```
IF (SYSTEM='G' AND (CHANNEL EQ 1 OR CHANNEL EQ 3 OR CHANNEL EQ 5 OR CHANNEL EQ 7)) OR
   (SYSTEM='H' AND (CHANNEL EQ 1 OR CHANNEL EQ 3 OR CHANNEL EQ 5 OR CHANNEL EQ 7)) THEN DO; *Downlookers;
     *Downlookers at units 11, 12, 13, 14, 15, 16, and 17;
     N_ANGLE=6.5;
     E_ANGLE=-0.0001300*Mid_Range**4 + 0.0077531*Mid_Range**3 - 0.1628108*Mid_Range**2 + 1.4355703*Mid_Range + 0.8058478;
     IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF SYSTEM='R' AND CHANNEL EQ 0 THEN DO; *1st Downlooker upstream of Intake 15b;
     N_ANGLE=6;
     E_ANGLE=-0.0000759*Mid_Range**4 + 0.0055374*Mid_Range**3 - 0.1450202*Mid_Range**2 + 1.6447507*Mid_Range - 1.6279483;
     IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF SYSTEM='R' AND CHANNEL EQ 1 THEN DO; *2nd Downlooker upstream of Intake 15b;
     N_ANGLE=6;
     E_ANGLE=-0.0000831*Mid_Range**4 + 0.0059709*Mid_Range**3 - 0.1532337*Mid_Range**2 + 1.6886241*Mid_Range - 1.4991839;
     IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF SYSTEM='R' AND CHANNEL EQ 2 THEN DO; *3rd Downlooker upstream of Intake 15b;
     N_ANGLE=6;
     E_ANGLE=-0.0000870*Mid_Range**4 + 0.0062105*Mid_Range**3 - 0.1570675*Mid_Range**2 + 1.6849015*Mid_Range - 1.1777958;
     IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
END;
IF SYSTEM='X' THEN DO;
  IF CHANNEL EQ 0 THEN DO; *uplooker at Unit 5;
     N_ANGLE=6;
     E_ANGLE=-0.0001550*Mid_Range**4 + 0.0093049*Mid_Range**3 - 0.2065035*Mid_Range**2 + 2.0395836*Mid_Range - 2.2392157;
     *The revised equation was based upon the average backscattering cross section converted to a TS;
     IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
  END;
  IF CHANNEL EQ 1 THEN DO; *downlooker at Unit 5;
     N_ANGLE=6;
     E_ANGLE= -0.0000538*Mid_Range**4 + 0.0033987*Mid_Range**3 - 0.0763793*Mid_Range**2 + 0.7104033*Mid_Range + 3.6292144;
     *The revised equation was based upon the average backscattering cross section converted to a TS;
     IF E_ANGLE=. THEN ANGLE=N_ANGLE; ELSE ANGLE=E_ANGLE; IF ANGLE LT 0 THEN ANGLE=0;
  END;
END;
```